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AFWL-TR-70-113, Vol IIIB

MULTIPLE-WHEEL HEAVY GEAR LOAD **PAVEMENT TESTS**

Volume III Part B

Presentation and Initial Analysis of Stress-Stain Deflection and Vibratory Measurements

Data and Analysis

R. H. Ledbetter

J. L. Rice

U. S. Army Engineer Waterways Experiment Station

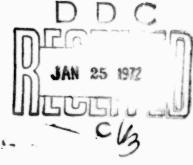
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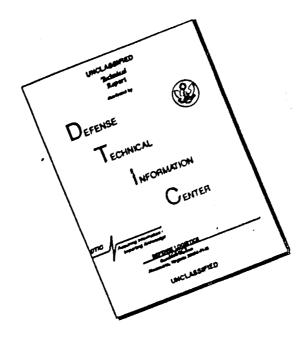
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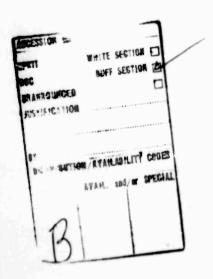
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UNCLASSIFIED Security Classification DOCUMENT CONTROL DATA - R & D (Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified) ORIGINATING ACTIVITY (Corporate author) 28. REPORT SECURITY CLASSIFICATION UNCLASSIFIED U. S. Army Engineer Waterways Experiment Station Vicksburg, Mississippi 39181 2b. GROUP MULTIPLE-WHEEL HEAVY GEAR LOAD PAVEMENT TESTS: Volume IIIB, Presentation and Initial Analysis of Stress-Strain Deflection and Vibratory Measurements - Data and Analysis 4. OESCRIPTIVE NOTES (Type of report and inclusive dates) 1 January 1968 through 1 August 1971 5. AUTHOR(5) (First name, middle initial, last name) Richard H. Ledbetter John L. Rice REPORT DATE 78. TOTAL NO. OF PAGES 75, NO. OF REFS November 1971 542 . CONTRACT OR GRANT NO. MIPR 68-7 94, ORIGINATOR'S REPORT NUMBER(S) b. PROJECT NO. 5224 AFWL-TR-70-113, Vol IIIB 9b. OTHER REPORT NO(5) (Any other numbers that may be assigned this report) 10. DISTRIBUTION STATEMENT

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13. ABSTRACT

(Distribution Limitation Statement B)

Flexible and rigid pavement test sections were constructed and tested to gain information on pavement and soil behavior under large aircraft loadings. These test sections incorporated instrumentation systems designed to determine the response of the pavement structures to static, dynamic (slowly moving), and vibratory loads and to traffic by full prototype loadings. The components of the instrumentation systems, their installation, and the test programs are described in Volume IIIA. This volume covers data reduction, analysis, and the findings of the instrumentation and vibratory testing programs; Appendixes A and B contain details of instrumentation measurements for flexible and rigid pavements, respectively. / Analysis of the maximum response data from the instrumentation program resulted in the following findings for the flexible pavement test section: (a) A load- and position-dependent moving zero reference level was identified for each deflection gage; (b) Limiting maximum clastic deflection and vertical elastic stress versus depth curves were established for static load test results. Analysis showed that the same relationships were true for static and dynamic load tests. as well as for the speed tests; (c) The soft layer in item 4 caused different stress and deflection distributions from those in item 3. The major findings for the rigid pavement test section indicated that the Westergaard algorithm can be used for reasonable prediction of pavement response to single-wheel, twin-tandem, and 12-wheel-assembly loadings.

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MULTIPLE-WHEEL HEAVY GEAR LOAD PAVEMENT TESTS

Volume III

Part B

PRESENTATION AND INITIAL ANALYSIS OF STRESS-STRAIN DEFLECTION AND VIBRATORY MEASUREMENTS

Data and Analysis

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FOREWORD

This report was prepared by the U. S. Army Engineer Waterways Experiment Station, Vicksburg, Mississippi, under MIPR 68-7. The research was jointly sponsored by the U. S. Air Force under Program Element 64708F, Project 5224, Task 04; the U. S. Army under Task 02, Work Unit 002; and the Federal Aviation Administration under Engineering Requirement FAA-ER-450-034a.

Inclusive dates of research were 1 January 1968 through 1 August 1971. The report was submitted 20 September 1971 by the Air Force Weapons Laboratory Project Officer, Mr. L. M. Womack (DEZ-M).

The investigation reported herein was conducted under the overall supervision of Messrs. W. J. Turnbull (retired), J. P. Sale, A. A. Maxwell (deceased), and R. G. Ahlvin, Soils Division, WES. Other Soils Division personnel actively en engaged in this study were Messrs. D. N. Brown, C. D. Burns, A. H. Joseph, W. H. Larson, A. L. Mathews, H. H. Ulery, Jr., R. H. Ledbetter, D. L. Cooksey, and J. W. Hall, Jr. Personnel of the WES Instrumentation Services Division engaged in the study were Messrs. L. M. Duke, G. C. Downing, W. S. R. Beane IV, and J. L. Ferguson. Early in the test program, a special WES Flexible Pavement Branch, Soils Division, group was established for the purpose of collecting, reducing, analyzing, and reporting the instrumentation measurements. This group was under the direction of Mr. Ulery, with Mr. Ledbetter as project engineer. Other members of the group were Messrs. G. L. Tucker III, J. D. Mathews, D. P. Wolf, H. G. Brown, and M. J. Trawle.

Personnel of the Construction Engineering Research Laboratory actively engaged in the investigation were Messrs. J. J. Healy, R. L. Hutchinson, J. L. Rice, F. W. Kearney, and J. B. Gambill.

The flexible pavement instrumentation portions of this report were written by Messrs. Ulery and Ledbetter, the rigid pavement portions of this report were written by Messrs. Rice, Kearney, and Gambill, and Mr. J. W. Hall, Jr., prepared the section on nondestructive vibratory tests. Messrs. Ledbettwer and Rice were the principal authors. Coordination between WES and CERL in preparation of the report was by Mr. Ulery.

This technical report has been reviewed and is approved.

M. WOMACK

Project Officer

USAF Lt Colonel

Chief, Aerospace Facilities Branch

Colonel USAF

Chief, Civil Engineering Research Division

ABSTRACT

(Distribution Limitation Statement B)

Flexible and rigid pavement test sections were constructed and tested to gain information on pavement and soil behavior under large aircraft loadings. These test sections incorporated instrumentation systems designed to determine the response of the pavement structures to static, dynamic (slowly moving), and vibratory loads and to traffic by full prototype loadings. The components of the instrumentation systems, their installation, and the test programs are described in Volume III-A. This volume covers data reduction, analysis, and the findings of the instrumentation and vibratory testing programs; Appendixes A and B contain details of instrumentation measurements for flexible and rigid pavements, respectively. Analysis of the maximum response data from the instrumentation program resulted in the following findings for the flexible pavement test section:

- a. A load- and position-dependent moving zero reference level was identified for each deflection gage.
- b. Limiting maximum elastic deflection and vertical elastic stress versus depth curves were established for static load test results. Analysis showed that the same relationships were true for static and dynamic load tests, as well as for the speed tests.
- c. The soft layer in item 4 caused different stress and deflection distributions from those in item 3.

The major findings for the rigid pavement test section indicated that the Westergaard algorithm can be used for reasonable prediction of ravement response to single-wheel, twin-tandem, and 12-wheel-assembly loadings.

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CONVERSION FACTORS, BRITISH TO METRIC UNITS OF MEASUREMENT

British units of measurement used in this report can be converted to metric units as follows:

Multiply	Ву	To Obtain
inches	2.54	centimeters
feet	0.3048	meters
square inches	6.4516	square centimeters
cubic inches	16.3871	cubic centimeters
pounds	0.45359237	kilograms
kips	453.59237	kilograms
pourds per square inch	0.070307	kilogram: per square centimeter
pounds per cubic foot	16.0185	kilograms per cubic meter
feet per second.	0.3048	meters per second
miles per hour	1.609344	kilometers per hour
Fahrenheit degrees	5/9	Celsius or Kelvin degrees*

^{*} To obtain Celsius (C) temperature readings from Fahrenheit (F) readings, use the following formula: C = (5/9)(F - 32). To obtain Kelvin (K) readings, use: K = (5/9)(F - 32) + 273.15.

SECTION I

INTRODUCTION

1. PURPOSE

The purpose of this investigation was to validate present criteria, or establish new criteria, for the evaluation and design of both flexible and rigid airfield pavements to be subjected to multiple-wheel heavy gear loads (MWHGL).

2. BACKGROUND

The multiple-wheel gears of large, new aircraft (such as the C-5A and Boeing 747) may impose loads on pavements that are radically different from those previously encountered. Extensions to the existing criteria for pavement evaluation and design are necessary to evaluate the effects of these loads. Data are also required to determine the relative destructive effects of new and proposed aircraft on pavement performance. The Army, Air Force, and Federal Aviation Administration jointly sponsored this investigation. The investigation was conducted by the U. S. Army Engineer Waterways Experiment Station (WES), Vicksburg, Miss. Overall supervision of the tests and all details pertaining to the flexible pavement portion of the tests were provided by WES. The rigid pavement testing was directed by the U. S. Army Construction Engineering Research Laboratory, Champaign, Ill.

3. SCOPE

The purpose of this investigation was accomplished by the construction and testing of a specially designed test section consisting of both flexible and rigid pavements as described herein. Testing consisted of instrumentation measurements of deflection, strain, and stress resulting from applied static and dynamic (slowly moving) loads of multiple-and single-wheel gear assemblies; nondestructive vibratory testing to determine wave velocity and stiffness; and traffic testing with multiple- and single-wheel gear assemblies.

The MWHGL study represented such an extensive effort that the report of the study was divided into the following volumes:

 I - Basic Report (background, summary of entire study, conclusions, and recommendations)

- II Design, Construction and Behavior Under Traffic
- III Presentation and Initial Analysis of Stress-Strain-Deflection and Vibratory Measurements
 - A. Instrumentation
 - B. Data and Analysis
- IV Analysis of Behavior Under Traffic

The authors felt that the subject matter of Volume III was too broad to be presented in a single report. Therefore, Volume III-A mainly described the instrumentation system and its installation and operation to collect the data required to determine the stress, strain, and deflections under various static and dynamic loads and wheel configurations, temperature and pore pressure effects, and soil behavior patterns. Volume III-A also included descriptions of the preliminary test program conducted to evaluate the performance of the system and the test procedures and application of loads for the major test program. This report, Volume III-B, describes the major test program and the interpretation and analysis of instrumentation data collected during static and dynamic load tests: stress, consolidation, deflection, pore pressure, temperature effects, and pavement strain. This report also describes the results of the tests to determine the effects of the speed of the vehicle during the dynamic load tests, as well as analysis of the soil behavior patterns.

SECTION II

FLEXIBLE PAVEMENT TEST PROGRAMS

1. INSTRUMENTATION

Static and dynamic load tests were made on the flexible pavement test section and the response of the pavement-soil system was monitored by a complex instrumentation installation. The test section and the instrumentation system are described in detail in Volume III-A. The related equipment necessary to operate and accurately monitor the instrumentation system is also described in Volume III-A.

A total of 52 cells and gages were installed in items 3 and 4 in order to obtain adequate measurements of stress, strain, and deflection. The primary measurements to be obtained at various depths within the pavement structure were vertical stress and vertical deflection. Supplementary information to be obtained was pore pressures, strain in the bottom of the pavement wearing course, and temperatures of the asphaltic concrete pavement. Most of the instrumentation was installed in duplicate to increase the probability that measurements could be obtained regardless of the failure of a gage or cell.

Vertical normal stresses were measured by 17 WES-designed soil pressure cells and by three commercial soil pressure cells (for comparison as a cheaper substitute) at locations that duplicated installation of a WES cell. Two soil pore water pressure cells were installed to determine if pore pressure developed that would have to be subtracted from readings of the soil pressure cells to obtain the effective stress in the soil under load.

Vertical normal deflections were measured by 18 WES-designed deflection gages. Two full-depth reference rods for remote optical reading were installed within the instrumentation grid to monitor movement of the 12-ft-deep reference plane in order to correct the response of the mechanical deflection gages.

Eight strain gages were placed at the bottom of the asphaltic concrete pavement and four thermistors were installed in the pavement.

A table of factors for converting British units of measurement to metric units is presented on page xxi.

Photoelectric cells were used to construct a tracking system that was found necessary for giving the location and position of a loaded assembly during dynamic load testing.

2. TESTING EQUIPMENT

Full-scale loads and wheel assemblies were used for conducting the static load, dynamic load, and traffic tests. Tests were conducted with one main 12-wheel landing gear of the C-5A Galaxy, a 6-wheel component of the main C-5A gear, a twin-tandem component of the Boeing 747 landing gear, and a single wheel. The tires used in all of the test carts were 49x17, 26-ply rating, which is the design tire for both the C-5A Galaxy and the Boeing 747.

3. PRELIMINARY TESTING PROGRAM

Prior to commencement of the major instrumentation testing program, a number of preliminary tests were performed to establish procedures to be followed in the test program. All of the preliminary tests except those for the tracking device were performed using the single-wheel 30,000-lb test cart, which was a C-5A tire mounted in a load vehicle. The 180,000-lb, 12-wheel assembly was used in developing and checking the tracking device. The preliminary tests are summarized below; details of the tests are given in Volume III-A.

Representative gages and cells at each depth were statically loaded and the response timed. The time lags for the static loading tests were determined to be a 2-min lapse after loading before recording deflection-gage response and a 30-sec lapse between loading and recording pressure cell response. The position-effects study showed that in order to achieve the best consistency possible for all static load tests, the loading point for each wheel configuration would have to be centered as accurately as possible over the gage and cell positions.

Data collected for study of soil response time-lag with depth and loadposition effect were used in determining the performance of the instrumentation system. The system was shown to be functioning correctly, and the response of the system was considered to be consistent to an acceptable degree.

Movement of the reference rods monitored during static loading indicated that (a) the 12-ft-deep reference plane was within the zone of influence of

the tests loads; (b) load-induced movements were occurring at the selected reference depth; and (c) the optical monitoring system was adequate and accurate enough to measure these deflections.

Operation of the single-wheel test cart down the test section over the instrumentation at less than 1 mph and at 1, 3, and 6 mph indicated that all gages and cells were functioning properly in response to the dynamic loading.

Static load tests were conducted when the asphaltic concrete was relatively cool (26 C) and again when the pavement was considerably warmer (28-36 C). Also, the surface strain gages were monitored to determine the temperature-pavement strain effects. These tests did not show a temperature effect in the ranges of temperatures investigated.

4. MAJOR TESTING PROGRAM

a. Schedule of Tests

The major instrumentation testing program was conducted after the preliminary tests were completed and before traffic tests were initiated. Additional static and dynamic load tests were conducted during the traffic testing and after the completion of the 12-wheel traffic on items 3 and 4.

Table 1 shows the clronology of the test loadings. The static test loadings were always conducted first and the dynamic runs second, both with the same assembly at a given load and tire inflation pressure. A summary of the major instrumentation test program is shown in tables 2 and 3.

b. Test Procedures

The major instrumentation test program included static and dynamic loading tests. The static tests were conducted by moving a loaded test cart or an empty prime mover into position over the test section loading points and recording the responses of the appropriate cells and gages. In conjunction with each of the static load tests, the same test cart would travel slowly over the same instrumentation and the reactions of soil and pavement were recorded (dynamic load tests). In addition, speed tests were performed to study the effects of varied rates of loading and unloading of the pavement system. Instrumentation responses were monitored with the single-wheel assembly, 30,000-lb load, moving at speeds of 1 to 10 mph. Test procedures, summarized below, are described in detail in Volume III-A.

Table 1

MWHGL Static and Dynamic Instrumentation Loadings of Flexible Pavement Test Section

Test Loading No.	Loading	Date Collection of Readings Completed	Static Loading Grid Pattern	Number of Static Readings
1	Preliminary tests	25 Apr 69	*	2,660
2	15 kips, 12 wheels, 45 psi	30 Apr 69	Partial	5,320
3	15 kips, SWL, 45 psi	6 June 69	Partial	2,660
14	30 kips, 12 wheels, 100 psi	19 June 69	Complete	5,360
5	30 kips, SWL, 100 psi	26 June 69	Complete	4,280
6	30 kips, 6 wheels, 100 psi	2 July 69	Partial	5,320
7	Prime mover (12 wheels)	9 July 69	*	1,660
8	30 kips, twin tandem, 100 psi	15 July 69	Complete	8,640
9	30 kips, twin tandem, 150 psi	18 July 69	Partial	2,760
10	Prime mover (twin tandem)	23 July 69	*	1,660
10a	30 kips, SWL, 100 psi (speed test)			
11**	6 kips, SWL, 10 psi	25 July 69	Partial	2,660
lla	30 kips, 12 wheel, 100 psi		* -	
12	50 kips, SWL, 165 psi	30 Oct 69	Partial	2,660
13	60 kips, twin tandem, 225 psi	6 Nov 69	Partial	2,760
			Total	48,400

Note: Test loading Nos. 1-10 represent both static and dynamic load tests. Test No. 10a represents only dynamic loading, and test Nos. 11-13 represent only static loading.

^{*} Selected locations.

^{**} Performed in conjunction with another project.

Table 2
Summary of Tests with Load Cart

		Tire Infla- tion	Test Loading No.**					
	Load	Pres- sure	Prelimi - nary	Pret	raffic Te		During Traffic	Additional Static
Assembly	Kips	psi*	Tests	Static	Dynamic	Speed	Static	Tests
12 wheel	180 360	100		2	2		 lla	==
6 wheel	180	100		6	6			
Twin tandem	120 240	100 150 225	 	8 9	9	=	Ξ	 13
Single wheel	6 15 30 50	10 45 100 165	1	11 3 5	3 5	10a		 12

^{*} Tire contact area for 120-kip twin-tandem load (tire pressure 150 psi) was 212 sq in. Tire contact area for all other test carts was 285 sq in.

** Test load numbers correspond with the numbers shown in table 1.

Table 3
Summary of Tests with Empty Prime Movers

Test Loading No.*	Prime Mover	Deadweight, 1b	Tire Inflation Pressure, psi
7	6 and 12 wheel	2 'ront tires - 58,000 2 rear tires - 44,000	25 24
10	Twin tandem pulled by a tractor	1 tire - 6,500 1 tire - 5,900	15 15

^{*} Test load numbers correspond with the numbers shown in table 1.

(1) Test assembly load points. The wheel configurations used were: 12 wheel, 6 wheel, twin tandem, and single wheel. Each configuration had its own distinct points of maximum loading, as shown in figure 1. These loading points were chosen as the points beneath which the maximum stress, strain, and, consequently, pore pressure would be induced in the pavement system being loaded. The load points were used in positioning the test cart for static tests and for positioning and traffic guidance during dynamic runs.

The maximum stress under the 12-wheel configuration migrated with depth from the surface under either of the back inside tires of the front 6 wheels, into the geometric center of the back axle of the front 6 wheels at depths of 2.5 to 12 ft, and then to the geometric center of the 12-wheel configuration at greater depths. For the 12-ft-deep pavement structure of the test section, point 1 under the center of the front axle and point 2 under either of the back inside tires represented the maximum load points. The 6-wheel configuration was the front 6 wheels of the 12-wheel configuration, and points 1 and 2 were the same as for the 12-wheel configuration.

For the twin-tandem wheel arrangement, the maximum stress was considered to migrate with depth from the surface under the left rear wheel to the geometric centroid of the configuration at depth. These two maximum load points were used as load points 1 and 2.

The point that gave the maximum stress path with depth for the single-wheel assembly was always directly beneath the geometric centroid of the tire.

(2) Instrumentation load patterns. Two main types of instrumentation loading patterns, static and dynamic, that were the same for both items 3 and 4, were designed and utilized in all of the instrumentation testing. The static loading patterns were further identified as complete, partial, and selected loading patterns. The complete pattern consisted of stopping the test cart on each location (X) in an item, shown in figures 2 and 3, and recording all of the instrumentation responses. The partial loading pattern consisted of stopping only on each location on the four instrumented rows in each item. The selected-location loading pattern was a modified partial loading pattern consisting of static loading only at selected or representative cells and gages in one or both items.

The dynamic loading pattern included collecting data from all instrumentation as the load cart traveled on each of the 23 rows shown in figure 4.

(3) Application of loads. Prior to each series of static load tests, all gages, cells, and reference rods were monitored to establish initial noload responses. Pertinent ambient and pavement temperatures and barometric pressure readings were recorded. Similar no-load readings were made at the completion of a run on each static or dynamic load row, after any interruption of loading in excess of 30 min, and upon completion of each static load test.

Figures 2-4 show the locations of the instrumentation as well as the grid lines painted on the pavement of the test section to locate the static and dynamic rows.

The static load tests were conducted by starting on static row 1 in item 4 and successively loading each pavement loading point. The test cart then traveled in reverse back to the east maneuver area, and no-load readings were made for both items. The test cart returned down the same row to item 3 and stopped on the first position to be loaded. The loading procedure used in item 4 was followed in item 3, and the test cart returned to the east maneuver area traveling in reverse. Series of no-load readings were made for both items before the test cart was maneuvered into alignment with the next row to be loaded, which depended on the grid pattern being followed.

In order to determine the magnitude of the effect of the dead load of the prime movers on the soil response, static load tests were performed using the empty 12-wheel and twin-tandem prime movers. Measurements indicated that the truck used in the single-wheel assembly had a negligible effect on soil response, and no corrections were therefore necessary.

After each static load grid pattern, dynamic load tests were made with the same test cart. The test cart followed each of the dynamic rows from the east maneuver area across items 4 and 3 and then covered the same row in both items traveling in reverse. Dynamic tests were also made using empty 12-wheel and twin-tandem prime movers. Each dynamic test followed the full dynamic pattern of 23 rows; however, due to the load influence, only 21 rows were used for the single-wheel tests.

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Dynamic speed tests were run only on the instrumented dynamic rows (5, 9, 11, and 15). The soil responses were monitored as the 30,000-1b single-wheel assembly traveled at each of the following speeds: 1, 2-3, 5-6, and 9-10 mph. These speeds were considered as very slow, normal traffic testing rate, twice normal, and fast, respectively.

Static load tests were conducted during and after traffic with the 12-wheel 360,000-lb assembly. Selected grid patterns were loaded with the same test cart after 438, 1718, and 2342 coverages in item 3 and after 447, 1727, and 2351 coverages in item 4. After traffic, static loading partial patterns were tested with a 50,000-lb single-wheel load and a 240,000-lb twin-tandem load. The loading procedure for each location was the same as the one established for the pretraffic static load tests.

(4) Monitoring soil instrumentation. Technicians read and recorded all instrumentation responses, temperature, and barometric pressure for each static load test. At the same time, the movement of the reference plane was monitored optically and recorded.

For all of the dynamic load tests, including the speed studies, monitoring of all of the instrumentation and tracking system was accomplished by oscillograph recorders. No-load and temperature readings were made and recorded directly on appropriate oscillograph records to serve as reference readings.

SECTION III

ANALYSIS OF DATA FOR FLEXIBLE PAVEMENT TESTS

Because of the great volume of both static and dynamic load test data obtained during the testing periods, only a very limited analysis of the data was complete at the time this report was prepared. Analysis of the maximum responses on the soil instrumentation in items 3 and 4 under both static and dynamic loadings was considered to be of primary importance and was undertaken first. These maximum responses are presented as depth versus maximum elastic deflection and maximum elastic stress curves. Interpretation and reduction of data for the development of the curves are given. Comparisons are made between soil response to static and dynamic loads and also between responses from the two instrumented items. The last presentation in this part is an analysis of the maximum responses and soil behavior patterns.

A portion of the actual instrumentation data was reduced and is presented in Appendix A along with evaluation of the consistency and reproducibility of the measuring instruments and the loss of instrumentation. The data are presented for both static and dynamic tests of the 30,000-lb-per-wheel loads, the static 50,000-lb single-wheel load, and the static 240,000-lb twin-tandem load.

The results of the maximum responses of the instrumentation are presented in figures 5-50. Figures 5-26 show deflections under both static and dynamic loads; figures 27-45 give stresses from both static and dynamic load testing; figures 46-48 show the results of speed tests; and figures 49 and 50 present pavement strain results. The actual data points used for developing each of the curves are shown on the curves. These data points represent averages of the responses of the gages or cells at each location. The accuracy and consistency of these points are discussed in Appendix A.

Figures 8, 15, 25, 29, 36, and 44 give summary comparisons of only the gear loads of primary interest: the single wheel, a 12-wheel component of the C-5A landing gear, and one twin-tandem component of the Boeing 747. The single-wheel and 12-wheel curves are for the 30,000-lb-per-wheel load; however, the twin-tandem curve is for 42,000 lb per wheel (the actual design wheel load of the Boeing 747). Finally, figures 51-62 show the results of

an anal wis of the soil behavior patterns exhibited in the MWHGL test section.

1. ANALYSIS OF LOAD-POSITION EFFECTS

Probably the most important result of the position-effects study (discussed in detail in Volume III-A) was the behavior of the soil as registered by the delication gages after the center point of the loaded wheel passed over a gage. This study was based on static load tests conducted by moving the single-wheel test cart toward and away from a gage position. The results showed that the maximum registration occurred after the load wheel passed the center of the gage; the distance of the point from the gage center decreased with depth. Similar behavior was noted under dynamic load tests but to a much smaller degree.

The procedure of loading and reloading the gage point demonstrated that the behavior was not due to the load tire being unbalanced in load distribution, which would only cause the maximum load point to either lead or lag the centroid of the tire with respect to forward movement. For the regular tests, the closest offset distances were 1 ft, and tests showed that the deflections registered with the load at 1-ft offsets were not in the area of influence of soil response discussed above. Nevertheless, to complete the position-effects study, an analysis was made of the behavior and possible explanations are presented in the following paragraphs.

One possible explanation is that the effect or behavior of the gages could be due to a combination of eccentric loading on the gage reference plate and, more so, to lateral earth pressure acting on the gage housing. The gage housing is 9-1/8 in. high and 2-1/4 in. in diameter. As the load tire approached a gage, lateral earth pressure, in addition to vertical normal stress on the gage plate, was building up on the side of the housing facing the approaching load tire. Also, the vertical normal stress distribution across the gage plate from an offset load point was probably not a uniform distribution. The nonuniform stress distribution on the gage plate, which would be an eccentric loading, and the lateral pressures on the gage housing probably had a balancing effect on the gage and prevented the eccentric load on the plate from causing a maximum reading or response before the load tire was centered on the gage. When the static load was centered on the gage, the true maximum response would have occurred because, at this point, the vertical normal stress

acting on the gage plate should have been of uniform distribution, and the lateral forces acting on the gage housing should have been balanced in all directions around the housing. As the load tire moved off and away from the gage center at the statically loaded offsets, the stress distribution across the gage plate would have been nonuniform, again causing eccentric loading on the gage. Also, as the load moved away, the lateral force would have become unbalanced and built up on the opposite gage housing face from the approaching load. This shift of lateral forces could have caused a shadowing or arching action effect on the opposite face of the rage housing, and this action plus the eccentric loading could have produced an over or larger response of deflection.

Another explanation could be that the beam action of the pavement layer or plastic response of the pavement-soil system caused or contributed to the indicated behavior. Still another explanation could involve the changing reference level (which is discussed in detail in the following sections) as the load tire approached, was over, and passed a gage location.

The above explanations seem credible; however, the true explanation of the indicated behavior still remains an unknown.

This phenomenon, as stated in Volume III-A, occurred whether the load tire was moving in forward or reverse static offsets; this maximum response is not believed to have been the true response of the scil. The true maximum deflection is believed to have been the one that occurred when the load was centered over the gage and all forces on the gage were balanced. This is the deflection reading that was used for every deflection gage in the data analysis of maximum responses, and this is the main reason for having the load points accurately centered. The soil pressure cells did not show this effect; they peaked at zero offset (centered). This pressure cell response reinforces the above reasoning for the response of the deflection gages. The soil pressure cells do not show eccentric loading because the construction of the cells is such that pressures across the entire cell face are averaged.

2. RESIDUAL STRESSES AND CONSOLIDATION

The instrumentation of items 3 and 4 showed a buildup of stresses and consolidation occurring in the test items from the installation of the cells

and gages, during the test section construction, and during the main testing programs to 26 January 1970, 3 months after completion of traffic testing.

a. Residual Stresses

A history of the response of each pressure cell in both items was kept from the time of installation of the cells in 1968 until a final reading in January 1970 (figures 63 and 64). These histories represent the noload stress readings taken either early in the morning or in the late afternoon, before or after either construction activity or test loads were applied. The readings were taken either daily or weekly during the construction phase of the project, each morning during the instrumentation testing program and traffic tests, and weekly or biweekly after the completion of all tests until January 1970. These stress histories for each cell were kept for the purposes of monitoring the behavior of the cells, to aid in the analysis of the stress induced under loadings, to give an indication when eells had failed or were approaching failure, and to help correct any reading that was recorded incorrectly. Raw indicator readings were used for the stress histories; these readings were converted into pounds of stress per square inch and were used to prepare the plots shown in figures 65 and 66. These figures include stress versus depth for theoretical overburden pressure, measured stress change during construction of the test section from the time of installation of the cells to the beginning of the test program, measured stress at the end of all tests including traffic, and measured stress on 26 January 1970 (3 months with no loads on the section). These plots show that the theoretical overburden curves for both items are approximately equal even though item 4 included a 3-ft layer of soft 2-CBR elay, but the stresses measured by the soil pressure cells show a difference in the stress distributions for the items.

(1) Item 3. Figure 65 shows that after construction of the item, the stresses registering on the soil pressure cells were approximately equal to the theoretical soil overburden pressure down to the 7.5-ft-depth pressure cells. No residual stresses due to the construction operations and compaction had built up in this area. At the 12-ft depth, the pressure cells did register stress increases of over 100 percent in excess of the theoretical overburden pressure. The construction operations and compaction apparently had created stress in the soil at this depth. This increase in measured pressure over theoretical pressure is believed to be due to stress concentration

due to arching action (reference 1). The stress concentration was caused by a highly rigid object (the pressure cell) placed in a plastic medium. As will be discussed later, this increased stress level at the 12-ft depth did not behave under loading tests as a true residual stress that had to be ever-come before stresses were registered on the cells; rather, it behaved as a reference level from which induced stresses operated. In this respect, it is questionable as to whether the stress should be called a residual stress or not. This concept of stress reference level will be discussed later.

After the completion of the testing program and traffic, the stress concentrations had increased at all depths except at the 0.75-ft depth, which decreased (figure 65). A large stress release had occurred at the 0.75-ft-depth cells, which were between the base and subbase. This stress release is not fully understood or the reasons known. One possible explanation could be that arching occurred above the cell in the crushed stone causing a stress release. The difference between any two curves is the stress increase or decrease.

Some of the stresses measured for the 90-day period between the end of tests to the final reading with no loads on the test sections showed a slight trend toward a decrease in the stress concentration after the testing period but did not return to the before-test stress level. Here again, as for the 12-ft-depth cells after construction, the stress concentration levels on all cells did not behave as residual stresses but as new reference levels for induced stresses. The stress histories during the testing program period showed the changing of the stress reference levels for each cell.

(2) Item 4. Figure 66 shows that much the same behavior trend occurred in item 4 during construction as in item 3, with the exception of the 4.5-ft-depth cells at the top of the soft 2-CBR layer. The histories show a definite reduced stress at this depth. The reduced stress readings are believed to be caused by the presence of material below the cells that is less stiff than the material above the cells. As for item 3, with the above exception, the stresses measured after construction were approximately equal to the theoretical soil overburden pressure down to the 7.5-ft depth. The pressure cells at the 12-ft depth in item 4 showed a 100 percent increase in stress over the theoretical overburden pressure. This increase was believed to be caused by the same mechanism as that already discussed for item 3. The

behavior of the induced stresses from load tests was also the same as item 3, with the increased stress level acting as a reference level.

During the testing period, item 4 showed an increase in the stress concentrations except at the 12.0-ft depth, which showed a slight decrease. The difference between any two curves is the stress concentration increase due to the load tests and traffic.

The curve for the 90-day period from the end of all tests to the final reading shows that a slight increase may have occurred in the stress concentration levels after the testing period, except for the stress at the 0.75-ft depth, which decreased (as discussed for item 3) to the beforetesting level. Again, as for item 3 and the 12-ft-depth cells, the stress concentration levels on all cells, whether increased or decreased, behaved as new reference levels of stress for the induced stresses. The stress histories for item 4 also show, for the testing program period, the changing reference stress levels for each cell.

b. Consolidation

(1) Field measurements. As for the stresses, histories of each deflection gage were kept from the time of installation of the gages in 1968 until January 1970. These histories, figures 67 and 68, are deflection readings taken at no-load conditions during construction, testing, and after completion of all tests. The readings were taken at the same time and on the same schedule as the stresses during construction, testing, and after completion of tests. The histories were kept for the same objectives in studying the behavior of the gages and soil strains as for the stress histories; i.e., to help analyze the test-loading deflection data, to determine if any gages displayed erratic behavior and were questionable as to reliability, and to make corrections for erratic or erroneous data. Data for figure 69 were taken from the deflection gage histories; the curve is the Taylor square-root-of-time fitting method of consolidation (reference 2) applied to the data from a deflection gage for the period from installation to the beginning of tests (construction period).

From the beginning of the installation of the deflection gages in both items 3 and 4 in the MWHGL test section, the deflection gages measured a continuous downward vertical movement during all periods of

construction and testing and from completion of testing through the readings taken in January 1970. The first deflection gages were installed on 30 August 1968, and measured deformations were still continuing at the time of this reporting.

(2) <u>Laboratory tests</u>. Laboratory consolidation tests were performed on two undisturbed soil samples from item 3. One sample was from the heavy clay subgrade at a depth of 2.75 ft. The other sample and the one considered herein was from the lean clay subgrade at a depth of 5.75 ft. Both samples were taken from the 4-CBR subgrades. The laboratory results and the calculations are given in figures 70-75.

The lean clay subgrade material was used in this analysis because the deflection gages showed that the movement occurring in the test section during the period from gage installation to the beginning of tests took place in the lower 4 ft of the pavement structure. This reasoning was based on the fact that all of the deflection gages at depths of 0 to 7.5 ft showed the same movement at any given time interval and all showed the same rate of movement. Because all of the deflection gages measured movement with respect to a plane at 12 ft and the first deflection gages were 4.5 ft above this plane, the movement must have occurred in the 4.5 ft of lean clay. This idea was also reinforced by the CBR strengths measured in this material. The design CBR of the lean clay was 4, which was on the wet side of the compaction curve with the material nearly saturated, but this strength was only achieved in the upper part of the lean clay subgrade. The in-place tests after construction (described in Volume II) showed the range of strengths given in table 4.

Table 4
In-Place CBR After Construction

Depth ft	CBR	Remarks	
5.75 6.75 7.75 8.75 9.75 10.75	4.5 3.7 3.9 1.8 1.1 Avg 2.2 1.9 2.2	Top of lean clay	

The initial void ratio for the lean clay was calculated to be 0.630, and the final void ratio was 0.499 (figure 70). Pertinent laboratory information for the lean clay is given in figure 71. The initial water content was 22.5 percent, and the initial degree of saturation was 94.3 percent. The final water content was 18.4 percent, and the final degree of saturation was 99 percent.

The consolidation tests were run using the Taylor square-root-of-time fitting method, which allowed each consolidation test to be run through a series of eight loads in one day. Figure 72 is the Taylor plot for the load increment of 1/2 ton per sq ft. The coefficient of consolidation $C_{_{\rm V}}$, calculated for the 1/2-ton-per-sq-ft load because this load is approximately the overburden weight of the soil, was 0.277 sq in./min (figure 73).

The void ratio e versus log pressure P curve is shown in figure 74. This curve did not exhibit a sharp curvature, which is characteristic of a remolded material. Preconsolidation pressure was calculated to be 2.85 tons per sq ft, but in a strict or theoretical sense, this cannot be considered a true preconsolidation, even though the soil was placed and field compacted to the desired state. The e log P curve also gave an indication that the lean clay behaved as a sensitive soil, possibly due to the high degree of saturation, low strength, and pore pressure buildup.

The ultimate settlement or consolidation settlement Δh was calculated for two conditions by using the existing soil pressure at the 7.5-ft-depth deflection gages and the preconsolidation pressure. Using existing soil pressure, Δh equaled 3.08 in., and using preconsolidation pressure, Δh equaled 0.26 in. The actual ultimate settlement due to construction and overburden weight is believed to be between these two conditions and is probably close to the settlement predicted from the actual measured movements by the Taylor fit method, figure 69. An approximate ultimate settlement for this period would probably have been about 1.5 in. if no loadings had been applied to the test section. Settlement during this time period is belified to have occurred below the first deflection gage in the bottom 4 ft of weak lean clay. The calculated field rate of consolidation given in figure 75 is not a good estimate because the layer cannot drain or dissipate pore pressures as fast as the coefficient of consolidation allows. This may be due to the location of the water table, or there may be a more impermeable

layer of soil beneath the test section. A truer time rate is believed to have been the field rate, as shown in figure 69.

pacted during construction, it would continue to consolidate under the weight of the overburden. Due to the nature of the material and its characteristics as a remolded material, the ultimate settlement before testing started is believed to be best indicated by the actual field settlement data and the predicted curve in figure 69. The field data and prediction curve gave a 100-percent primary consolidation value of the ultimate settlement as approximately 1.11 in. and a predicted time for 100 percent primary consolidation as approximately 290 days. The time predicted for 100 percent primary consolidation was not allowed to elapse between construction and testing due to the time limits involved and the need to begin the load testing program of the project.

Laboratory tests were performed only on the undisturbed soil samples from item 3 because the deflection gage data from item 4 were the same as the data from item 3. The conclusions drawn for item 3, based on the laboratory results and the deflection gage histories, are believed to also be true for item 4 and can probably be applied or concluded for the non-instrumented items of the test section.

started on the test section on 7 April 1969 before the primary consolidation under the overburden weight was completed. The soil deformation histories for both items during the preliminary special tests before the regular scheduled tests show that, in general, consolidation continued at about the same rate on all gages except the surface gages and the shallow 0.75-ft-depth gages in item 4. The surface gage in each item registered a definite permanent movement or seating during the preliminary tests. The 0.75-ft-depth gages in item 3 showed no movement different from the other gages, but the 0.75-ft-depth gages in item 4 did show different movement. One showed a seating movement and the other showed a release or upward movement. These movements for the surface gages and shallow gages were not believed to be irregular behavior due to these regions being areas where initial movements were expected in the base and subbase attributed to tightening or compacting under the first loads. The other gages in the items show approximately the same movements at the same

rates for the remaining depths, which again pointed to continued consolidation in the bottom 4 ft of the weak lean clay.

During the first regular scheduled static and dynamic load tests, which were conducted with 15,000-lb loads per wheel, all soil deflection gage histories for each item show that the consolidation in the bottom of the test section had approximately stopped, completing primary consolidation. The histories show that in general, the gages in each item were reflecting the same movement with no excessive downward or upward movement at any one gage. Generally the deflection gages in item 3 that showed any movement, registered downward movement, possibly secondary consolidation, with the shallow gages showing the most movement during the load tests. All deflection gages in item 4 showed consistent behavior; the general trend was a release or slight upward movement. What appears to be slight erratic behavior of the gages in both items during this period of load tests will be discussed later under analysis of data. Item 4 deflection gage histories show a slightly more erratic behavior than item 3, and this difference will also be discussed later.

The next scheduled load tests, static and dynamic, were with loads of 30,000 lb per wheel. The deflection gage histories of both items for this period show that the heavy loads caused an induced consolidation. This induced consolidation under load is different from the previously discussed consolidation in the lean clay. All indications before the 30,000-1b load tests were that the consolidation was a constant amount in all layers and occurred in the bottom 4 ft of the lean clay subgrade. This occurred under the overburden weight and was not affected by the loads of 15,000 lb per wheel, whereas, the consolidations that occurred during the 30,000-1b load tests were induced by the heavy loads and occurred in different amounts in different layers. In other words, consolidation was induced in all layers at all depths, not just the bottom 4 ft. The soil deflection gage histories show approximately the same consolidations in similar layers of each item. These histories show a decrease in consolidation with depth, with the surface and 0.75-ft-depth gages showing the most consolidation or permanent movement, which indicated densifying of the subbase under the heavy loads and possibly small lateral movements or shear failures occurring in the gravelly sand. At the 2.75-ft depth, the gages showed less permanent movement or consolidation

than the shallower depths but greater than the deeper gages. The deflection gages at 4.5 and 7.5 ft in item 3 showed approximately the same consolidation in these layers, but in item 4, the 4.5-ft-depth gages showed a little more consolidation than the 7.5-ft-depth gages, which showed only a slight permanent movement. The 4.5- and 7.5-ft-depth gages in item 3 registered approximately the same movement as the 4.5-ft pages in item 4, but the 7.5-ft-depth gages in item 4 registered less movement than item 3. In this 30,000-lb-per-wheel load test period, item 4 deflection gages again showed slightly more erratic behavior than the gages in item 3.

For the period of traffic tests, which were conducted with the 360,000-1b 12-wheel assembly, the deflection gage histories again show the same behavior for items 3 and 4, but with item 4 showing more permanent deformation or consolidation. This again was induced consolidation in both items at all depths due to the heavy load. The histories of both items show that, during the first month of applied traffic in August 1969, the traffic caused either no permanent deformation or very slight deformation with a release or upward movement registered on a few gages. Towards the end of the first month of applied traffic, all soil deflection gages in both items began to show a downward, induced-consolidation trend that lasted throughout the remainder of applied traffic, which terminated 3 October 1969. This induced consolidation also occurred in all layers, at all depths, and in different amounts per layer. Item 4 experienced more induced consolidation than item 3 as registered on all gages. The surface and 0.75-ft-depth gages in both items registered large, sudden permanent deformations towards the end of August that did not decrease or stop until the first of September. The 0.75-ft-depth gage in each item, on the inside deflection gage row (static row 7, figure 4). registered two to three times the movement that was registered at the 0.75-ft depths on the outside deflection gage row (static row 11). The surface deflection gages were located on the inside soil pressure cell row (static row 5) in each item. These large permanent deformations in the middle of the traffic lane were evidenced by the visible rutting in the middle of the traffic lane. This rutting or depression was larger in the middle of the traffic lane than on the sides, as evidenced by visual observations and by registrations of the 0.75-ft-depth gages on the outside deflection gage row (static

row 11), which was within the traffic lane. The other deflection gages showed a decrease in consolidation with depth. The 2.75-ft-depth gages did not show the large, sudden permanent movements as the shallower gages but did show larger movements than the deeper gages. In both items, the 4.5-ft-depth gages showed more consolidation than the 7.5-ft-depth gages, with the ones in item 4 showing more than those in item 3. The 7.5-ft-depth gages also showed more consolidation in item 4 than item 3 but to a lesser degree than the 4.5-ft-depth gages. All deflection gage histories show a decrease in erratic behavior for both items during the applied traffic period.

After the end of applied traffic, the histories show that the consolidation continued in items 3 and 4 in lane 1, but was beginning to decrease in February 1970, 4 months after the termination of applied traffic. However, there has been activity on the test section items since the termination of traffic that may be the cause for the continued consolidation. Five days after the termination of traffic, static load selected pattern tests were run with the 360,000-1b 12-wheel test cart. At the end of October and the first of November 1969, static load partial pattern tests were run with a 50,000-1b single-wheel load and twin-tandem 240,000-1b load, which were the largest loads used. These static load tests induced another large, sudden permanent movement (consolidation) that registered on most of the deflection gages. A few shallow-depth gages showed a release or uplift (this behavior will be discussed later in analysis). These sudden changes and the continued consolidation can be seen on the deflection gage histories. Between the static load tests on 10 and 29 October 1969 and afterwards, the test section experienced a small amount of vehicle and construction equipment traffic. The items also underwent vibratory tests with the large WES mechanical vibrator. The small amounts of traffic are believed to have kept the consolidation continuing and, primarily, the vibratory tests to have induced consolidation. The deflection gage histories show that a few gages stopped registering movement in January 1970 and that all movement or consolidation decreased in February 1970. The histories also illustrate a marked decrease in erratic behavior, and after the last static load tests, the rates of consolidation at all depths tended to be about the same again as before any testing started. To enforce the evidence of consolidation, the pore pressure histories in figure 76 show that the pore pressures have been dissipating since the additional static load tests.

3. INTERPRETATION OF DEFLECTION DATA

a. Static Load Tests

The initial reduction of the static load deflection data is presented in the data tables in Appendix A. Induced movements for each load were calculated by taking the difference between the load data and the no-load conditions before and after the load tests. This yielded the data shown in values labeled total and rebound.

Previous work on soil behavior under prototype aircraft loadings indicated that residual strains and stresses would occur in the MWHGL test section under the load tests. If residual strain or locked-in deflections did occur under loading, the next load test would theoretically have to overcome these locked-in strains before measurable deflections would be registered. If deflections occurred under the next load, the residual strains from the previous loads or load would have to be added to these to obtain the total induced deflections. The above reasoning is the basis for running the light-load tests first and the heavy-load tests last.

The first step in analysis of data was to establish the zero reference of each deflection gage. This zero reference is the datum from which the gage is operating under load and is the reference from which all movements are to be taken and calculated. Logical considerations would point to either a horizontal reference datum with respect to time or a gently sloping reference with time. The horizontal reference would assume no permanent deformation or induced consolidation and would allow for residual strains induced under load in the soil. A gently sloping reference would allow for permanent deformation, induced consolidation, and residual strains to be induced under load.

An early consideration was to use the previously discussed deformation history that was kept for each gage as the reference datum from which each gage was operating. A line of best fit or a line encompassing all of the data would be established. This reference datum would represent the no-load conditions of the soil at the particular gage location, and it would be used by subtracting the load-induced responses of the gage from it in order to obtain the total deflection experienced by the gage. The value obtained from this procedure would assume that residual strains had occurred and were accounted for by the method. Total elastic deflection would be obtained, and the

permanent deformation would be taken care of by the sloping reference datum. Once the difference between the reference and the induced response was obtained, this value would then be multiplied by the gage calibration factor, discussed in Volume III-A, to convert it into inches of deflection. Residual strain could also be separated from this value of deflection. This procedure seemed reasonable and appeared to be satisfactory based on the deformation histories of the deflection gages for the 15,000-lb-per-wheel load tests. These histories showed the behavior of the deflection gages was consistent and appeared to yield an almost horizontal line with time, which would indicate very little, if any, induced consolidation or permanent deformation.

Upon conducting the 30,000-lb-per-wheel loads tests, the deformation histories showed a definite change in behavior (figures 67 and 68): more induced consolidation occurred than under the 15,000-lb-per-wheel load tests, and the gages appeared to be erratic. These deformation histories for the 30,000-lb-per-wheel load test period made the first consideration of a reference datum doubtful. A reference datum line was established from the gage histories for the 30,000-lb-per-wheel load tests; however, it yielded different, not comparable, amounts of deflections under duplicate load points and on duplicate gages. This clearly proved that a reference datum established from the above procedure was not operating in the measured soil behavior data and in the soil behavioral patterns.

Based on the above results, a rigorous analysis of the static load data was undertaken in order to find and analyze the trends and patterns exhibited by the soil-response data and to arrive at the best method for presenting the final results. This analysis yielded some very interesting results pertaining to the soil behavior of the MWHGL test section.

In this analysis the raw data taken under all static loads for both items were plotted. All deflection gage responses were plotted in the form of offset distances versus deflection for the gage depths. Four values were plotted at each offset for a gage: initial no-load reading, load reading, immediate final no-load reading, and a delayed (10 minutes to several days) no-load reading. The taking of these readings and the times were discussed under major testing program. These plots yielded four curves for a particular static load test on each gage. The curves were labeled load curve, elastic rebound curve, delayed elastic rebound curve, and initial no-load reference

curve. Figures 77 and 78 show plots that are typical examples for all deflection gages in both items. The particular curves shown are for item 3; figure 77 is for the 7.5-ft deflection gage and figure 78 is for the 0.75-ft gage. Both curves represent actual data taken on these gages under the 360,000-lb 12-wheel static load tests with tire inflation pressures of 100 psi and at load point 1 of the assembly. For both figures, the offset axis represents offsets perpendicular (north-south) to the direction of travel (eastwest). As an example of constructing these plots, at any given offset distance before the load was moved into position, an initial no-load reading existed for the deflection gage. Upon moving the load into position and after waiting for stability to be reached, a load reading was taken. The load was moved off and a rebound reading was taken immediately; however, at some later time, 10 minutes, an hour, or several days (over a weekend), another final no-load reading was taken. These readings were then plotted at the offset position as initial nc-load, load, rebound, and delayed rebound readings, respectively. For the next offset position to be loaded, the final no-load reading (the delayed reading) from the last offset position served as the initial no-load reading if only a short time had elapsed or if the reading had not changed (the gage readings did not change after the first delayed noload reading), and the load and unload procedures were repeated for this offset. After plotting all offset readings for a gage, including zero offset, the four curves representing the soil behavior were then drawn.

Several interesting trends of soil behavior were apparent from this method of analysis. As can be seen in the example figures, the initial noload reference, delayed elastic rebound, and elastic rebound curves follow the behavior of what is labeled as the load curve. This behavior is dramatically shown in figure 78. Also shown in figure 78, to a greater extent than figure 77, is the shift of the initial no-load reference. This occurs because it is actually the delayed elastic rebound curve shifted one unit of offset. The values on these curves, delayed rebound and initial, are the same; however, at one point a value represents a delayed final no-load reading, and at another point the same value represents an initial no-load reading.

Figure 78, which is for the 0.75-ft-depth gage, better illustrates the curves following the load curve because this is a shallow gage, and it consequently reflects the individual effects of each load tire from assembly

load point 1 perpendicular to the direction of travel (see figure 1). Figure 77, which is for the 7.5-ft-depth gage, illustrates that the individual effects of the various loaded tires are reduced with depth, and the maximum response is being attained at load point 1 where the effects of the various loaded tires are additive with depths. Another interesting phenomenon is the curve labeled delayed elastic rebound; it appears to be almost parallel to the immediate elastic rebound curve and approximately at a constant difference from the rebound curve. The data points shown on this delayed rebound curve represent readings delayed from around 10 minutes to several days. In other words, a point on this curve might represent a delayed reading of 15 minutes and a point at another offset might represent a 3-day delayed reading; however, the curve formed by these points is a constant amount different and parallel to the immediate elastic rebound curve. A delayed rebound occurred, within a few minutes, that remained constant and did not appear to be time dependent for more than a few minutes. This rebound reading remained constant for several days or even a week until another load was applied.

The difference between points on the initial no-load reference curve, or the delayed rebound curve, at different offset values is not believed to be residual strain or permanent deformation that occurred in the soil under load. As ean be seen on these plots, there does appear to be a very small strain that is released when loading at the wide offsets. These plots show this at the 10- to 12-ft offsets by both the immediate elastic rebound and the delayed rebound values being less than the initial no-load values.

Also ading support to the belief that residual strain did not occur under load is the fact that for each deflection gage, the next static test, whether it was with a different assembly or load (lighter or heavier) or both, started operating from an initial no-load reference that was approximately the same as the last delayed reading for the previous test. This occurred even after several days of dynamic load testing between static load tests.

The erratic behavior observed on the deformation histories (figures 67 and 68), especially during the 30,000-lb-per-wheel test period, occurred mainly during the dynamic load tests. The reference level of the soil and a gage appeared to be a function of the distance from a gage (the row) at which testing stopped after a day of dynamic runs. In other words, if a dynamic load test stopped on a row representing a 4-ft south offset from a gage, a

certain reference level in the soil was established, which was lower than the initial reference level at which the dynamic runs started several rows further south. This reference level was similar to the behavior shown in figures 77 and 78, and it held whether several hours or days elapsed before the next test. Upon continuing the dynamie load tests the next morning or after a weekend, the reference level continued to go down for rows eloser to the gage until the row upon which the particular gage was located was run. At this row the reference level for the gage reached its lowest point and the maximum deflection registered by the gage occurred. If dynamic load runs were stopped on this row for several hours or days, the reference level remained at a constant value as before. When dynamic load tests were resumed, these tests would be on rows going north away from the particular gage row, and the reference level would come up with the distance away from the gage. On the last dynamic row run, which would be the most northern row from the gage, the reference level would be back up to approximately the same value at which it started at the first most southern dynamic row. This value would also be approximately equal to the last delayed reading for the previous static load tests, and it would maintain its stability until the next static load tests were started, whether they were several days later or less.

Figures 77 and 78 show the responses of deflection gages on the outside gage row; therefore, these curves do not show the loaded assembly passing over the gage because this was the last static row upon which tests were conducted. The curves, as shown in these plots, drawn for the deflection gages on the inside gage row show the same behavior for the static load tests as that described above for dynamic load tests. Curves for these inside gages move upward after the maximum load points pass over the gages. (They came up in incremental moves, with respect to the offsets going north away from the gages, shown by both the immediate clastic and delayed rebound readings being less than the initial no-load values.) They were not allowed to move up completely due to the north-south static load offsets being a maximum of 4 ft after the gages were passed over.

The most interesting result from the previous discussions of the dynamic and static load tests was that a reference level for each deflection gage was following what is called the load curve from both static and dynamic load tests. This reference level represents a load- and position-dependent, movable reference from which a gage and the soil behavior were

operating. This reference level moves up and down with the offset from a gage. If the last static load test on a gage was at the maximum or zero offset, then the responses from the next tests with a different assembly, whether they were dynamic or static loadings, started operating from this reference level. Also, if the last static load test for a gage was at an offset, the reference level would have moved up from the zero offset level and would be the reference level at which the next series of tests started operating. The next series of tests would start on the most southern static row if static tests and on the most southern dynamic row if dynamic tests. The start of this next series of tests would cause further movement upward of the reference level for a few offset distances; then the reference level would start down. This behavior would occur whether the next tests were with lighter or heavier loads.

This moving reference level is not believed to be residual strains being built into the soil and then being released. If residual strains are assumed to be active in the soil and if they are corrected for by adding them to the load readings under symmetrical load points (assembly load point 2 for the 12- and 6-wheel assemblies), then duplicate deflections do not occur on the same deflection gage at a given depth. nor do they occur on the duplicate gage at that depth. When no residual strains are assumed and the soil behavior is assumed to be acting from the moving reference, duplicate deflections do occur on the same and duplicate gages at symmetrical assembly load points. Duplicate deflections also occur at duplicate gages under the singlewheel tests if the moving reference is used. As discussed previously, this moving reference level continues to rise at the start of another series of tests for a few offsets toward the gage before it starts downward. In other words, a peak occurs at the beginning of each test series, and the difference between these peaks represents the permanent deformation or induced consolidation caused by the last test series.

Based on the foregoing discussion and analysis of the soil behavior, the conclusion from this behavior must be that, for lack of better terms, the soil acted as a plastic and elastic mass (similar to put;), but not as a viscoelastic material. It was plastic to the extent of being stable at various levels to which it might be worked under loaded conditions without inducing appreciable residual strains; however, it exhibited elastic behavior at each of its changing levels of plasticity with the elastic behavior operating

from the varying level. Based on this conclusion and actual field behavior under the lighter loads, the sequence of running lighter loads first did not matter. They could have been run any time because no residual strains that would have to have been overcome were induced under the heavy loads.

Working under the hypothesis just stated, the fact is evident that at a given load point, the true total deflection, including permanent and elastic, cannot be determined because the rebound of the soil may be greater than the initial movement due to the changed reference level. This also implies that the true initial no-load reference point is not known due to the changed reference level; therefore, the only truly known point of reference is the rebound value, which defines the moving reference level, and consequently the only truly known measure of movement is the rebound.

Due to the large quantity of data as previously discussed, only an analysis of the maximum soil response has been made because of the time limit for this report. This analysis of maximum response is the soil response with depth under the assembly load points, and this will be presented in the following sections of this part. The maximum response results were based on the soil behavior analysis and hypothesis discussed in the preceding paragraphs. As can be seen from the hypothesis of soil behavior, only the elastic response of the soil could be determined. From the soil behavior curves drawn for each gage and loaded assembly, the maximum elastic response was determined and is the difference at a point between the load curve and the delayed elastic rebound curve. Therefore, the data presented in tables A2-A13 are the initially reduced data and are slightly different from the values used to develop the depth versus maximum elastic deflection curves. These tabulated data values of rebound do not include the delayed rebound. The delayed rebound at a point has to be determined at each gage depth from the offset versus deflection curves of the soil behavior.

The second step in the analysis of data was to establish the movements of the 12-ft-depth reference plane and consequently the corrections to be applied to all deflection gage responses under load. Correction curves were required for each load assembly. As discussed in Appendix A, the data obtained from the optical reference rod readings were not very accurate and had a large variability due to the methods that had to be employed in obtaining the data. A curve of best fit through the scattered data plotted as offset versus elastic

deflection was not felt to be adequate; therefore, several methods of analyzing the data to obtain a good correction curve were tried. Offset versus theoretical elastic deflection curves were drawn by using various modulus of elasticity values and assuming Poisson's ratio of 0.5. The shapes of the theoretical curves were hoped to be useful to establish curves through the data; however, comparisons with the curves from actual measurements at the 7.5-ft depths proved they could not be used. Many offset versus theoretical elastic deflection curves for the 12- or 6-wheel assembly effects at 7.5-ft depth can be fitted across the actual measured data curves (see figure 79).

The method finally arrived at and felt to be accurate and applicable will be described in the following paragraphs. Offset versus vertical elastic stress curves were drawn for all loads and assembly effects at the 7.5-ft depth; these were drawn using the actual measured vertical elastic stress as registered on the WES pressure cells at this depth. The vertical stress axis of each was normalized to a percent scale with the maximum stress at 100 percent. Next, the deflection axes of the offset versus elastic deflection data curves at a 7.5-ft depth for each load and assembly were normalized to a percent scale with the maximum deflection at 100 percent. If these normalized curves of stress and deflection are overlaid or plotted on top of each other for each load and assembly, the stress and deflection curves almost coincide. In other words, for a given loaded assembly, the normalized elastic stress curve is the same as the normalized elastic deflection curve. The above procedure makes no assumptions of soil properties and no theoretical assumptions. Applying the procedure t. the 12-ft-depth plane is following the soil behavior patterns.

On the basis of normalized vertical elastic stress versus offset plots made from the WES pressure cell responses at the 12-ft depth under all loads and assemblies, the shapes of the offset versus elastic deflection correction curves for the loads and assemblies were obtained. For the 12-ft reference plane, the data obtained from the 6-wheel 180,000-lb static load test were the best obtained with the optical measuring system: therefore, the shape of the normalized curve of offset versus elastic deflection for the 6-wheel 180,000-lb load was forced at the maximum elastic deflection point. Thus the correction curve for the 6-wheel 180,000-lb static load tests was obtained. Curve shapes of all other loads and assemblies were forced at maximum elastic

deflection points determined from the ratio of their maximum elastic stress to the maximum elastic stress under the 6-wheel 180,000-1b tests; this was found to be true for the maximum elastic deflections and stresses at 7.5-ft depths. In other words, the ratio of maximum elastic deflection for two loads and/or assemblies was found to be equal to the ratio of the maximum elastic stresses of the same two loaded assemblies. This procedure for matching the curve shapes to the maximum elastic deflection points at 12 ft is also compatible with the soil behavior. The resultant correction curves established for each load and assembly by the foregoing procedures fell within the scatter of data for each. The fact that the actual data for each load and assembly fell around the curve for that load and assembly gives some validity and weight to the correction curves. These correction curves for all loads and assemblies are given in figure 80. These curves must be used to make corrections to all deflection gage responses by adding the 12-ft-depth reference plane movements to each gage response.

The third step in the analysis of data was to determine the separate effects in the soil of the prime movers and consequently to establish correction values to be subtracted from the load data. This was the purpose of performing tests with the empty prime movers, as described previously under major testing program. An analysis of the soil deflection data collected under the 12- and 6-wheel prime mover without the load carts yielded negligible amounts of elastic deflection, if any, for both items 3 and 4. Even though the dead loads were high (approximately 30,000 lb per wheel), the outrigger wheels were spaced wide enough apar and the tire inflation pressures were sufficiently low so that no corrections were needed.

The single-wheel load vehicle had a deadweight of only 6000 lb that had no measurable effects on the measured soil response. However, the dead load of the tw. -tandem prime mover did have effects that required correction of the test data. The dead loads were high and the outrigger wheels were closely spaced. An analysis of the elastic deflections produced by the twintandem prime mover yielded the corrections given in table 5 for each assembly load point and for both items 3 and 4. As can be seen, the deflections were greater in item 4, and only maximum load point corrections are listed. These

corrections must be subtracted for all assembly load data taken with the twintandem test cart in each item.

Table 5

Corrections Due to Prime Mover To Be Applied to All Twin-Tandem Maximum Deflections

for MWHGL Flexible Pavement Tests

Item	Depth ft	Correction Point 1 in.	Correction Point 2 in.
3	0.00	0.002	0.003
	0.75	0.002	0.003
	2.75	0.002	0.002
	4.50	0.001	0.002
	7.50	0.001	0.001
	12.00	0.000	0.000
l,	0.00	0.00	0.007
	0.75	0.00/	0.007
	2.75	0.005	0.00
	4.50	0.001	0.0014
	7.50	0.001	0.002
	12.00	0.001	0.001

Once the reference level for each deflection face under each loaded assembly was established, the elastic deflections determined, the 12-ft-depth reference plane corrections made, and the prime mover effects corrected, then static load elastic deflection curves were drawn. Depth versus maximum elastic deflection curves were drawn for both load points 1 and 2 for each loaded assembly except for the single wheel, which had only one maximum load point. In the upper 2 to 3 ft of the pavement structure, load point 2 is the maximum elastic deflection curve, and beneath 2 to 5 ft, load point 1 is the maximum elastic deflection curve. The curves of load points 1 and 2 cross generally at about the 3-ft depth. From these two curves, what is labeled a limiting maximum elastic deflection curve can be drawn. It is formed by drawing a tangent between the upper portion of load point 2 curve and the lower portion of load point 1 curve; the tangent bridges the point where the

two curves cross. This limiting curve is then in three parts: load point 2 curve at shallow depths, the tangent at intermediate depths, and load point 1 curve at deeper depths. The limiting maximum elastic deflection curve represents the maximum values with depth that would ever occur at any point under the loaded assembly; in other words, elastic deflections at any point under the loaded assembly would be less than or equal to, never greater than, the limiting curve values. These three static load curves (load point 1, load point 2, and limiting curve) versus maximum elastic deflection are given for each load and assembly and for both items 3 and 4 in the next section.

In developing the depth versus maximum elastic deflection curves for item 3, the duplicate deflection gages had equivalent responses; therefore, the values used to draw the curves are averages of the responses at each depth. The consistency of these responses is discussed in Appendix A. However, a difference existed in the readings from the duplicate deflection gages in item 4, and the cause was undeterminable. The cause can possibly be attributed to something in the complete electrical system for the duplicate gage row. As will be discussed later, there was a difference in the stress and strain distributions of items 3 and 4. Item 4 experienced larger induced stresses and strains than item 3 due to the soft 2-CBR layer built into item 4. This soft layer is between the 4.5- and 7.5-ft depths: therefore, it mainly affected the stresses and strains above the 7.5-ft depth.

When the deflection data from duplicate gages in item 4 were plotted, a difference that increased with increase of load was apparent. This difference, as discussed in Appendix A, was of a constant amount at each duplicate deflection gage location for a given loaded assembly. The outside deflection gage row yielded results at the 7.5-ft-depth gage that were comparable with the duplicate gages at 1. It in item 3 under each loaded assembly; the inside gage row of item 4 showed responses that were always greater. No method exists for determining which gage row in item 4 was in error. Based on the comparison at the 7.5-ft depth with item 3 and the 12-ft corrections being the same for both items, the cutside deflection gage row of item 4 was assumed to have yielded the correct results, and these results are presented on the curves for item 4 in the next section of this part. The curves presented, as for item 3, represent the average of duplicate responses of the gages.

b. Dynamic Load Tests

Only one value is given in the data tables in Appendix A for the responses on each gage with the forward and reverse runs of the dynamic load tests. This value corresponds closely to the maximum elastic values determined for the static load tests, using the procedures discussed in the preceding paragraphs. Basically, the analysis of the dynamic load data was the same and has the same associated problems as the analysis of the static load data.

The first step in the analysis of dynamic load data was to establish the zero (no-load) references from which each deflection gage was responding. Behavior of the soil during dynamic loading was discussed previously with the static load behavior. Based on the behavior exhibited during the dynamic and static load tests and to be consistent with the analysis of the static load test data, a reference was chosen that would be comparable to the static load test data reference. The delayed rebound reference level was chosen for the static load tests, and, consequently, the reference level chosen for the dynamic load tests was after the test cart had passed over the gages in a dynamic run. This reference level represents the immediate elastic rebound value; however, the delayed rebound did not appear to be as large, if it existed at all, as that for the static load tests. The procedures for obtaining the data from oscillograph records is given in Appendix A.

Mover during dynamic runs. The 12- and 6-wheel prime mover did not have an effect on the gages for the main instrumented rows. As determined from the static load tests, the single-wheel vehicle also had no effect. The effects of the tvin-tandem prime mover were determined by the same procedure as for a loaded assembly and were subtracted from the total response.

Once the data were obtained from the oscillograph records and corrected if required, they were plotted in comparison with the static local test data without the 12-ft reference plane corrections. These comparisons showed that the dynamic load results were approximately the same as the static loadings; consequently, the corrections for movement of the referenced plane determined for the static load tests were applied to the dynamic load test results. Where the dynamic load curves were slightly different from those for

the static loads, the dynamic load curves were extended on down to the 12-ft depth keeping about the same difference as that at the 7.7-ft depth. The above comparison and procedure were followed after the limiting maximum elastic deflection curves were drawn for the assemblies of the dynamic load tests the same as for the static load tests discussed previously.

The dynamic load test results for item 4 showed the same difference between the duplicate deflection gage rows as discussed for the static load tests; therefore, the dynamic load test results on the outside deflection gage row in item 4 were used to develop the depth versus deflection curves. Depth versus maximum elastic deflection curves and limiting curves for all dynamic load tests are presented later. Direct comparisons with the static load curves are also presented. All curves presented, as for the static load tests, represent averages of responses on the gages; the consistency and reproducibility of the dynamic load tests are discussed in Appendix A.

4. DEFLECTION TEST RESULTS

a. Item 3

Maximum elastic deflections under static and dynamic loads in item 3 are presented in figures 5-11. Figure 5 gives the static load deflections with depth in item 3 at assembly load point 1 (see figure 1) for all loads and assemblies. Also given in this plot are the limiting curves for all assemblies, with the exception of the single wheel. The single wheel has only one load point, and it is always the maximum: therefore, the single-wheelload curve is automatically a limiting curve. Assembly load point 2 static load deflection curves for item 3 are shown in figure 6. The curves for the single-wheel load (which does not have load point 2) are also shown but only for comparative curposes. As can be seen in these two figures for load points 1 and 2, the twin-tandem 120,000-1b-load curves show that the different tire inflation pressures were effective only at shallow depths and that the deflections under the 6-wheel 180,000-1b load were not much less than the deflections under the 12-wheel 360,000-1b load due to the large spacing between the two 6-wheel groups of the C-5A 12-wheel assembly (see figure 1). Also clearly shown are the effects of the large 240,000-1h twin-tandem load.

Figure 7 gives the curves of load points 1 and 2 together with the tangent between them, which forms the limiting curve, for each loaded assembly

in item 3 except the single wheel. This figure shows the comparisons of load point curves for each assembly. The horizontal scale of the plot is constant with the deflection axis variable. In other words, the curves for each loaded assembly have been spaced in such a way that a minimum of overlap would occur; the zero point of the deflection axis for each loaded assembly is different. Values along the deflection axis apply only to a particular loaded assembly; these values are the reference points for each assembly. Any values taken from these curves must be calculated from the reference point for the loaded assembly using the horizontal scale of the plot. These curves are presented in this combined form only to show the comparison between load points for each assembly; they are not used to obtain specific values. The curves are the same curves as presented in figures 5 and 6.

To summarize the previous figures for the loaded assemblies that were of primary interest to this study and to the sponsors, the limiting curves for the single wheel at 30,000 lb, the 12 wheels at 350,000 lb, and the twin tandem at 168,000 lb were replotted in figure 8 for item 3. The twin-tandem 168,000-lb-load curve is an interpolated curve for which the basis and procedures will be given later.

The next three figures (9-11) show the deflections measured during dynamic load tests in item 3: figure 9 shows assembly load point 1 and limiting curves; figure 10, assembly load point 2 with the single-wheel results shown for comparison; and figure 11 shows the comparisons of load point curves and the tangents for the limiting curve of each loaded assembly. No dynamic load tests were run with the single-wheel 50,000-lb load or the twin-tandem 240,000-lb load. The deflections at the 12-ft depth came from the static load tests, as discussed in analysis of data, and the basis for this will be presented later. Finally, no summarization is presented for the dynamic load test, as was done in figure 8 for the static load tests, because the dynamic load deflections were approximately equal to those for the static load tests. Figure 8, is therefore, true for both static and dynamic load deflections, as will be shown later.

b. Item 4

Figures 12-18 present maximum deflections for static and dynamic loads for item 4. Figures 12-14 are for static load deflections of load

point 1, load point 2, and comparisons of the load point curves, respectively. The limiting curves are also shown on these plots. Figure 15 summarizes the limiting curves for the loaded assemblies that were of primary interest: the single-wheel 30,000-lb load, 12-wheel 360,000-lb load, and the interpolated twin-tandem 168,000-lb load. Also shown is the location with depth of the soft 2-CBR layer in item 4. Figures 16-18 show the dynamic load deflections of load point 1, load point 2, and comparisons of the load point curves, respectively. The dynamic load test results were not summarized because they were approximately equal to the static load deflections.

c. Surface Deflection Basins

Figures 19-21 show the static load deflection basins measured by the surface deflection gages for both items under the 12-wheel 360,000-1b load, the single-wheel 30,000- and 50,000-lb loads, and the twin-tandem 120,000and 240,000-1b loads. The deflection basins represent total deflections, so they could be compared to the optically measured surface deflection basins presented in Volume II. (The optical measurements could not be made with enough accuracy to distinguish between total and elastic deflections.) Optically measured basins are shown superimposed on these deflection gage curves, and, as can be seen, the optical system was not accurate enough to show the true shapes of the curves. These figures show the deflection basins both parallel and transverse to the direction of traffic. No surface instrument measurements were available for the single-wheel 50,000-1b load or the twintandem 240,000-1b load in item 4. These static load tests were run after traffic testing and, consequently, after the surface deflection gage in item 4 had become inoperable (discussed in Appendix A). An inconsistency between the optically measured basin and the deflection gage measured basin parallel to traffic for the twin-tandem 240,000-1b load is shown in figure 21. Examination of the data for both types of measurement revealed no explanation of the difierences.

d. Comparison of Limiting Curves

(1) Static versus dynamic loading. Figures 22 and 23 show comparisons of static and dynamic maximum elastic deflection limiting curves for each item. These curves were plotted for comparative purposes only and are the actual curves presented previously but are plotted on a variable deflection axis for the purpose of getting all comparisons on one plot with a

minimum of overlap. If these curves are to be used for obtaining specific values, the reference value for each loaded assembly on the deflection axis must be used to calculate deflection values for the particular loaded assembly.

As can be seen in figure 22, the dynamic load deflections in item 3 are very close in agreem at with the static load deflections below a depth of about 3 ft. This was the basis for extending the dynamic load deflection curves down to the 12-ft depth, and discussed under analysis of data. From the 7.5-ft depth up to the surface, the curves show the actual comparison as if the 12-ft reference plane movements were subtracted from both. If the 12-ft correction were to be subtracted, the complete curves would shift to the left a constant amount equal to the given deflection at 12 ft. Also noticed on these curves is the fact that all dynamic load deflection curves lie to the left of the static load curves. The reason for the dynamic and static load curves being in such good agreement is that maximum elastic deflections were used for their development.

Elastic deflections should not be dependent upon slow-speed load application; in other words, the speed of a slowly moving vehicle should not appreciably affect elastic deflections. Elastic deflection is not time dependent, whereas plastic deflection or deformation is time dependent. The difference in the curves could be accounted for by the static load elastic deflection including delayed rebound (discussed under analysis of data) and the dynamic load elastic deflection not including this delayed action. All speeds for the dynamic load test carts were approximately 2-3 mph.

Comparisons of static and dynamic load tests for item 4 are shown in figure 23, plotted the same way as for item 3. The previous discussion for item 3 also applies to these curves; however, the static and dynamic load data are not in as good an agreement as for item 3. This difference between the static and dynamic load curves in item 4 could be caused by the influence of the soft 2-CBR layer increasing the delayed action more than that in item 3. As in item 3, all dynamic load curves lie to the left of the static; the speed of the dynamic load test carts was the same as for item 3.

(2) Item 3 versus item 4. Figure 24 gives a comparison of limiting maximum elastic deflection curves for static loading of item 3 versus item 4. These comparisons are plotted on a variable deflection axis, the same as for

previous comparisons and for the same reasons. In figure 24 the soft 2-CBR layer in item 4 is delineated, and as can be seen, this soft layer greatly affects the strain distributions under all loaded assemblies in item 4. This effect, as shown, also increases with load increase, and the action of this soft layer can be seen to be mainly effective from the bottom of the layer (7.5 ft) upward, with the main difference between item curves occurring within the soft layer. Deflections at the 7.5-ft level are approximately equal in both items for the lighter loads, with the difference increasing with increase in load. This close agreement at the 7.5-ft depth for both items was the hasis for assuming that the outside deflection gage row of item 4 was yielding correct results, as was discussed under analysis of data.

Figure 25 presents a summary of the static load limiting curves of primary interest: the single-wheel 30,000-lb load, 12-wheel 360,000-lb load, and the twin-tandem interpolated 168,000-lb load. This plot is not on a variable deflection axis. These curves are the exact data curves presented previously, except for the twin-tandem interpolated curve, but they are in proper perspective with respect to the deflection axis. Again, the effect of the soft layer is very evident.

Figure 26 gives the comparison of limiting maximum elastic deflection curves for dynamic load tests of item 3 versus item 4. These curves are presented in the same manner as the previous static load test comparisons with respect to a variable deflection axis and the soft layer of item 4 being delineated. As is evident from the previous comparisons of dynamic to static loading in each item and then comparisons of static load test results in item 3 to item 4, these curves show the exact same relationships as previously discussed for item 3 versus item 4 static load comparisons. The fact that these dynamic load curves for each item are also in close agreement at the 7.5-ft depth adds some confirmation to the assumption that the gages in the outside row in item 4 were registering correctly. A summary of the dynamic load curves of primary interest is not presented because it would be the same as that shown for static load tests in figure 25.

The conclusion from comparisons of static and dynamic load deflection curves of item 3 versus item 4 must be that each item has different soil strain distributions as a result of the soft 2-CBR layer in item 4. This soft layer appeared to have large elastic deflections; however,

it was deep enough that its action was not detrimental to the overlying pavement structure. It appears to be acting almost as a layer of springs beneath a semirigid structure.

5. INTERPRETATION OF STRESS DATA

a. Static Load Tests

The initial reduction of the static load vertical stress was as presented in the data tables in Appendix A. Induced stresses for each load were calculated by taking the difference between the load and the no-load conditions before and after the load tests. This resulted in the values of total and rebound listed in the data tables.

The same steps in analysis as those taken for the deflections had to be made: a zero or no-load reference and corrections for each pressure cell had to be determined. Initial analysis of the vertical stress data also had to begin with the determination of the reference datum from thich each cell was operating under load. As can be seen from the stress histories in figures 63 and 64, the histories indicate a horizontal reference with time for each cell during the testing periods. The erratic behavior exhibited on these histories is believed to indicate residual stresses that are a function of the last offset position of the test assembly before the readings were taken; the behavior is similar to the varying reference levels discussed for the deflection gages. However, the long-time trend of the stress histories is a horizontal reference for each WES pressure cell. Based on the behavior shown on these plots, as previously discussed, the SA-E pressure cell data were not used or considered in the final analysis.

In order to verify the stress history indications, an analysis similar to that performed on the raw deflection data was conducted by plotting the raw stress data for each soil pressure cell in the form of offset versus stress. The stress was plotted in units of strain but could be changed directly to psi by the cell calibration factor. As was done for the deflection gages, four values were plotted at each offset for a cell: initial no-load reading, load reading, immediate final no-load reading, and a delayed reading. The soil pressure cells did not register a delayed change as the deflection gages did; therefore, the delayed readings were approximately the same as the immediate final no-load readings. These two readings did vary, but the variation was within, and is believed to be due to, the degree of resolution or

accuracy of the strain indicator. Also, the final no-load readings were approximately equal to the initial no-load readings varying around it by a small amount due to the reason given above for the delayed readings.

Figure 81 shows the stresses registered by a WES pressure cell at a 12-ft depth under the 12-wheel 360,000-lb load test for assembly load point 1. The slight variations of the initial and final no-load readings can be seen. A line of best fit through these values would slope down, but if the plot were continued on the other side of the assembly load point 1, the line would slope up. As in the deflection analysis, if a cell was the last load position for a loaded assembly, the initial values would increase with the start of the next series of tests. The difference between the initial values at an offset and at the centered position is believed to be due to residual stress. This residual stress increased for the shallow-depth cells; in other words, induced residual stress was most evident at the shallow-depth pressure cells and decreased with depth.

Residual stresses were active on the soil pressure cells and were induced and released depending on loading positions. If the residual stresses on the cells were not added to the initial readings, equivalent induced vertical stresses at symmetrical assembly load points and at duplicate pressure cell locations did not result. However, when residual stresses were added to the initial readings, equal vertical stresses were induced on duplicate pressure cells and at symmetrical assembly load points. This analysis of the data from soil pressure cells verified the indications of the stress histories, and a horizontal reference datum was established for each pressure cell and for each series of tests. For each series of tests, the values used to develop the maximum vertical elastic stress versus depth curves (presented later) were the differences between the horizontal reference datum for a particular cell and the load responses of that cell.

Three curves of stress versus depth were developed similar to the deflection curves discussed previously. For all but the single-wheel loads, a load point 1 curve, a load point 2 curve, and a maximum limiting curve were drawn. The physical meaning and relation of these three curves are the same as discussed previously for the deflection curves. These curves, as for the deflection curves, represent averages of responses on individual and duplicate cells. The data used for these curves were considered elastic stresses

because the active residual stresses were completely recoverable. Residual stresses have not been added to the data presented in Appendix A.

No corrections were required for the effects of the dead loads of the assembly prime movers. A study of the results of the static load data taken under the prime movers without the wheel assemblies showed that negligible changes did occur, but they were not within the resolution or accuracy of the strain indicator. Therefore, they must be considered random errors in the reading or monitoring of the pressure cells.

All of the above procedures were applicable to items 3 and 4. Item 4 did show different stress distributions than item 3 due to the soft layer in item 4; however, no discrepancies between cell rows existed as they did for the deflection gage rows.

b. Dynamic Load Tests

Only one value is given in the data tables for the responses on each pressure cell with the forward and reverse runs of the dynamic load tests. These values correspond closely to the maximum elastic stresses determined for the static load tests in the previous analysis. The analysis of the dynamic load tests with respect to initial no-load reference and corrections was basically the same as that for the static load tests. However, a study of the dynamic load test results of vertical stress indicated that residual stresses were not occurring under the dynamic loading, possibly because of the effect of the continuously moving load. To be consistent with the analyses of stresses resulting from static loads and deflections from the dynamic load tests, the reference datum for each pressure cell was taken as a horizontal line tangent to the cell's unload static trace. The data reduction procedures are given in Appendix A.

As for the static load tests, no corrections were necessary for the effects of the empty prime movers on the soil pressure cells of the dynamic test rows analyzed. For data from the outside dynamic rows, corrections for the empty prime movers would have to be made. No 12-ft-depth reference plane corrections are necessary for the pressure cell responses; however, pressure cells were located at this depth so that stress versus depth curves could be drawn to the 12-ft plane. Depth versus maximum vertical elastic stress curves and limiting curves for all dynamic load tests are presented in the next section. Direct comparisons with the static load stress curves are also made.

All dynamic load response curves represent averages of responses.

6. STRESS TEST RESULTS

a. Item 3

Maximum vertical elastic stresses and limiting curves for static and dynamic load tests of both items are given in figures 27-40. A single-wheel test cart has only one load point, and as for the deflections previously discussed, this load point produces the maximum limiting curve. Static load elastic stresses versus depth at assembly load point 1 for all loads and assemblies in item 3 are given in figure 27 along with the limiting curves, which were discussed in analysis of data. Figure 28 shows assembly load point 2 curves in item 3 with limiting curves; however, the single-wheel curves are also shown for comparative purposes. These two figures show the same relationship between the 6- and 12-wheel assemblies as did the previous deflection plots; i.e., the 6-wheel groups of the 12-wheel assembly are spaced in such a way that little stress effects of the two groups are additive. Also clearly shown are the large stresses under the twin-tandem 240,000-1b load.

Figure 29 gives, on a variable static stress axis similar to the variable deflection axes discussed previously, the comparisons of the curves of load points 1 and 2 and the limiting curve tangent for each load and assembly in item 3. The curves of primary interest are summarized for the static load stresses in figure 30. Presented are the limiting maximum elastic stress curves of the single-wheel 30,000-lb load, 12-wheel 360,000-lb load, and an interpolated twin-tandem 168,000-lb load. This twin-tandem curve was interpolated on a linear basis between the actual twin-tandem loads of 120,000 and 240,000 lb.

Dynamic load test results of vertical elastic stress in item 3 are presented in figures 31-33. The sequence of presentation on these figures is exactly the same as for the static load tests just discussed. No summarization of the curves of primary interest is given for the dynamic load tests because the stresses are approximately equal to the static load stresses, and figure 30 is representative of the dynamic load as well as the static load stresses. This fact will be established later.

b. Item 4

Figures 34-40 present static and dynamic load vertical elastic stresses in item 4. This series of figures is the same as those for item 3 just discussed. Figures 34-36 show the static load stresses at the assembly load points 1 and 2, respectively, as well as the limiting curves for each test load. Figure 37 summarizes the curves of primary interest for the static load vertical stresses in item 4 with the interpolated twin-tandem curve developed as described for item 3. Figures 38-40 present the dynamic load stresses at assembly load points and limiting curves for all assemblies. No summary for the dynamic load tests is presented because the stresses are approximately equal to the static load stresses.

c. Comparison of Limiting Curves

(1) Static versus dynamic loads. Figures 41 and 42 give the comparisons of limiting maximum elastic stress curves of static and dynamic load tests in items 3 and 4, respectively. These curves are plotted for comparative purposes only; they are the actual limiting curves presented previously but are plotted on a variable stress axis. The purpose for the variable stress axis is the same as for all other comparisons of either stress or deflection.

Figure 41 is the comparison of static and dynamic load stresses of item 3. As can be seen, the stresses are very close in agreement as were the deflections in this item. The discussion for the deflection comparisons also applies to these stress comparisons. Figure 42 gives limiting stresses for static and dynamic loads in item 4 presented in the same form as for item 3. As for item 3, these stresses are also in good agreement.

(2) Item 3 versus item 4. Figure 43 gives the comparison of static load limiting maximum elastic stress curves for item 3 versus item 4. The comparisons are plotted on a variable stress axis similar to all other comparisons. In this figure the soft 2-CBR layer in item 4 is delineated, and as can be seen, it influenced the stress distributions. This soft layer appears to have influenced the stress distributions more with increase of load and was effective for the full 12-ft depth of the test section.

A summary of the curves of primary interest for the static load stresses is shown in figure 44. These are the limiting curves for the

single-wheel 30,000-lb load, 12-wheel 360,000-lb load, and the interpolated twin-tandem 168,000-lb load for items 3 and 4. This is not a variable stress axis plot; therefore, the curves are in proper perspective. Also delineated is the soft layer of i am 4, and the effect of this soft layer on the stress distributions can be seen. These are the exact curves presented previously.

Figure 45 gives the comparison of the dynamic load limiting maximum elastic stress curves for item 3 versus item 4. These curves are shown on a variable stress axis. The soft layer of item 4 is again delineated on this plot. These curves show exactly the same relationships as previously discussed for item 3 versus item 4 static load comparisons, as is evident from the static versus dynamic load comparisons. A surmary of the dynamic load curves of primary interest is not presented because it would be the same as that shown for static load tests in figure 44.

These comparisons of item 3 versus item 4 for both static and dynamic load vertical elastic stresses show that the stress distributions of each of the items are different. This difference must be concluded to be due to the soft 2-CBR layer in item 4.

7. PORE PRESSURES AND TEMPERATURE EFFECTS

As stated earlier in this volume, pore pressures in the soil were not induced except the negligible pore pressures that developed under the maximum load tests: 50,000-lb single-wheel and 240,000-lb twin-tandem loads. Therefore, no analysis of pore pressures is made in this report. The fact that no pore pressures were induced under load was completely consistent with laboratory tests on the soil showing that the soil was not at 100 percent saturation. With no pore pressures developing, the soil pressure cell responses under load were the effective stresses induced in the soil.

A few load tests were conducted specifically at different temperatures of the air and pavement, but the temperature differential was not sufficient to cause measurable effects in the pavement structure. Therefore, no correlation between temperatures and pavement or soil behavior could be made.

8. INTERPRETATION OF PAVEMENT STRAIN DATA

Loss of the pavement strain gages and their consistency and reproducibility are discussed in Appendix A. Laboratory tests were not conducted with the strain gages prior to installation; therefore, the manufacturer's gage calibration factor had to be used to reduce the small amount of data that was obtained. Only one gage appeared to be operating properly at the beginning of the tests, but it did not operate long. The best results of this gage are presented in the next section, and since both the magnitude of response and behavior of the gage are doubtful, no reliance should be placed on the presented curves.

The problem of establishing a reference from which each gage was operating existed with the analysis of the strain gage behavior as with the deflection gages and pressure cells. Both the initial no-load gage readings and the final no-load gage readings were so scattered that a definite operation reference level was almost impossible to determine. The final no-load readings appeared to give the best reference. Use of this reference gives the elastic strain in the pavement, and this approach is also consistent with the methods used to obtain the elastic values of deflection and stress for the soil.

Once the reference was established, the load readings were subtracted from it and the difference multiplied by the gage calibration factor, resulting in the elastic strain induced at the bottom of the pavement. The best results obtained (presented in the next section) were for static load tests of the 12-wheel assembly loaded to 360,000 lb with tire inflation pressures of 100 psi. These data are presented as curves of offset versus strain.

9. PAVEMENT STRAIN RESULTS

The results presented here were the best obtained and are included only to give an indication of the induced strains at the bottom of the asphaltic concrete pavement of the test section. These results are from one strain gage in item 4 that measured strains transverse (north-south) to the direction of travel. Also these strains are for static load tests; no strains are available for dynamic load tests.

The results are presented in figures 49, 50, and 82. Figure 82 shows temperatures at the bottom and top of the pavement versus strain for no-load conditions. These measurements were made for several days with no testing or equipment allowed on the section. As can be seen, the bottom pavement strains are a linear function of the pavement temperatures. Figure 49 shows offset strains at distances parallel to the direction of forward movement for assembly load point 2 of the 360,000-1b 12-wheel assembly. As can be seen, the

gage did respond to the different wheels in alignment with load point 2 (see figure 1). In figure 50, strain at offset distances from load point 1 of the same 12-wheel assembly are plotted. At the top of the figure are offsets perpendicular to forward movement versus strain for which the row numbers correspond to the row on which point 1 was located when the strain was measured (figure 3 should be used with figure 50). The plot at the bottom of figure 50 is for strains at offset distances parallel to the forward movement for assembly load point 1. This plot, as for figure 49, shows the effects of the different sets of wheels. In this plot and figure 49, the letters on the offset axis correspond to the grid in figure 3.

10. SPEED TEST RESULTS

Figures 46-48 give the results of the speed tests (discussed under major test program) of the single wheel at the 30,000-lb load. These speed tests were conducted at four speeds: slow, about 1-2 mph; normal, about 2-3 mph; twice normal, about 5-6 mph; and fast, about 9-10 mph. Figure 46 shows the results of the maximum elastic deflection versus depth for both items. As can be seen, the speeds had a neglibigle effect on results of tests, and these curves are the same as the dynamic load single-wheel curves for the 30,000-lb loads presented previously. Also, these curves add evidence to the discussion presented earlier for the dynamic load elastic deflections at slow speeds being approximately equal to the static load elastic deflections.

Figures 47 and 48 give the dynamic load elastic stress of the same speed tests for each item. These curves are also the same as the previously presented dynamic load elastic stress curves, and they show no effect of slow speeds on induced elastic stresses.

11. ANALYSIS OF SOIL BEHAVIOR PATTERNS

In this last part will be given the first results of an analysis of the soil behavior patterns exhibited by the previously presented static and dynamic load test curves. The curves and plots presented in this section come from the actual data shown on the previous plots. Figures 51-53 are the results of this analysis. Figure 51 shows the deformation or induced consolidation versus depth that occurred under only the traffic testing phase of the project in the 12-wheel traffic lane. These curves are presented for both instrumented items with two curves per item: one curve represents the inside

deflection gage row, and the other represents the outside deflection gage row (see figures 2 and 3). The deformation was calculated from the beginning to the end of the traffic tests, and figure 51 shows the amounts that occurred at each deflection gage with respect to the 12-ft reference plane (this is why the curves go to zero at the 12-ft depth and does not imply that consolidation did not occur below 12 ft). Consolidation in the various layers can be calculated by subtracting the amount of consolidation at one depth from the amount of consolidation at a lesser depth.

The upper part of these curves, above 2.75 ft, shows the same results as found in test pits opened after traffic tests (see Volume II). These curves show that the movement, rutting, and heaving shown on the surface of the test section occurred in the subbase material with very little movement at the top of the subgrade. This subbase movement was probably lateral movement or lateral shear failure. The inside deflection gage row curves show that more movement occurred in the center of the traffic lane than at the sides of the traffic lane, shown by curves for the outside gage row. This was also evident on the surface. The sides of the traffic lane were probably compensated by material moving out from the center and over under the sides. Also evident on this plot is the fact that item 4 experienced slightly more induced consolidation and at a faster rate than did item 3. The consolidation in item 4 appears to have been slightly greater in the soft layer.

Figures 52 and 53 show plots of the theoretical elastic deflections (see reference 3) as compared to the actual measured elastic deflections for the 12-wheel 360,000-1b static load tests for items 3 and 4, respectively. The theoretical elastic deflection curves were computed for a homogeneous, isotropic, linearly elastic half-space with Poisson's ratio of 0.5; the curves were forced to match the actual data curve at the surface. Matching was accomplished by using the known elastic deflection and solving for the modulus of elasticity; therefore, this modulus was used to calculate the theoretical deflections to a depth of 12 ft. As can be seen, the comparison is worse for item 4 than for item 3. Also evident is the fact that the elastic deflection distributions of each item were different from those predicted by elastic theory.

Figure 79 shows for item 3 a comparison of the measured elastic deflection basin (offset versus deflection) at a depth of 7.5 ft with the

theoretical basin (reference 2). At a point on a horizontal plane in a mass, the assumptions of a linearly elastic, homogeneous, isotropic half-space should be approximately valid and the theoretical elastic deflection basin should be a good prediction; however, as can be seen, the comparison is worse, than for the theoretical and measured maximum elastic deflection versus depth curves. A similar plot for item 4 is not included, but it would show the same results.

In figure 54, the theoretical equivalent single-wheel load (ESWL) curve has been plotted for each item versus the ESWL curve calculated from the actual data. These curves are for the 12-wheel 360,000-lb load. The theoretical ESWL is based on the same theoretical deflection factors used for the curves in figures 52 and 53. A complete discussion of the theory and concepts of the ESWL is given in Volume IV of this series.

Figures 55-62 include only item 3 because plots for item 4 showed exactly the same behavior even though the values were different. These curves also show only the static load test data presented in figures 27-30; however, the dynamic load test data would produce the same curves.

Figure 55 is a log-log plot of wheel load versus elastic deflection for the single wheel. A curve results for each gage depth and the series of curves are approximately parallel. The important result to notice on this plot is that curvilinear relationships exis. Figure 56 is for the same single-wheel data but on a semilog plot; the curves show a greater degree of curvilinear relationship. Figure 57 is the single-wheel data again out on an arithmetic plot; however, as is evident, the relationships are linear for the range of loads run in the MWHGL tests.

Figure 58 is an arithmetic plot of wheel load versus elastic deflection for the 12-wheel assembly. The plot shows that a curvilinear relationship exists and is opposite to the results of the single-wheel arithmetic plot. Figure 59 is the same 12-wheel assembly data on a log-log plot; however, opposite to the arithmetic plot for the same load and opposite to the log-log single-wheel plot, this plot shows linear relationships. If this log-log plot were carried out for several more log cycles of both wheel load and elastic deflection, the plots would still be linear and would try to approach zero. On this plot, the lines pass through a range 0.001 to 0.003 in. on the deflection axis.

The twin-tandem wheel loads versus elastic deflections plotted on log-log scales show the same linear behavior as the 12-wheel plots. This is shown in figure 60. If the linear relationships on the log-log plots are assumed to be true, then the twin-tandem 42,000-lb wheel load (design wheel load of the Boeing 747), which is bracketed by both the 30,000- and 60,000-lb wheel loads, is immediately and accurately known. This is the interpolation for the twintandem 168,000-lb load elastic deflections presented earlier in figure 8 for item 3. The same interpolation was performed for item 4, resulting in the twin-tandem 168,000-lb elastic deflections in figure 15. Extending the above linear concept to the 6-wheel tests, which included only one wheel load, would result in the log-log plot in figure 61.

The last figure presented in this analysis is figure 62, which is stress versus strain for item 3. Strains were calculated by taking the difference between deflection gage elastic responses for each load and assembly and dividing by the distance between the gages. Stresses were obtained from the elastic stress versus depth plots for each load at the midpoint of the deflection gage distances. Stress versus strain curves, drawn from the calculated data, represent each layer or depth range. All of these curves are curvilinear. Actual values used for obtaining these curves are shown.

The main and most important conclusions drawn from this brief analysis of soil behavior patterns with respect to the MWHGL test section are: (a) the soil has a nonlinear stress-strain behavior that varies with depth and also load intensity; (b) the theoretical predictions of deflections are not good; (c) behavior of the pavement structure under multiple-wheel loads is substantially different from behavior under single-wheel loads, which indicates that the principle of superposition is not valid; and (d) even though item 4 showed different strain distribution characteristics, its soil behavior patterns on log-log plots are the same as those of item 3 but are shifted slightly to the right due to the elastic deflections being greater.

SECTION IV

KIGID PAVEMENT TEST PROGRAMS

1. INSTRUMENTATION

The rigid pavement ters section was instrumented to measure pavement deflection, surface strain, and subgrade pressure during static and dynamic load tests and under traffic. Complete descriptions of the test section, the instrumentation, and the techniques used in installation of the transducers are given in Volume III-A, as well as details of the sophisticated data acquisition system.

A total of 67 data points were established in the four rigid pavement test items. The locations were selected to collect data to adequately define the response of the pavement structure to multiple-wheel heavy gear loads.

Soil pressure was measured by eight pressure cells located at the pavement-subgrade interface, two positioned 3 ft deep in the subgrade, and two cells installed 7 ft deep in the subgrade directly under the 3-ft-deep cells. These locations were chosen because the pavement-subgrade interface was expected to be the area of highest pressure, the 3-ft-depth was the point at which the pressure was anticipated to be one-half of the interface pressure, and the 7-ft depth was the point at which the areas of influence of the leading and trailing six-wheel bogies were estimated to start overlapping.

Twenty-seven deflection gages were installed to measure both total and partial deflection. The total- and partial-deflection gages were intended to measure the recoverable and nonrecoverable deflections occurring in the entire rigid pavement structure and within a selected depth of the subgrade material, respectively.

Strain gages were installed to measure strain at the top surface and near the bottom surface of the rigid pavement.

2. TESTING EQUIPMENT

The testing equipment was the same as that used for the static load, dynamic load, and traffic tests of the flexible pavement test section.

3. PRELIMINARY TEST PROGRAM

Before the major instrumentation program was initiated, preliminary tests

were made to describe the magnitude of the response of the pavement to various loading conditions and to check the operation of the instrumentation system. The preliminary tests are described in Volume III-A and are summarized below.

Based on the results of plate bearing tests and confirmed by initial static load tests, a minimum of 3 min was established for the load to be in position during static load tests. The recordings made during these initial tests, conducted without high-frequency noise filters, showed poor signal-to-noise ratio. Electrical filters were installed and gain settings were then established for anticipated strain, deflection, and pressure response for all programmed load conditions.

4. MAJOR TESTING PROGRAM

a. Schedule of Tests

The major instrumentation testing program was initiated upon completion and evaluation of the preliminary tests. The major testing program can best be described by breaking the testing program into three different parts:

(1) static load tests, (2) dynamic load tests, and (3) traffic tests. The static and dynamic load tests were conducted with single-wheel, twin-tandem, 6-wheel, and 12-wheel gear configurations with loads of 15,000 lb per wheel and 22,500 lb per wheel. The traffic tests were conducted with the 12-wheel assembly loaded to 30,000 lb per wheel and with the twin-tandem assembly loaded to 41,500 lb per wheel. These were the regular traffic tests (described in Volume II) juring which the responses of the pavement system to traffic were monitored.

b. Test Procedures

The details of the test procedures used in the major instrumentation test program are presented in Volume III-A; a brief summary is given below.

(1) Loading patterns. The loading patterns, i.e., the sequence in which the static loadings were applied, were not important as all loads were relatively small and did not approach the failure loads for the test items. The loading patterns for the dynamic load tests were selected to complement information to be gained during the traffic testing portion of the program.

The lines of application were selected to obtain information on the effects of moving loads near a longitudinal joint in the center of each test item and at various locations between these two extremes. The width between lines was established by the tire print width by making the lines very nearly one tire print width apart. The loading pattern consisted of one forward pass and one reverse pass on each line.

The loading pattern selected for the 12-wheel-assembly traffic portion of the test was chosen to achieve a crude approximation of normal distribution laterally across the longitudinal joint. A complete loading pattern consisted of 22 passes of the test cart.

The loading pattern for the twin-tandem-assembly traffic portion of the test was selected in an attempt to provide an approximation of normal distribution laterally across a 120-in.-wide traffic area. Traffic was applied to the center of the north paving lane; that portion of the test item near the longitudinal joint saw no traffic. A traffic pattern consisted of 30 passes of the twin-tandem assembly.

(2) Loading points. The Corps of Engineers rigid pavement design method is based on a correlation between stresses developed in the pavement slab through flexural behavior under load with performance under cyclic loading. The loading points for the static load portion of the program were selected to provide comparative data on jointed edge loading versus interior loading, to provide comparative readings for single-wheel, twin-tandem, and 6-wheel- and 12-wheel-assembly loadings, and to provide information on interaction between wheels for the assemblies containing more than one wheel.

The equipment used to apply the 12-wheel loadings was a large prime mover with four low-pressure outrigger wheels towing special load boxes. A finite element analysis was performed to determine the influence of the outrigger wheels on pavement deflection and stress. The results of the analysis indicated that the behavior of the test section was not felt to be influenced to a measurable degree by the outrigger wheels.

(3) Application of loads. A no-load reading was taken for all gages immediately prior to testing. The no-load readings were taken with the loading rig completely off the test item. The load was then positioned as required and data recorded for at least 3 min before the test cart moved to the next location. This test procedure was employed for all static load tests: single-wheel, twin-tandem, and 12-wheel assemblies. Sequence of load positions was

dictated by convenience, i.e., the least amount of maneuvering of the test cart.

Dynamic load tests were conducted on all test items with the single-wheel, twin-tandem, and 12-wheel assemblies. Loads were applied along each of six traffic lines with the test cart facing west and traveling west and then the test cart was backed along the same line. Each item was tested separately to provide the most accurate no-load readings.

The traffic test portion of the study using the 12-wheel assembly was conducted with a 30,000-lb-per-wheel loading (gross loading 360,000 lb). Traffic was applied along five traffic lines in a sequence that would produce a favorable transverse distribution of traffic across the pavement.

After completion of the 12-wheel-assembly traffic, traffic was applied to the north lane with the twin-tandem assembly loaded to 41,500 lb per wheel (166,000 lb gross load). Twin-tandem traffic was applied along five traffic lines that were positioned so as to predict the performance of a pavement loaded with the twin-tandem assembly operating parallel to a joint by inference from observation of the performance of the pavements near the transverse joints. This was necessary because the 12-wheel-assembly traffic had already been placed across the longitudinal joint and had failed the keyed joint for the entire length of the test track.

During the 12-wheel-assembly trafficking phase of the test, periodic tests were conducted with the Dynaflect on all test items at the end of the day.

(4) Monitoring instrumentation. The oscilloscope monitor was used for calibration and to check the instrumentation system prior to actual testing. Continuous, permanent records of all tests were obtained on magnetic tape. Voice logging was used to identify all test parameters to aid in the analog playback of data. Oscillograph printouts were used to periodically sample the output channels for preliminary data analysis on a real-time basis.

SECTION V

RESULTS AND ANALYSIS OF DATA FOR RIGID PAVEMENT

A listing of the basic data collected during the rigid pavement tests is presented in Appendix B to this volume. These data are complementary to the information presented in the following paragraphs. The analysis includes data for static and dynamic load tests for single, twin-tandem, 12-wheel-, and 6-wheel-assembly loadings, from 15,000 to 41,500 lb per wheel. The data consist of measurements of deflection, strain, pressure, crack width, and deflection response to vibratory loading.

1. STATIC LOAD TESTS

The data collected under single-wheel, twin-tandem, and 12-wheel-assembly loadings agreed reasonably well with that predicted by Westergaard analysis. Poor results were obtained with the embedded strain gages due to corrosion and with the pressure cells due to loss of bond between the strain gage and pressure-sensing diaphragm.

Design calculations indicated that approximately 50, 75, and 90 percent of the pavement structure deflection should occur within subgrade depths of 3, 5, and 9 ft, respectively. The results of the static load tests indicated that the above-mentioned percentages versus depths were reasonably close for single-wheel and twin-tandem assemblies, but were somewhat in error for the 12-wheel assembly. Under the 12-wheel assembly, the percentages were closer to 30, 60, and 80 percent for the same depths mentioned above. It should be noted that the design calculations were crude and represent an average for all test items, as do the 30, 60, and 80 percentage figures cited above.

The static load test data indicated that the 3-min waiting period for the full deflection to develop was reasonable. The deflection versus time curve was somewhat linear during the first 15 sec of loading and appeared to become asymptotic at about 3 min.

The loads chosen for the static load tests were selected to avoid distress in any of the test items. The results of all tests, i.e. static, dynamic, and traffic, apparently confirmed that no measurable distress resulted from any of the static tests.

2. DYNAMIC LOAD TESTS

The dynamic tests were intended to provide data on pavement response to rolling loads and comparative data on single-wheel, twin-tandem, and 12-wheel loadings.

As indicated by analytical studies, the deflections in the vicinity of the longitudinal joint were slightly larger than deflections along the transverse joint and in the interior of the test pavements. The embedded strain gages loacted near the longitudinal and transverse joints were too erratic to permit generalizations to be drawn, but using the deflection measurements and analysis as a basis of comparison, strains in the vicinity of the joints were probably higher near the longitudinal joint than at the transverse joint or slab interior. Generally speaking, the dynamic deflections were between 75 and 80 percent of the 3-min static deflection reading, indicating the time dependency of the pavement structure deflection. The test carts were traveling at about 3 mph during these tests.

3. TRAFFIC TESTS

a. 12-Wheel Assembly

The instrumentation data collected during the traffic portion of the study are presented in Appendix B to this report. These data were reduced from oscillograph traces produced periodically on site during the entire traffic test period. They represent peak values of strain or deflection for each pass of the test cart for each traffic line. Graphical representations of these data are included in figures 83-104. An attempt was made to predict when the keyed longitudinal construction joint failed under traffic from these plots.

Theoretical deflections are shown in the figures for gages PD and DSJL. These values represent theoretical deflections for a perfectly efficient joint, or interior loading, and for a completely inefficient joint, or free-edge loading. From these plots it appears that the keyed joint failed at the following traffic levels:

Item 1 - 15 traffic patterns

Item 2 - 58 traffic patterns

Item 3 - 25 traffic patterns

Thus it is apparent that the keyed joint failed rather early in the traffic tests.

In rigid pavement design and analysis, a rather complex problem arises when the loadings are applied by wheels in tandem such that some interaction occurs. It is never clearly evident whether the pavement has responded to two separate loadings or one large loading or some level of loading between the two. The 12-wheel assembly was quite complex in this respect as the load wheels are asymmetric and produce a complex waveform when traversing across a point on the pavement. The strain and deflection transducers show a definite distinction between the two leading wheels and the four trailing wheels of each 6-wheel set, and some interaction between the 6-wheel sets occurs as the pavement is subjected to the 12-wheel load. This response is typified by the plot shown in figure 105. It should be noted that the response traces varied with changes in the radius of relative stiffness and figure 105 is intended merely to indicate a typical trace. The approach that has been used in the past to handle this situation was to treat the largest strain or stress or deflection as one loading and ignore smaller values. The approach loses validity as the number of load wheels increases and as the gear configuration becomes more complex. A more reasonable approach can be used to compare pavement performance with a history of all strain, stress, or deflection excursions that occur as a particular gear passes a point on the pavement. An approach of this type would provide a method for handling multiplewheel gears, which tend to wrinkle the pavement extensively but do not stress any particular point unduly. This approach would also accommodate the randomness in which loads are applied to real pavements.

An analysis of this type was attempted for the data collected during 12-wheel traffic tests. Hard copies of instrumentation output were produced periodically during the entire period of accelerated traffic testing. Data were reduced from these hard copies manually, i.e., peak values of strain and deflection were computed for each operational transducer. These data are presented in Appendix B to this report. Histograms were prepared from these data to indicate the number of times a deflection or strain of a certain magnitude was experienced by the pavement (figures 106-111). A linear interpolation was applied to the data to predict values that were not reduced from hard copies. For example, referring to Appendix B, Table B15, Test Item 3,

Gage 3SCL registered a maximum strain 36 µin./in. for traffic pattern 15 in traffic lane 1 on pass number 1 and registered a maximum strain of 44 µin./in. for traffic pattern 20 for the same t.affic lane and pass number. The maximum strains registered in traffic patterns 16, 17, 18, and 19 were predicted by linear interpolation as follows:

Pattern	Interpolation	Maximum Strain
15	None	36 Measured
16	$\frac{114 - 36}{20 - 15} \times (16 - 15) + 36$	38 Predicted
17	$\frac{144 - 36}{20 - 15} \times (17 - 15) + 36$	39 Predicted
18	$\frac{144 - 36}{20 - 15} \times (18 - 15) + 36$	41 Predicted
19	$\frac{144 - 36}{20 - 15} \times (19 - 15) + 36$	42 Predicted
20	None	44 Measured

These data were then grouped into sets of the nearest $5 \, \mu in./in.$ and the number of times each set of $5 \, \mu in./in.$ was experienced was plotted. An example for gage 3SLC is shown in figure 111. This plot indicates the number of times the maximum strain reached certain values within a range of $5 \, \mu in./in.$ For example, referring to figure 111, the maximum strain was between 27.5 and 32.5 (30) 520 times. This figure includes all traffic patterns and all traffic lanes.

A typical trace of strain versus distance was then selected from the hard copies for a particular traffic lane and the total strain excursions experienced by the gage were plotted, see figure 105. These strain excursions were considered typical for a particular transducer and a particular traffic lane. The representative trace for a particular traffic line was considered to be the trace that occurred most frequently. Using this trace as the base, the probable excursions for other traces with different maximums were calculated by straight-line interpolation. For example, the trace shown in figure 105 indicates a maximum strain of 71 μin./in. and a series of excursions of 71, 29, 20, 42, 50, 40, 22, and 52. A trace along the same traffic line, but with a maximum of 50 μin./in. would be predicted to have a series of excursions of 50, 20, 14, 30, 35, 28, 15, and 37 by multiplying by a constant of

50/71. The technique was employed to produce histograms of strain and deflection excursions for each gage.

The histograms show the severity of the excursion as well as the number of times any excursion level was experienced. These figures include maximum values as well as minor excursions and incorporate the influence of loadings at some distance from the transducer as well as those directly over the transducer. They relate directly to the total amount of strain energy being introduced into the rigid pavement slab.

A relative index was established for comparison of the histograms. Weighted areas were calculated for the histograms at the initial-crack level and at the end of the test. The weighting functions were based on arbitrary values of deflection and strain. All deflection excursions were ratioed to a deflection of 0.05 in. and multiplied by the number of occurrences for a weighted area. The value of 0.05-in. deflection was chosen because this is the approximate value of deflection at initial failure for most rigid pavements. All strain excursions were ratioed against a strain of 200 μ in./in. as this is the approximate value of strain at initial failure for most rigid pavements. Weighted areas thus computed are presented in table 6.

This method of describing the total energy put into the pavement seems to have merit even though it is in a rudimentary stage of development. A relationship between thickness and weighted area may be established to arrive at an allowable energy input that would consider all loadings rather than only maximum values.

b. Twin-Tandem Assembly

Only strain data were collected during the twin-tandem trafficking portion of the study. These data are presented in tabular form in Appendix B to this report in table B17. These values presented in the table represent only the maximum strains observed during a given pass of the assembly. These data are presented in graphical form in figures 112-118. The graphical form is a consolidation of the tabular data in that only the Largest strain observed during one traffic pattern is presented, whereas the tabular data represent the largest strain observed during one pass of traffic.

The strain data under twin-tandem loading also reflects strain reversals and strain relief as the assembly traverses a particular point on the

Table 6
Weighted Areas for Histograms

Item	Gage	Weighted Areas				
No.	Identification	First Crack	End of Test			
1	13PD	1,668	28,215			
	19PD	8,830	31,981			
	1SCL	1,064	7,919			
	1SCT	325	6,425			
	ISNJL	379	4,576			
5	29PD	51,378	57,041			
	2DSJL	59,412	66,001			
	SCL	11,029	12,248			
	2SCT	2,853	3,165			
	2SWJT	10,046	11,153			
	2SSJL	13,969	15,495			
3	33PD	11,787	27,695			
	3DC	12,071	26,809			
	3DEJT	28,617	66,258			
	3DWJT	28,754	64,223			
	3JCL	911	2,066			
	3JCT	2,793	6,562			
	3SWJT	4,312	9,799			

pavement. This wrinkling of the pavement again raises the question of how to handle strain relief between the tandem wheels and how much relief is required before the pavement performs as if it were trafficked by two independent twin-wheel assemblies. Histograms were prepare for the twin-tandem-assembly traffic data in the same manner as described for the 12-wheel assembly. Histograms for the entire traffic test proiod are presented in figures 119 and 120. Unfortunately, these histograms are incomplete because of strain gage failures. Only gages 2NSCT and 2NSCL survived the entire 68 patterns of twin-tandem traffic. Gage 2NSEJT failed after one traffic pattern, so no histogram was prepared for that gage. All strain gages were cemented to the top slab surface and were 12 jected to damage by wheel loads and some were failed by cracking of the test pavements. Sufficient data were available, however, to indicate the general shape the histograms tended to develop.

4. DYNAFLECT MEASUREMENTS

Some typical results of the periodic Dynaflect tests are shown in Appendix B to this report, table B16. These results are rather difficult to interpret as the deflections were extremely small and subject to considerable influence from temperature effects. No general trends appear in the data except for those at widely spaced time intervals, such as those taken in late October and early December 1969. The general trend in this time frame is reduction in deflection, which may have resulted from an increase in the subgrade modulus. Considerable pumping had occurred on some of the items during this time frame, which should have been reflected as a general increase in deflection. Also, when the apparatus was operated in the center of the slab, the deflections were higher on a slab that had been overlaid with a nonrigid overlay than previous measurements made on the same slab immediately prior to overlapping. These anomalies tend to reduce the usefulness of the Dynaflect data.

SECTION VI

NONDESTRUCTIVE VIBRATORY TESTS

The nondestructive vibratory tests, which were conducted during the construction of both the flexible and rigid pavement test sections, during application of traffic, and at the completion of traffic, are described in Volume III-A. Testing was continuing at the time this series of reports was written. The following is a brief statement of preliminary findings; a detailed analysis and a tentative evaluation procedure will be published at the completion of the nondestructive testing program (reference 4).

1. WAVE VELOCITY MEASUREMENTS

Wave velocity data were obtained on both the flexible and rigid pavement sections. One half of the wavelength has been found to be approximately the effective depth of the measurement, and the wave velocities were plotted at a depth equal to one half the wavelength.

Wave velocity tests were made on the flexible pavement items on top of the various pavement layers during construction. This information is shown in figures 121-125. There is an apparent increase in the velocities of the underlying layers due to the overburden effect. Wave velocities prior to application of traffic are presented in figures 121-125 for the flexible section, figures 126-129 for the south lane of the rigid sections, and figures 130 and 131 for items 1 and 4 of the rigid pavement with asphaltic concrete overlay. Actual pavement thicknesses are also shown in figures 121-131; these indicate that the half-wavelength theory is not exact, especially in determining thickness of the upper layers. Changes in velocity measurements during trafficking of the flexible pavement sections are shown in figures 132-134.

Poisson's ratio and E-moduli determinations, based on shear- and compression-wave velocity measurements, are given in table 7 for the flexible pavement items, table 8 for the rigid pavement items, and table 9 for the rigid pavement with an asphalt overlay. Poisson's ratio for the rigid pavement slabs was assumed to be 0.20.

2. PAVEMENT RESPONSE TO VIBRATORY LOADING

Figures 135 and 136 present plots of elastic deflection and elastic stress,

Table 7
Wave Velocity Test Results, Flexible Pavement Lane 1

Item No.	Approximate Depth \(\lambda/2\) ft	Wave Velocity V _s , fps	Poisson's Ratio	Compression Modulus E, psi	Item No.	Approximate Depth \(\lambda/2\) ft	Wave Velocity V _s , fps	Poisson's Ratio	Compression Modulus E, psi
1	0.235	2810 3000	0.25	774.0	3	15.30 22.60	455 452	0.47	15.5 15.9
	0.48 0.62 0.79	1910 1120 1100	0.25 0.27 0.29	313.7 107.8 108.5	4	0.25	2950 2890	:	: A
	0.81 1.40 1.50	810 800 580	0.49 0.49 0.40	53.1 51.8 22.3		0.42 0.49 0.56	2490 1948 1680	0.25 0.25 0.25	533.2 326.3 242.7
	2.00	600 540	0.40	23.9 19.4		0.64 0.66 0.68	1280 1190 1090	0.25 0.25 0.29	140.9 121.8 105.0
	3.10 3.30 3.40	549 455 506	0.41 0.45 0.43	20.0 14.2 17.6		0.78 0.80	885 1120	0.37	72.0 84.5
	4.40 5.50 7.00	440 440 417	0.45 0.41 0.42	13.3 12.9 12.6		0.91 0.36 1.10	905 955 873	0.49 0.49 0.49	66.2 73.7 61.6
	7.70 9.60 13.60	385 382 405	0.44 0.44 0.43	11.1 10.9 12.3		1.40 1.90 2.20	840 840 832	0.49	57.1 57.1 56.0
2	26.30	525	0.37	19.3		2.20 2.40 3.10	820 720 615	0.49	57.1 42.0 26.0
	0.32 0.52 0.74	3170 2180 1330	0.25 0.25 0.25	891.3 421.5 156.9		3.50 3.70	630 592	0.44	27.3 24.1
	0.87	870 889	0.49	61.2 63.9		4.10 5.30 6.70	535 525 530	0.46 0.46	19.7 19.0 19.3
	0.89 1.30 1.60	885 798 790	0.49 0.49 0.49	63.3 51.5 53.7		7.30 8.30 10.30	430 415 412	0.47 0.36 0.36	12.0 11.9
	2.10 2.20 2.60	828 670 6 5 0	0.49 0.41 0.42	55.4 31.2 29.3		13.80	414	0.36	11.9
	3.10 3.20 3.25	567 645 520	0.42	23.1 28.9 19.4	5	0.20 0.255 0.28	3200 3570 3370	0.50 0.50 0.50	1026.0 1277.0 1138.0
	4.00	527 550	0.45	20.0		0.31 0.48	3100 2850	0.25	800.5 676.6
	6.60 6.90 8.20	530 415 410	0.34 0.41 0.42	19.6 12.5 12.2		0.60 0.72 0.77	2400 1440 1380	0.25 0.25 0.25	479.8 172.7 158.6
	10.30 15.70	410 440	0.42	12.2 14.0 21.8		0.90 1.00 1.04	940 825 1040	0.49 0.49 0.49	71.4 55.0 108.4
3	26.50 0.20 0.25	530 3040 2510	0.50	••		2.10 2.30 2.60	820 805 780	0.49	54.4 52.4 49.2
	0.34	2020 1540	0.25	372.9 216.7 164.1	E	3.10 3.20	620 576	0.49	31.1 26.8
	0.45 0.68 0.71	1340 1360 1280	0.25 0.25 0.25	169.1 149.7		3.70 4.40 5.60	585 575 555	0.45 0.45 0.46	23.5 22.7 21.2
	0.77 0.86 1.10	1080 860 880	0.25 0.49 0.49	106.6 59.8 62.6		7.20 7.50 10.70	572 447	0.31	18.4
	1.20	732 750	0.49	43.3 45.5		14.20	426 410 463	0.40 0.41 0.49	10.9 10.1 13.9
	3.00 3.10 3.40	600 558 536	0.45 0.45 0.46	24.8 21.4 19.8					
	4.00 5.20 6.40	520 520 500	0.46 0.46 0.37	18.6 18.6 17.5					
	7.05 10.30	423 410	0.41	12.9					

Table 8
Wave Velocity Test Results, Rigid Pavement South Lane

2395.8 23.91.6 23.95.8 3.60 2.80 1.80 2.80	3 1.80 5950 0.45 3.60 2.80 4.200 0.45 3.60 3.600 0.45 3.60 3.600 0.45 3.60 0.45 3.60 0.45 3.60 0.45 3.60 0.45 3.60 0.45 3.60 0.45 3.70 2.20 3.300 0.45 3.70 2.20 3.300 0.45 3.70 2.20 3.300 0.45 3.70 2.20 3.300 0.45 3.70 2.20 3.300 0.45 3.70 2.20 3.45 0.45 3.70 2.20 0.45 3.70 2.20 0.45 3.70 2.20 0.45 3.70 2.20 0.45 3.70 3.300 0.45 3.70 3.300 0.45 3.70 3.300 0.45 3.70 3.300 0.45 3.70 3.300 0.45 3.70 3.200 0.45 3.70 3.70 3.70 3.70 3.70 3.70 3.70 3.70	28	Wave Velocity Vs, fps	8	Poisson's Ratio	Compression Modulus E, psi	Item No.	Approximate Depth λ/2 ft	Wave Velocity V _s , fps	Poisson's Ratio	Compression Modulus E, psi
2.80 4200 0.45 2.10 2.040 0.40 0.40 0.40 0.40 0.40 0.40 0.	3191.6 1836.3 1836.3 1836.3 1836.3 1836.3 1836.0 1836.0 194.6 195.2 196.	0.69 5650		Ĭ	0.50	2395.8	က	1.80	5950	0.45	2479.9
3.50 3.50 7.80 8.40 10.20 10.20 10.20 10.50	14.85.3 14.85.3 14.85.3 15.20 16.	6750		C	 	3191.6		8.8	1,200	0.45	1235.7
7.20 1800 0.40 7.80 1330 0.40 10.20 1120 1670 0.40 10.50 636 0.40 11.20 4800 0.45 11.45 4360 0.45 11.45 4360 0.45 11.45 935 0.40 5.50 2200 0.45 5.50 840 0.40 6.00 1500 0.45 7.90 636 0.40 9.50 475 0.40	1418.5 1938.3 17.20 1830 154.6 154.6 10.50 18.40 1180 118.4 11.20 14.20		5120	0 (÷.	1836.3		3.60	3600	9.	782.6
7.20 1800 0.40 7.80 1330 0.40 10.20 1120 0.40 10.60 636 0.40 11.20 4420 0.45 11.45 4360 0.45 11.70 3010 0.45 2.20 3300 0.45 5.45 935 0.40 5.60 840 0.40 7.40 814 0.40 7.90 636 0.40 9.50 475 0.40	238.3 322.2 322.2 7.80 1330 0.40 85.5 8.40 10.20 1120 0.40 10.50 118.4 10.50 118.4 11.50 11		4500	0	.+5	1418.5		5.10	2 2 00	9.0	251.3
7.80 8.40 8.40 10.20 10.20 1120 12.3	322.2 322.2 8.40 154.6 8.40 10.20 10.20 1120 0.40 118.4 118.4 118.4 10.60 636 0.40 0.40 118.4 118.4 11.20 14.7 12.30 12.30 14.5 11.4	3990		0	.45	938.3		7.20	1800	9.0	195.7
8.40 1670 0.40 10.20 10.20 1120 0.40 10.50 1120 0.40 1120 0.40 1120 0.40 1120 11.45 11.20 11.45 11.20 11.45 11.20 11.45 11.20 11.45 11.45 11.20 11.45	154.6 154.6 10.20 10.20 1120 1120 1120 1120 1131 118.4 11.20 12.30 12.30 13.6 13.7 12.30 13.7 12.30 13.7 12.30 13.7 12.4 13.7 12.4 13.7 13.7 13.7 13.7 14.5 14.7 14.5 15.0 14.5 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15			0	94.	322.2		7.80	1330	o.to	106.8
10.20 1120 0.40 12.30 0.40 633 0.40 1.30 1.45 1.30 1.45 1.45 1.30 0.45 1.45 1.30 1.45 1.45 1.45 1.45 1.45 1.45 1.45 1.45	26.3 10.60 636 0.40 118.4 4 1.20 4800 0.45 105.2 1.30 4420 0.45 105.2 1.30 4420 0.45 11.70 1.45 4360 0.45 11.70 3010 0.45 12.4 2.80 2800 0.45 13.7 3.70 2220 0.45 22.80 2800 0.45 13.7 3.70 2220 0.45 13.7 3.70 2220 0.45 13.7 3.70 2220 0.45 13.7 3.70 2220 0.45 14.80.2 7.40 814 0.40 134.1 5.50 6.00 0.40 134.1 5.50 6.00 0.40 134.1 5.50 6.00 0.40 134.1 5.50 6.00 0.40 134.1 5.50 0.40 134.1 5.50 0.40 134.1 5.50 0.40 134.1 5.50 0.40	0091		0	₽.	154.6		8.40	1670	0.40	168.4
10.60 636 0.40 12.30 613 0.40 12.30 4420 0.45 1.45 4420 0.45 1.70 3300 0.45 2.20 3300 0.45 2.20 3300 0.45 5.45 935 0.40 5.50 2220 0.40 5.50 840 0.40 7.40 814 0.40 7.90 636 0.40 8.40 500 0.40 9.50 477 0.40	26.3 10.60 636 0.40 118.4 118.4 1.20 1480 24.7 12.4 12.4 12.4 12.4 12.4 12.4 2.20 3300 0.45 13.7 1480.2 1755.7 1480.2 1790 2280 0.40 2580 0.40 258	0611		0	4.	85.5		10.20	1120	0.10	75.7
12.30 613 0.40 1.20 4800 0.45 1.45 4360 0.45 1.70 3010 0.45 2.80 2800 0.45 3.70 2220 0.45 5.45 935 0.40 5.50 840 0.40 7.40 814 0.40 7.50 636 0.40 8.40 500 0.40 9.50 477 0.40	18.4 t 1.20 t 480 0.45 24.7	099		0	3.	26.3		10.60	989	0.40	7,42
4 1.20 4800 0.45 1.30 4420 0.45 1.30 4420 0.45 1.70 3010 0.45 1.70 3010 0.45 2.20 3300 0.45 5.50 2220 0.40 5.60 840 0.40 6.60 0.40 6.36 0.40 6.36 0.40 6.36 0.40 6.36 0.40 6.36 0.40 6.36 0.40 6.36 0.40 6.36 0.40 6.30	118.4 4 1.20 4,800 0.45 24.7 2.30 4,420 0.45 178.6 1.45 4,360 0.45 178.6 1.70 3010 0.45 18.4 2.80 2800 0.45 13.7 3.70 2220 0.40 22438.4 5.50 2200 0.40 1755.7 5.60 840 0.40 1480.2 735.5 7.40 814 0.40 218.0 8.40 500 0.40 218.1 25.3 20.3	1120		o.	2	75.7		12.30	613	0.40	22.7
2.20 4420 0.45 1.70 3300 0.45 2.20 0.40 2.20 0.40 2.40 0.40 2.50 0.40 2	105.2 4 1.20 4420 0.45 1.78.6 1.45 4360 0.45 1.70 3010 0.45 1.70 3010 0.45 1.70 3010 0.45 1.24 1.20 4420 0.45 1.20 4420 0.45 1.20 4420 0.45 1.20 420 0.45 1.20 1.20 1.20 1.20 1.20 1.20 1.20 1.20			0	3	118.4			1000	-1-0	
1.30 1.45 1.70 2.20 3.300 3.70 2.20 3.70 2.20 3.70 2.20 3.70 2.20 3.70 2.20 3.70 2.20 3.70 2.20 3.70 2.20 3.70 2.20 3.70 2.20 3.70 3.70 2.20 3.70	24.7 1.76.6 1.15.0 1.46.1 1.17 1.18.6 1.17 1.19 1.10 1.10 1.10 1.10 1.10 1.10 1.10	1320		4.0	0	105.2	4	1.20	30	0.42	1613.9
1.70 2.80 2.80 3.70 3.70 5.45 5.45 5.45 5.45 5.50 6.00 1.50 6.00 1.50 6.00 1.50 6.00 1.50 6.00 1.50 6.00	178.6 11.7 11.7 11.7 11.7 11.7 11.7 11.7 11	049		4.0	0	24.7		5.1. 5.1.	200	0.4°0 0.4°0	1308.5
2.20 3300 0.45 2.80 2800 0.45 3.70 2220 0.45 5.45 935 0.40 5.50 2200 0.40 6.00 1500 0.40 7.90 636 0.40 8.40 0.40 9.50 4.75 0.40	14.7 12.4 12.4 13.7 13.7 2.80 2.80 2.80 0.45 2.80 2.80 2.80 0.45 2.80 2.80 0.45 2.80 2.80 0.45 2.80 2.80 0.40 2.80 0.40 2.80 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0	1720		7.0	0	178.6		1.45	4360	0.47	1331.6
2.80 2800 0.45 3.70 2220 0.40 5.45 935 0.40 5.50 2200 0.40 6.00 1500 0.40 7.90 636 0.40 8.40 500 0.40 9.50 4.75 0.40	2438.4 2438.4 2220 0.45 3.70 2220 0.45 5.45 935 0.40 5.45 935 0.40 5.50 840 0.40 1755.7 1480.2 7.40 814 0.40 7.50 6.00 0.40 8.40 500 0.40	. £64		7.0	Q	14.7		5.5	3010	0.42	634.6
2.80 2.80 3.70 2.20 5.45 5.45 935 0.40 6.00 1500 0.40 7.40 814 7.30 814 0.40 9.50 9.50 9.50 9.40 9.50 9.4	2438.4 2438.4 223.0 223.1 223.1 223.1 223.1 223.1 25.5 25.0 25	101		-	ç			۷۶.۶	3300	0.47	762.8
3.70 2220 0.40 5.45 935 0.40 5.50 840 0.40 6.00 1500 0.40 7.40 814 0.40 7.90 636 0.40 8.40 500 0.40 9.50 475 0.40	2438.4 2438.4 2213.1 1755.7 1480.2 1755.7 1480.2 134.0 134.1 25.3 20.3 20.0 218.0 25.3 20.0 218.0 25.3 20.0			0 0	2 9	+ · · c ·		2.80	2800	0.45	549.2
5.45 5.50 5.50 6.00 7.40 814 7.30 8.40 8.40 9.50 4.75 9.50 9.50 9.50 9.50 9.50 9.50 9.50 9.50	2438.4 5.45 935 0.40 2213.1 5.50 2200 0.40 1755.7 6.00 1500 0.40 735.5 7.40 814 0.40 218.0 636 0.40 8.40 500 0.40 134.1 950 475 0.40	0/+		5	2	73.		3.70	2220	0.10	297.6
5.50 2200 0.40 5.60 840 0.40 6.00 1500 0.40 7.40 814 0.40 7.90 636 0.40 9.50 475 0.40	2213.1 1755.7 1480.2 1480.2 735.5 735.5 7.90 8.40 8.	5700		C	c	20138 11		5.45	935	0.10	52.8
5.60 840 0.40 6.00 1500 0.40 7.40 814 0.40 7.90 636 0.40 8.40 500 0.40 9.50 4.75 0.40	1755.7 1480.2 1480.2 735.5 7.40 814 0.40 7.90 836 0.40 8.40 8.40 8.40 9.50 4.75 0.40 25.3 20.3	Orlon		14) L	2013 1		5.2	2200	0.10	292.3
6.00 1500 0.40 7.40 814 0.40 7.30 636 0.40 8.40 500 0.40 9.50 4.75 0.40	1480.2 735.5 7.40 814 0.40 303.0 8.40 536 0.40 218.0 9.50 475 0.40 25.3 20.3			0	'n	1755.7		2.60	OF 8	9.0	42.6
7.40 814 0.40 7.90 636 0.40 8.40 500 0.40 9.50 4.75 0.40	735.5 7.40 814 303.0 218.0 218.0 134.1 25.3 20.3	0101		4.0	S	1480.2		9.00	1500	0.40	135.9
7.90 636 0.40 8.40 500 0.40 9.50 4.75 0.40	303.0 218.0 8.40 500 0.40 134.1 25.3 20.3	3480		4.0	Q	735.5		7.40	814	0.to	0.03
8.40 500 0.40 9.50 4.75 0.40	218.0 134.1 25.3 20.3	0,100		•	(0000		7.30	989	0.40	7,42
0,00 4,75 0,40	134.1 25.3 20.3	2000		0 0	2 (0.00		8.40	200	0.40	15.1
	25.3 20.3			¥ 2		20.01		9.50	1475	0.40	13.6
20.3				0 0	0	134.1					
20.3				9.0	0 (25.3					
				÷.0		£0.3					

Table 9
Wave Velocity Test Results, Rigid Pavement
with Nonrigid Overlay, North Lane

Item No.	Approximate Depth 1/2 ft	Wave Velocity V _s , fps	Poisson's Ratio	Compression Modulus E 10 ³ psi
1	0.55	6475	0.20	4060.0
	0.905	6650	0.20	4280.0
	1.38	5700	0.45	2275.9
	1.495	5375	0.45	2023.7
	2.56	4095	0.45	1274.6
	3.38	4720	0.40	1345.3
	3.70	2960	0.40	529.1
	5.08	2030	0.40	248.8
	6.43	1158	0.40	80.0
	10.00	800	0.40	38.6
2	0.815	5900	0.50	3265.7
	0.99	5155	0.20	1994.4
	1.36	4960	0.20	1846.4
	1.57	5090	0.20	1944.4
	1.58	4750	0.20	1693.4
	2.26	4500	0.45	1418.5
	2.66	4000	0.45	1020.8
	3.88	3605	0.45	910.3
	5.98	2985	0.45	624.1
	8.86	2660	0.40	427.3

respectively, with depth for various conditions of vibratory loadings and static loadings on item 4 of the flexible test section. Deflection and stress produced by the vibrator, although only a fraction of corresponding values beneath the static wheel loads, are proportional with depth. Deflection at a depth of 12 ft was read from a reference rod with the load cart located adjacent to the rod; the 12-ft deflection was not obtained beneath the vibrator.

3. SURFACE DEFLECTION TESTS

a. Load-Deflection Relationships

Vibralla loss deflection data obtained prior to application of trairic to the pavement test items are shown in figures 137 and 138. The data points for each test item represent frequencies of 5-15 Hz. Also shown

AFWL-TR-70-113

in these plates are deflections measured beneath static single-wheel loads with contact areas of 285 sq in. In figure 137, except for the 40-kip load, data for single-wheel static load tests on items 3 and 4 were obtained from instrumentation response. All other data were obtained from optical readings. Figure 139 shows a change in the vibratory load-deflection relationship with application of traffic and different pavement temperatures. At the time this report was written, testing was continuing on untrafficked areas to determine the change in deflection with temperature. During a particular test, it was found that varying the eccentric setting of the rotating masses did not affect the load-deflection relationship, as shown in figure 140, even though the force level was varied at a given frequency. The data for figure 140 were taken along the north edge of the flexible sections that have not been subjected to traffic.

b. Vibratory Pavement Stiffness

Table 10 presents stiffness values for the various pavement sections. Pavement temperature was found to have a significant effect on stiffness of the flexible pavements. Stiffness values measured on the flexible test items prior to application of traffic were found to correlate with total pavement thickness above the subgrade, as can be seen in figure 141. Thickness of the portland cement concrete also showed a relationship to stiffness as shown in figure 142. The data used in figure 142 were taken on 16 October 1969 after trafficking had begun because pretraffic data were not felt as reliable due to equipment problems.

c. Deflection Basins

A comparison of typical basin shapes for each test item is given in figure 143 for the flexible pavement and in figure 144 for the rigid pavement. Dynamic force applied to the pavement to produce the deflection basins is shown in the figures along with the frequency of vibration.

Table 10
Vibratory Stiffness

Date	Type Pavement	L∉ne	Item	Cover- ages*	Pave- ment Temp, deg	Eccen- tricity deg	Stiff- ness kips/in.
4 Aug 69 8 Sept 69 13 Jan 70	Flexible	1 3A 2A	1 1 1	o 0 6	110 100 55	10 10 10	510 740 940
4 Aug 69 8 Sept 69 14 Jan 70		1 3A 1	2 2 2	0 0 200	110 100 45	10 10 10	650 900 1100
4 Aug 69 26 Aug 69 8 Sept 69 8 Sept 69		1 1 (Untrafficked)	3 3 3	0 1302 2342	115 130 110 110	10 10 10 10	728 1025 800 1025
5 Aug 69 26 Aug 69 8 Sept 69 8 Sept 69		1 1 1	4 4 4	0 1311 2351 2351	100 130 115 115	10 10 10 10	760 790 800 915
4 Aug 69 26 Aug 69 8 Sept 69 19 Feb 70		1 1 1	5 5 5 5	0 1320 2360 3208	120 130 120 50	10 10 10	950 2300 1000 1050
6 Aug 69 1 Oct 69 16 Oct 69 8 Jan 70		South South South North w/overlay	1 1 1	0 0 160 0	 50	10 10 10	1360 18 2 0 1240 2540
6 Aug 69 16 Oct 69 8 Jan 70 13 Jan 70	Rigid	South South South North	2 2	0 160 5008 0	:	10 10 10 10	1230 2700 2540 2500
6 Aug 69 1 Oct 69 16 Oct 69 9 Jan 70		South South South North	3 3 3	0 0 160 0		10 10 10 10	2500 2400 4100 3200
6 Aug 69 1 Oct 69 16 Oct 69 9 Jan 70		South South South South w/overlay	4 4 4	0 0 128 4416**	 144	10 10 10	1300 1530 1530 2200

^{*} The term coverages as used for the traffic tests on the flexible pavement indicates a measure of wheel load repetitions for the full tire print width on any given area of the pavement surface. For rigid pavements, coverage is a measure of the number of maximum stress repetitions that occur in the pavement due to the applied traffic. Discussion of maximum stress repetitions for each load cart is given in Volume II of this series of reports.

** Additional 240 coverages applied before nonrigid overlay was placed on rigid pavement.

SECTION VII

CONCLUSIONS AND RECOMMENDATIONS

The following conclusions and recommendations are believed justified for the instrumentation test programs of the flexible and the rigid pevement test section. Discussions of the nondestructive pavement testing were based on the testing accomplished at the time this report was written. Therefore, no conclusions or recommendations were considered warranted for the nondestructive pavement testing; they will be published when the project is completed (reference 4).

1. CONCLUSIONS

a. Flexible Pavement

- (1) <u>Instrumentation</u>. Two of the flexible pavement items were instrumented with stress, strain, deflection, pore pressure gages, and temperature probes. The two items were the same, except for a soft layer at depth in one of them. The following conclusions are based mainly on data presented in Appendix A.
- (a) At the conclusion of the static and dynamic load tests, 16 WES soil pressure cells out of a total of 17 were operating. In general, the WES cells functioned satisfactorily with accuracies of about +10 percent of the cell pressure indication or better.
- (b) While all three SA-E soil pressure cells functioned throughout the entire static and dynamic load test periods, the output signals were erratic and were considered very unreliable.
- (c) At the conclusion of the static and dynamic load tests, 16 WES soil deflection gages out of a total of 18 were operating. In general, the WES soil deflection gages functioned satisfactorily with accuracies of about ±0.002 in. for the full linear range.
- (d) Only two out of a total of eight pavement strain gages worked throughout the static and dynamic load tests, and they were of questionable behavior.
 - (e) One thermistor probe out of a total of four stopped working

during the static and dynamic load tests. Generally, the thermistor probes worked satisfactorily.

- (f) Both WES pore pressure cells worked satisfactorily throughout the testing periods.
- (2) Interpretation of data. A thorough analysis of the soil deflections under load, as depicted by the deflection gages, was conducted and resulted in identification of a load- and position-dependent moving zero reference level for each deflection gage with no residual strains being induced. The soil at all levels appeared to be behaving as a plastic and elastic mass (for lack of better terms) similar to putty, but not as a viscoelastic material.
- (a) Equivalent elastic deflections were found for equivalent loading situations, either repeated loading of a gage or loadings at symmetrical loading points.
- (b) An analysis of the soil stresses induced under load indicated an almost constant horizontal zero reference per soil pressure cell and the data indicated active residual stresses.
- (c) Equivalent elastic stresses were found for equivalent loading situations, either repeated loading of a gage or loadings at symmetrical loading points.
- (3) Results of instrumentation measurements. Due to the large amount of data available from both static and dynamic load tests and due to time limitations, only the maximum responses were evaluated.
- (a) For this project the loaded assemblies that were of primary interest were the single wheel with a 30,000-lb load, 12 wheel with a 360,000-lb load, and twin-tandem interpolated 168,000-lb load. Limiting maximum elastic deflection and limiting maximum vertical elastic stress versus depth curves for these primary loaded assemblies were established for static load test results. Data developed in the analysis showed that the same relationships are true for the static and dynamic load tests.
- (b) The results of dynamic load tests (2-3 mph) and speed tests (1-10 mph) showed that elastic deflections and stresses are not affected by the range of speeds run in the MWHGL tests and that the dynamic

load test results are approximately equivalent to the static load results.

- (c) The pavement temperature effects study was inconclusive due to the limited range of temperatures, and the pavement strains study yielded no appreciable results due to the unreliability of the strain gages used.
- (4) Analysis of soil behavior patterns. Limited study of soil behavior patterns indicated the following:
- (a) Elastic deflection comparisons and elastic vertical stress comparisons for item 3 versus item 4 showed that the stress and deflection distributions of the two items were different. The difference was caused by the soft layer in item 4.
- (t) If the soil is assumed to act as an elastic material, the theoretical predictions of deflection versus depth or of offset versus deflection are valid only for a single-wheel load.
- (c) Analysis of behavior patterns shows that behavior under a single-wheel load is different from that under a multiple-wheel assembly.
- (d) Log-log plots of wheel load versus deflection for the two items show exactly the same behavior patterns even though the instrumented items have different strain distribution characteristics; the curves are just shifted on the deflection axis.
- (e) Based on the analysis, the principle of superposition is not valid, and the stress-strain characteristics of the soil are nonlinear and dependent on stress level.

b. Rigid Pavement

- (1) <u>Instrumentation and equipment.</u> The four items of the rigid pavement test section were instrumented with strain and deflection gages and soil pressure cells, which were monitored during static and dynamic loading, trafficking, and Dynaflect testing. Based on these tests, the following conclusions were made.
- (a) The techniques employed to install the instrumentation were satisfactory except for the embedded strain gages, which failed early in the pavement life.

- (b) The Dynaflect testing device can be used to formulate a crude quantitative evaluation of the pavement structure, but it is of little value in providing definitive data on pavement condition. This is perhaps due to the lack of correlation between pavement performance and changes in the elastic modulus of the subgrade.
- (c) The output signals from the SA-E pressure cells were found to be erratic and continuous recordings were not made during the test program.
- (2) Analysis of data. The following conclusions are considered appropriate.
- (a) The recoverable deformations that occurred at the depths of 3, 5, and 9 ft in the subgrade were not accurately predicted by a composite analysis involving the finite element analysis and the semi-infinite elastic half-space analysis. Closer agreement was achieved between theory and measured data for nonrecoverable deformations than for recoverable deformations. The reason for this is unknown; however, the correlation is more due to coincidence since both analyses assumed that elastic behavior occurred in the entire pavement structure including the subgrade.
- (b) The Westergaard algorithm yields strain and deflection values about 25 percent greater than the measured values. This is consistent with findings from previous similar test sections.

2. RECOMMENDATIONS

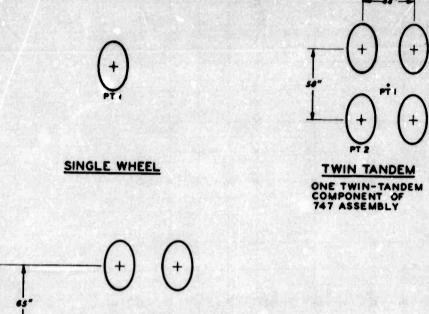
Based on the results of tests of the flexible and rigid pavement test section, the following recommendations are made.

a. Flexible Pavement

- (1) Analysis of data and results needs to be continued. Further and complete analysis of the large quantity of data and the soil behavior patterns of the MWHGL test section would provide a basis for, if not entirely, a completely nonlinear-inelastic constitutive equation, in terms of fundamental material constants, which would provide a fundamentally correct thesis from which a rational pavement design and evaluation procedure could be developed.
- (2) A method or instrument for accurately measuring strains in pavements needs to be developed.

b. Rigid Pavement

- (1) Embedment-type strain gages should be placed by a method other than that used on this test pavement. Perhaps casting the embedment gages in a beam under laboratory conditions and then embedding the beam in the pavement would yield satisfactory results.
- (2) Further study of the reversals in strain and deflection under multiple-wheel assemblies should be undertaken. Some method, such as the histogram technique, is needed to incorporate the effects of interactions between the load wheels.
- (3) Further studies of the data collected should be undertaken. No attempt was made to account for environmental effects, which would normalize the data and might indicate trends that are not apparent without normalized data.
- (4) The LVDT gage is an excellent means of measuring rigid pavement deflection, but means of accessibility to the transducer should be provided insofar as practical.



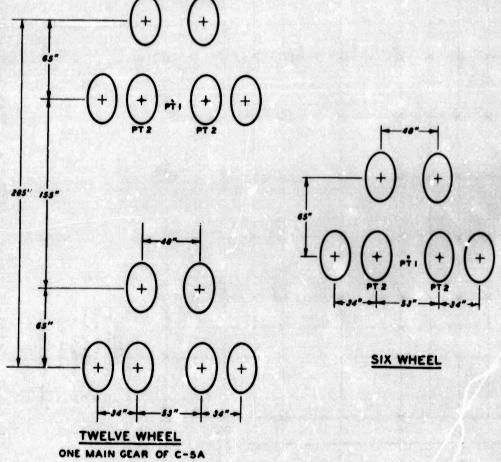
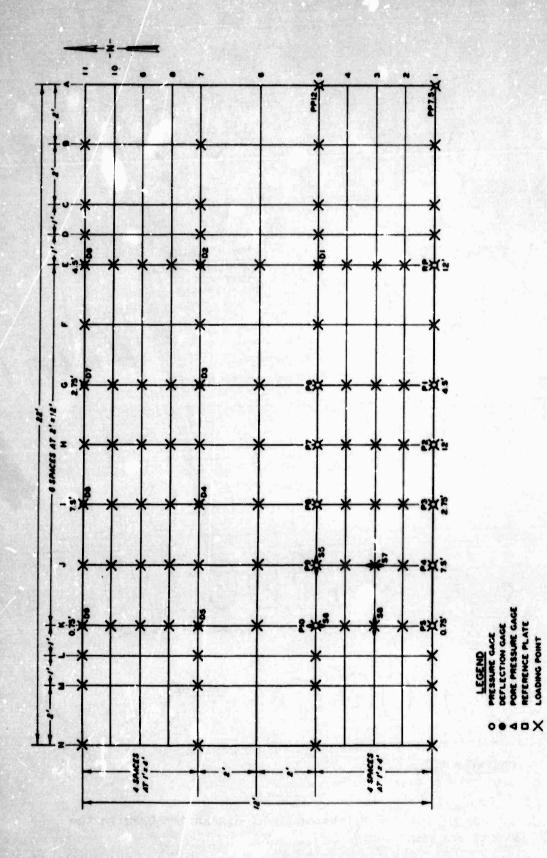


Figure 1. Locations of Loading Points of Wheel Assemblies Used in the Flexible Pavement Tests

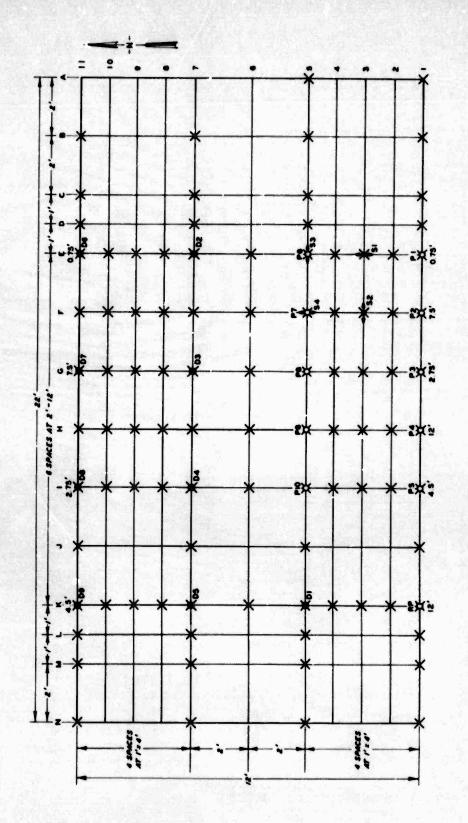


Static Loading Grid System, Item 3, Flexible Pavement Tests. Instrumentation Identification (Type, Number) Beside Each Symbol Figure 2.

A PORE PRESSURE OF REFERENCE PLAT

X LOADING POINT

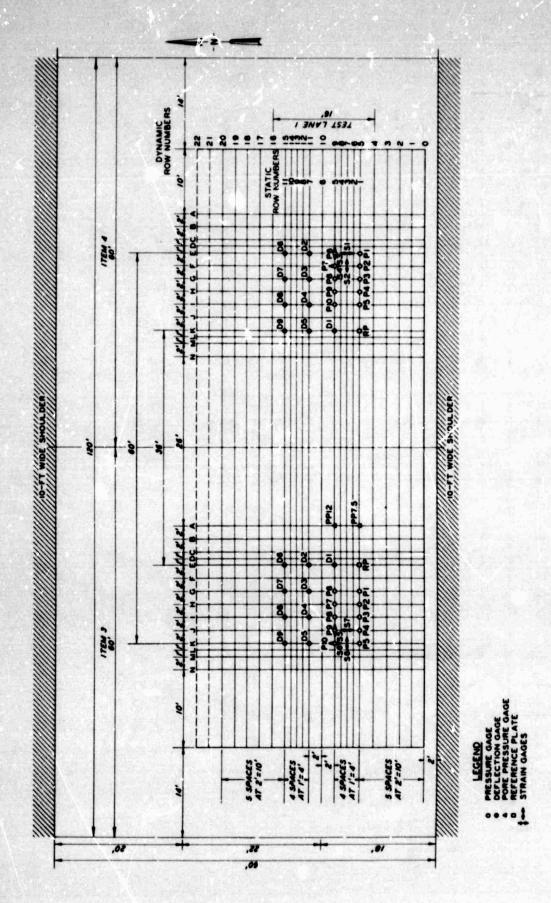
** STRAN CAGES



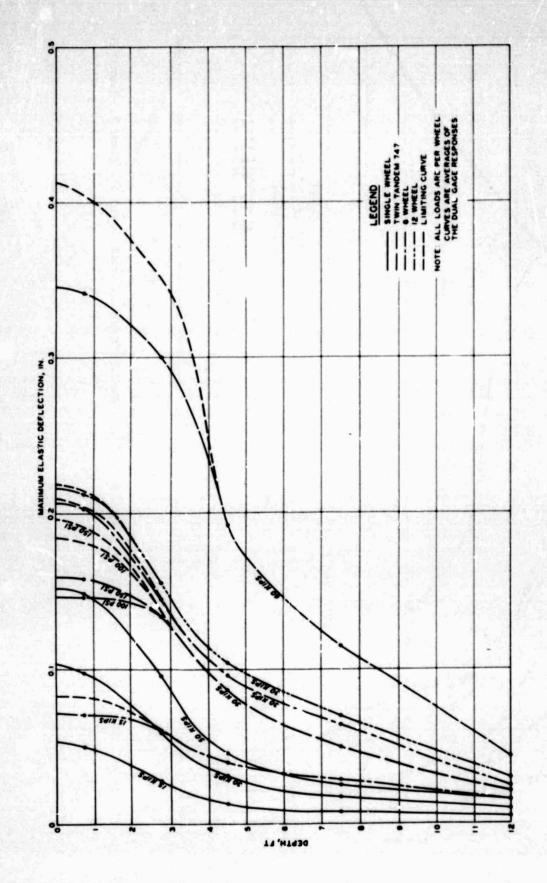
O PRESSURE CACE
O DEFLECTION CACE
O REFERENCE PLATE
X LOADING POINT

The STRAIN CAGES

Static Loading Grid System, Item 4, Flexible Pavement Tests. Instrumentation Identification (Type, Number) Beside Each Symbol Figure 3.



Static and Dynamic Load Grid System Used for Flexible Pavement Tests. Instru-mentation Identification (Type, Number) Beside Each Symbol Figure 4.



Depth Versus Deflection for Static Load Tests, Assembly Load Point 1, Item 3, Flexible Pavement Figure 5.

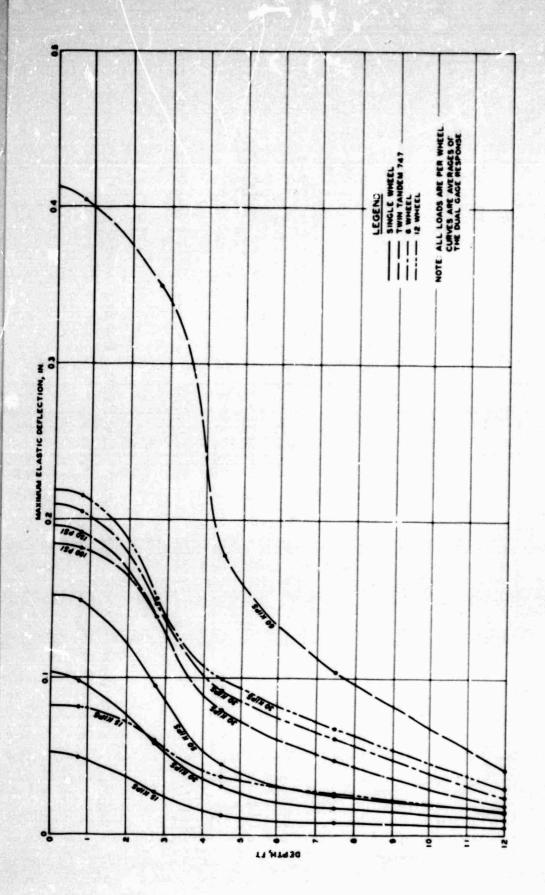
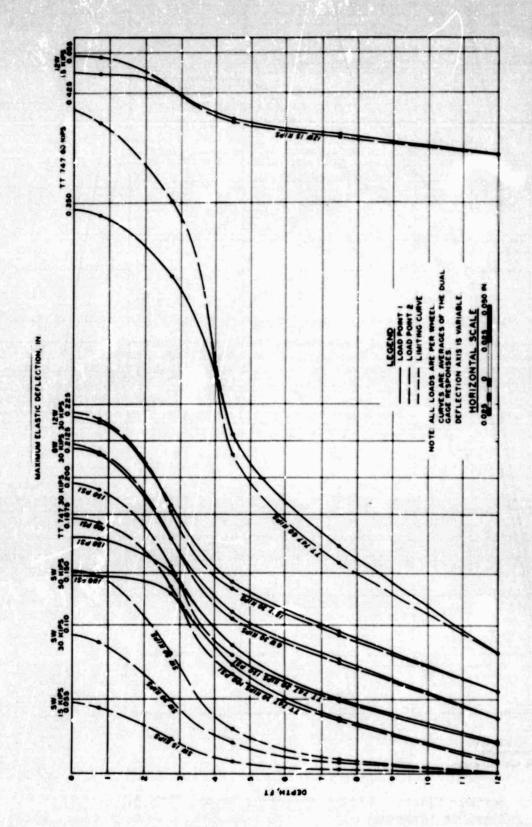
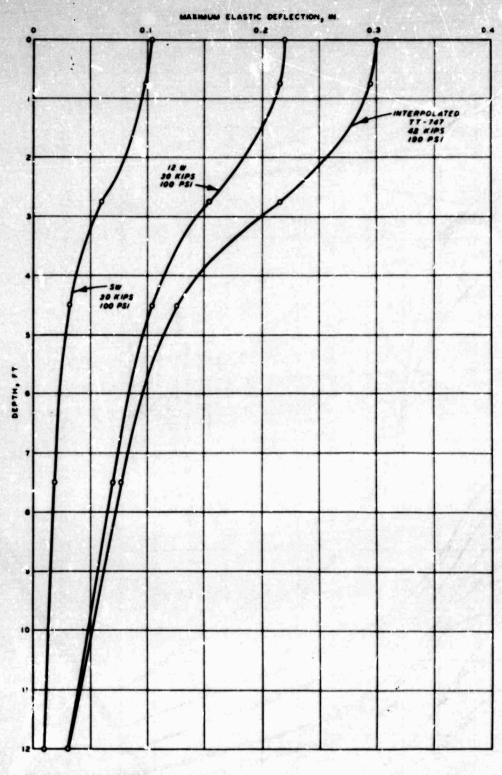


Figure 6. Depth Versus Deflection for Static Load Tests, Assembly Load Point 2, Item 3, Flexible Pavement

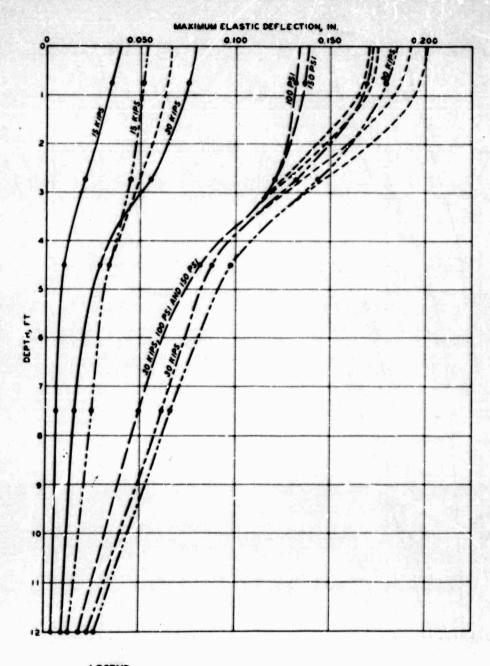


Comparison of Assembly Load Point Curves for Deflection Under Static Loads, Item 3, Flexible Pavement Figure 7.



MOTE: CURVES ARE AVERAGES OF GASE RESPONSES. ALL LOADS ARE PER WHEEL.

Figure 8. Maximum Elastic Deflection Versus Depth, Item 3, Flexible Pavement



LEGEND

SINGLE WHEEL
TWN TANDEM 747

WHEEL
IS WHEEL
LIMITING CURVE

NOTE: ALL LOADS ARE PER WHEEL.
CURVES / RE AVERAGES OF THE
DUAL GAGE RESPONSES.

Figure 9. Depth Versus Deflection for Dynamic Load Tests,
Assembly Load Point 1, Item 3, Flexible Pavement

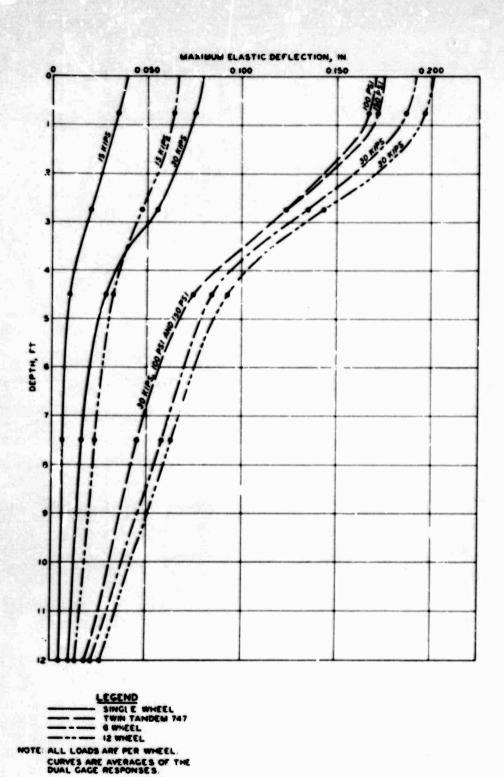


Figure 10. Depth Versus Deflection for Dynamic Load Tests,
Assembly Load Point 2, Item 3, Flexible Pavement

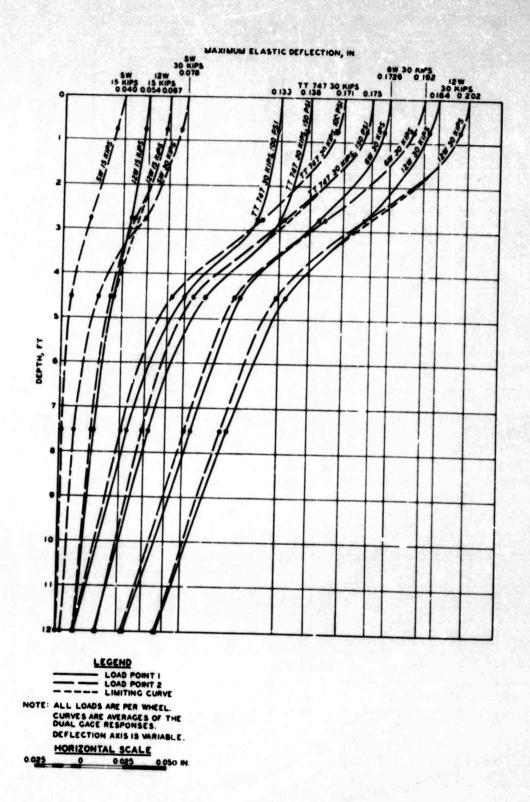


Figure 11. Comparison of Assembly Load Point Curves for Deflection Under Dynamic Loads, Item 3, Flexible Pavement

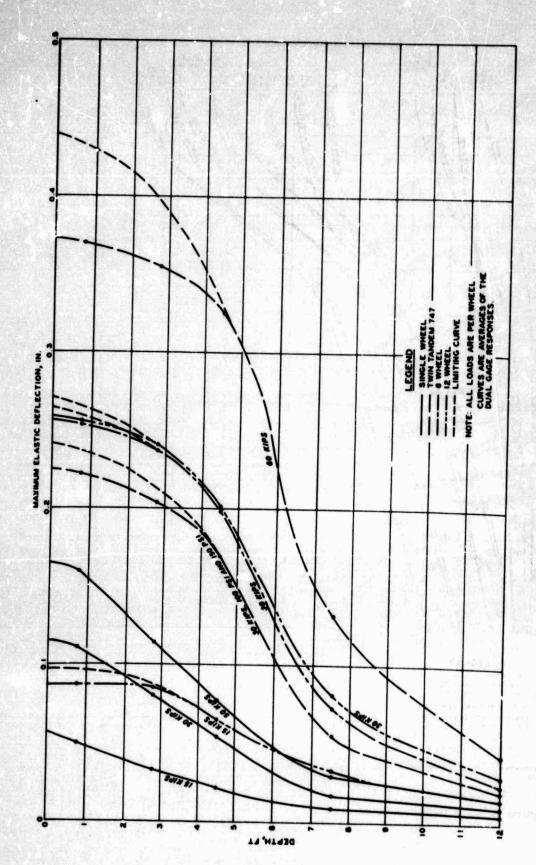
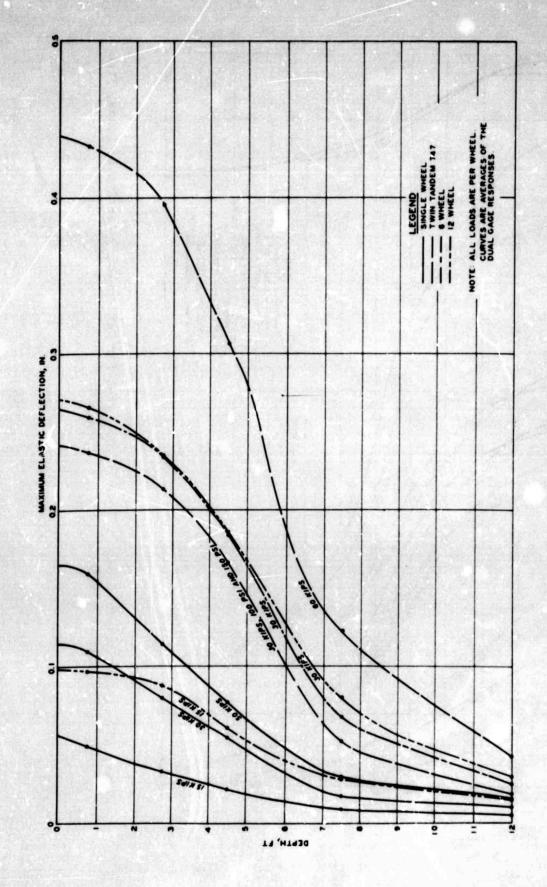
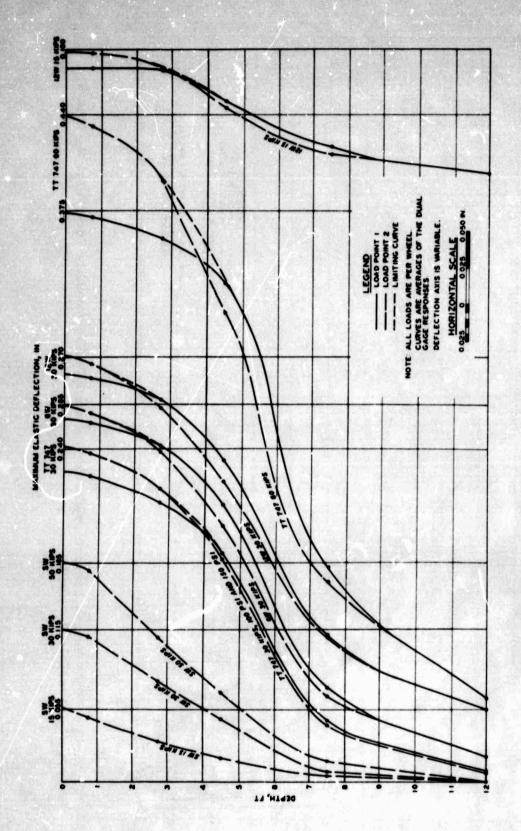


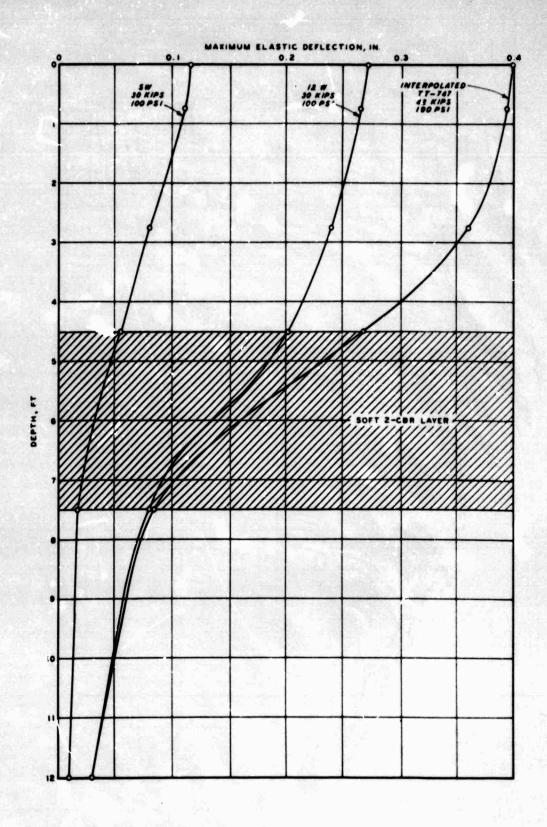
Figure 12. Depth Versus Deflection for Static Load Tests, Assembly Load Point 1, Item 4, Flexible Pavement



Depth Versus Deflection for Static Load Tests, Assembly Load Point 2, Item 4, Flexible Pavement Figure 13.

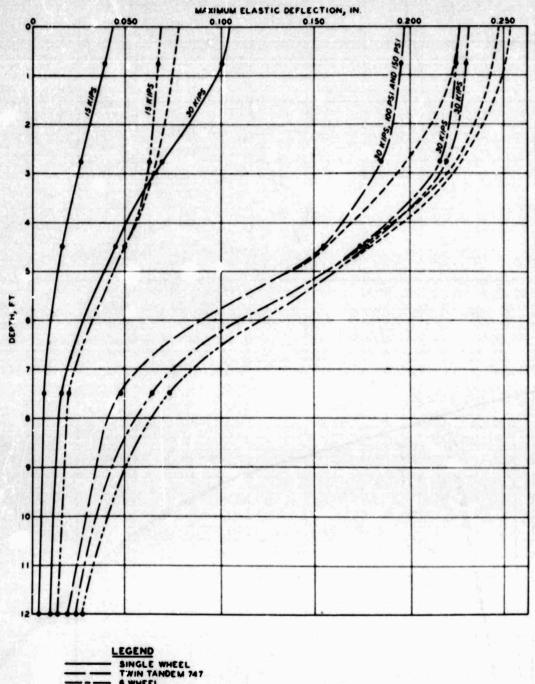


Comparison of Assembly Load Point Curves for Deflection Under Static Loads, Item 4, Flexible Pavement Figure 14.



HOTE: CURVES ARE AVERAGES OF GAGE RESPONSES. ALL LOADS ARE PER WHEEL.

Figure 15. Maximum Elastic Deflection Versus Depth, Item 4, Flexible Pavement



SINGLE WHEEL

TWIN TANDEM 747

SWHEEL

IS WHEEL

LIMITING CURVE

NOTE: ALL LOADS ARE PER WHEEL.

CURVES ARE AVERAGES OF THE
DUAL GAGE RESPONSES.

Figure 16. Depth Versus Deflection for Dynamic Load Tests, Assembly Load Point 1, Item 4, Flexible Pavement

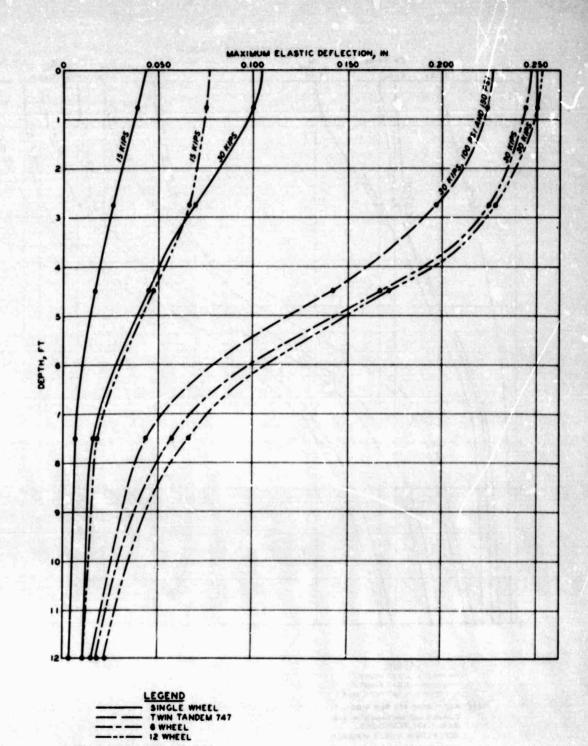
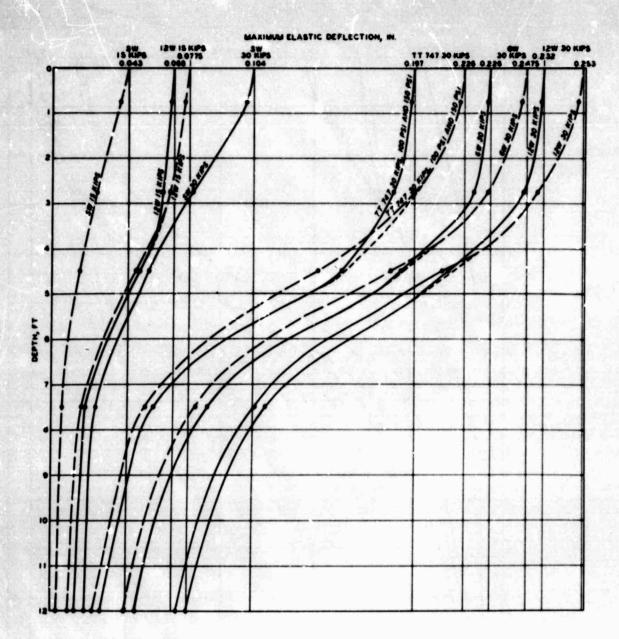


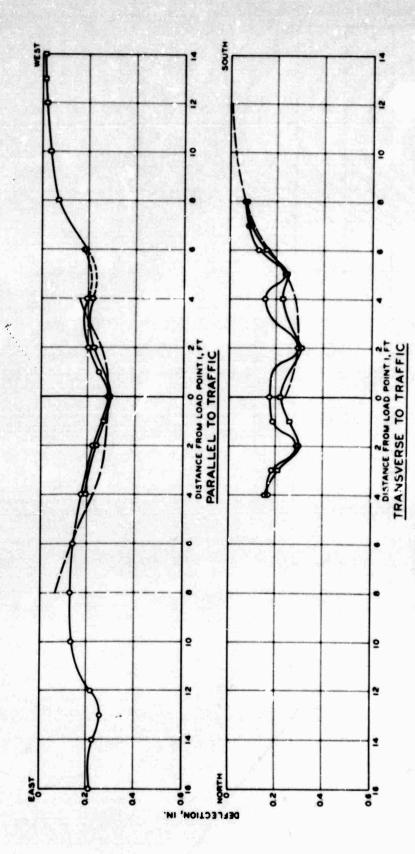
Figure 17. Depth Versus Deflection for Dynamic Load Tests, Assembly Load Point 2, Item 4, Flexible Pavement



LEGEND

LOAD POINT I
LOAD POINT Z
LOAD POINT

Figure 18. Comparison of Assembly Load Point Curves for Deflection Under Dynamic Loads, Item 4, Flexible Pavement



GASE ITEM
O 3
OPTICAL*
OPTICAL*
OPTICAL*
A FROW VOLUME II

Surface Deflection Basins, 12-Wheel, 360-kip Load (100-psi Tire Pressure), Flexible Pavement Tests Figure 19.

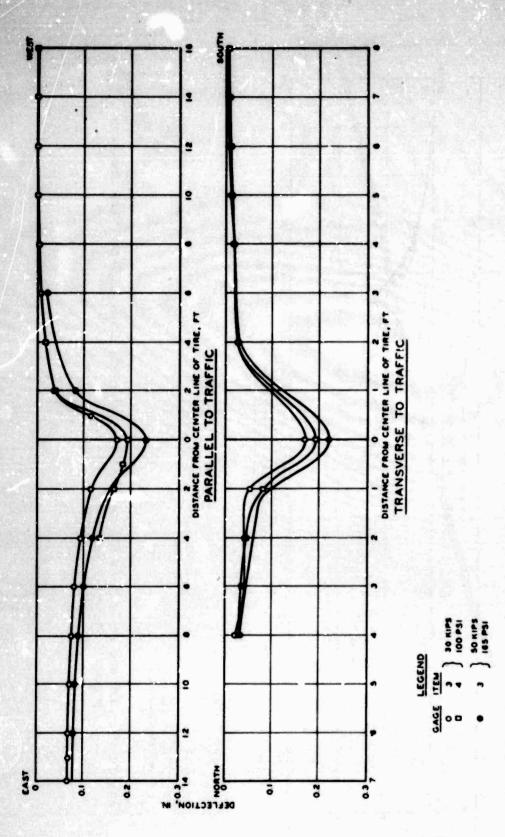
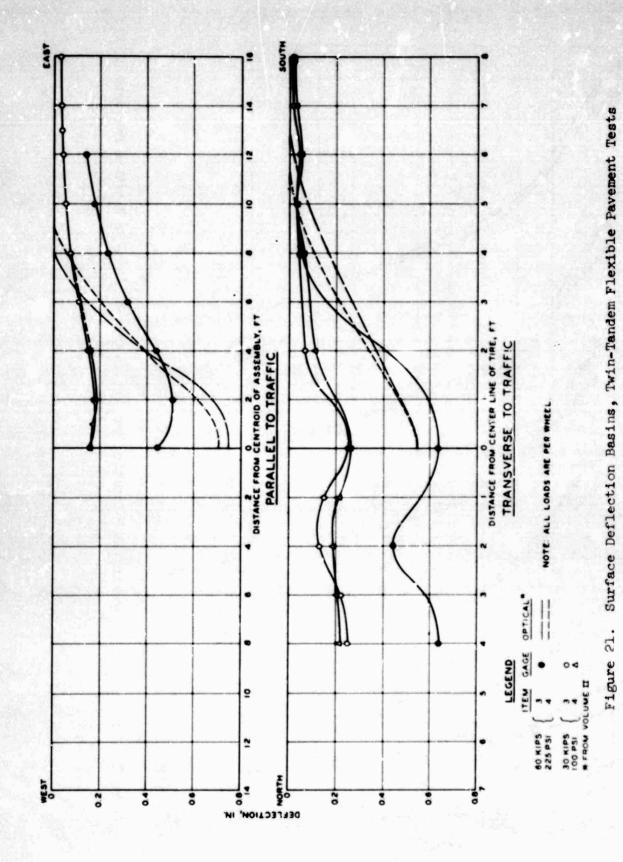


Figure 20. Surface Deflection Basins, Single-Wheel Flexible Pavement Tests



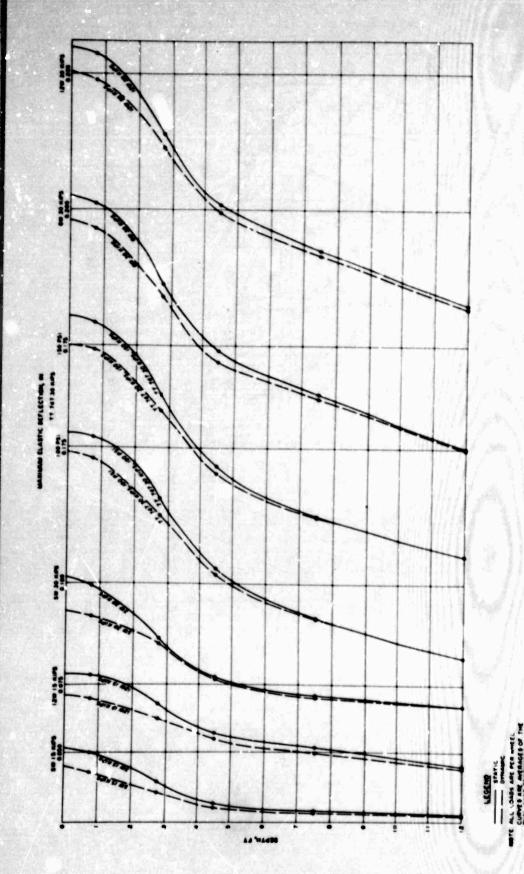
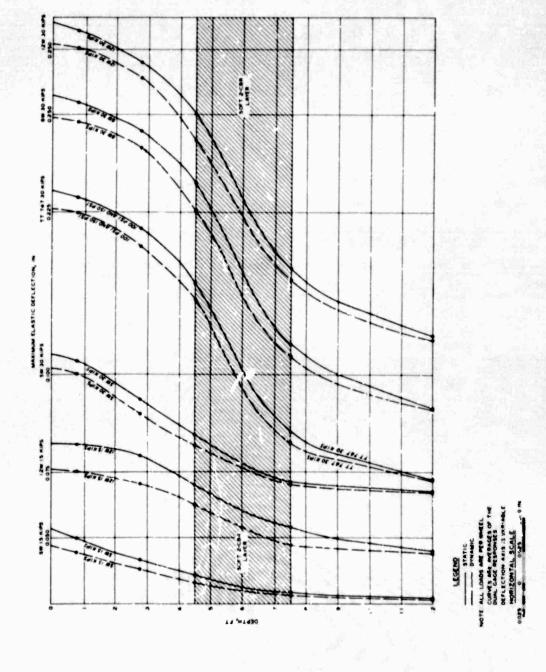


Figure 22. Static Versus Dynamic Load Limiting Deflection Curves, Item 3, Flexible Pavement



Static Versus Dynamic Load Limiting Deflection Curves, Item $\boldsymbol{\mu}_{\text{s}}$ Flexible Pavement Figure 23.

NOTE: Figure 24 is a folded sheet and is enclosed at the back of this volume.

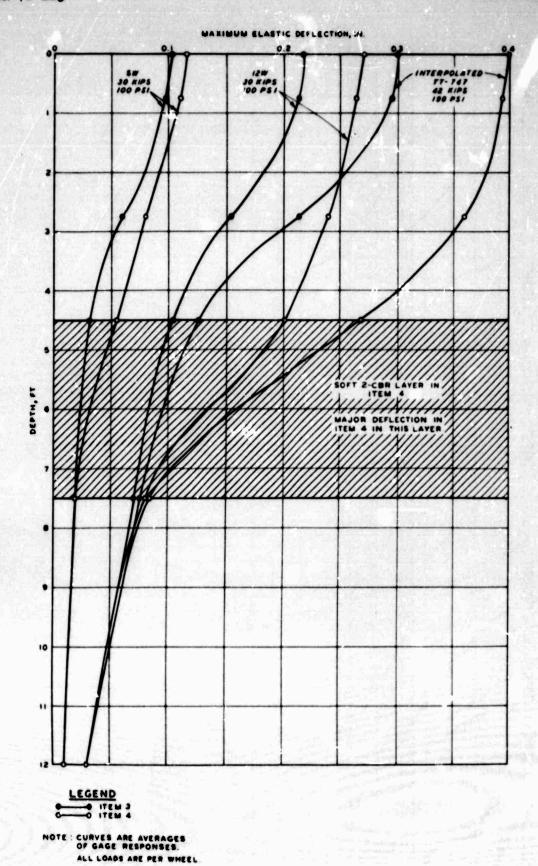
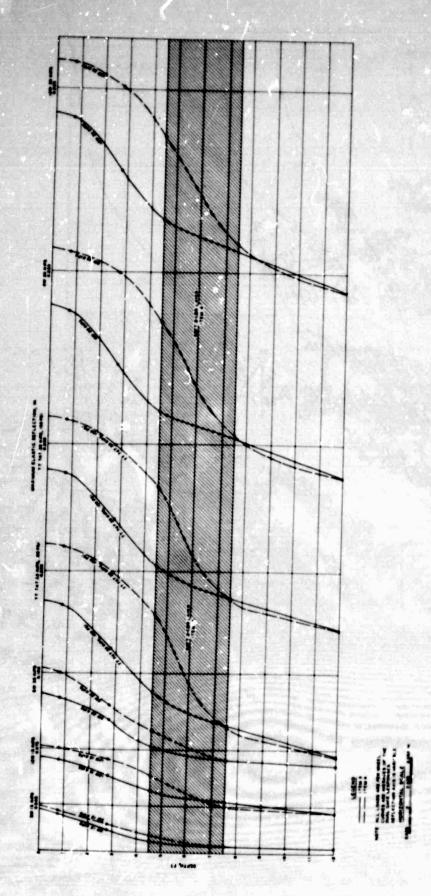


Figure 25. Comparison of Maximum Elastic Deflection Versus

Depth, Items 3 and 4, Flexible Pavement Tests



Item 3 Versus Item 4 Limiting Deflection Curves, Dynamic Load Flexible Pavement Tests Figure 26.

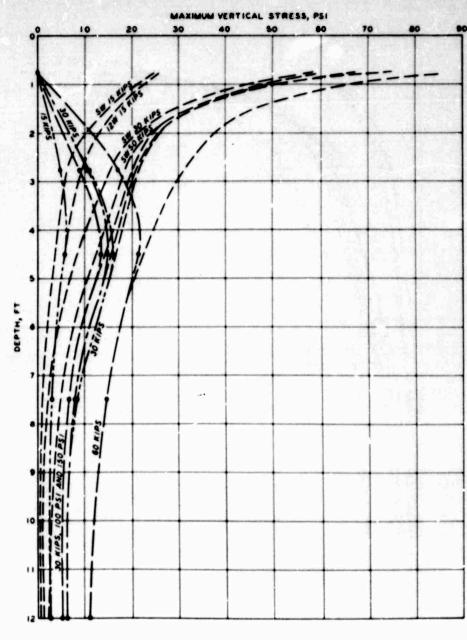


Figure 27. Depth Versus Vertical Stress for Static Load Tests,
Assembly Load Point 1, Item 3, Flexible Pavement

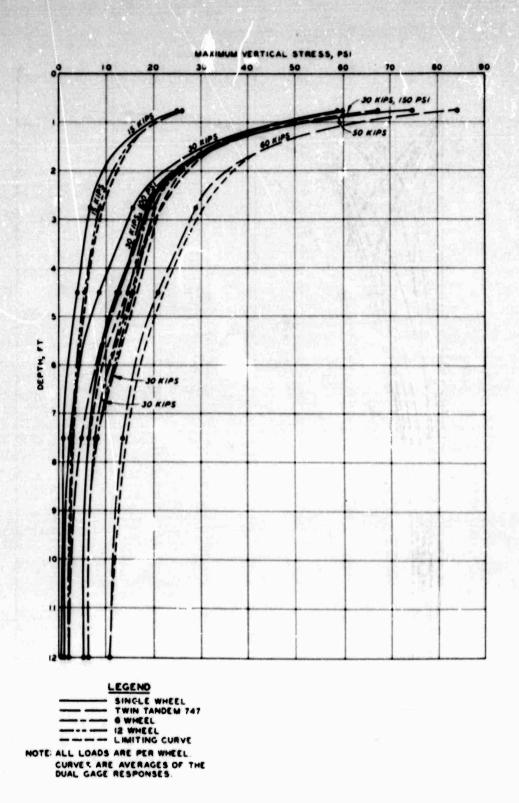


Figure 28. Depth Versus Vertical Stress for Static Load Tests, Assembly Load Point 2, Item 3, Flexible Pavement

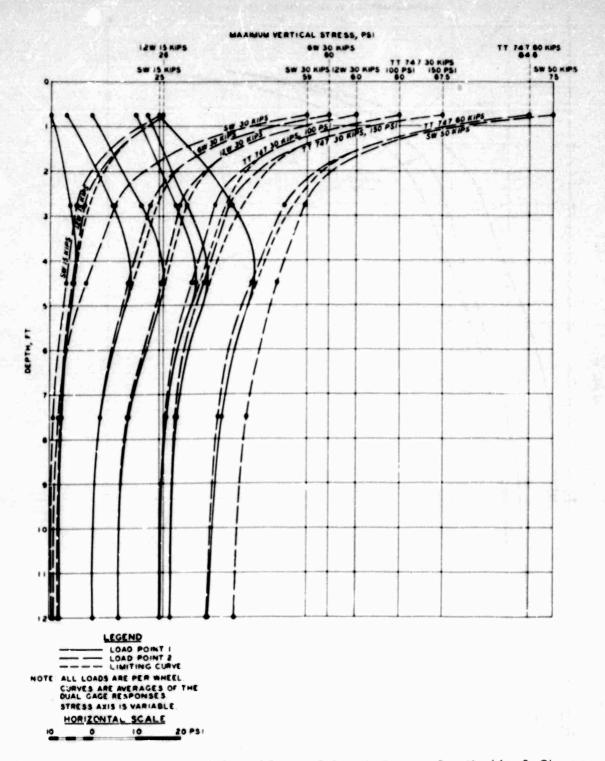


Figure 29. Comparison of Assembly Load Point Curves for Vertical Stress Under Static Loads, Item 3, Flexible Pavement

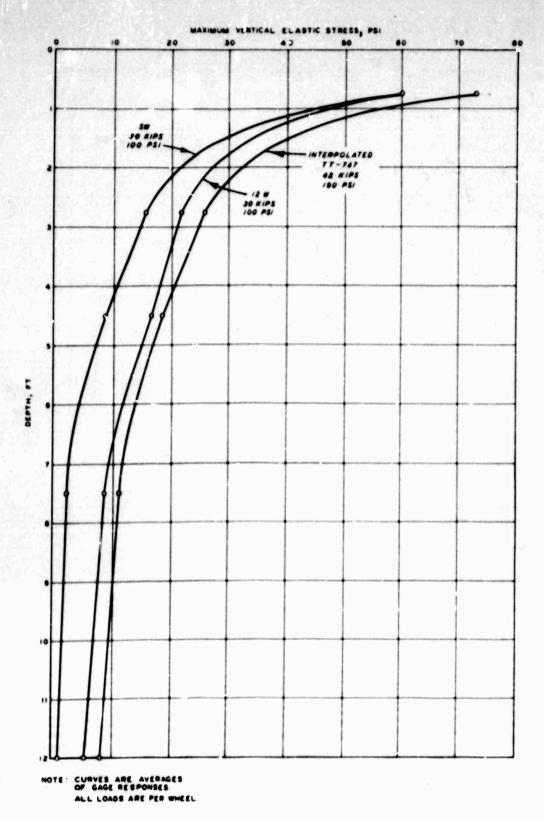
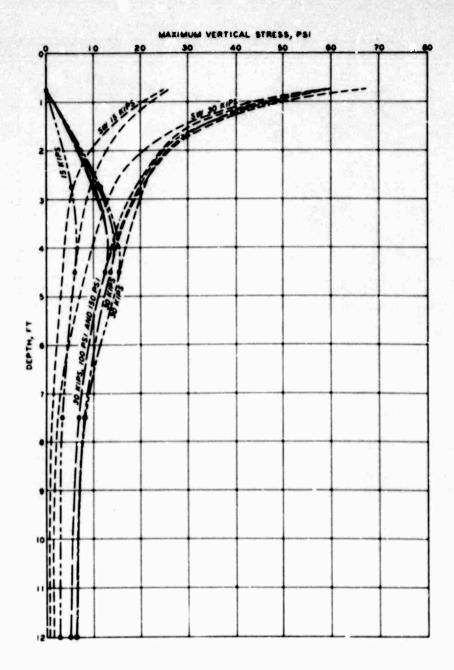


Figure 30. Elastic Stress Versus Depth, Item 3, Flexible Pavement



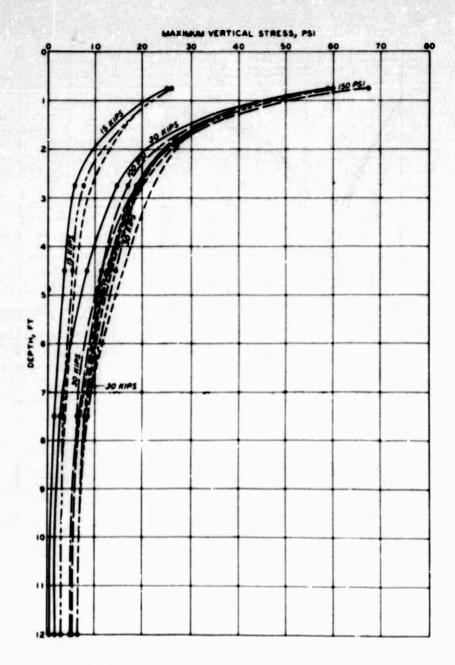
TWIN TANDEM 747

WHEEL

IS WHEEL

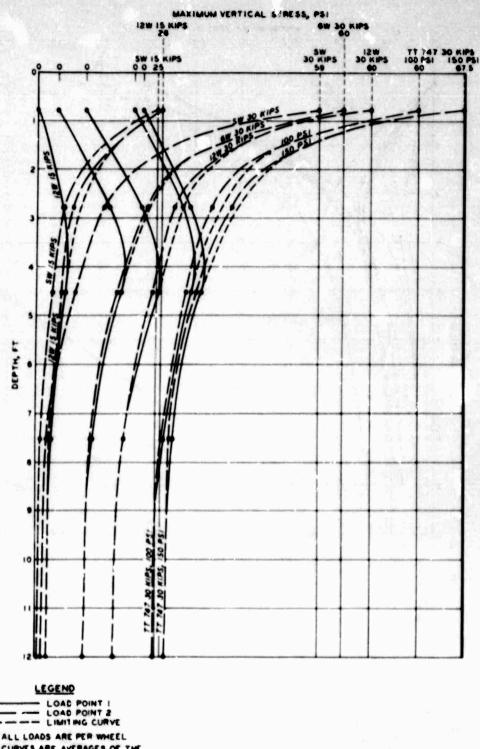
LIMITING CURVE

Figure 31. Depth Versus Vertical Stress for Dynamic Load Tests, Assembly Load Point 1, Item 3, Flexible Pavement



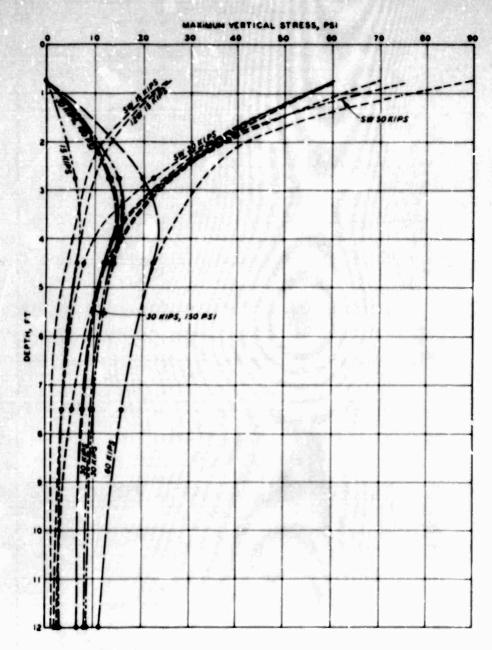
LEGEND
SINGLE WHEEL
TWIN TANDEM 747
O WHEEL
IZ WHEEL
LIMITING CURVE

Figure 32. Depth Versus Vertical Stress for Dynamic Load Tests, Assembly Load Point 2, Item 3, Flexible Pavement



NOTE: ALL LOADS ARE PER WHEEL
CURVES ARE AVERAGES OF THE
DUAL GAGE RESPONSES
STRESS AXIS IS VARIABLE
HORIZONTAL SCALE

Figure 33. Comparison of Assembly Load Point Curves for Vertical Stress Under Dynamic Loads, Item 3, Flexible Pavement



TWIN TANDEM 747

Figure 34. Depth Versus Vertical Stress for Static Load Tests,
Assembly Load Point 1, Item 4, Flexible Pavement

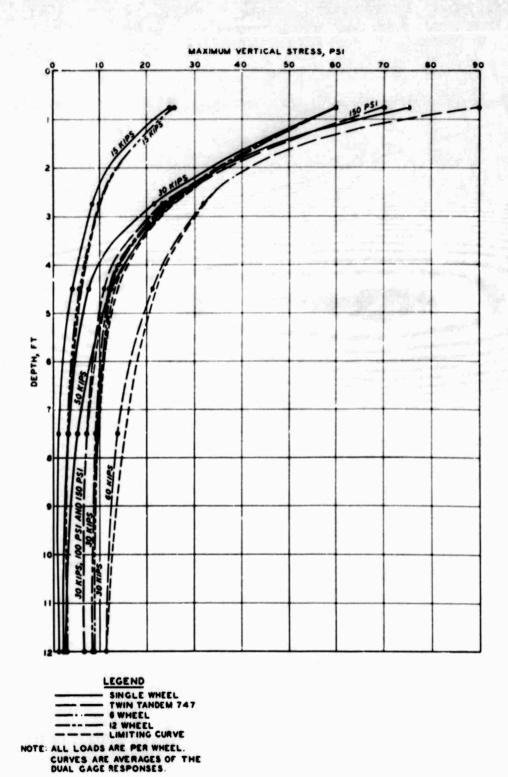


Figure 35. Depth Versus Vertical Stress for Static Load Tests,
Assembly Load Point 2, Item 4, Flexible Pavement

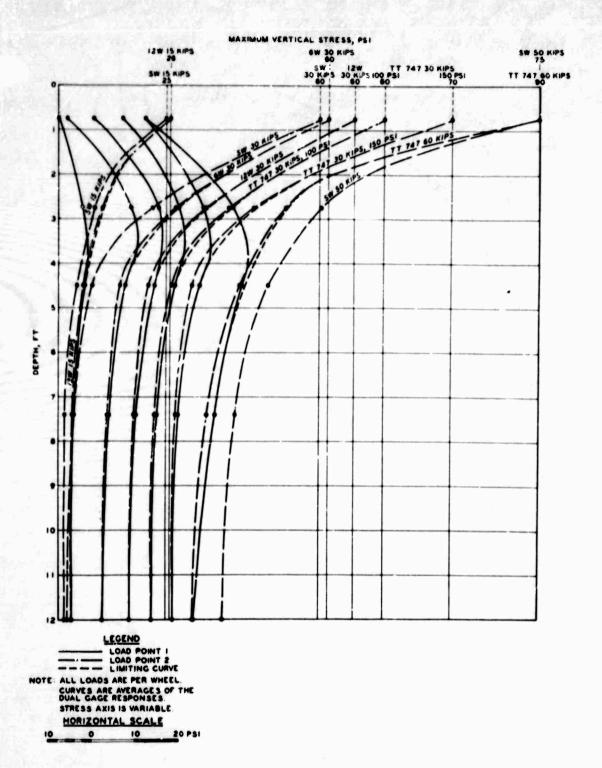
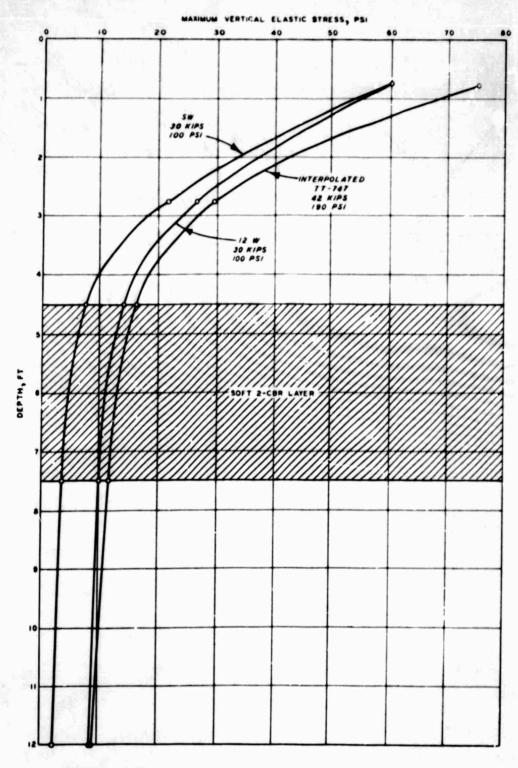
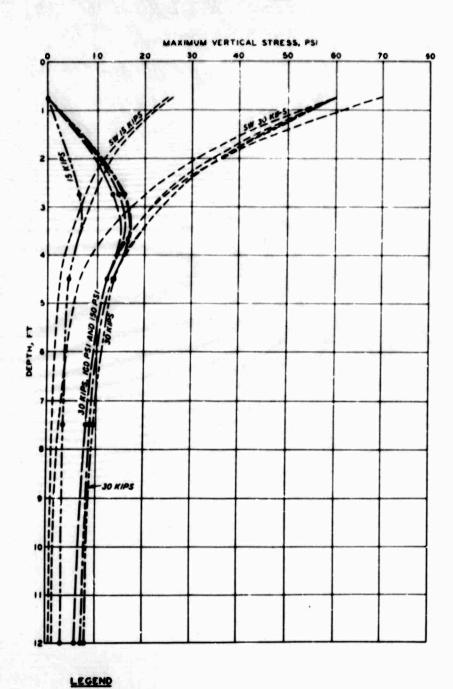


Figure 36. Comparison of Assembly Load Point Curves for Vertical Stress Under Static Loads, Item 4, Flexible Pavement



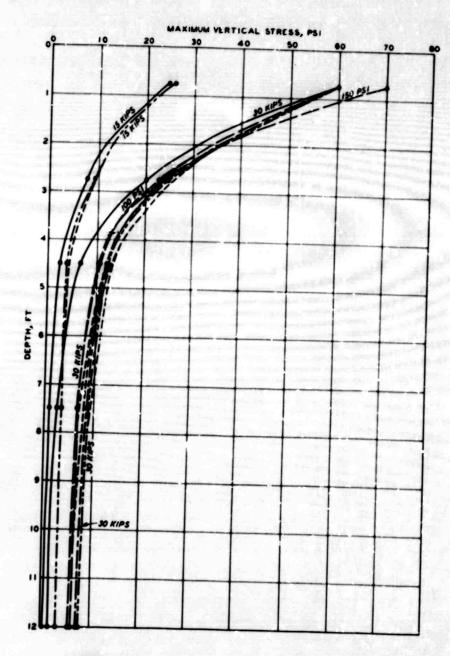
NOTE: CURVES ARE AVERAGES OF GAGE RESPONSES. ALL LOADS ARE PER WHEEL.

Figure 37. Elastic Stress Versus Depth for Static Load Tests, Item 4, Flexible Pavement



TWIN TAND

Figure 38. Depth Versus Vertical Stress for Dynamic Load Tests, Assembly Load Point 1, Item 4, Flexible Pavement



LEGEND
SINGLE WHEEL
TWIN TANDEM 747
O WHEEL
12 WHEEL
LIMITING CURVE

Figure 39. Depth Versus Vertical Stress for Dynamic Load Tests, Assembly Load Point 2, Item 4, Flexible Pavement

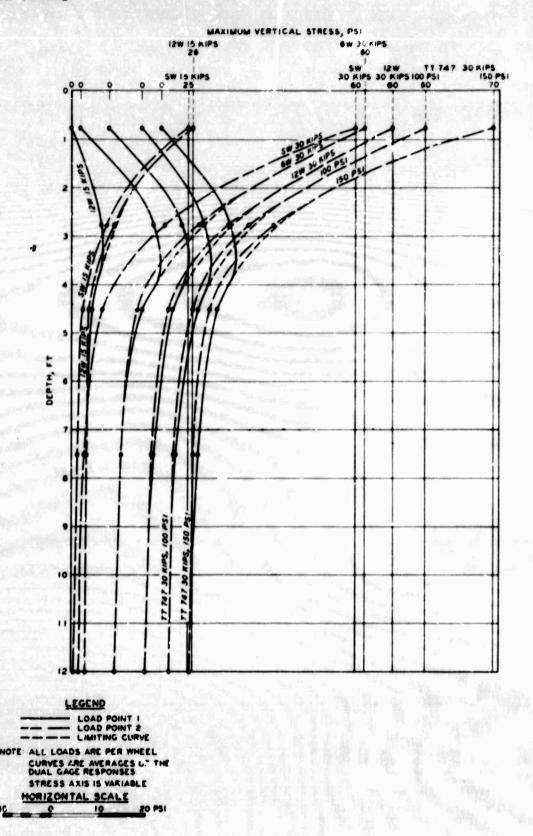


Figure 40. Comparison of Assembly Load Point Curves for Vertical Stress Under Dynamic Loads, Item 4, Flexible Pavement

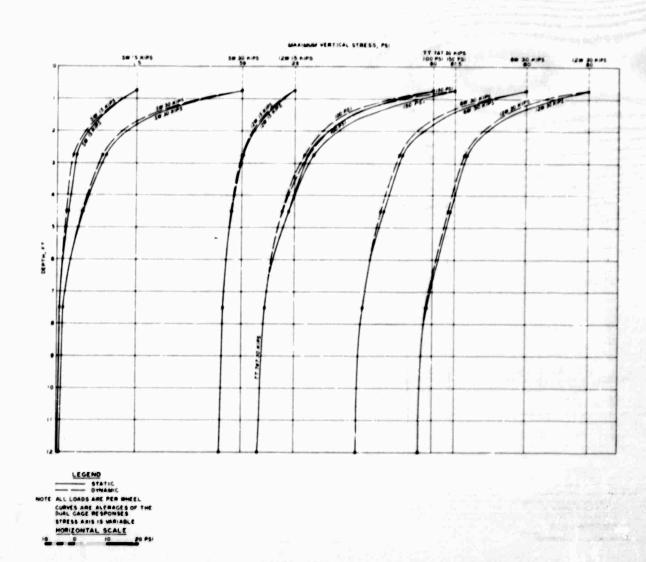


Figure 41. Static Versus Dynamic Load Limiting Vertical Stress Curves, Item 3, Flexible Pavement

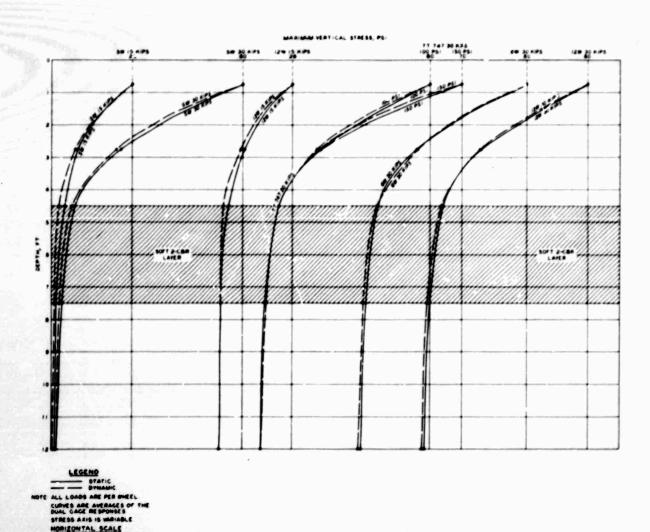


Figure 42. Static Versus Dynamic Load Limiting Vertical Stress Curves, Item 4, Flexible Pavement

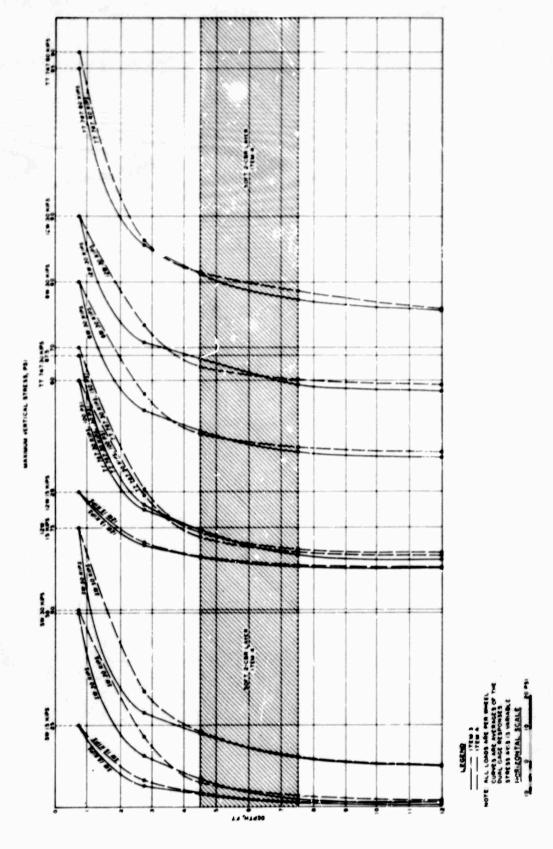


Figure 43. Item 3 Versus Item 4 Limiting Vertical Stress Curves, Static Load Flexible Pavement Tests

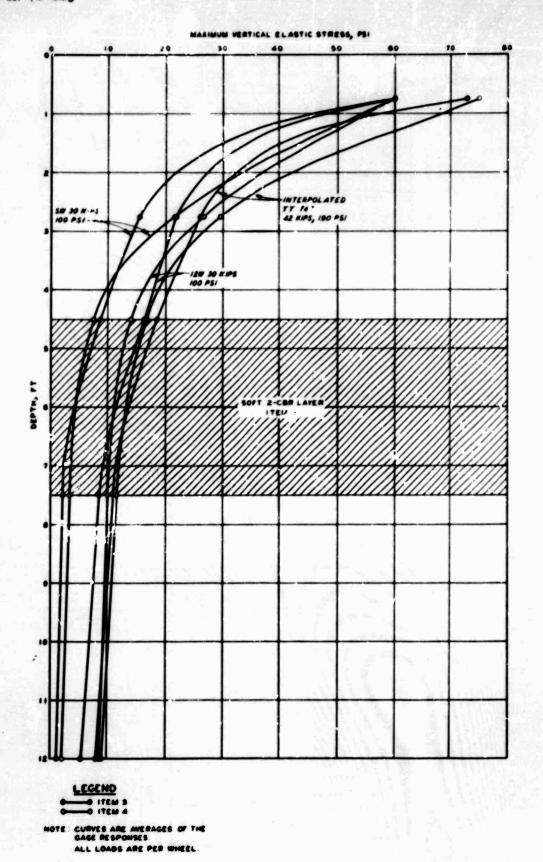


Figure 44. Comparison of Flastic Stress Versus Depth for Static Load Tests, Items 3 and 4, Flexible Favement

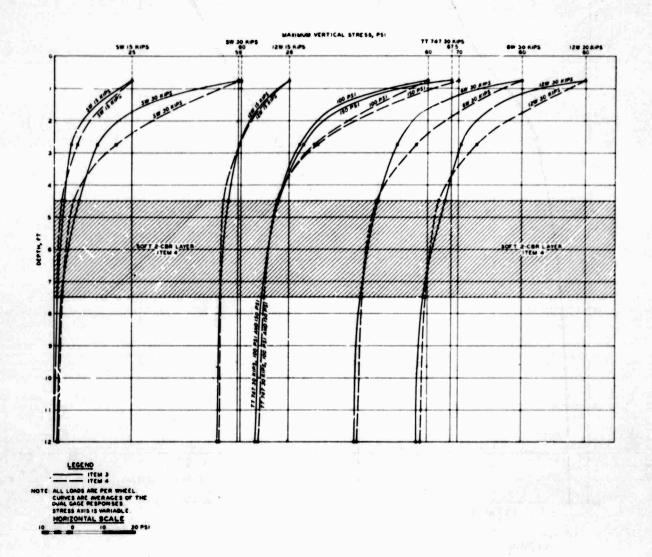
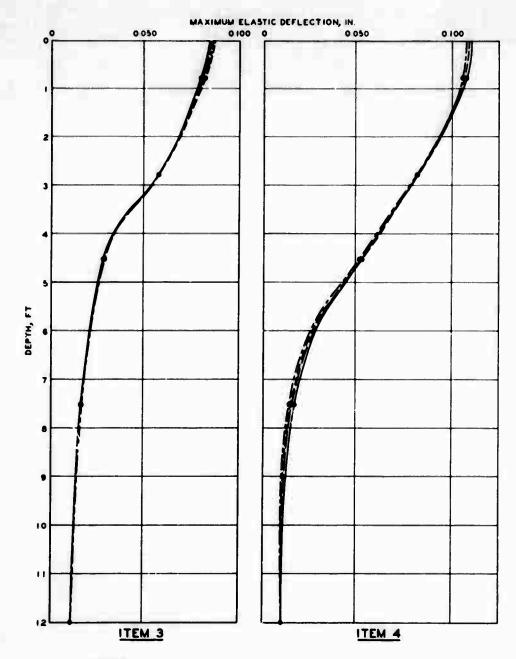


Figure 45. Item 3 Versus Item 4 Limiting Vertical Stress Curves,
Dynamic Load Flexible P. rement Tests



SLOW (I-2 MPH)
NORMAL (APPROX 3 MPH)
2 X NORMAL (5-6 MPH)
FAST (9-10 MPH)

NOTE: CURVES ARE AVERAGES OF THE DUAL GAGE RESPONSES.

Figure 46. Depth Versus Deflection for Speed Tests, Items 3 and 4. Single-Wheel, 30-kip Load, Flexible Pavement Tests

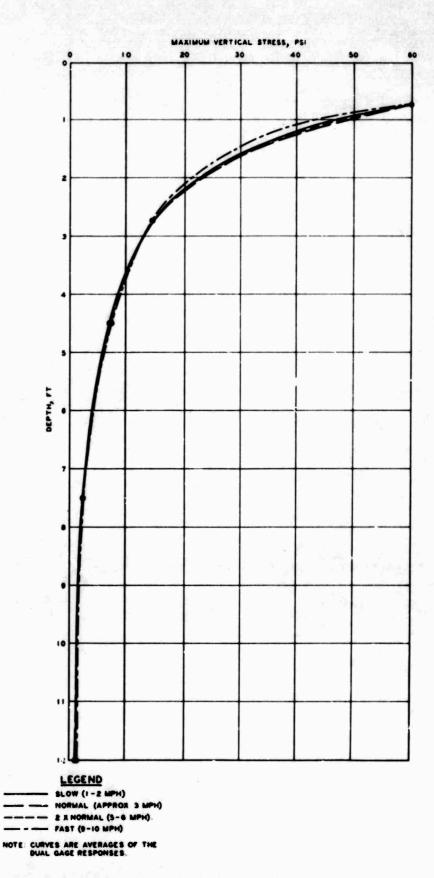


Figure 47. Depth Versus Vertical Stress for Speed Tests, Item 3. Single-Wheel, 30-kip Load, Flexible Pavement Tests

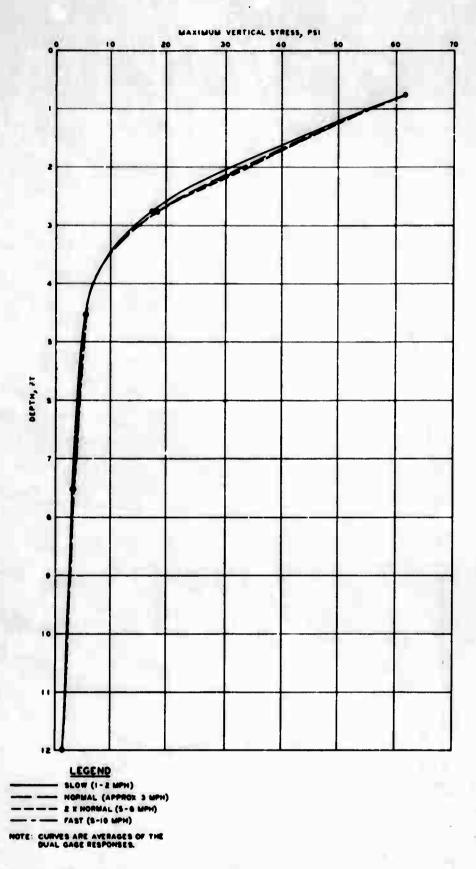


Figure 48. Depth Versus Vertical Stress for Speed Tests, Item 4. Single-Wheel, 30-kip Load, Flexible Pavement Tests

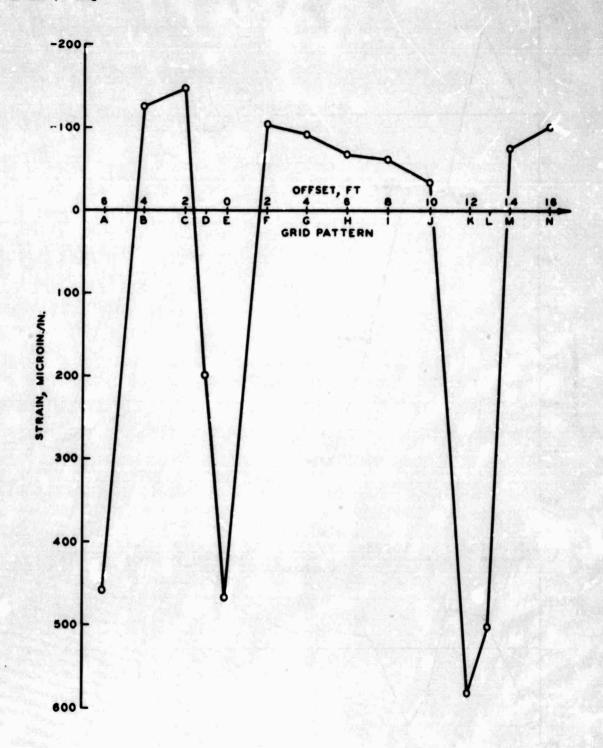
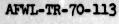


Figure 49. East-West Offsets Versus Pavement Strain for Assembly Load Point 2, Static Load Tests, 12-Wheel, 360-kip Load. Gage S1 (1N), Item 4, Flexible Pavement. Offset Distances Are Parallel to the Direction of Forward Movement of the Assembly; Offset Distances and Grid Pattern Are Shown in Figure 4.



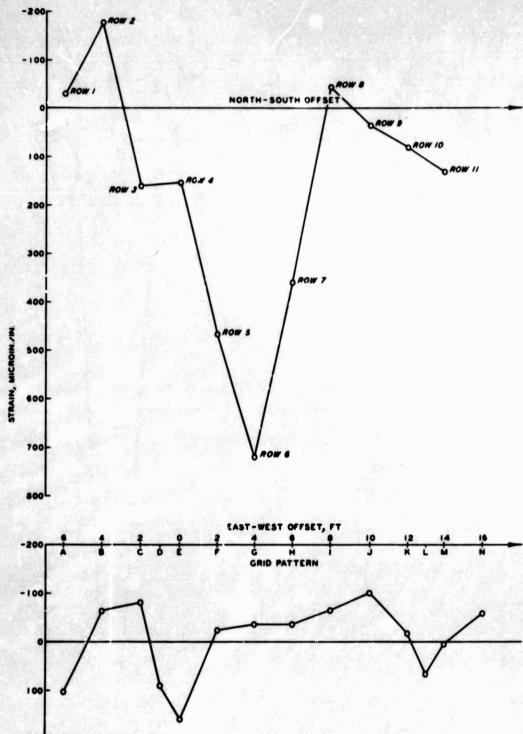
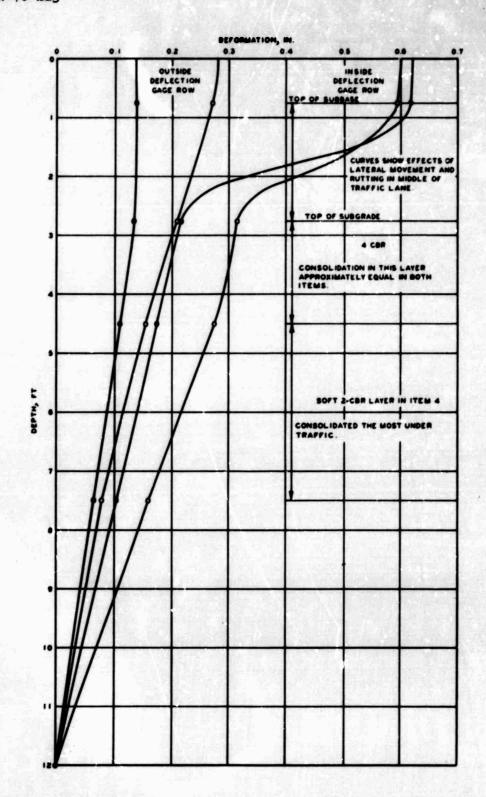
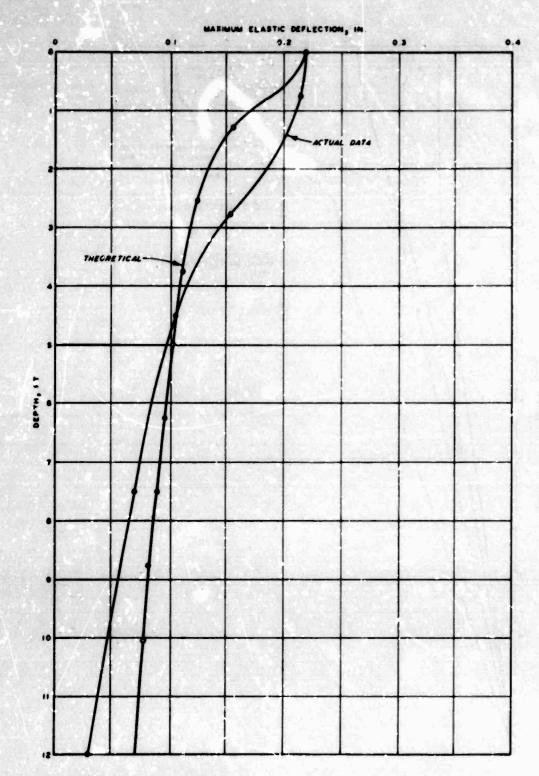


Figure 50. East-West and North-South Offsets Versus Pavement Strain for Assembly Load Point 1, Static Load Tests, 12-Wheel, 360-kip Load. Gage Sl (IN), Item 4, Flexible Pavement. N-S and E-W Offset Distances Are Parallel and Perpendicular, Respectively, to the Direction of Forward Movement of the Assembly. Offset Distances, Row Numbers, and Grid Patterns Are Shown in Figure 4.



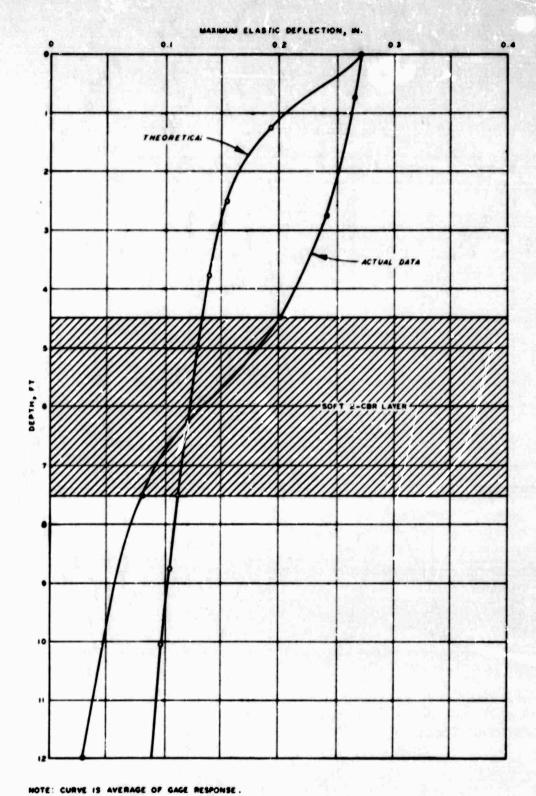
LEGEND 17EM 2

Figure 51. Deformation for the Elapsed Time Period of Traffic Tests Versus Depth for Items 3 and 4, Flexible Pavement



NOTE: CURVE IS AVERAGE OF GAGE RESPONSE. LOAD IS PER WHEEL.

Figure 52. Comparison of the Computed and Actual Data for Maximum Elastic Deflection Versus Depth for 12-Wheel, 30-kip Load (100-psi Tire Inflation Pressure), Item 3, Flexible Pavement



LOAD IS PER WHEEL.

Figure 53. Comparison of the Computed and Actual Data for Maximum Elastic Deflection Versus Depth for 12-Wheel, 30-kip Load (100-psi Tire Inflation Pressure), Item 4, Flexible Pavement

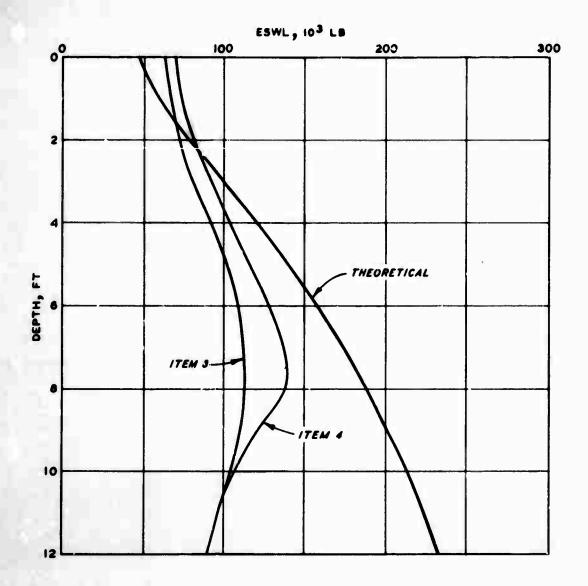
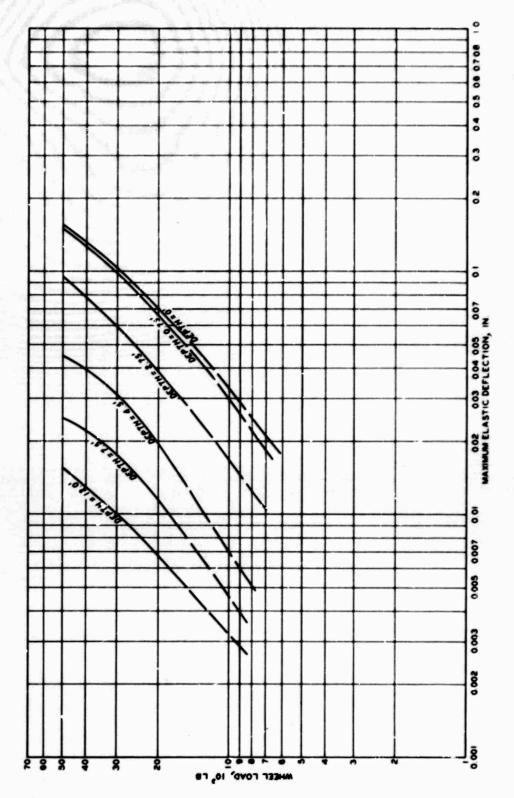
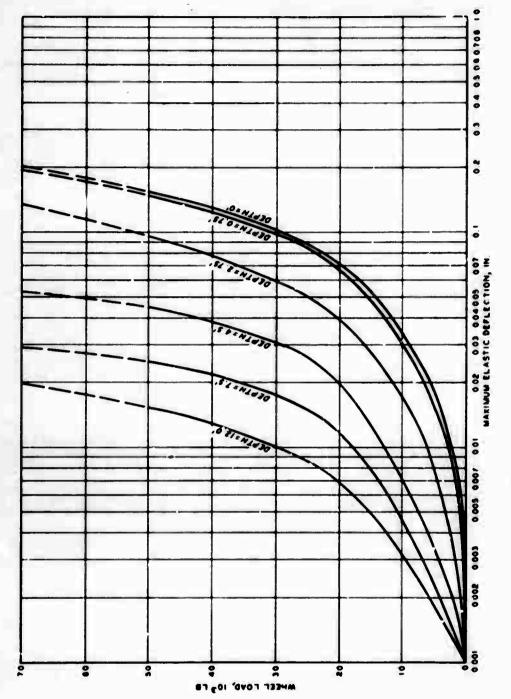


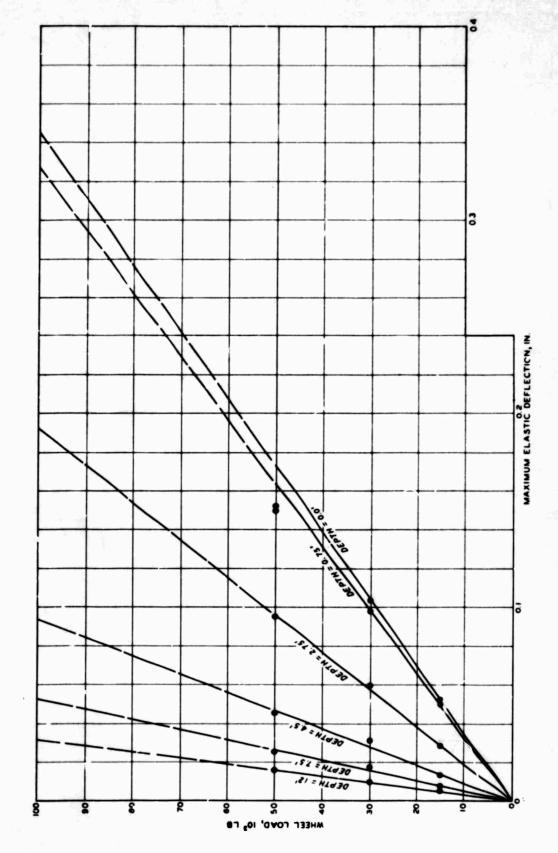
Figure 54. Comparison of the Computed Curve with Actual Data for ESWL Versus Depth. 12-Wheel, 360-kip Load, Flexible Pavement Tests



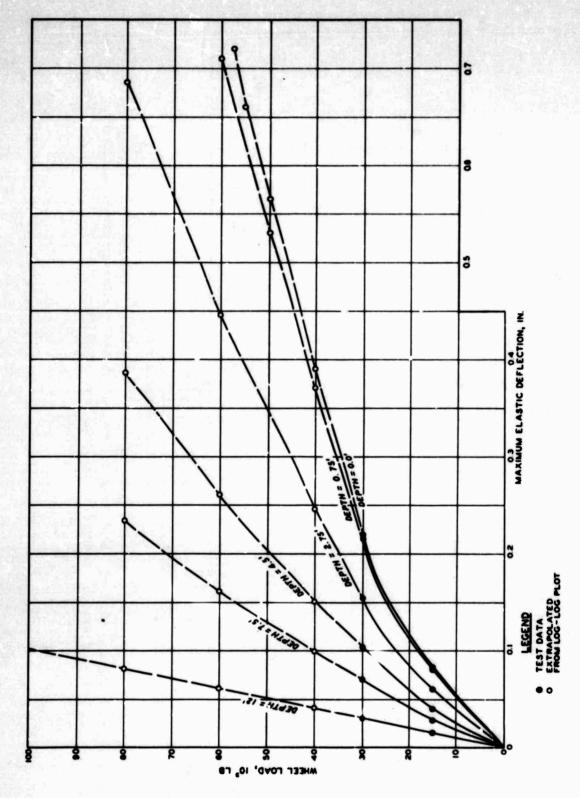
Log-Log Plot of Wheel Load Versus Deflection for Static Load, Single-Wheel Tests, Item 3, Flexible Pavement Figure 55.



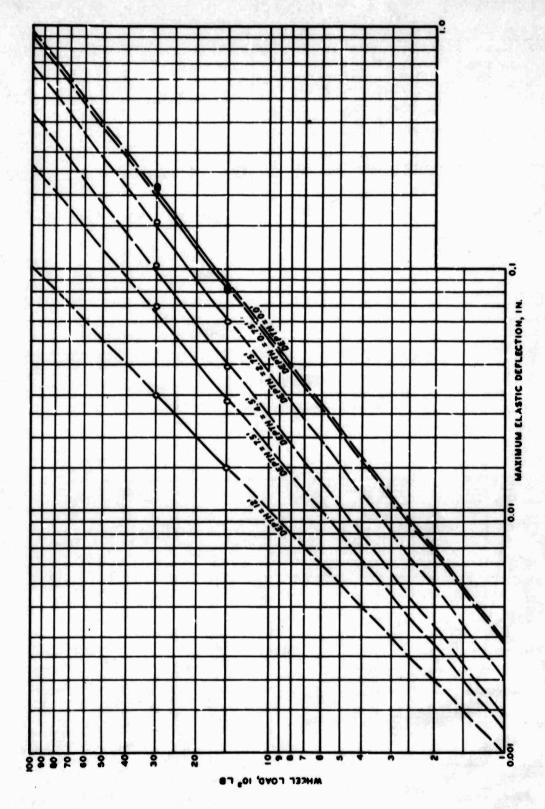
Semilog Plot of Wheel Load Versus Deflection for Static Load, Single-Wheel Tests, Item 3, Flexible Pavement (Same Data Shown in Figure 55) Figure 56.



Arithmatic Plot of Wheel Load Versus Deflection for Static Load, Single-Wheel Tests, Item 3, Flexible Pavement (Same Data Shown in Figure 55) Figure 57.



Arithmetic Plot of Wheel Load Versus Deflection for Static Load, 12-Wheel Tests, Item 3, Flexible Pavement (Data Extrapolated from Figure 59) Figure 58.



Log-Log Plot of Wheel Load Versus Deflection for Static Load, 12-Wheel Tests, Item 3, Flexible Pavement (Same Data Shown in Figure 58) Figure 59.

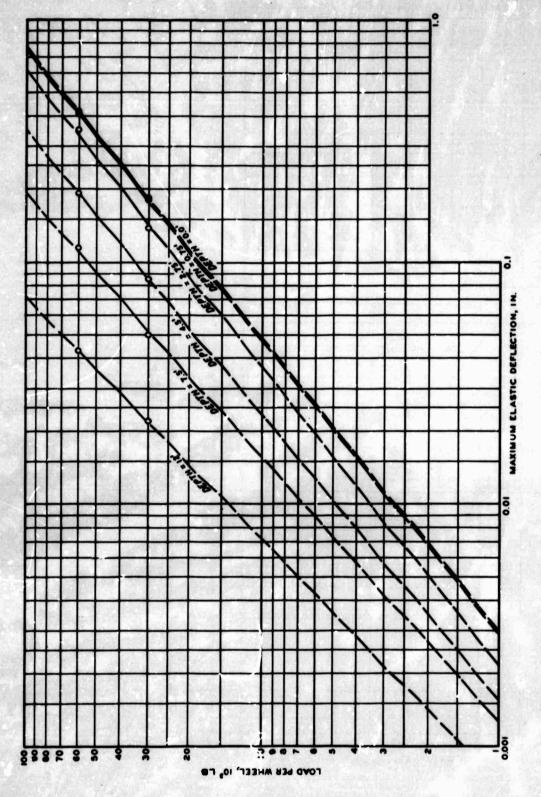


Figure 60. Wheel Load Versus Deflection for Static Load, Twin-Tandem Tests, Item 3, Flexible Pavement

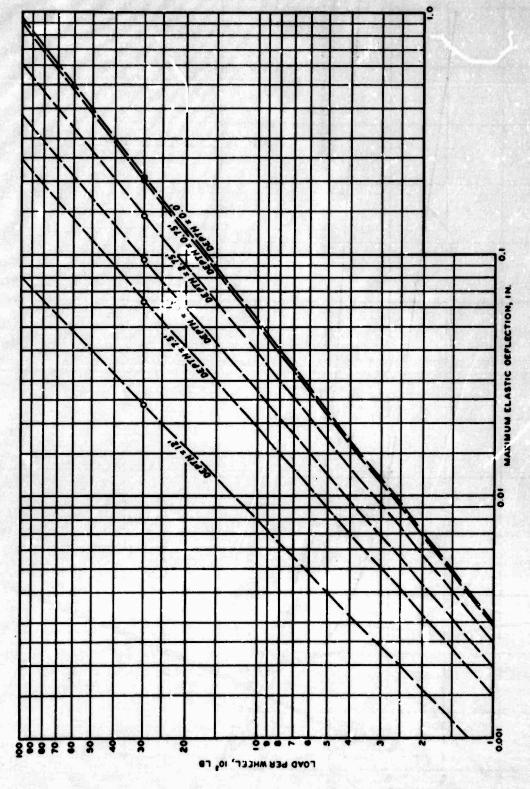
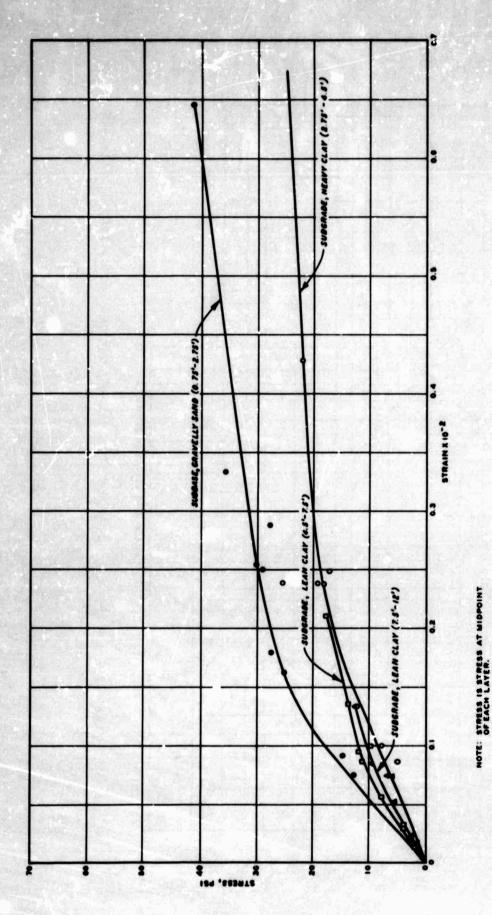


Figure 61. Wheel Load Versus Deflection for Static Load, 6-Wheel Tests, Item 3, Flexible Pavement



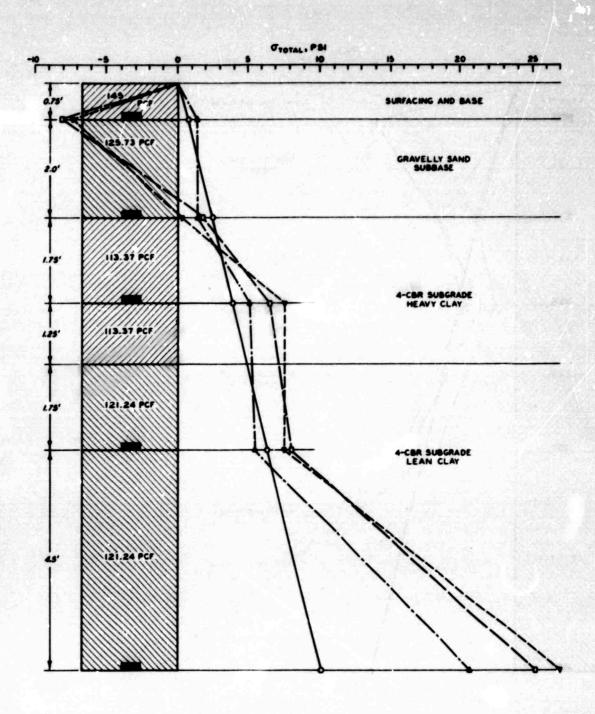
Stress Versus Strain for Static Loading, All Wheel Assemblies, Item 3, Flexible Pavement Figure 62.

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NOTE: Figure 63 is a folded sheet and is enclosed at the back of this volume.

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NOTE: Figure 64 is a folded sheet and is enclosed at the back of this volume.



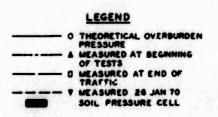
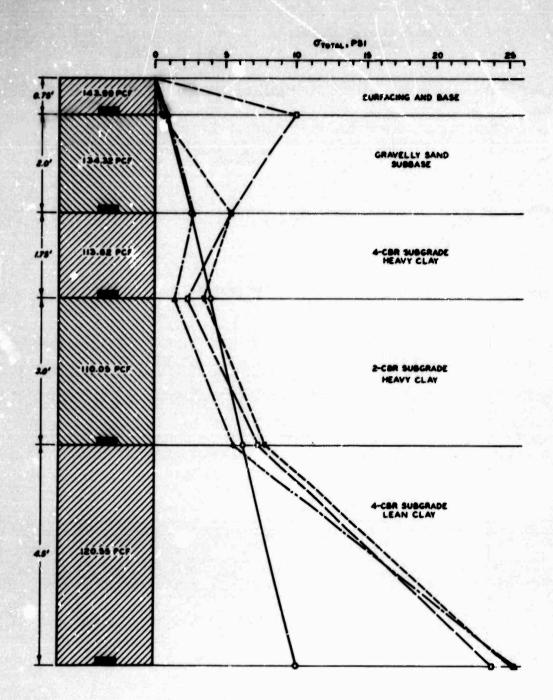


Figure 65. Change in Total Stress ototal with Depth, Item 3, Flexible Pavement



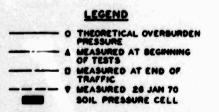


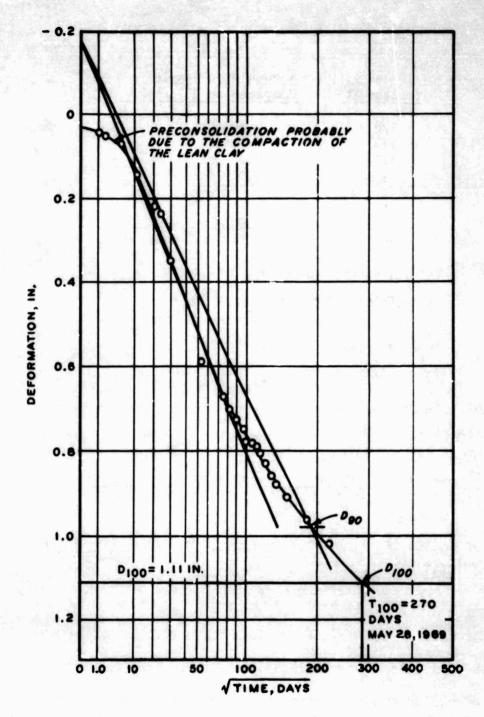
Figure 66. Change in Total Stress ottotal with Depth, Item 4, Flexible Pavement

AFWL-TR-113

NOTE: Figure 67 is a folded sheet and is enclosed at the back of this volume.

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NOTE: Figure 68 is a folded sheet and is enclosed at the back of this volume.



D₉₀ = Graphically determined point for 50 percent primary consolidation

D₁₀₀ = Graphical slope-ratio determined point of 100 percent primary consolidation

T₁₀₀ = Graphical slope-ratio determined time for 100 percent primary consolidation

Figure 69. Taylor Square-Root-of-Time Fitting Method Applied to Field Deflection Data for a Deflection Gage at 7.50-ft Depth, Flexible Pavement Test Section

Load tons/sq ft	Accumulated Sample Compression H, in.
1/8	0.00340
1/4	0.00632
1/2	0.01108
	0.01840
2	0.02970
4	0.04240
8	0.07620
12	0.09270

Initial water content w_i, % 22.5

Final water content w_f, % 18.4

Final weight of solids w_s, gm 442.32

Specific gravity of solids G_s 2.69

Unit weight of water γ_w, gm/cc 1

To find initial void ratio, e:

Assume soil fills ring at end of test

Final total volume
$$V_T$$
 = (Area of sample x (Final sample height)
= $\frac{91.52 \text{ cm}^2}{6.45 \text{ cm}^2/\text{in}^2}$ (1.0614 in.) or 15.1 in³

Final volume of solids
$$V = \frac{W_s}{G_s \gamma_w} = \frac{\frac{142.32 \text{ gm}}{(2.69)(1 \text{ gm/cc})(16.38 \text{ cm}^3/\text{in}^3)}$$

= $\frac{142.32}{14.1}$ in or 10.1 in 3

Final volume of voids $V = V_T - V = 15.1 \text{ in}^3 - 10.1 \text{ in}^3 \text{ or } 5 \text{ in}^3$

Initial height of solids H = 0.707 in.

Final height of solids change after test or load involvement ΔH = 0.0927 in.

Final void ratio change $\Delta e = \frac{\Delta H}{H_g} = \frac{0.0927}{0.7074}$ or 0.131

Final void ratio $e_{final} = \frac{V_T - V_S}{V_S} = \frac{V}{V} = \frac{5}{10.1}$ or 0.499

Initial void ratio $e_0 = e_f + \Delta e = 0.499 + 0.131$ or 0.630

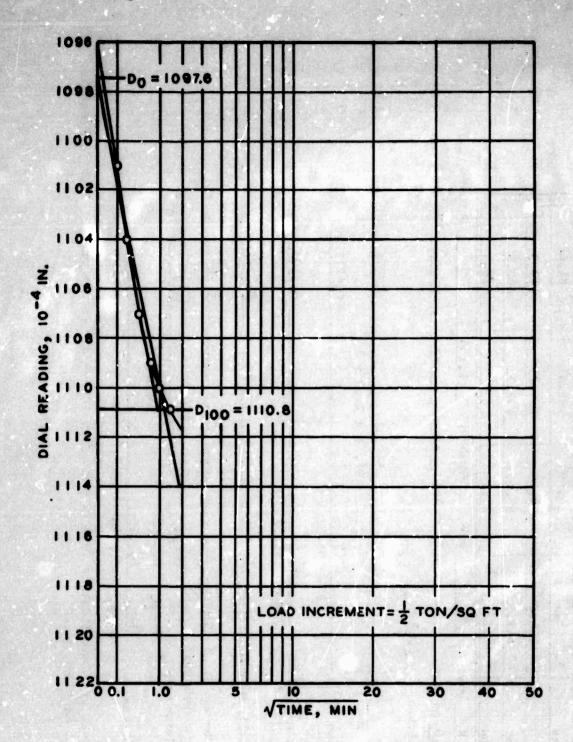
Figure 70. Laboratory Consolidation Test of Lean Clay (CL) from the Subgrade of Item 3, Flexible Pavement Test Section

		Before Test		After Test	
	AII	Screps	Sd	IIV VIII	
Tare No.	Ring & Plates	15	67	69	
Tare + Wet Soil. grams	1759.2	315,51	90*059	643.13*	*Correction =
Tare + Dry Soil. grams	(1661.3)	278.62	561.65	561.65	6.93 grams
Weight of Water. grams	Ww 97.9	36,89	14*88	W _{wf} = 81,48	
Tare Weight, grams	1218,0	119,06	119,33	119.33	
Weight of Solid. grams	(442,3)	159,56	442,32	W. = 442.32	
Water, Content, percent	Wo = 22.1 %	23.1		W _f = 18.4	×

in	5	
1,154	i	
Height. H = 1.1	Nos.	
52 cm ²	Weight of Plates Nos.	ist in
Area, A = 91		2.69
Consolidometer No. K Area, A = 91,52 cm ²	Weight of Ring 1218.0 gm	Specific gravity of Solids, s. = 2.69 est

Height of Solids, H	Н		0,7074 in.	Ę
A×S ×Y W	2.54 x 91.52 x 97.9	2.69 x 1	0.4211	
Original freight of water, five A × Y.	2.54 × 91.52 × 1			Ė
Final Height of Water, H.,	81,48		0,3505 in.	Ë
A×Y 2.5	1× 91.52 × i			
Net Change in height of Specimen at end of test, Δ H = -	test, Δ H =		0.0927	Ė
Height of Specimen after test, H, - H + ΔH			1,0613	Ħ
Specimen did not rebound H	0.4211		94.3	
99440 H-H 0.4466	99770 "Н			R
Degree of Saturation after test. G, = Hwt	0,3505		99.0	ĸ
1- H	0.3540			

Data Sheet for Consolidation Test of Lean Clay (CL) from the Subgrade of Item 3, Flexible Pavement Section Figure 71.



D_O = Value obtained for corrected primary consolidation zero point according to the Terzaghi theory

D₁₀₀ = Graphical slope-ratio determined point of 100 percent primary consolidation

Figure 72. Taylor Square-Root-of-Time for Consolidation Tests of Lean Clay (CL) from the Flexible Pavement Test Section

Initial void ratio e = 0.630

Load tons/sq ft	Void Ratio Change, Δe	Void Ratio
1/8	0.00481	0.6252
1/4	0.00893	0.6211
1/2	0.01566	0.6143
1	0.02601	0.6040
2	0.04198	0.5880
4	0.05994	0.5701
8	0.10772	0.5223
12	0.13104	0.4990

Coefficient of consolidation
$$C_v = \frac{T_{90}H_d^2}{t_{90}} = \frac{(0.848)(0.572)^2}{1 \text{ min}}$$

= 0.277 in²/min or 0.0298 cm²/sec

where

Time factor in Terzaghi theory corresponding to 90 percent

consolidation
$$T_{90} = 0.848$$

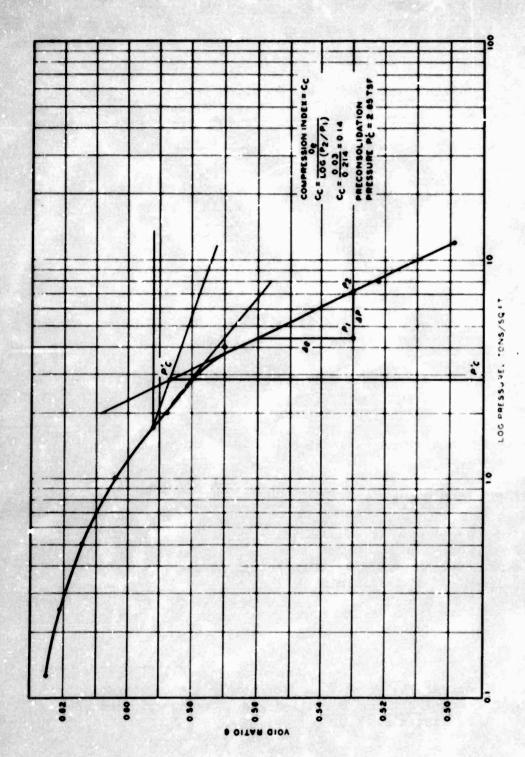
Maximum drainage length $H_d = \frac{H_s - \Delta H}{2} = \frac{1.154 - 0.0111}{2}$

or 0.5715 in.

Laboratory consolidation test time at 90 percent primary consolidation t₉₀ = 1 min

Note: At a load of 1/2 ton/sq ft, which is approximately the overburden pressure at the elevation of the first deflection gage, the coefficient of consolidation $C_v = 0.277 \text{ in}^2/\text{min}$.

Figure 73. Determination of Coefficient of Consolidation from Data Shown in Figure 70



P' = Preconsolidation pressure C = Compression index

 $\Delta P = Pressure increment (P_2 - P_1)$ $\Delta e = Void ratio change in an increment$

 $(e_1 - e_2)$

P = Applied pressure

e = Void ratio

Void Ratio Versus Log of Consolidation Pressure. Lean Clay (CL) from the Flexible Pavement Test Section Figure 74.

Using an ultimate field settlement $\Delta h_{final} = 1.5$ in.

Δh_U = Field settlement at U percent consolidation

T_U = Time factor for U percent consolidation from Terzaghi theory

 t_{U} = Field time for U percent consolidation to occur

$$t_{U} = T_{U} \left(H_{d}^{2}/c_{v} \right)$$

where

Coefficient of consolidation $C_v = 0.277 \text{ in}^2/\text{min} = 0.0298 \text{ cm}^2/\text{sec}$ Drainage length $H_d = 4.5 \text{ ft}$ (Drained only at bottom of layer) $H_d^2/C_v = (4.5 \text{ ft})^2/0.277 \text{ in}^3/\text{min} = 10,520 \text{ min}$

 $t_U = T_U \times 10,520 \text{ min}$

U Percent	Field Settlement Ah,, in.	Time Factor	Field Time	
Consolidation	<u></u>	<u>_</u>	minutes	days
0	0	0	0	0
0.1	0.15	0.0077	81	_
0.2	0.30	0.0314	331	
0.3	0.45	0.0707	745	
0.4	0.60	0.126	1,327	
0.5	0.75	0.196	2,065	
0.6	0.90	0.286	3,015	
0.7	1.05	0.403	4,240	
0.8	1.20	0.567	5,975	
0.9	1.35	0.848	8,940	
0.95	1.43	1.129	11,900	8.3
1.0	1.50	••		-

Figure 75. Computation of Field Rate of Consolidation

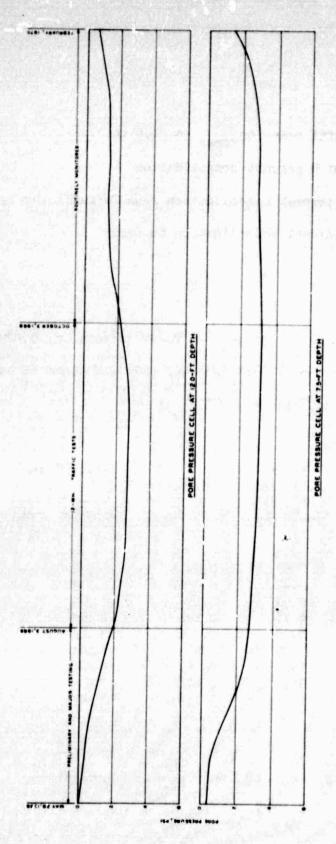


Figure 76. Pore Pressure Histories, Item 3, Flexible Pavement

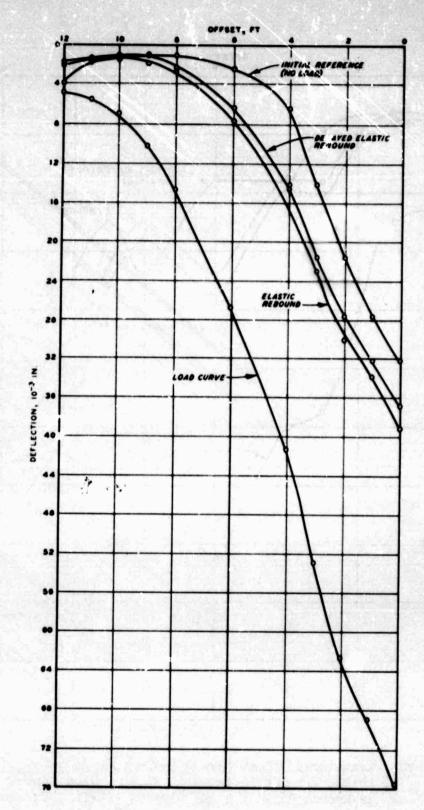


Figure 77. Transverse Offset Versus Deflection at 7.5-ft Depth, for Static Loading, Assembly Load Point 1, 12-Wheel, 360-kip Load, Item 3, Flexible Pavement

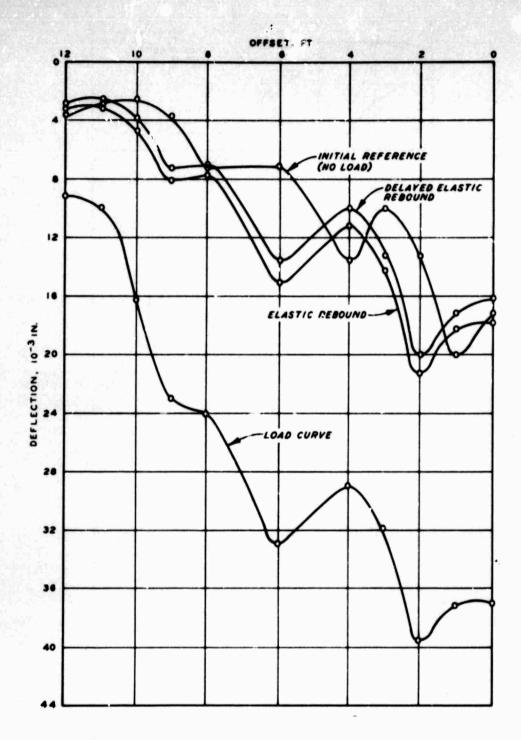
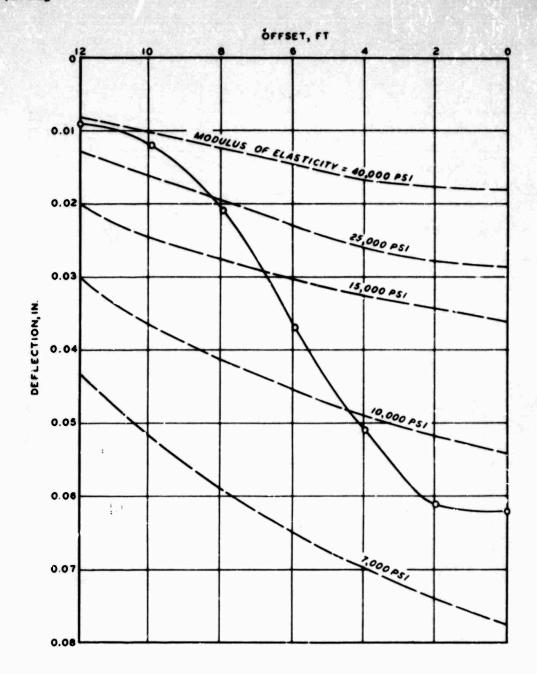


Figure 78. Transverse Offset Versus Deflection at 0.75-ft Depth, for Static Loading, Assembly Load Point 1, 12-Wheel, 360-kip Load, Item 3, Flexible Pavement



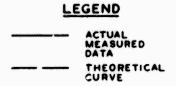


Figure 79. Transverse Offset Versus Theoretical and Measured Deflection at 7.5-ft Depth, 6-Wheel, 180-kip Load, Static Load Test, Item 3, Flexible Pavement

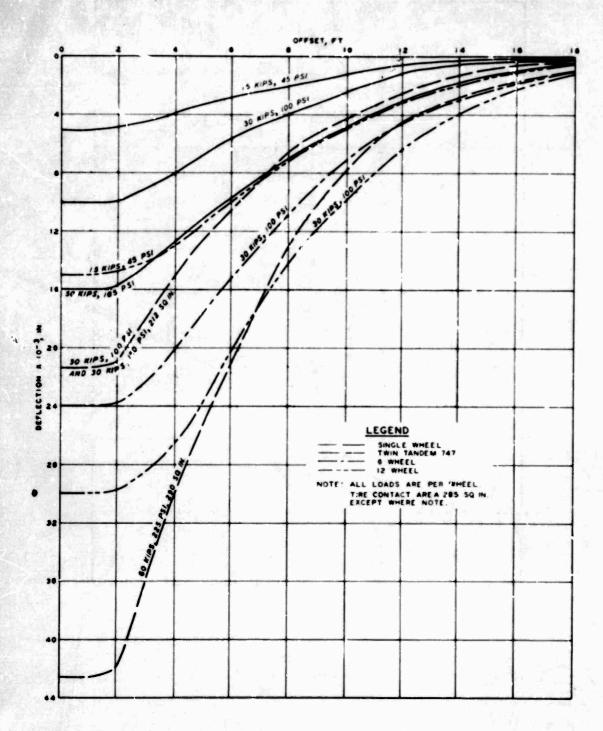


Figure 80. Transverse Offset Versus Deflection at 12-ft Depth, All Assemblies, Flexible Pavement Tests

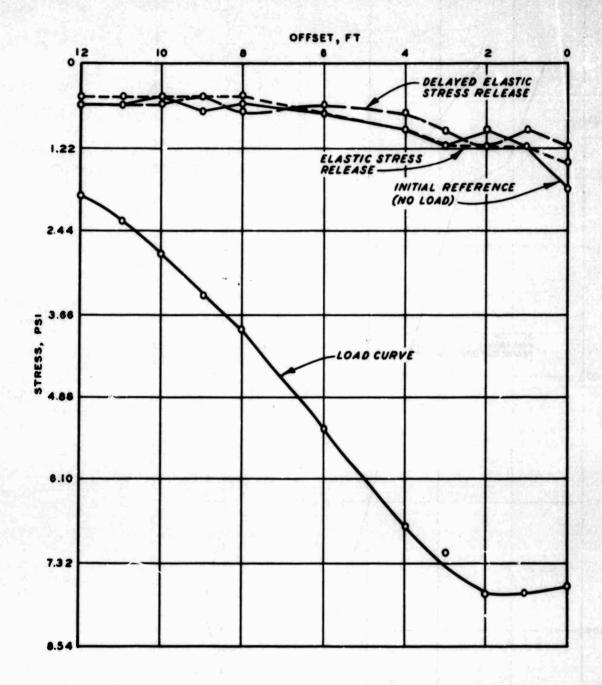


Figure 81. Transverse Offset Versus Stress at 12-ft Depth for Static Loading, Assembly Load Point 1, 12-Wheel, 360-kip Load, Item 3, Flexible Pavement

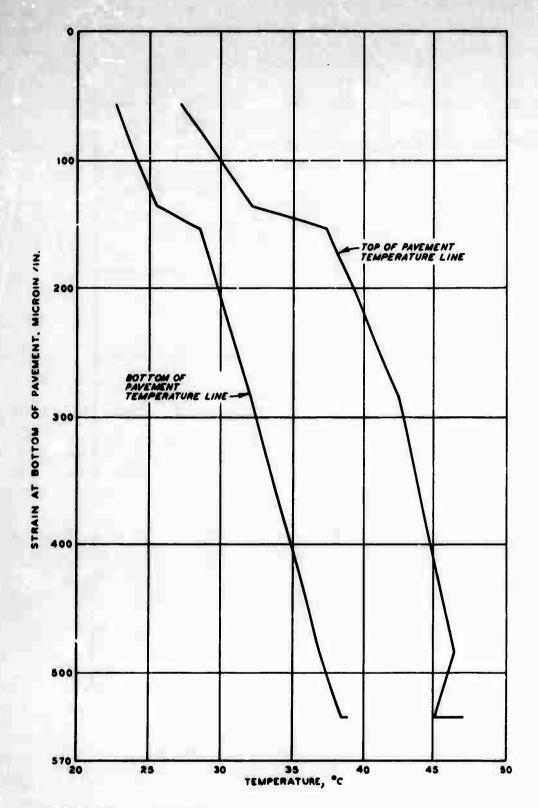
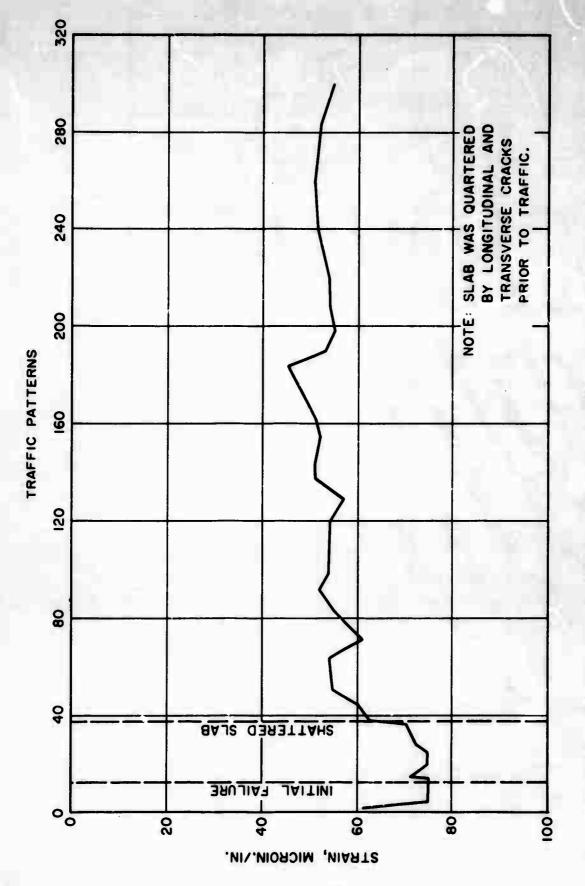


Figure 82. Temperature Versus Strain, Flexible Pavement



Strain Versus 12-Wheel Traffic Level, Gage ISCL, Offset No. 1, SW Slab, Item 1, Rigid Pavement Test Section Figure 83.

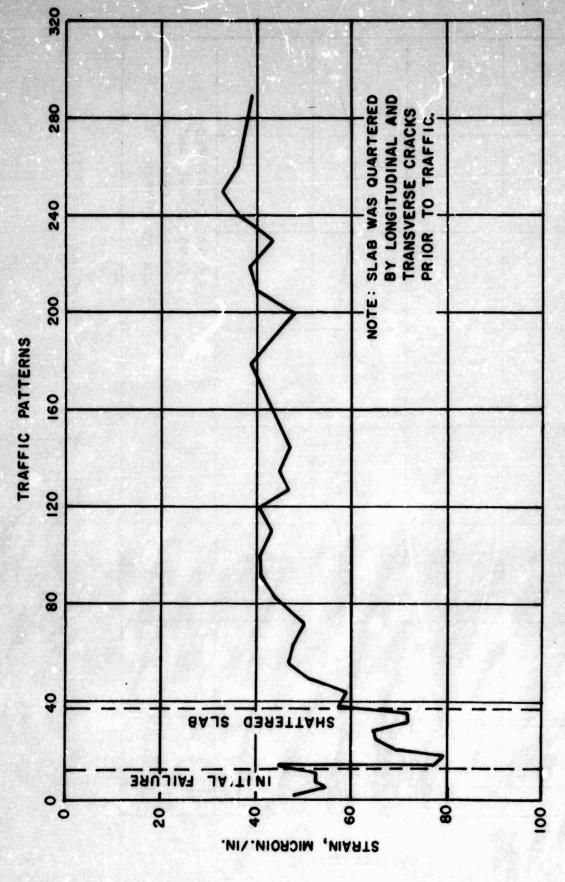
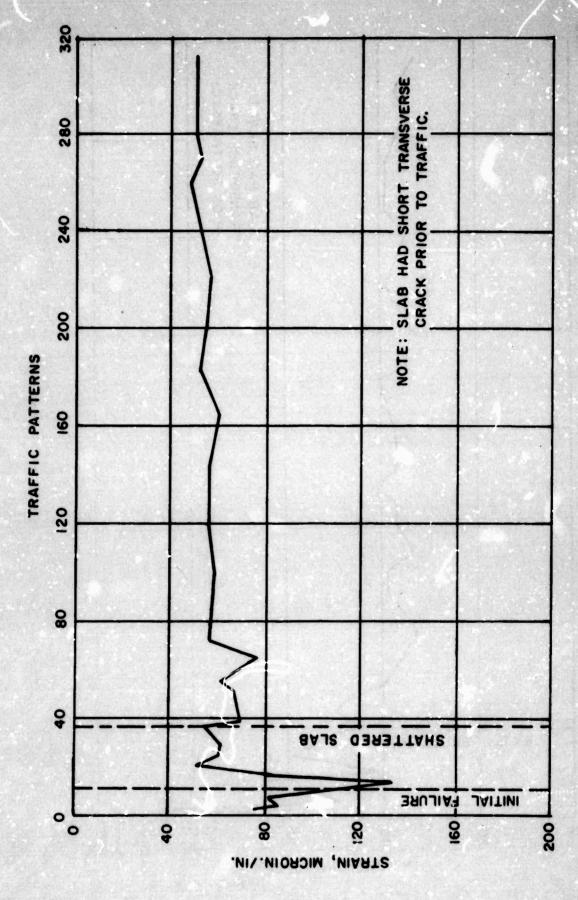
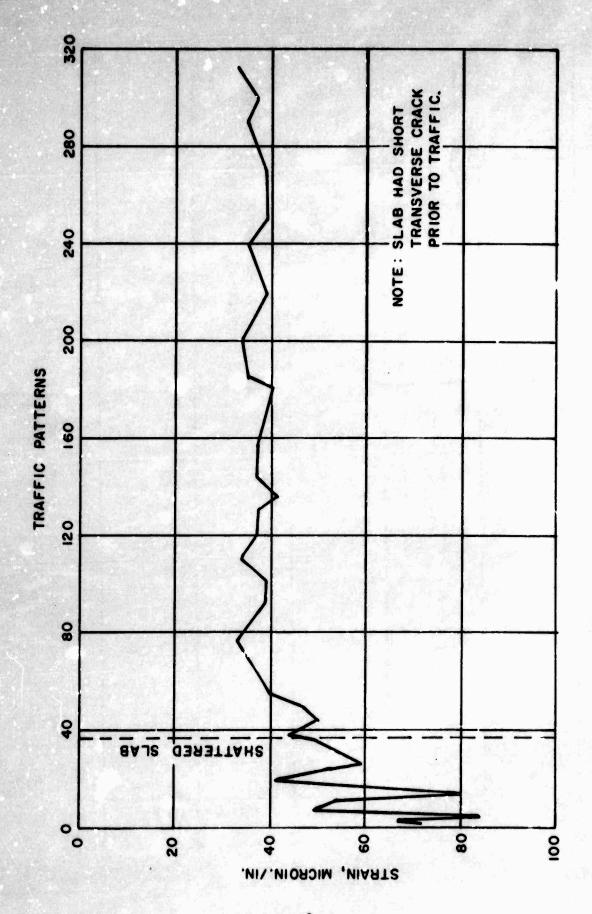


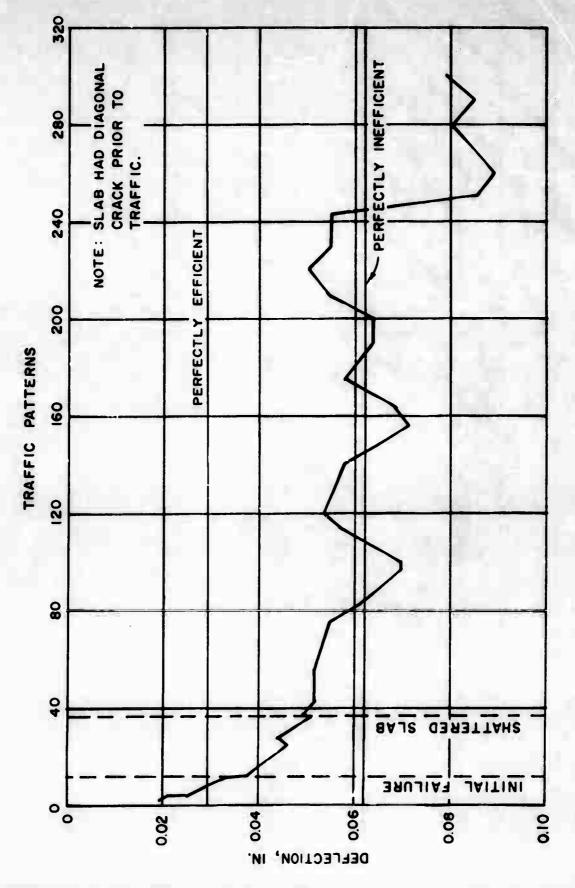
Figure 84. Strain Versus 12-Wheel Traffic Level, Gage ISCT, Offset No. 1, SW Slab, Item 1, Rigid Pavement Test Section



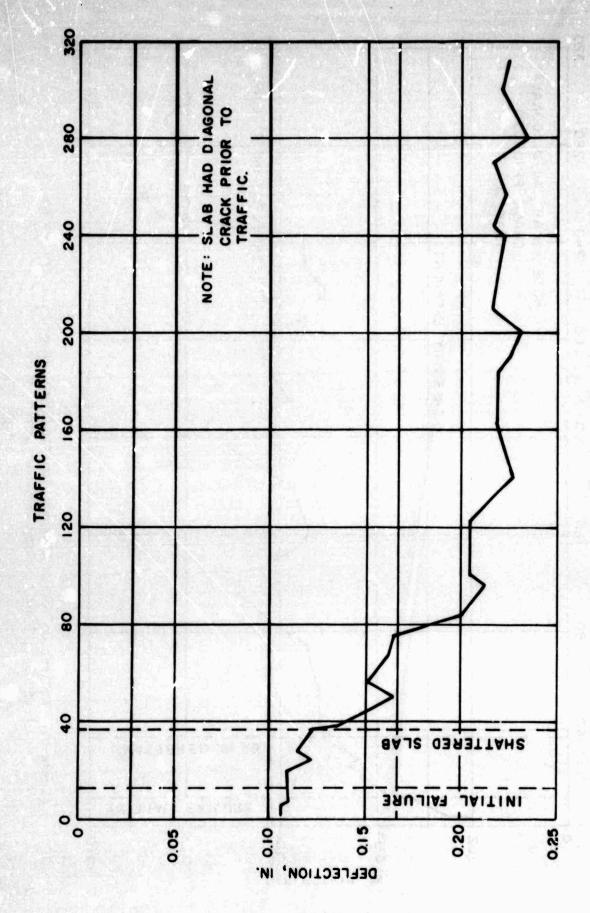
Strain Versus 12-Wheel Traffic Level, Gage ISNJL, Offset No. 4, NW Slab, Item 1, Rigid Pavement Test Section Figure 85.



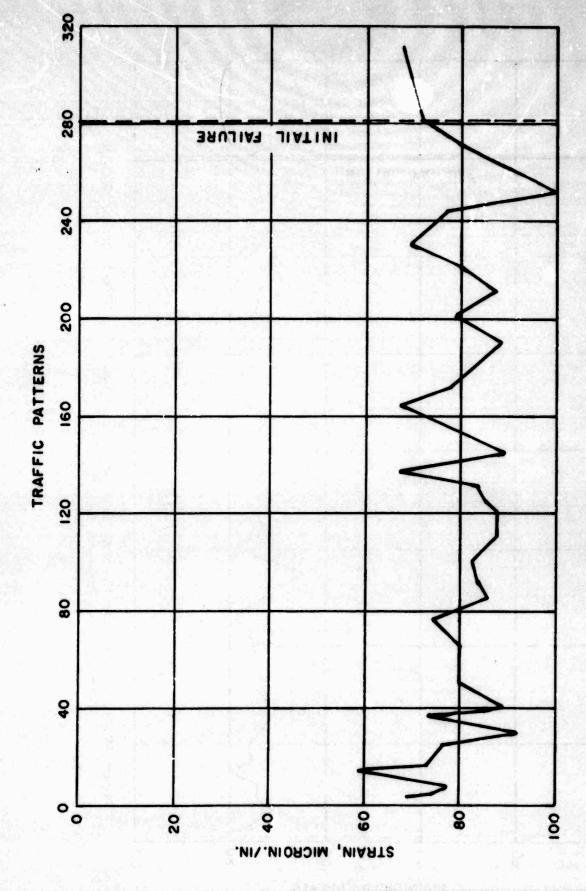
Strain Versus 12-Wheel Traffic Level, Gage ISNJL, Offset No. 5, NW Slab, Item 1, Rigid Pavement Test Section Figure 86.



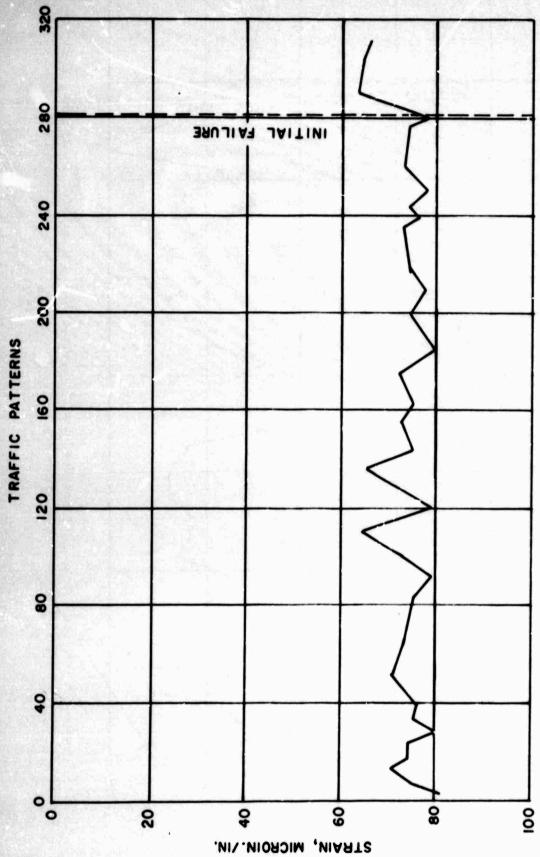
Deflection Versus 12-Whoel Traffic Level, Gage 13FD, Offset No. 5, SE Slab, Item 1, Rigid Pavement Test Section Figure 87.



Deflection Versus 12-Wheel Traffic Level, Gage 19FD, Offset No. 5, SE Slab, Item 1, Rigid Pavement Test Section Figure 88.

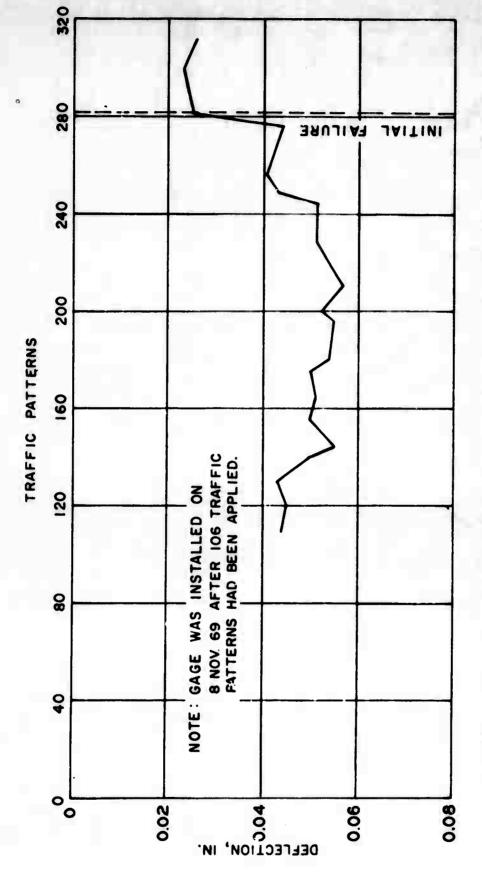


Strain Versus 12-Wheel Traffic Level, Gage 2SCT, Offset No. 1, SW Slab, Item 2, Rigid Pavement Test Section Figure 89.

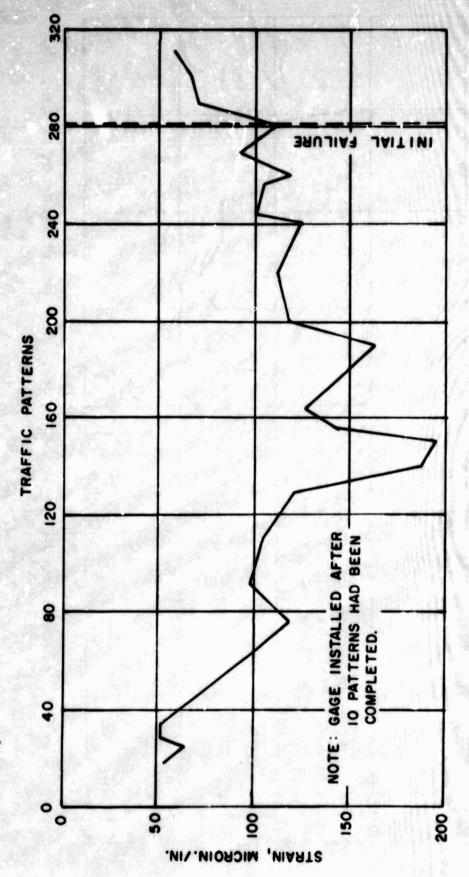


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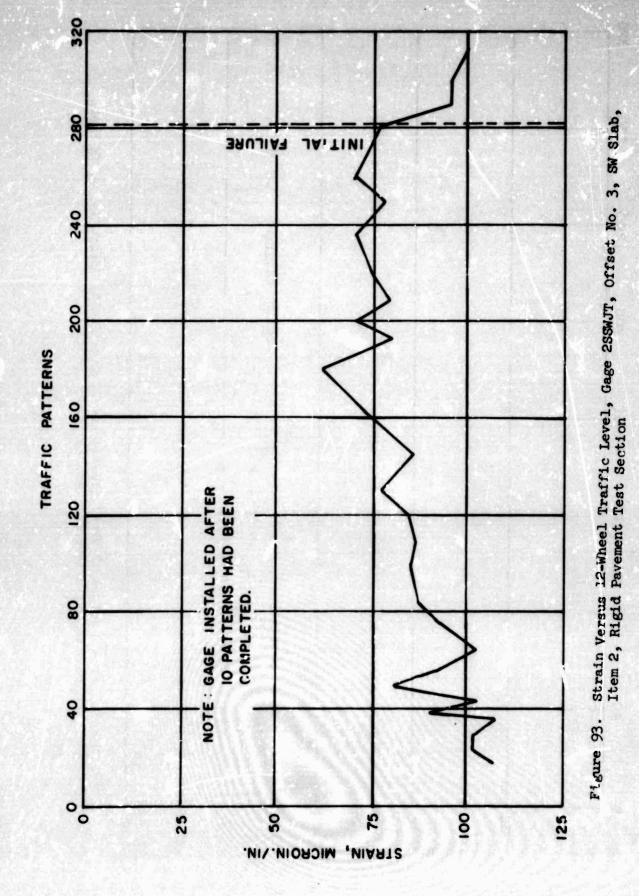
Strain Versus 12-Wheel Traffic Level, Gage 2SCL, Offset No. 1, SW Slab, Item 2, Rigid Pavement Test Section Figure 90.



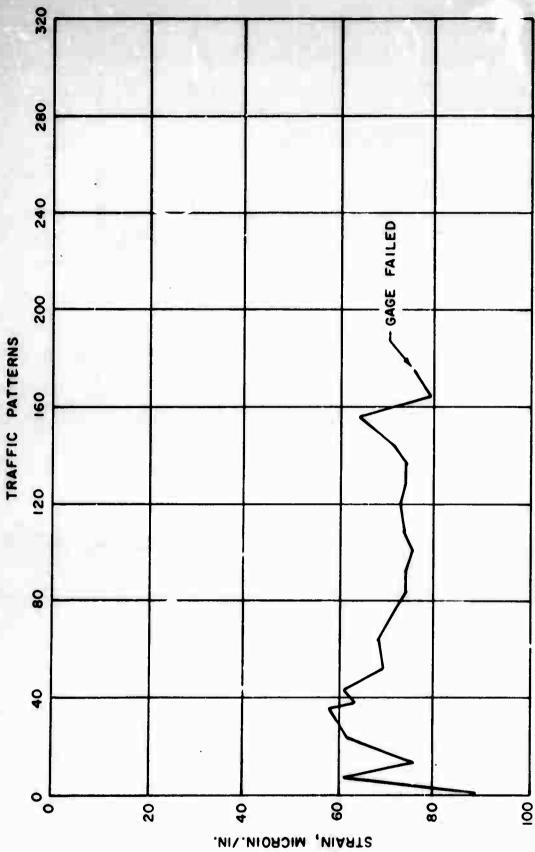
Deflection Versus 12-Wheel Traffic Level, Gage 2DC, Offset No. 1, SW Slab, Item 2, Rigid Pavement Test Section Figure 91.



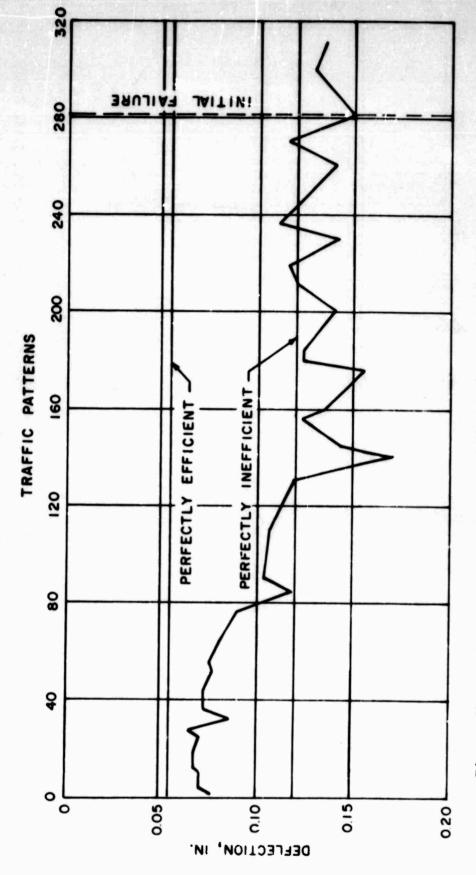
Strain Versus 12-Wheel Traffic Level, Gage 2SSJL, Offset No. 3, SW Slab, Item 2, Rigid Pavement Test Section Figure 92.



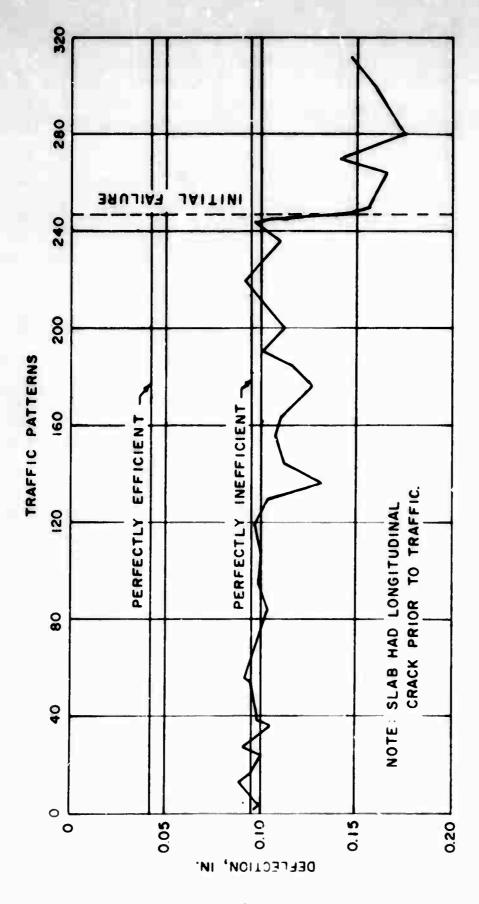
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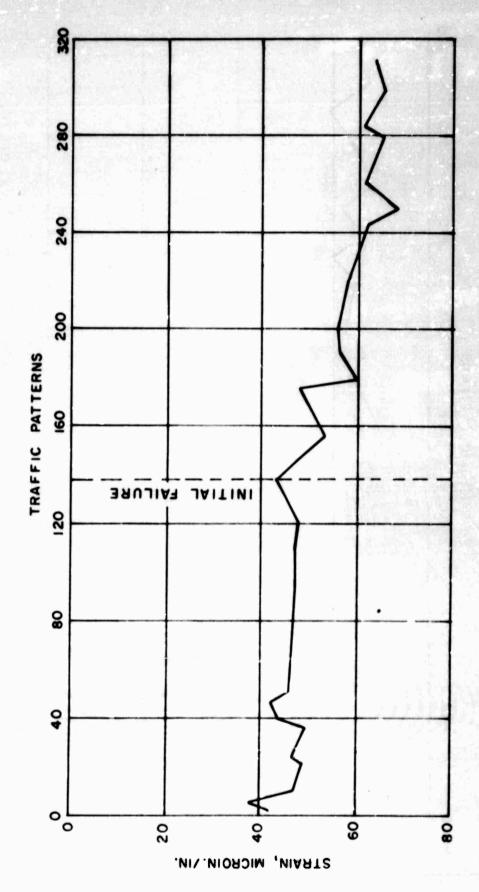
Strain Versus 12-Wheel Traffic Level, Gage 2SNJL, Offset No. 4, NW Slab, Item 2, Rigid Pavement Test Section Figure 94.



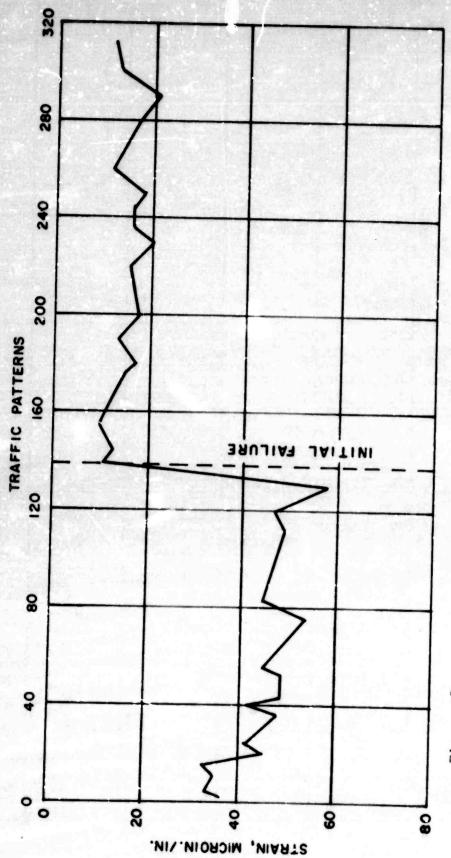
Deflection Versus 12-Wheel Traffic Level, Gage 2DSJL, Offset No. 5, Sw Slab, Item 2, Rigid Pavement Test Section Figure 95.



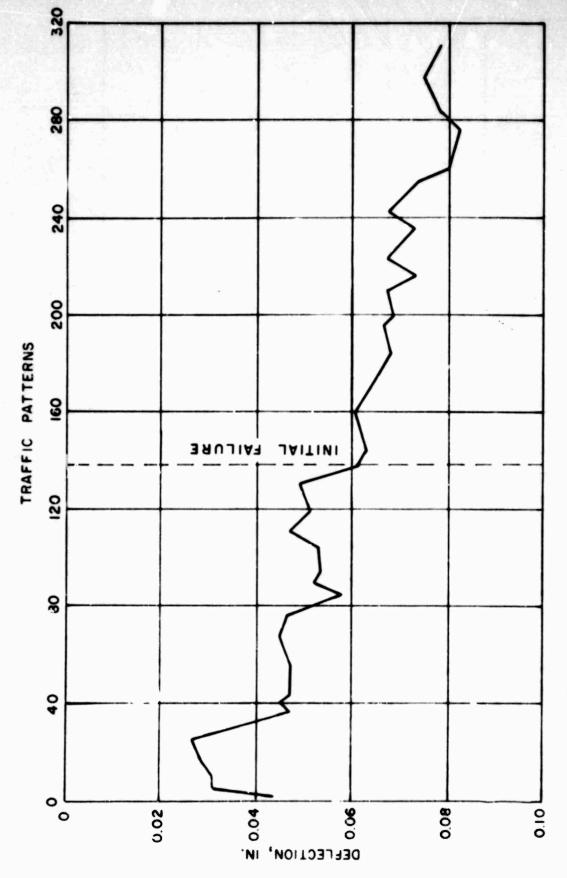
Deflection Versus 12-Wheel Traffic Level, Gage 29FD, Offset No. 5, SE Slab, Item 2, Rigid Favement Test Section Figure 96.



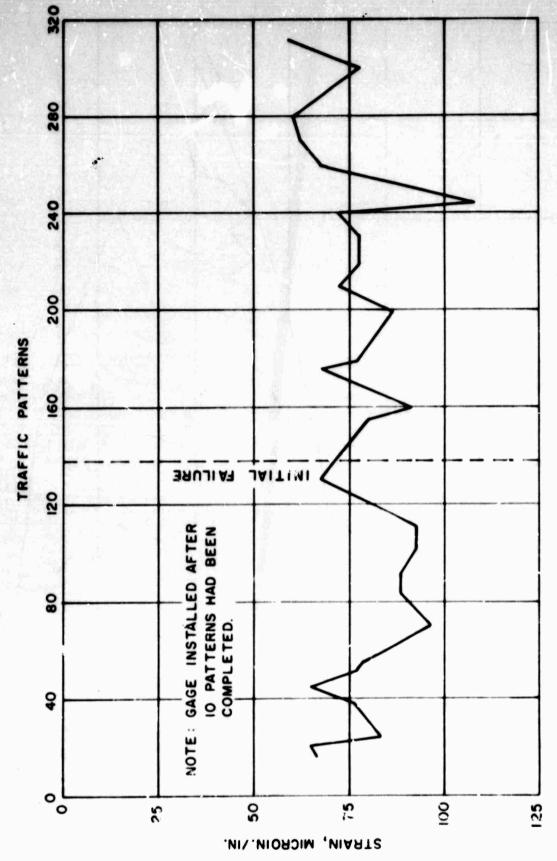
Strain Versus 12-Wheel Traffic Level, Gage 3SCT, Offset No. 1, SW Slab, Item 3, Rigid Pavement Test Section Figure 97.



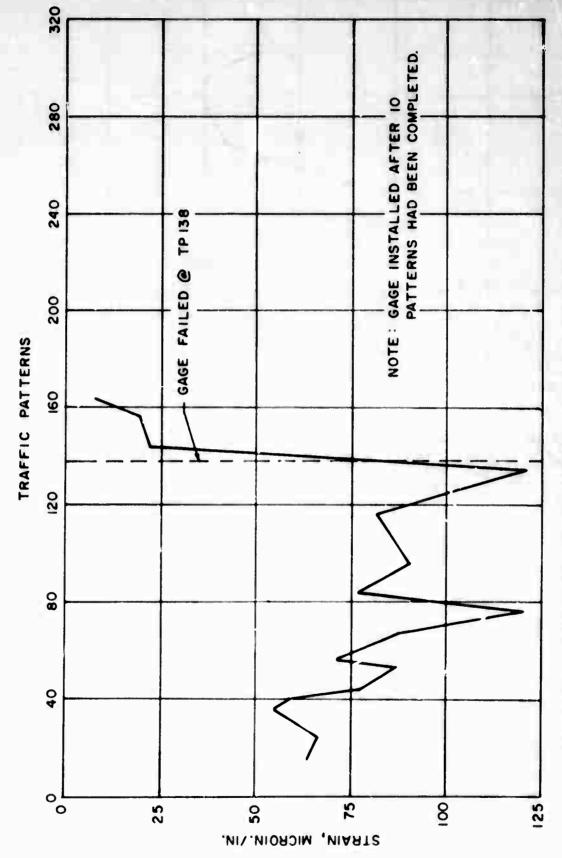
Strair Versus 12-Wheel Traffic Level, Gage 3SCL, Offset No. 1, SW Slab, Item 3, Rigid Pavement Test Section Figure 98.



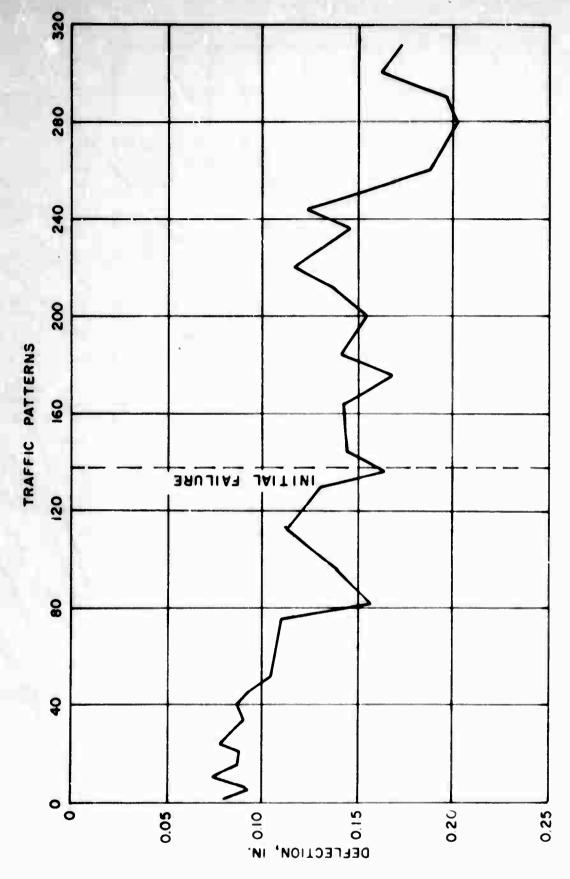
Deflection Versus 12-Wheel Traffic Level, Gage 3DC, Offset No. 1, Sw Slab, Item 3, Rigid Pavement Test Section Figure 99.



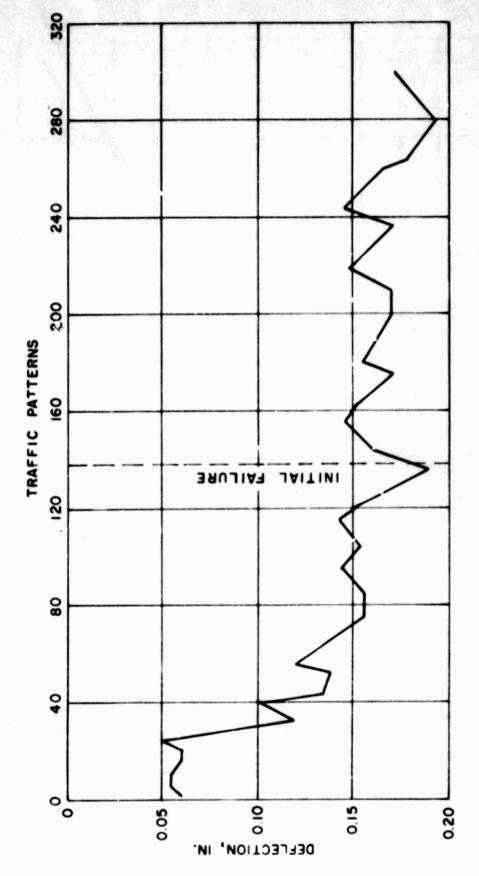
Strain Versus 12-Wheel Traffic Level, Gage 3SSWJT, Offset No. 3, SW Slab, Item 3, Rigid Pavement Test Section Figure 100.



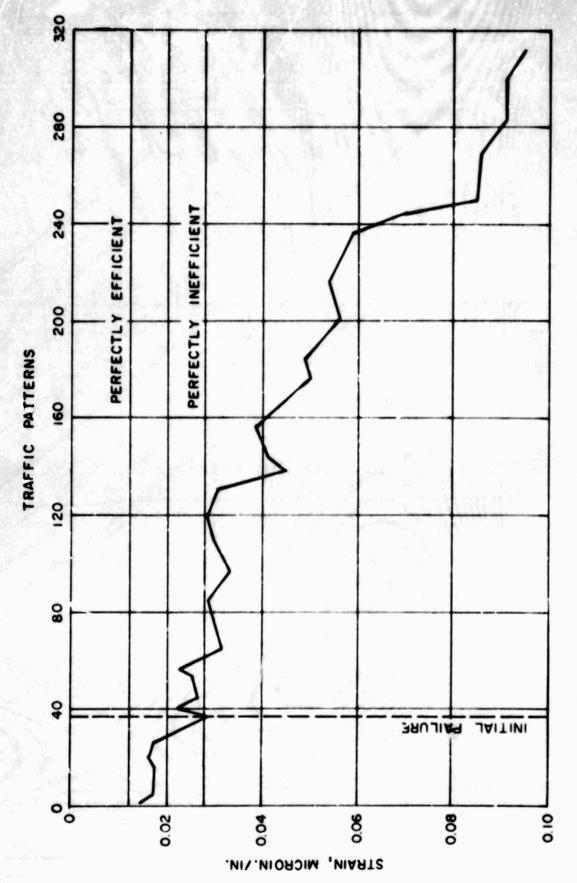
Strain Versus 12-Wheel Traffic Level, Gage 3SSJL, Offset No. 3, SE Slab, Item 3, Rigid Favement Test Section Figure 101.



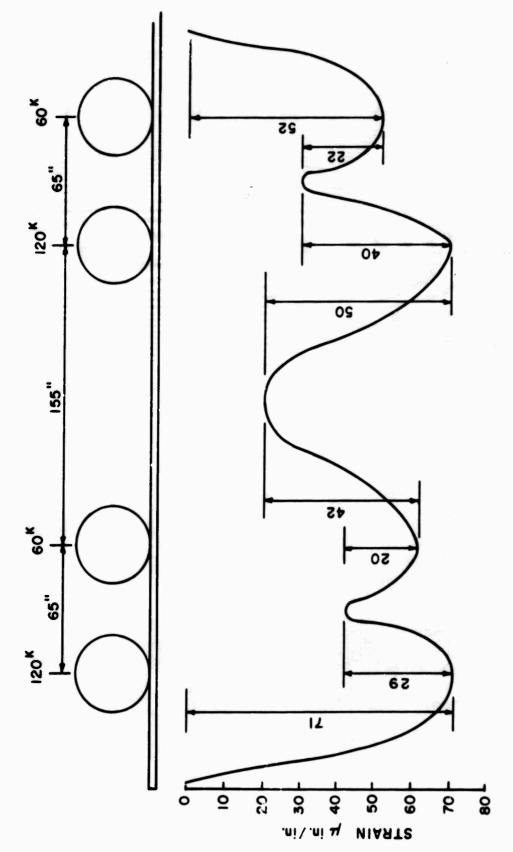
Deflection Versus 12-Wheel Traffic Level, Gage 3DEJT, Offset No. 5, T. Slab, Item 3, Rigid Pavement Test Section Figure 102.



Deflection Versus 12-Wheel Traffic Level, Gage 3DWJT, Offset No. 5, SW Slab, Item 3, Rigid Favement Test Section Figure 103.



Deflection Versus 12-Wheel Traffic Level, Gage 33FD, Offset No. 5, SE Slab, Item 3, Rigid Pavement Test Section Figure 104.



Typical Strain Trace Under 12-Wheel Traffic Showing Strain Profile for One Pass.

Note: Gage 2SCL, Test Item 2; Surface Strain Gage; Longitudinal Direction; Gear on Traffic Line 2; Thickness = 12.1 in.; k = 78 pci; Concrete Flexural Strength = 800 psi. Outside Wheel of Gear is Fassing Gage at a Distance of 16 ft Figure 105.

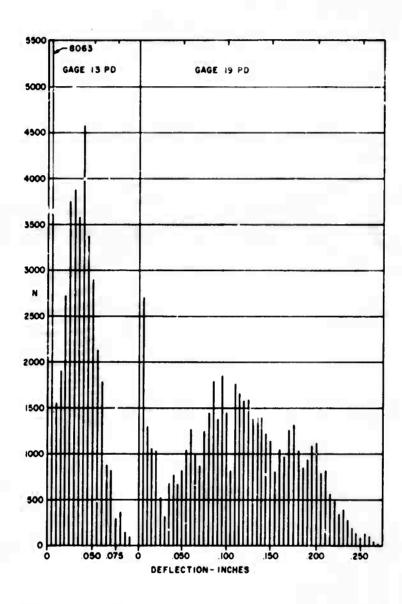


Figure 106. Histograms for Deflection Excursions Under 12-Wheel Traffic, Item 1, Rigid Pavement Test Section

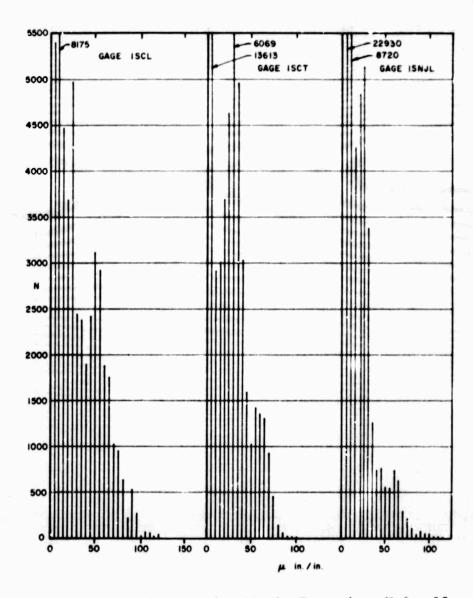


Figure 107. Histograms for Strain Excursions Under 12-Wheel Traffic, Item 1, Rigid Pavement Test Section

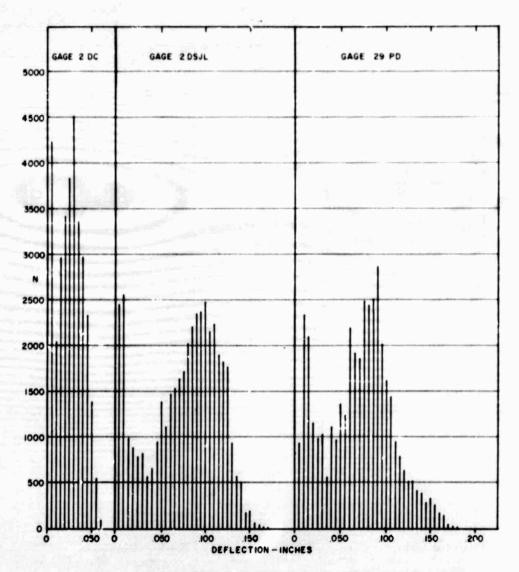


Figure 108. Histograms for Deflection Excursions Under 12-Wheel Traffic, Item 2, Rigid Pavement Test Section

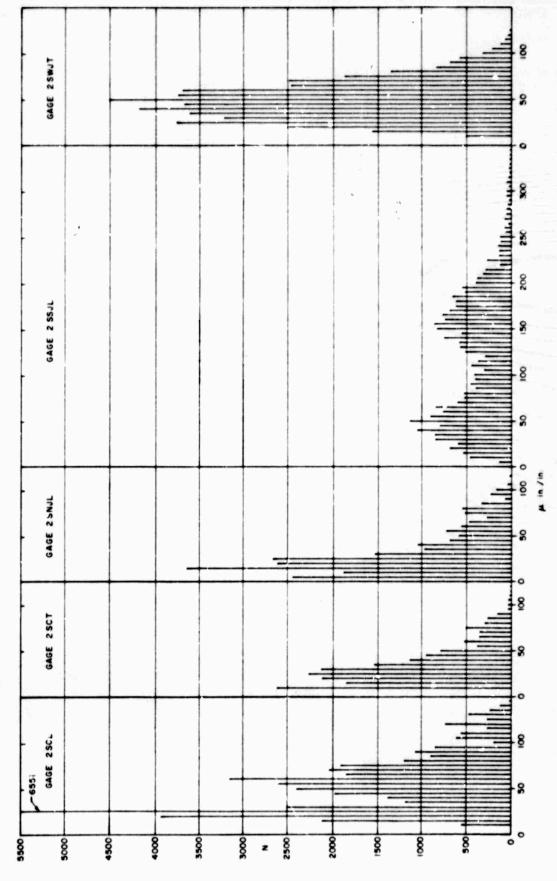
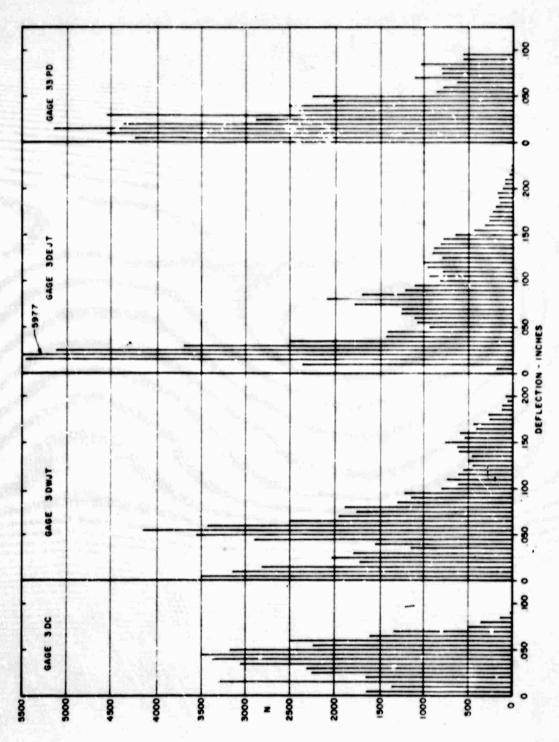


Figure 109. Histograms for Strain Excursions Under 12-Wheel Traffic, Item 2, Rigid Pavement Test Section



Histograms for Deflection Excursions Under 12-Wheel Traffic, Item 3, Rigid Pavement Test Section Figure 110.

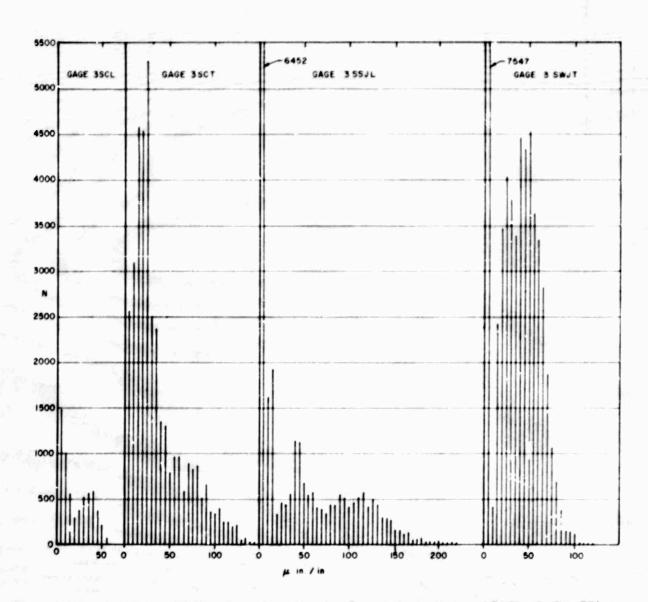
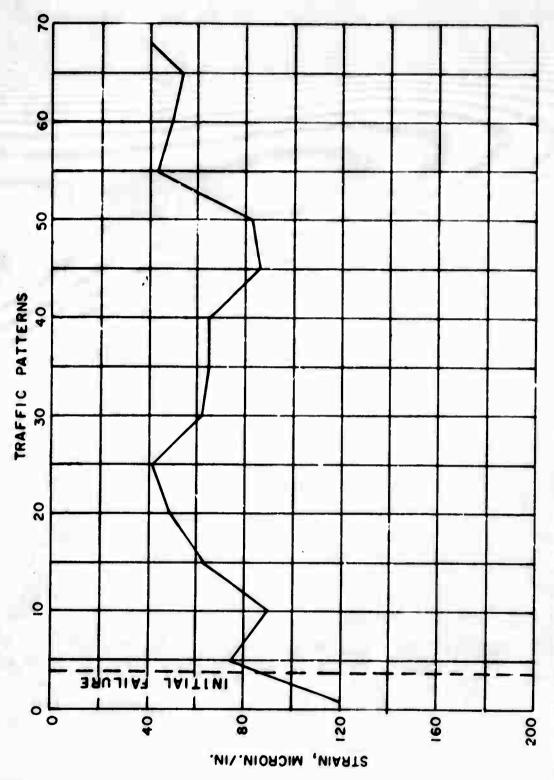
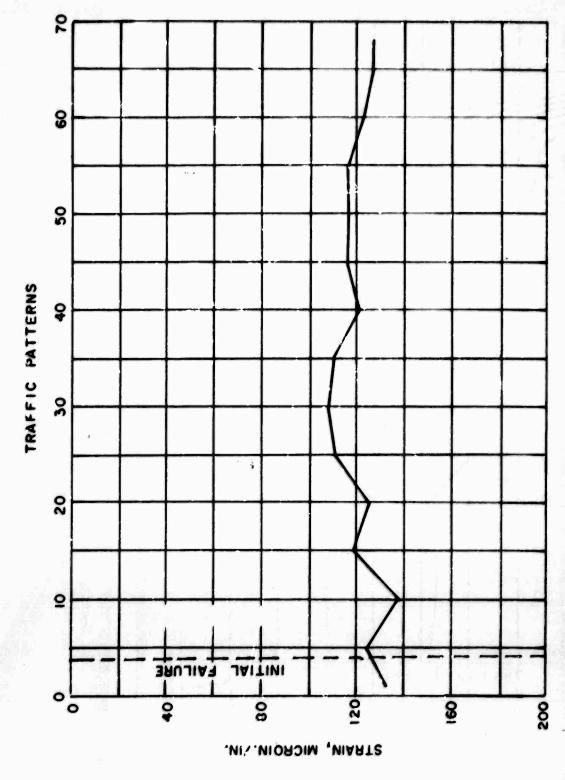


Figure 111. Histograms for Strein Excursions Under 12-Wheel Traffic, Item 3, Rigid Pavement Test Section



Strain Versus Twin-Tandem Traffic Level, Gage 2NSCT, NE Slab, Item 2, Rigid Pavement Test Section Figure 112.



Strain Versus Twin-Tandem Traffic Level, Gage 2NSCL, NE Slab, Item 2, Rigid Pavement Test Section Figure 113.

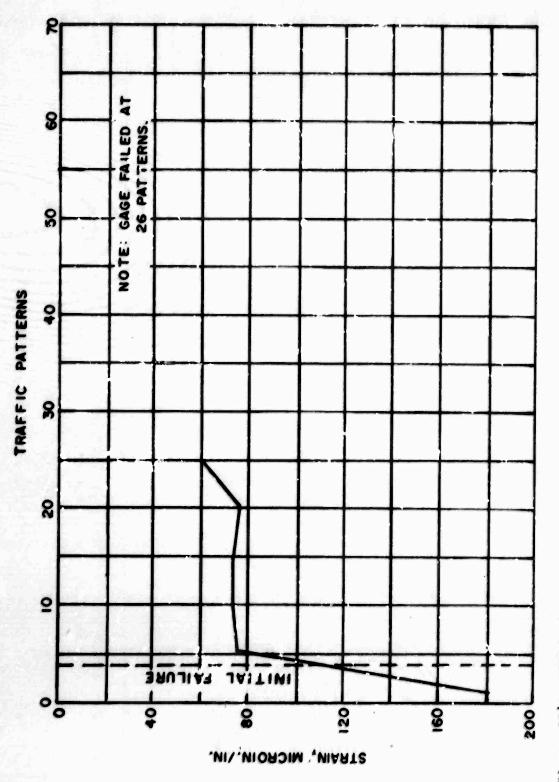
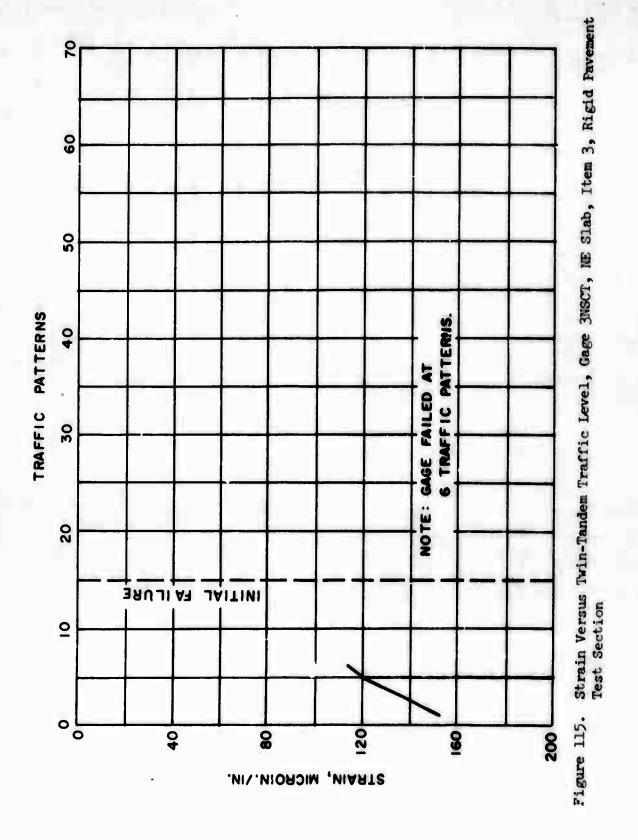
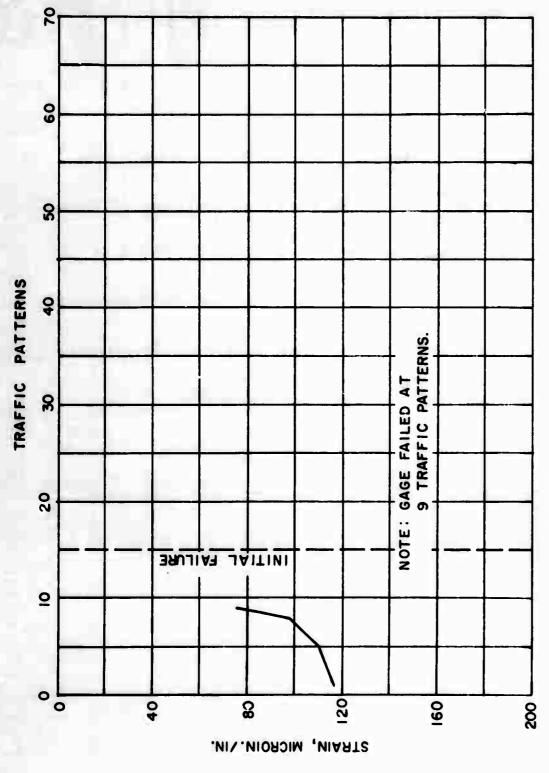


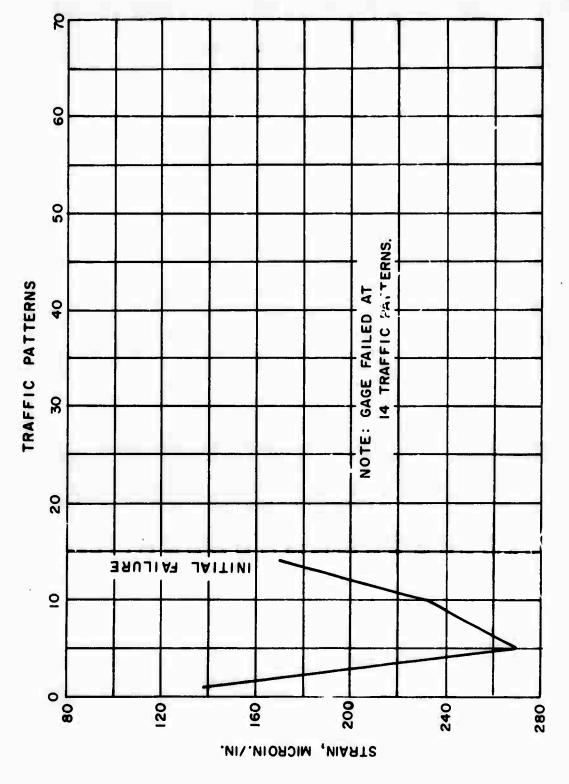
Figure 114. Strain Versus Twin-Tandem Traffic Level, Gage 2NSWJT, NW Slab, Item 2, Rigid Pavement Test Section



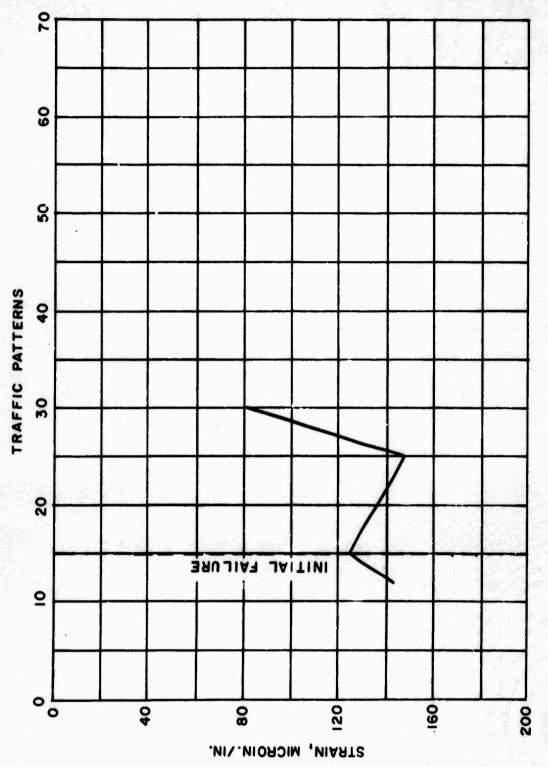
187



Strain Versus Twin-Tandem Traffic Level, Gage 3NSCL, NE Slab, Item 3, Rigid Pavement Test Section Figure 116.



Strain Versus Twin-Tandem Traffic Level, Gage 3NSWJT, NW Slab, Item 3, Rigid Pavement Test Section Figure 117.



Strain Versus Twin-Tandem Traffic Level, Gage 3NSSEJT, NE Slab, Item 3, Rigid Pavement Test Section Figure 118.

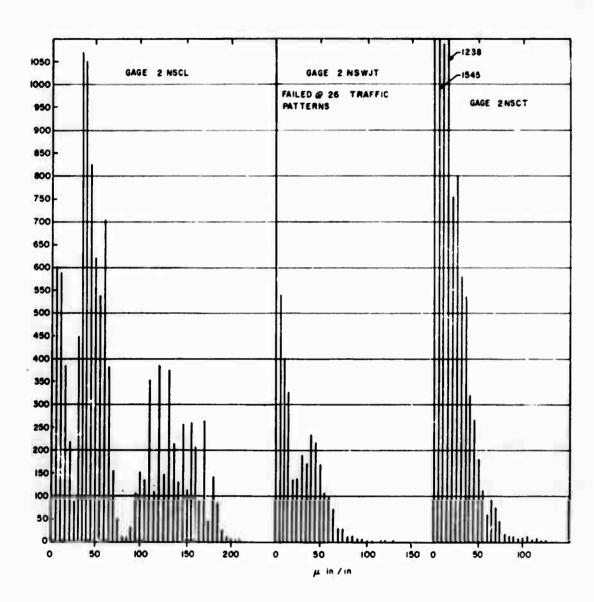
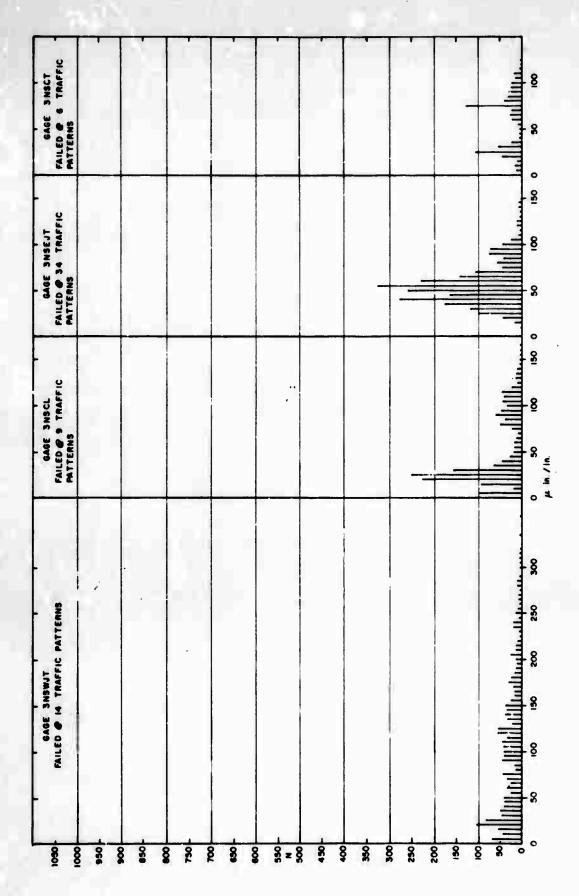


Figure 119. Histograms for Strain Excursions Under Twin-Tandem Traffic, Item 2, Rigid Pavement Test Section



Histograms for Strain Excursions Under Twin-Tanden Traffic, Item 3, Rigid Pavement Test Section Figure 120.

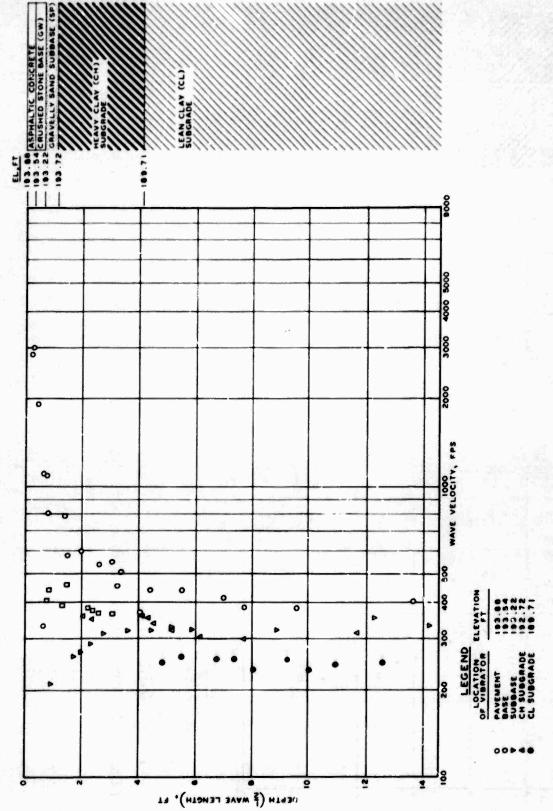
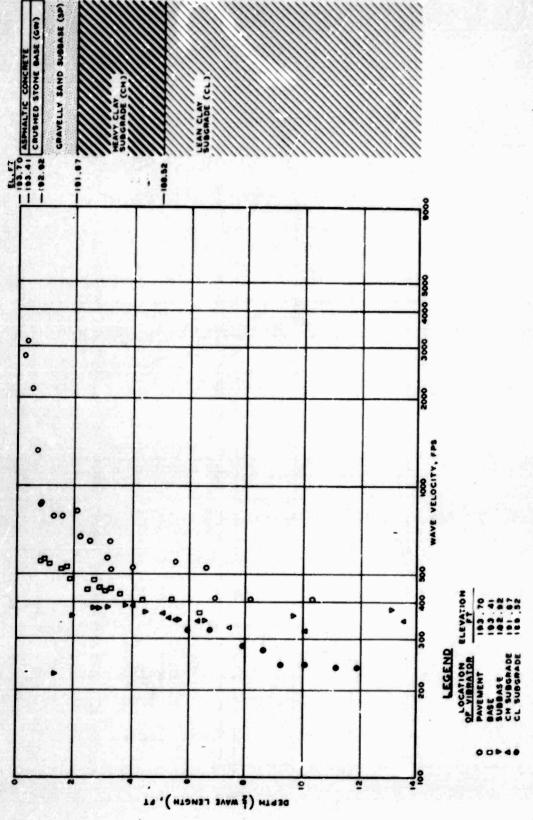
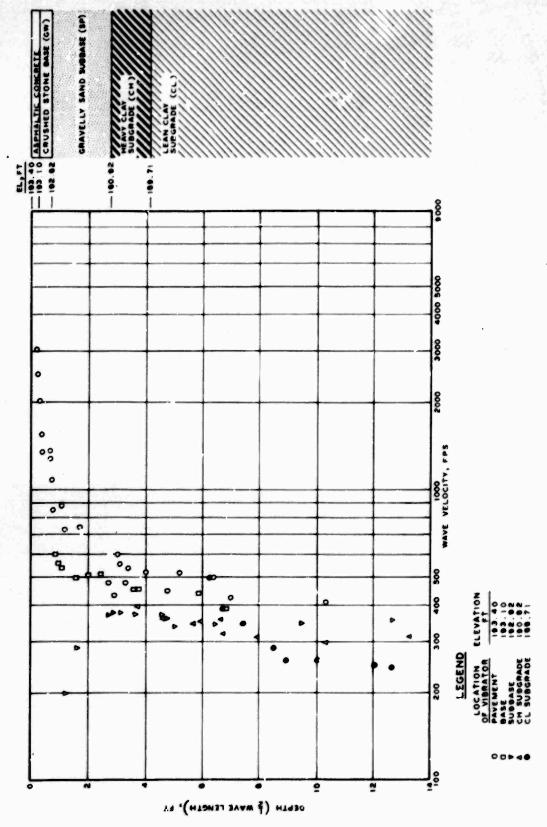


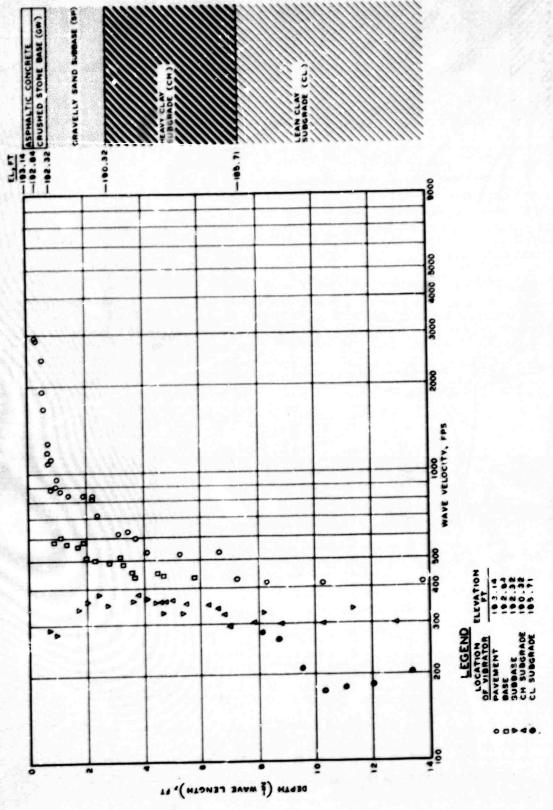
Figure 121. Wave Velocity Versus Depth for Flexible Pavement Lane 1, Item 1, As Constructed



Wave Velocity Versus Depth for Flexible Pavement Lane 1, Item 2, As Constructed Figure 122.



Wave Velocity Versus Depth for Flexible Pavement Lane 1, Item 3, As Constructed Figure 123.



Wave Velocity Versus Depth for Flexible Pavement Lane 1, Item 4, As Constructed Figure 124.

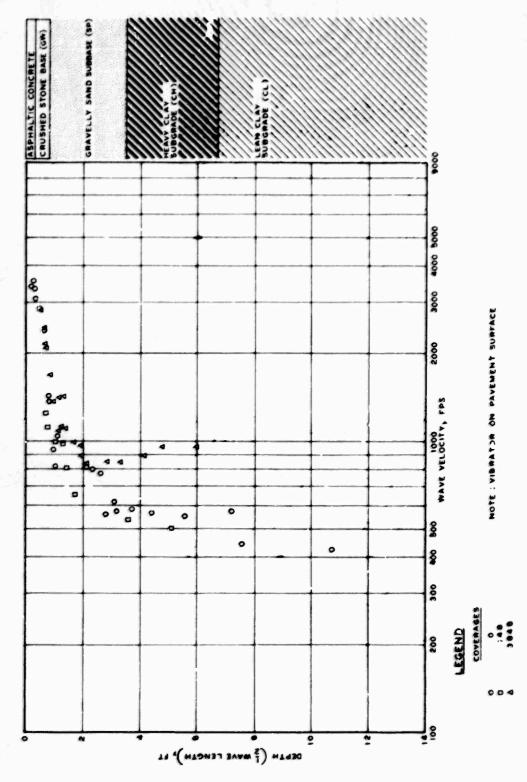


Figure 125. Wave Velocity Versus Depth for Flexible Pavement Lane 1, Item 5, As Constructed

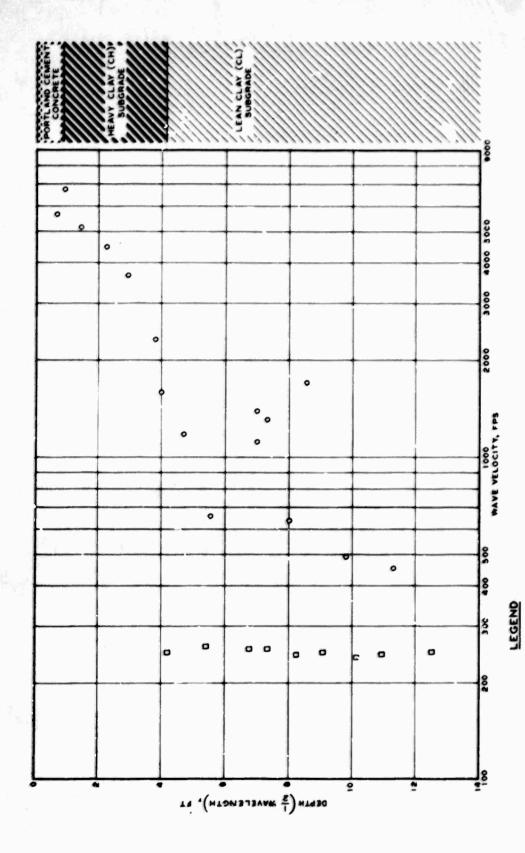
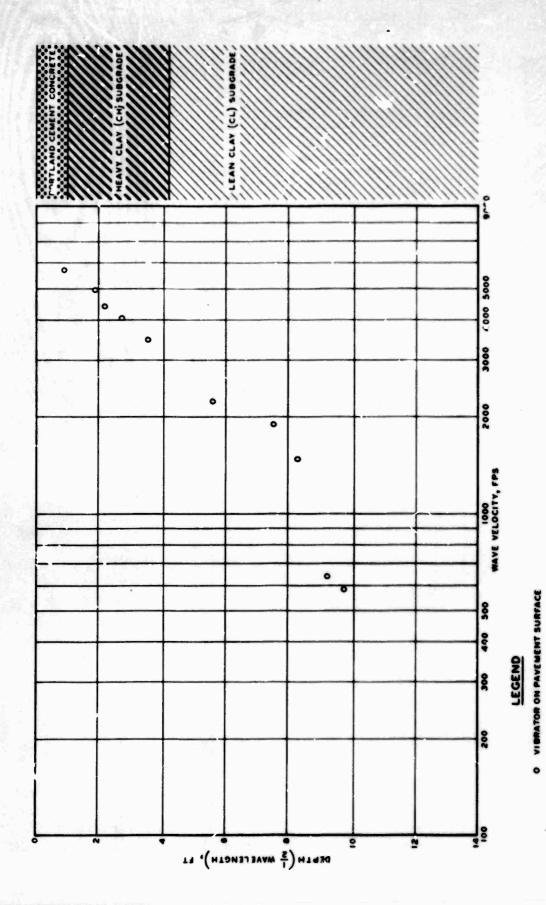


Figure 126. Wave Velocity Versus Depth for Rigid Pavement Item 1, South Lane, As Constructed

O VIBRATOR ON PAVEMENT SURFACE, O COVERAGES D VIBRATOR ON CL SUBGRADE



Wave Velocity Versus Depth for Rigid Pavement Item 2, South Lane, As Constructed Figure 127.

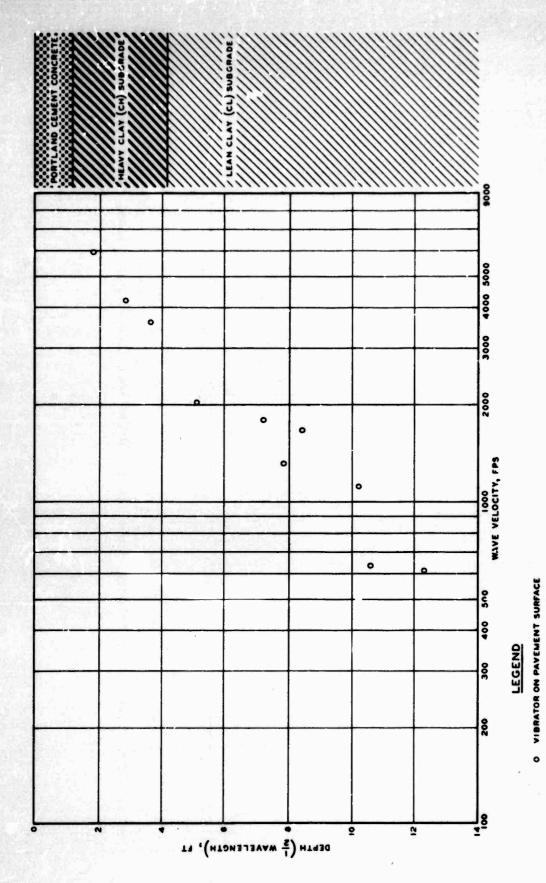


Figure 128. Wave Velocity Versus Depth for Rigid Pavement Item 3, South Lane, As Constructed

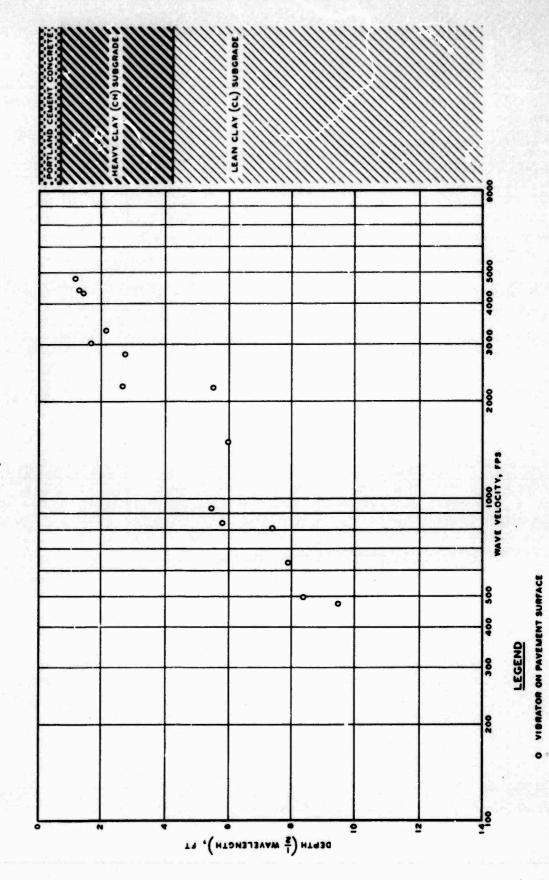


Figure 129. Wave Velocity Versus Depth for Rigid Pavement Item 4, South Lane, As Constructed

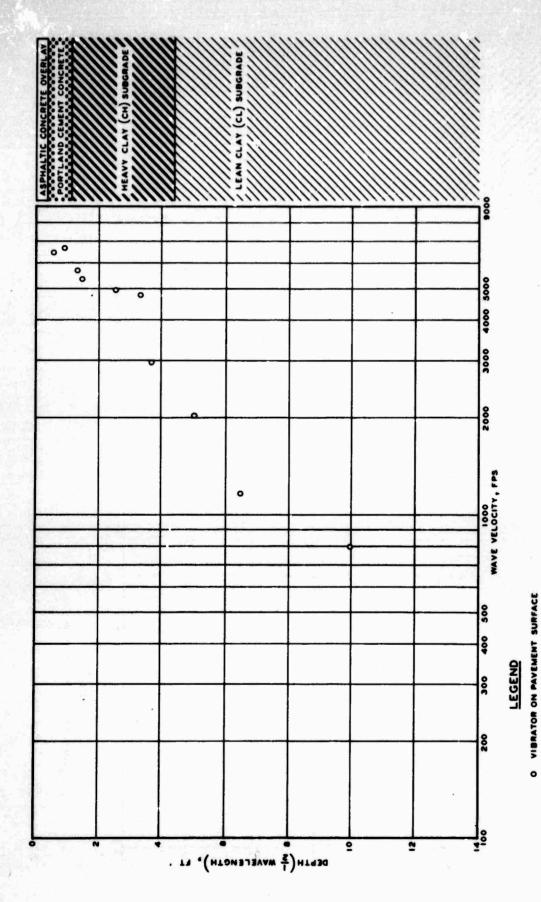


Figure 130. Wave Velocity Versus Depth for Rigid Pavement with Nonrigid Overlay, Item 1, North Lane, As Constructed

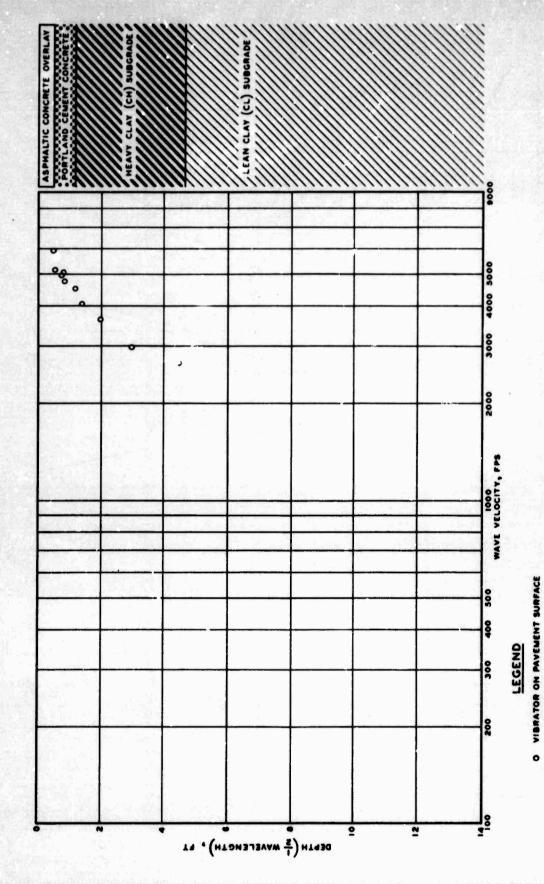


Figure 131. Wave Velucity Versus Depth for Rigid Pavement with Nonrigid Overlay, Item 4, North Lane, As Constructed

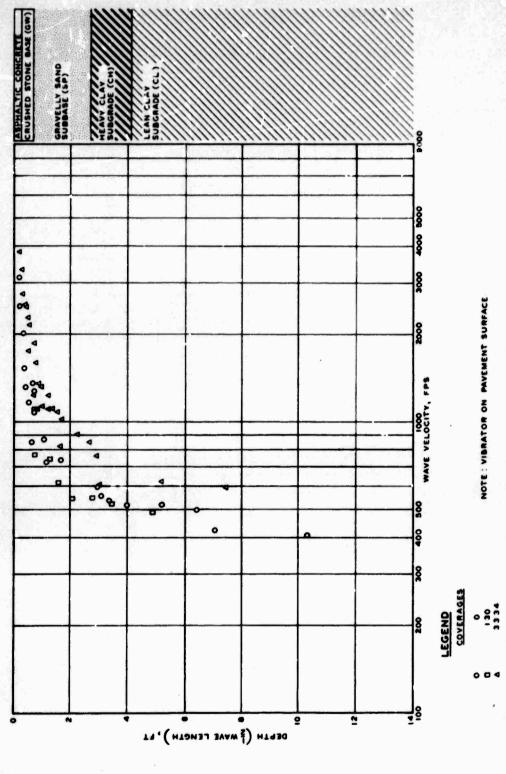


Figure 132. Wave Velocity Versus Depth for Flexible Pavement Lane 1, Item 3, During Traffic Tests

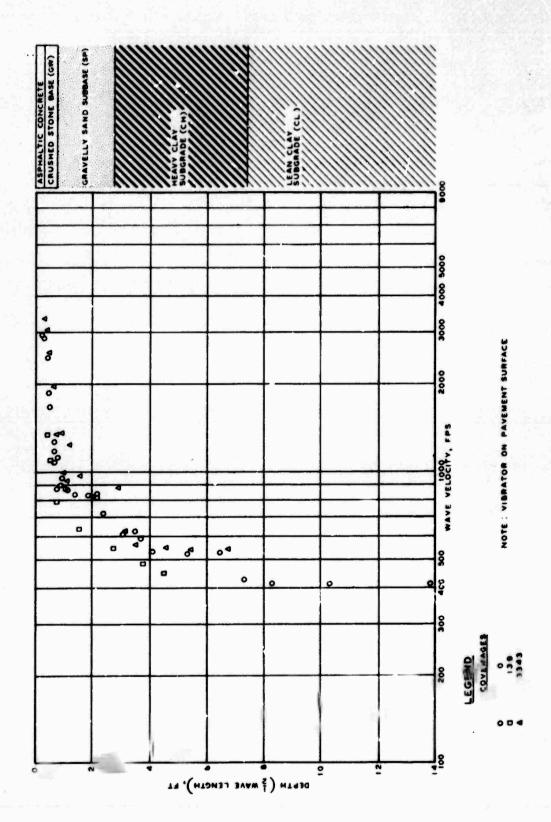


Figure 133. Wave Jelocity Versus Depth for Flexible Pavement Lane 1, Item 4, During Traffic Tests

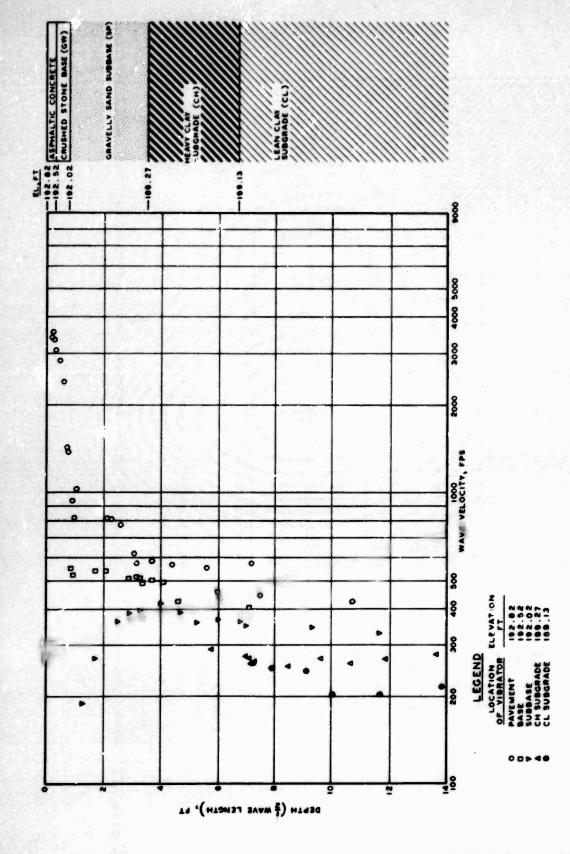


Figure 134. Wave Velocity Versus Depth for Flexible Pavement Lane 1, Item 5, During Traffic Tests

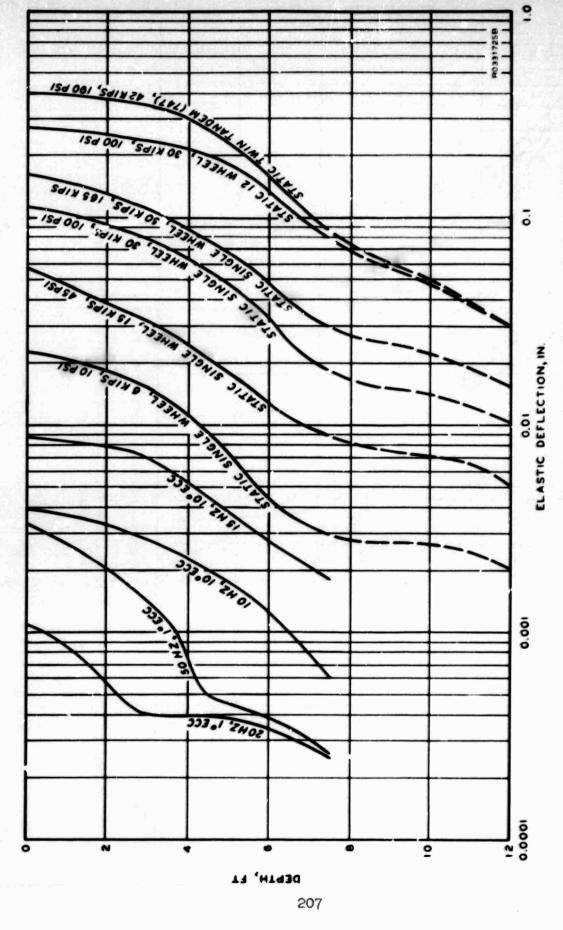


Figure 135. Deflection Versus Depth for Static and Vibratory Loading of Flexible Pavement, Lane 1, Item 4

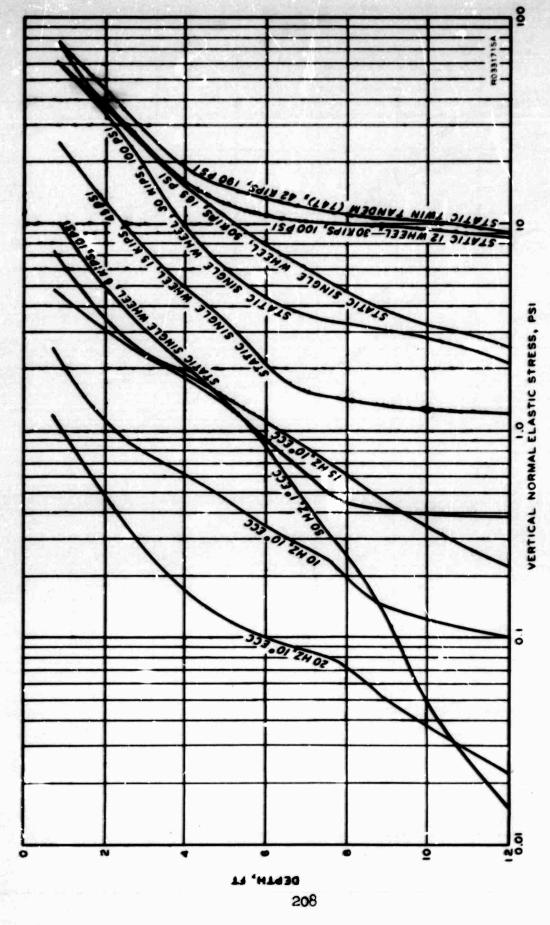


Figure 136. Stream Versus Depth for Static and Vibratory Loading of Flexible Pavement, Lane 1, Item 4

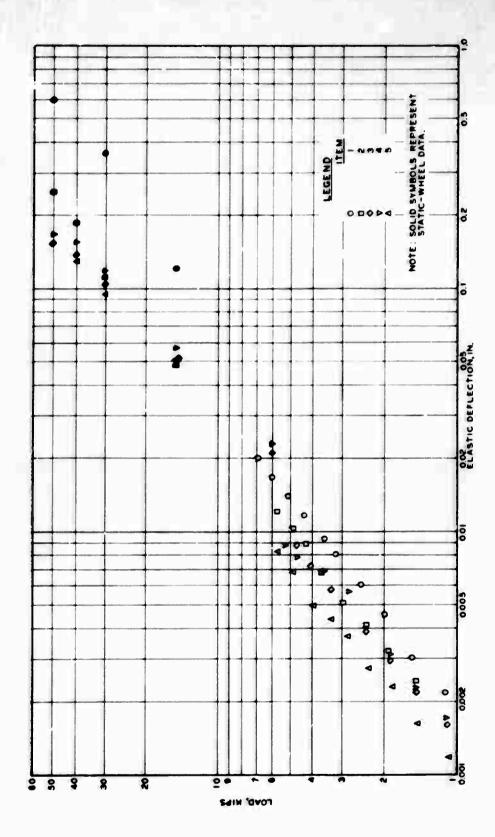


Figure 137. Deflection Versus Load for Flexible Pavement Lane 1, As Constructed

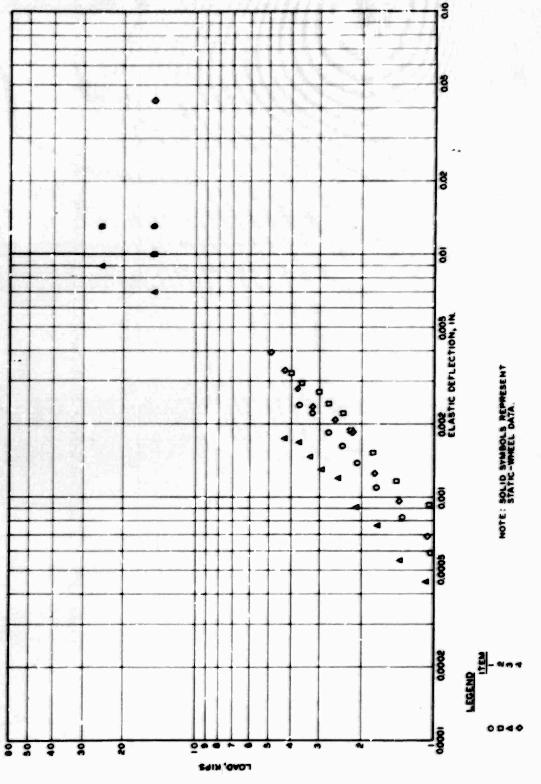
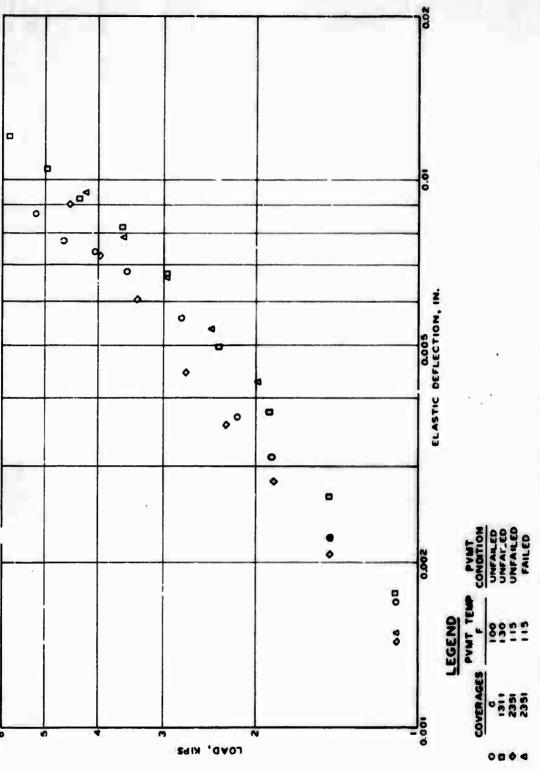
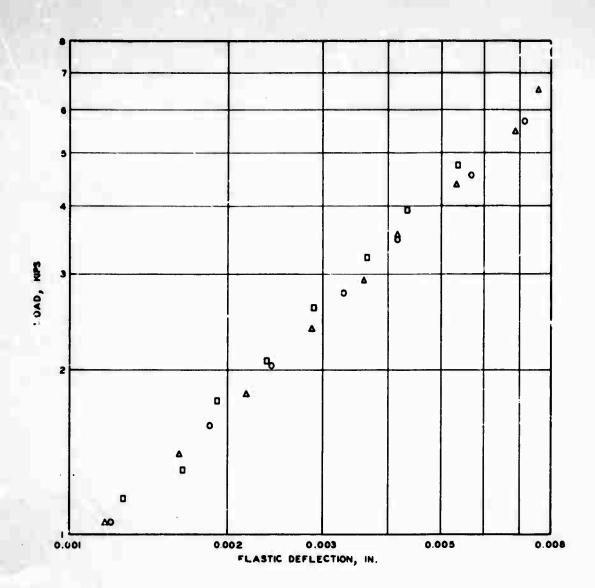


Figure 138. Deflection versus Load for Rigid Pavement, South Lane, As Constructed

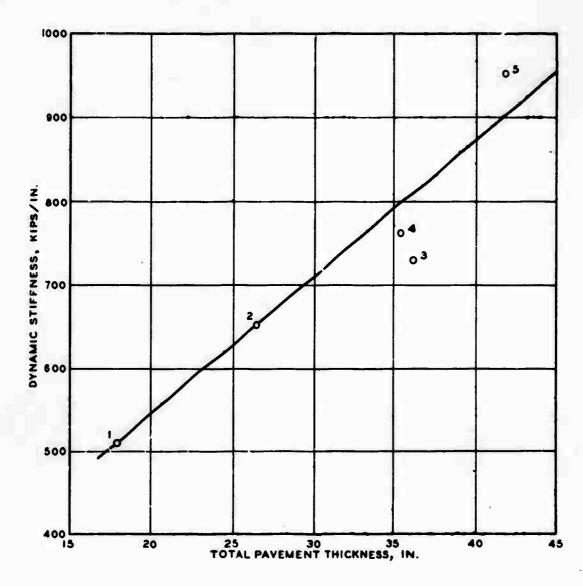


re 139. Temperature Effects on Deflection Versus Load for Flexible Pavement, Lane 1, Item 4



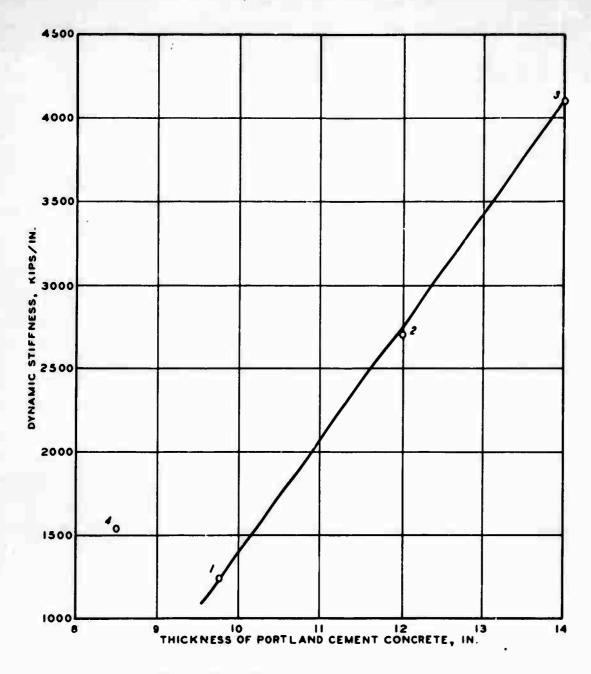
	LEGEND
	ECCENTRIC SETTING, DEG
0	2
0	5
Α	10

Figure 140. Effect of Vibratory Load on Deflection Versus Load for North Edge of Flexible Pavement, Item 2



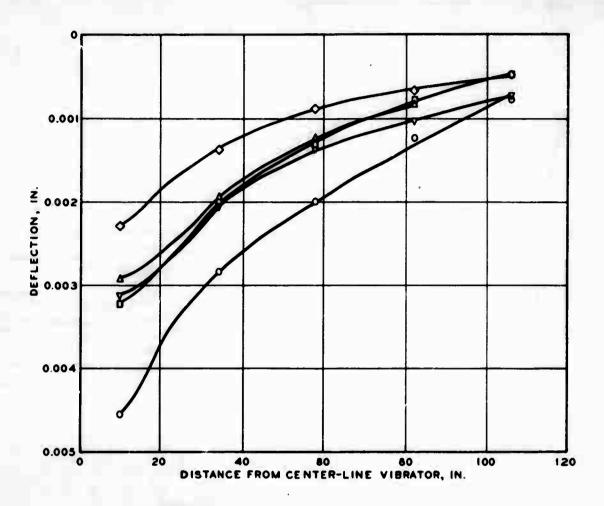
NOTE: NUMBERS BESIDE SYMBOLS ARE ITEM NUMBERS.

Figure 141. Dynamic Stiffness Versus Total Pavement Thickness for Flexible Pavement, Lane 1



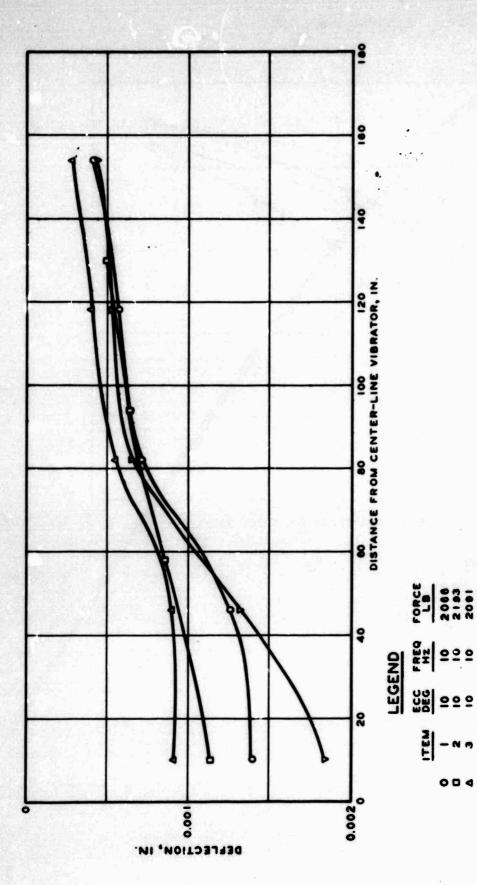
NOTE: NUMBERS BESIDE SYMBOLS ARE ITEM NUMBERS.

Figure 142. Dynamic Stiffness Versus Pavement Thickness for Rigid Pavement, South Lane



		LEG	END	
	ITEM	ECC	FREQ	FORCE
0		10	•	1994
0	2	10	9	1903
Δ	3	10	9	1883
7	4	10	9	1877
0	5	10	9:	1847

Figure 143. Vibratory Deflection Basin, Flexible Pavement Lane 1



Vibratory Deflection Basin, Rigid Pavement South Lane

APPENDIX A: FLEXIBLE PAVEMENT INSTRUMENTATION MEASUREMENTS

SECTION I

INTRODUCTION

This appendix presents a listing of a portion of the static and the dynamic (slowly moving) load instrumentation data collected under the various loadings and wheel assemblies of the multiple-wheel heavy gear load (MWHGL) tests in items 3 and 4 of the flexible pavement test section. These data were reduced from the original records in order to select the values of maximum response to be used in the analysis of the behavior of the test section. Stresses and deflections up are static and dynamic loads are presented in their initial reduced form with no corrections applied. For the case of static load stress and deflection measurements, selected data were further reduced and analyzed and are presented in the main text of this report. The values of stress and deflection under dynamic loads shown in tabular form in this appendix are the values used in the analysis of data as shown in the main text. This appendix discusses the reduction and the consistency of the data and the loss of instrumentation.

Listings of pore pressure data, temperature data, and pavement strain data are not presented in tabular form; however, the consistency of these data is discussed in this appendix and under analysis in the main text. These data are not presented because no significant pore pressures developed, the temperature effects on measured stresses and deflections were inconclusive, and the pavement strain data were considered to be unreliable.

1. NUMBER AND TYPE OF MEASUREMENTS

Table A-1 gives the approximate number of static readings taken for each load and wheel configuration tested. The total number of static load readings, including the static load tests run during traffic tests, was approximately 50,000 readings for both items. Many times this quantity exists on oscillographic recordings of the dynamic load tests run with each load and wheel configuration. These 50,000 static readings represent only raw data, that is, data in units of volts and microinches per inch. In the reduction of data, which will be discussed in the next section, each of the 50,000 readings

Table A-1

MWHGL Static and Dynamic Instrumentation Loadings of

Flexible Pavement Test Section

Test Loading No.	Loading	Date Collection of Readings Completed	Static Loading Grid Pattern	Number of Static Readings
1	Preliminary tests	25 Apr 69	*	2,660
2	15 kips, 12 wheels, 45 psi	30 Apr 69	Partial	5,320
3	15 kips, SWL, 45 psi	6 June 69	Partial	2,660
4	30 kips, 12 wheels, 100 psi	19 June 69	Complete	5,360
. 5	30 kips, SWL, 100 psi	26 June 69	Complete	4,280
6	30 kips, 6 wheels, 100 psi	2 July 69	Partial	5,320
7	Prime mover (12 wheels)	9 July 69	*	1,660
8	30 kips, twin tandem, 100 psi	15 July 69	Complete	8,640
9	30 kips, twin tandem, 150 psi	18 July 69	Partial	2,760
10	Prime mover (twin tandem)	23 July 69	*	1,660
10a	30 kips, SWL, 100 psi (speed test)			
11**	6 kips, SWL, 10 psi	25 July 69	Partial	2,660
11a	30 kips, 12 wheel, 100 psi		*	
12	50 kips, SWL, 165 psi	30 Oct 69	Partial	2,660
13	60 kips, twin tandem, 225 psi	6 Nov 69	Partial	2,760
			Total	48,400

Note: Test loading Nos. 1-10 represent both static and dynamic load tests.

Test No. 10a represents only dynamic loading, and test Nos. 11-13 represent only static loadings.

^{*} Selected locations.

^{**} Performed in conjunction with another project.

was converted to units of displacement or pressure; and for each reading, two values of change were calculated. This means approximately 100,000 values of usable static load data are a matter of record. The raw data and also the reduced data contain, in addition to the load readings, no-load readings taken before, after, and between tests. Also collected were support data of pavement temperatures, air temperatures, and barometric pressure. The data consist of the following five basic types:

- a. Soil and pore pressure data.
- b. Barometric pressure readings. Continuous recordings were made but were only read simultaneous with and for the correction of pore pressure readings.
- c. Deflection data that included reference rod readings.
- d. Asphalt pavement strain data.
- e. Temperature readings ambient, pavement surface, and pavement/base interface

A rough approximation of the percentage of each of the basic types of data is shown in table A-2.

Table A-2

Basic Data Types for Static Loadings

	Approximate Percentage of	Number of
Type of Data	Total Amount	Values
Soil and pore pressure	48.9	49,000
Barometric pressure	0.2*	200
Deflection	41.9	42,000
Pavement strain	8.0**	8,000
Temperature	1.0	1,000

^{*} Additional data available from continuous recordings.

The same basic types of data exist on oscillograph records for the dynamic load tests, and the above percentages of each type apply also to the dynamic load test data; however, the total number of usable values is much greater.

^{**} These data are not usable, as will be explained later.

2. PRESENTATION OF DATA

All of the static test measurements of deflections, stresses, and strains were reduced and tabulated; however, only the data for static loads of 30,000 and 60,000 lb per wheel are presented in this appendix due to the time factor as well as the space limitations considered reasonable. Because of time limitations, only a minimum of the dynamic test data has been taken from the oscillograph records, reduced, and tabulated; this includes deflection and soil pressure measurements for the 30,000-lb-per-wheel assembly load points on the four instrumented rows of items 3 and 4. This was considered to be the minimum information required for analysis. Table A-3 describes the static and dynamic load test conditions for the data presented in tables A-4 through A-21.

Table A-3
Description of Loading Conditions

Assembly	Total Load kips	Tire Inflation Pressure, psi	Static Tests	Dynamic Tests
Single wheel	30	100	x	x
Twin tandem	120	100	x	x
		150	x	
	240	225	x	••
6 wheel	180	100	x	
12 wheel	360	100	x	ж

For static load data (tables A-4 through A-15), two values, total and rebound, were determined for vertical pressure and vertical deflection. The total values represent the difference between readings of the loaded condition and the initial no-load condition, whereas the rebound values represent the difference between readings of the loaded condition and the final, or after-load, no-load condition. Each table includes data for only one item (3 or 4), and in the top half of the table, all of the readings from soil pressure cells in that item are tabulated for both total and rebound values. The lower half of each table is a tabulation of the total and rebound values for all of the deflection gages in that item. On the left side of each table, three columns of information are given. This information is to be used in conjunction with figure Al and figure A2 or A3, as appropriate.

Table A-4.
Multiple-Wheel Heavy Gear Load Flexible Pavement Test, Static Instrumentation Loading Data
Item 3; Load Condition: 30 kips per Wheel, Single Wheel, 100 psi

1						Tot	7		121		Tod Values II That ist	14 91 1110	at indicates cell	6118		Febol	pur	l	l		
 Point	tion	4	20	2	a,	2	P6	P7	8	4.0	10	4	2	a.	a 3	P ₅ F	P6	P7	P _B	8	10
-4	*	0.28	0.23	0.37	0.32	0.34	1.02	0.12	91.0	00.00	92.0	-0.65	39.0	0.37	0.32	-1.20	0.81	0.00	44.0	8.32	-0.10
	m	0.37	0.23	64.0	0.45	0.25	0.92	0.12	0.16	0.00	92.0	-0.56	0.68	0.49	0.42	-1.29	17.0	0.00	0.44	8.32	-0.10
	U	0.74	0.45	0.61	0.53	0.08	0.82	0.24	0.16	0.00	0.86	-0.19	0.00	0.61	0.53	-1.46	19.0	0.12	0.44	8.32	0.00
	a	1.29	0.68	0.73	0.53	0.00	0.72	0.24	0.39	0.00	0.95	96.0	1.13	0.73	-53	-1.16	0.51	0.12	0.52	8.32	0.00
	(m)	2.12	0.91	0.85	69.0	0.08	0.82	0.2	0.35	0.00	0.75	1.19	1.36	0.85	0.63	-1.46	0.61	0.12	0.61	8.32	-0.10
	ja,	5.17	1.58	1.10	0.84	0.34	1.00	0.36	44.0	0.00	0.86	4.24	2.03	1.10	0.84	-1.20	0.8.	0.24	0.70	8.32	0.00
	O	7.75	5.03	1.22	0.84	0.77	1.05	09.0	0.61	0.00	5.0	6.82	2.48	1.22	0.84	-0.77	0.81	0.48	0.87	8.33	0.0
	br:	4.89	1,36	1.46	1.05	6.35	1.43	0.95	1.03	0.00	0.95	3.95	1.61	1.46	8	4.81	1.22	0.83	1.31	9	0.00
	н	2.40	0.45	1.46	0.95	15.29	1.63	1.55	1.31	-0.18	0.9	1.47	0.00	1.46	0.9	13.75	1.42	1.45	1.57	6.14	0.0
	47	1.48	-0.11	1.22	0.84	7.13	1.05	1.90	1.49	0.69	0.9	0.55	0.34	1.22	0.84	5.59	0.81	1.78	1.3	9.0	0.00
	×	1:11	-0.45	16.0	0.63	2.40	0.41	1.55	1.22	54.42	94.0	0.18	0.00	0.97	0.63	0.8	0.20	1.43	1.48	62.74	-0.10
	ü	1.11	-0.45	0.73	0.42	1.89	0.41	1.31	1.05	94-9-	0.76	0.18	0.00	0.73	0.42	0.35	0.50	1.19	1.31	1.56	-0.10
	×	0.93	-0.15	0.73	0.42	1.54	D.0	1.07	61.0	-8.49	0.86	0.00	0.00	0.73	0.42	0.00	0.10	8.0	3.3	-0.17	0.00
	10.	0.93	-0.45	64.0	₽.°	1.28	0.41	0.71	0.35	-8.32	0.0	0.00	0.00	64.0	0.21	-0.26	0.20	0.59	19.0	0.00	0.0
						1		Ve	rtical D	Vertical Deflection,	n. in.	in., at indicated Gages	ted Gage	40					ç		
		6	c	c	d	4	6	4	-	-		6	6	-	1	PEDOCANO	6	6	6	6	
		1	2	7	12	52	9	7	80	0		4	25		57	3	92	2,	8	0	
г	<	0.002	0.001	•0.001	0.005	00000	0000	-0.003	00000	0.00		0.007	0.002	0.000	0.000	-0.0C	0.000	0000	0.000	0.000	
	m	0.005	0.002	-0.001	0.005	00000	0.000	-0.003	0.000	0.000		0.010	0.003	0.000	0.000	-0.001	0000	0.000	0.000	0.000	
	ņ	0.010	0.002	0.000	0.002	100.00	0.000	-0.003	0.300	0.000		0.015	0.003	0.001	0.000	0.000	0.000	0.000	0.000	00000	
۰	Q	0.013	0.003	0.001	0.002	100.0	0.000	-0.002	0.000	0.000		0.018	0.00	0.002	0.000	0.000	0.000	0.001	0.000	0.000	
	(m)	0.015	0.003	0.001	0.002	+0.001	000.3	-0.003	0.000	0.000		0.020	0.170	0.002	0.000	0.000	0.000	0.38	0.000	0.000	
	lin.	0.012	0.002	0.002	0.003	-0.001	0.000	-0.002	0.000	0.000		0.017	0.03	0.703	0.001	0.00	0.000	0.001	0.000	0.000	
	Ø	0.007	7.002	0.005	0.003	100.00	0.000	-0.00	0.000	0.000		0.012	0.003	0.003	0.001	0.000	0.000	0.001	0.000	0.000	
	æ	0.001	0.001	0.02	0.00	-0.002	0.000	-0.05	0.000	00000		0.005	0.002	0.003	0.000	0.001	0.000	0.001	0.000	0.000	
	н	-0.001	0.000	0.001	0.004	0.00	0.000	-0.303	0.000	0.001		0.00	0.001	0.002	0.002	0.003	0.000	0.000	0.000	0.001	
	•9	-0.003	0.000	0.000	0.004	0.005	0.000	-0.003	0.000	0,001		0.002	0.001	0.001	0.002	0.004	0.000	0.000	0.000	0.001	
	×	-0.00th	-0.001	-0.001	0.003	0.005	0.000	-0.0c3	0.000	0.001		0.001	0.00	0.000	0.001	0.005	0.000	0.000	0.000	0.00	
	-1	100.0	-0.001	-0.001	0.003	0.000	0.000	-0.003	0.000	0.001		0.001	0.000	0,000	0.001	0.005	0.000	0.000	0.000	0.00	
	30	-0.00	-0.001	-0.001	0.003	0.005	0,000	-0.003	0.000	0.001		0.001	0.000	0.300	0.031	0.00	0.000	-0.000	0.000	0.00	
	je.	-0.005	-0.001	-0.001	0.002	0.00	0.000	-0.004	0.000	0.001		0.000	0.000	0.000	0.000	0.003	0.000	-0.003	0.000	0.001	

(1 of 11 sheets)

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	0.17 -0.19 0.70 -0.28 1.22 -0.19 1.74 -0.37 1.56 -0.37	200.0 000.0 000.0
Π	0.41 0.68 1.33 1.33 1.068 1.068	0.000.000.000.000.000.000.0000.0000.0000
lli.		
	1.0 2.0 1.0 1.0 2.0 2.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3	2 0.000 0.00
NO.	1.01 2.82 1.13 0.45 0.45	20.00.00.00 80.00.00.00
2 a.	0.00 0.00 0.00 0.00	0.001 0.001 0.000 0.000
a [™]	0.148 0.83 1.31 1.66 1.66	100.0 200.0 200.0 200.0
1110 L	1.38 9.48 9.88 9.98	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
P 2	0.49	0.004 0.003 0.003 0.000
T Linds	1.75 5.43 3.31 1.29 0.46	1.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000
10	0.75 0.75 0.57 0.57 0.38	the state of the s
٥	0.35 0.36 1.40 1.92 2.10	1 pc
8	0.10 0.31 1.02 1.73 0.31	PB P
2	0.64 1.06 1.15 0.95 0.53	Ver 0.000 0.001 0.001 0.001 0.001 0.001 0.000
9	1.24 1.36 0.68 0.45	20.00 00.00 00.00 00.00 00.00 00.00 00.00
P Tot	0.17 0.34 0.17 0.34 0.65	0.000 0.000 0.000 0.000
a. ²⁷	0,% 0.48 0.83 1.31 1.66 1.43	
4	0.52 2.92 7.82 3.09 0.00	2.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002
	. 22.1 23.1 23.1 23.1 20.0 7	0.00 0.00 0.00 0.00 0.00 0.00
	2.33 2.93 0.93 0.10 0.10	0.036 0 0.024 0 0.018 0 0.015 0
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(2 of 11 sheets)

Table A-4 (Contammed)

1	1	10	0.38	0.38	0.28	0.28	00.0	00.0									
		٥	0.26				2.10		1	1	6	0000	80	0.00	300	300	2000
		P.B	-1.08	្	0.82	3.0	1.00	8.0			es es	0.00	0000	000.0	0.00	0.00	
		P7	0.53	0.0	1.06	10.5	0.85	0.6	l		D	0.00	0 00	0.002	0.001	0.0	0.00
	pur	4 P	9.1	5.30	3.8	1.69	0.68	0.0			90	0.00	0.001	0.00	0.000	0.000	0000
	Rebound	25	0.18	-0.18	-0.18	0.18	-0.18	-6.35		Rebound	20	-0.00	0000	0.001	0.003	0.007	0.00
		O.T	₹.0	0.148	0.71	1.19	1.43	1.19			⁷ G	0.00	0.00	0.003	0.003	0.003	0.00
1110		Д.	09.0	8	1.89	3.8	1.97	0.51			ď.	0.00	0.008	0.006	0.00	0.002	0.001
at Indicated Call		P2	0.61	98	1.22	1.22	96.0	0.72	ed Gages		25	0.00	0.003	0.000	0.00	0000	00000
at This		P	1.85	90.4	2.68	11.1	0.56	0.19	ection, in. at Indicated Gages		ι	0.00	0.003	-0.005	-0.008	-0.011	-0.01
nre. pei		10	-0.37	-0.37	-0.47	-0.47	-0.75	-0.75	in . e								
Vertical Pressure.		P 9	0.43	8.0	1.39	1.92	2.27	1.92	flection		67	0000	0.001	0.00	0.00	0.00	0.000
Vertic		8	0.00	٥.2 د	1.8	4.08	2.04	1.23	tical De		DB	0000	0000	0.000	0.00	0.001	0.000
		4	0.63	8:	1.16	1.16	6.0	0.74	Ver		20	0000	0.0	0.001	0.000	0.000	0.000
	7	9	1.46	5.73	4.29	41.5	1.13	29.0			D6	0.00	0.00	0.00		0.000	0,000
	Tota	2	0.52	0.52	0.52	0.52	0.52	0.35		Total	5	0.00	0.00	0.003	0.005	0.009	0.03
		a,	2.24	84.0	7.7	61.1	£4.3	67-1			ล้	0.00	0.00	5 303	0.003	0.003	0.002
		-M	9	0.43	1.38	3.1	1.16	0.0			م ا	0.005 0.003 0.000 0.000	0.007	0.005	0.003	0.001	0000
		25	19.0	98.0	1.22	1.22	96.0	0.73			25	0.005	0.003	0.002	0.001	00000	0.000
		 -	1.38								r L	0.033	0.017	0.00	900.0	0.003	0.003
	-000	tion	843	o	H	н	ы	×		•	•	(m)	ø	m	н	19	м
		Point	7									4					
		Row	m									m					

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1	,a	-0.38	-0.19	60.0	-0.19	0.0	8.8									
	P ₉							1	1	4	00000	00000	0.001	0.002	0.003	0.003
	8	-3.05	-2.85	-0.30	4.89	1.33	0.00			80	00000	00000	0.00	0.001	0.00	0.001
	74	0.64	6.0	1.17	1.17	6.0	0.74			2	0.00	0.00	0.002	0.00	0.00	00000
g	9	95.0	2.00	5.19	1.8	29.0	0.22			90	0.002	0.001	0.00	0.000	0000	0.000
Rebou	3	0.00	0.0	0.00	00.00	-0.17	-0.17		Rebound	2	000.0	0.00	0.00	900.0	0.00	5.00.0
	4	0.24	94.0	0.59	0.33	0.95	0.83		a.	ď	0.001	0.003	0.004	0.004	0.004	0.003
9110	4	0.52	69.0	98.0	1.03	09.0	0.17			2	900.0	0.011	0.00	900.0	0.003	0.002
ndicated Cells	P2	0.61	1.10	1.10	1.10	0.85	0.61	George		20	0.007	0.005	0.003	0.002	0.00	0.001
1	4	1.66	2.58	1.7	0.74	0.37	0.19	Indicat		占	0.049	o.a9	0.00	0.005	0.003	0.002
ertical Pressure, pet	야.	-0.19	0.00	0.10	0.00	61.0	8.00	4								
Press.	Pg	0.35	0.87	1.40	2.10	2.45	2.10	Ject for		۵	00000	0.000	0.00	0.002	0.003	0.003
Vertice	8	0.20	00.00	2.55	7.7	4.18	2.65	Heal De		8	0.000	0.000	0.00	0.001	0.001	0.0m
	$\frac{1}{L_d}$	22.0	1.05	1.21	1.27	1.05	9.0	Ver		70	0.00	0.002	0.00	0.001	0.00	0000
	9	1.80	8.24	6.43	3.16	1.91	1.46			90	0.002	0.00	0.00	0.000	0.000	00000
Tota	2	46.0	9.34	0.34	0.34	0.17	71.0		Total	25	0.002	0.003	0.00	0.008	0.012	0.01
	27	N.24	94.0	0.59	0.83	6.9	0.83			ล้	0.00	0.003	0.004	0.004	0.004	0.003
	F	0.17	₩.0	0.51	0.68	0.25	-0.18			3	0.005	0.00	9000	0.005	0.002	0.00
	2				0.98					25	0.007	0.005	0.003	0.002	0.00	0.00
	4				61.0					P.	0.046	0.00	0.007	0.00	0.000	-0.00L
				m	1	2	*				M	o	m	н	•	×
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Table A-4(Continued)

$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$								Total	7		Vertic	Tres	Vertical Pressure, psi	4	at Indicated Cells	911.6		Rebound	pur				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	Sin Sin	tion	P.	4 6	-M	P.	2		P	g _S	6	P10	4	P2	۳,	Q.	P5	P. P.	ă.	8	20	P10
0.47 0.48 0.48 0.48 0.48 0.49 0.49 0.49 0.49 0.49 0.48 0.49 0.48 0.49 0.48 0.49 0.49 0.49 0.49 0.49 0.49 0.49 0.49	2	٦	٧	0.19	0.25	0.26	0.00	-0.86	10	0.32	0.21	0.17	60.0	0.37	0.37	9.36	0.24	1.21	-0.23	0.32	-1.42	2.17	-1.12
0.37 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.13 0.14 0.13 0.14 0.13 0.14 0.13 0.14 0.13 0.14 0.15 0.14 0.13 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.14 0.15 0.14 <t< td=""><td></td><td></td><td>M</td><td>88.0</td><td>0.37</td><td>0.26</td><td>0.0</td><td>0.35</td><td>0.11</td><td>0.32</td><td>0.21</td><td>0.35</td><td>0.0</td><td>94.0</td><td>67.0</td><td>0.3¢</td><td>0.24</td><td>0.00</td><td>-0.23</td><td>0.35</td><td>-1.42</td><td>0.35</td><td>-1.50</td></t<>			M	88.0	0.37	0.26	0.0	0.35	0.11	0.32	0.21	0.35	0.0	94.0	67.0	0.3¢	0.24	0.00	-0.23	0.35	-1.42	0.35	-1.50
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			U	94.0	0.37	0.17	0.12	0.35	0.45	0.53	0.0	0.35	0.0	0.64	64.0	0.17	0.36	00.00	0.11	0.53	-1.63	0.35	-1.50
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			Q	0.55	64.0	0.17	0.12	0.35	19.0	19.0	0.00	0.35	0.0	0.73	19.0	0.17	0.36	0.0	0.33	0.0	-1.63	0.35	-1.50
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			Œ	0.92	6. 6	0.17	0.12	0.35	1.58	0.74	-0.10	0.35	0.0	1.10	0.73	0.17	0.36	0.00	1.2	0.74	-1.73	0.35	-1.50
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			N	1.29	6.73	0.17	0.24 0	0.35	4.51	6.0	-0.10	0.52	0.00	1.47	0.85	71.0	0.48	0.0	4.17	6.0	-1.73	0.52	1.4
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			o	1.48	0.85	0.35	0.24	0.35	7.33	1.06	-0.20	0.87	0.0	1.66	6.0	0.35	0.48	0.00	6.99	1.06	-1.83	0.87	-1.41
			H	0.98	96.0	0.52	0.48	0.35	5.19	1.17	2.45	1.57	0.0	1.10	1.10	0.52	0.72	0.0	1.85	1.17	0.82	1.57	-1.41
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			14	0.37	0.85	0.60	4.0	0.35	2.25	1.17	7.13	5.09	0.0	0.55	0.97	0.60	6.0	0.0	1.9	1.17	5.50	5.09	-1.50
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			ר	0.0	0.85	0.35	4.0	0.35	1.13	6.0	3.47	2.44	74.0	0.18	0.97	0.35	6.0	0.00	0.79	0.95	1.8	2.44	-1.03
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			M	-0.09	0.61	0.17	4.0	0.35	0.67	0.74	1.43	1.92	31.40	0.09	0.73	0.17	6.0	0.00	0.33	0.74	-0.20	1.92	8.62
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			1	-0.18	0.37	0.17	0.48	0.35	0.45	19.0	1.23	1.66	n.06	0.0	64.0	0.17	9.72	0.0	0.11	19.0	-0.40	1.66	9.56
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			×	-0.18	0.37	0.00	0.148	0.35	0.45	0.53	1.00	1.22	5.06	0.0	61.0	0.0	0.72	0.00	0.11	0.53	-0.61	1.22	0.5
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			m	-0.18	0.25	0.00	0.24	0.35	o.34	0.35	1.02	69.0	1.69	0.0	0.37	0.0	0.48	0.0	0.00	0.32	-0.61	69.0	0.19
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$										Ver	tical De	Mection	1. fn.	t Indica	bed Gages			1					
b₂ b								Total									ı	Rebound					
0.004 0.002 0.003 0.000 <th< th=""><th></th><th></th><th></th><th>L L</th><th>20</th><th>arl</th><th>ď</th><th>2</th><th>90</th><th>D2</th><th>88</th><th>60</th><th></th><th>ď</th><th>25</th><th>P_D</th><th></th><th>2</th><th>90</th><th>27</th><th>89</th><th>6</th><th></th></th<>				L L	20	arl	ď	2	90	D2	88	60		ď	25	P _D		2	90	27	89	6	
0.000 0.000 <th< td=""><td></td><td>7</td><td>4</td><td>0.005</td><td>0.00</td><td>0.002</td><td>0.001</td><td>0.00</td><td>0.00</td><td>0000</td><td>0.000</td><td>0000</td><td></td><td>-0.065</td><td>0.003</td><td>0.00</td><td>0.000</td><td>0.00</td><td>0.00</td><td>0000</td><td>0000</td><td>0000</td><td></td></th<>		7	4	0.005	0.00	0.002	0.001	0.00	0.00	0000	0.000	0000		-0.065	0.003	0.00	0.000	0.00	0.00	0000	0000	0000	
0.431 0.004 <th< td=""><td></td><td></td><td></td><td>0.01</td><td>0.007</td><td>0.00</td><td>0.001</td><td>0.00</td><td>0.00</td><td>0000</td><td>0000</td><td>0.00</td><td></td><td>-0.059</td><td>0.00</td><td>0.00</td><td>0000</td><td>0.003</td><td>0.00</td><td>0.00</td><td>0000</td><td>00000</td><td></td></th<>				0.01	0.007	0.00	0.001	0.00	0.00	0000	0000	0.00		-0.059	0.00	0.00	0000	0.003	0.00	0.00	0000	00000	
0.411 0.005 0.004 0.005 0.000 0.003 <th< td=""><td></td><td></td><td>υ</td><td>0.030</td><td>0.010</td><td>0.00</td><td>0.00</td><td>0.002</td><td>0.002</td><td>2.001</td><td>0000</td><td>0.00</td><td></td><td>-0.040</td><td>0.00</td><td>0.00</td><td>0.00</td><td>0.00</td><td>0.00</td><td>0.00</td><td>0000</td><td>0000</td><td></td></th<>			υ	0.030	0.010	0.00	0.00	0.002	0.002	2.001	0000	0.00		-0.040	0.00	0.00	0.00	0.00	0.00	0.00	0000	0000	
0.001 0.002 0.002 0.002 0.002 0.000 <th< td=""><td></td><td></td><td>A</td><td>201.0</td><td>0.01</td><td>0.00</td><td>0.001</td><td>0.01</td><td>0.003</td><td>0.00</td><td>0000</td><td>0.00</td><td></td><td>0.037</td><td>0.00</td><td>0.005</td><td>0.000</td><td>0.03</td><td>0.003</td><td>0.00</td><td>0000</td><td>0000</td><td></td></th<>			A	201.0	0.01	0.00	0.001	0.01	0.003	0.00	0000	0.00		0.037	0.00	0.005	0.000	0.03	0.003	0.00	0000	0000	
0.000 0.0012 0.0002 </td <td></td> <td></td> <td>ы</td> <td>0.161</td> <td>0.0</td> <td>0.008</td> <td>0.002</td> <td>0.00</td> <td>0000</td> <td>0.00</td> <td>0000</td> <td>0.00</td> <td></td> <td>0.091</td> <td>0.00</td> <td>0.008</td> <td>0.001</td> <td>0.00</td> <td>0.003</td> <td>0.002</td> <td>0000</td> <td>0000</td> <td></td>			ы	0.161	0.0	0.008	0.002	0.00	0000	0.00	0000	0.00		0.091	0.00	0.008	0.001	0.00	0.003	0.002	0000	0000	
0.007 0.013 0.003 0.002 0.003 0.001 0.003 <th< td=""><td></td><td></td><td></td><td>0.108</td><td>0.00</td><td>0.012</td><td>0.002</td><td>0.002</td><td>0.002</td><td>0.003</td><td>0.001</td><td>0.00</td><td></td><td>0.038</td><td>0.00</td><td>0.012</td><td>0.00</td><td>0.00</td><td>0.00</td><td>0.003</td><td>0.001</td><td>0000</td><td></td></th<>				0.108	0.00	0.012	0.002	0.002	0.002	0.003	0.001	0.00		0.038	0.00	0.012	0.00	0.00	0.00	0.003	0.001	0000	
0.005 0.021 0.005 0.021 0.005 0.004 0.001 0.005 0.004 0.005 0.004 0.005 <th< td=""><td></td><td></td><td>o</td><td>0.087</td><td>0.007</td><td>0.015</td><td>0.003</td><td>0.00</td><td>0.002</td><td>0.003</td><td>0.001</td><td>0.001</td><td></td><td>0.07</td><td>0.006</td><td>0.a5</td><td>0.00</td><td>0.00</td><td>0.00</td><td>0.003</td><td>0°00</td><td>0.001</td><td></td></th<>			o	0.087	0.007	0.015	0.003	0.00	0.002	0.003	0.001	0.001		0.07	0.006	0.a5	0.00	0.00	0.00	0.003	0°00	0.001	
0.003 0.004 0.005 0.009 0.009 0.001 0.003 0.000 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.004 <th< td=""><td></td><td></td><td>Ħ</td><td>0.076</td><td>0.005</td><td>0.01</td><td>0.005</td><td>0.00</td><td>0.001</td><td>0.003</td><td>0.001</td><td>0.002</td><td></td><td>9000</td><td>0.004</td><td>0.01</td><td>0.00</td><td>900.0</td><td>0.00</td><td>0.003</td><td>0.00</td><td>0.002</td><td></td></th<>			Ħ	0.076	0.005	0.01	0.005	0.00	0.001	0.003	0.001	0.002		9000	0.004	0.01	0.00	900.0	0.00	0.003	0.00	0.002	
0.002 0.004 0.005 0.004 0.000			н	10.0	0.003	9000	0.005	0.00	0.00	0.002	0.00	0.003		0.001	0.00	0.006	0.004	0.011	0.00	0.00	0.00	0.003	
0.001 0.002 0.004 0.017 0.000 0.001 0.001 0.007 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.001			4	0.068	0.00	0.00	0.00	0.01	0000	0.001	0.001	0.00		-0.002	0.001	0.00	0.00	0.016	0.00	0.001	0.001	0.00	
0.001 0.001 0.003 0.016 0.000 0.001 0.001 0.007 -0.003 0.000 0.001 0.002 0.018 0.000 0.001 0.001 0.001 0.001 0.002 0.003 0.000 0.001 0.002 0.003 0.000 0.001 0.002 0.003 0.000 0.000 0.001 0.000			M	0.67	0.00	0.00	0000	0.017	00000	0.001	0.001	0.005		-0.003	0.000	0.00	0.003	0.00	00000	0.00	0.00	0.005	
0.001 0.001 0.003 0.013 0.000 0.000 0.001 0.005 -0.004 0.000 0.001 0.002 0.015 0.000 0.000 0.001 0.000 0.001 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000			u	0.067	0.00	0.00	0.003	0.016	0000	0.001	0.00	0.00		-0.003	0000	0.00	0.002	0.018	0000	0.00	0.00	0.005	
0.001 0.000 0.002 0.008 0.000 0.000 0.000 0.004 -0.004 0.000 0.000 0.001 0.010 0.000 0.000 0.000			×	0.066	0.001	0.001	0.003	0.013	00000	0000	0.00	0.005		-0.004	0000	0.00	0.00	0.005	0.000	00000	0.00	0.00	
				0.066	0.001	0000	0.002	0.00	0.00	0.000	0000	0.00		-0.00	0.00	0.00	0.001	0.00	0000	0.000	0.000	0.00	

Table A-4 (Continued)

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			1							Vertical		seure, pe	Pressure, psi, at Indicated Cells	dicated C	ells							
7		Locas					10	7									Debos	72				
K	Potet	ttos	1100 P1 P2 P3 P1 P5 P	4	4	a.*	2	9	4	8	٥	P10	a. 1	4.5	4	PL	PS	9.	P7	8	0	100
	-1	H	0.37	0.3	0.00	0.0	-0.17	1.3	0.63	-0.50	0.35	0.65	0.56	0.40	0.0	7	8	8	69 0	6	110	
		0	0.55	0.40	00.0	0.24	-0.17	8	a	6	9	73 0	i						5		5	0:0
								1	3		60.0	0000	*	0.13	3	0.40	8	8	0	2.5	0.78	99.0
		*	0.31	6.40	8	7.	-0.17	3.	S. 38	-0.30	7.	95.0	0.56	0.73	%	94.0	0.0	2.93	6.0	2.2	1.13	99.0
		н	0.18	64.0	0.18	0.2	-0.17	94.0	6.0	0.41	1.57	0.37	0.37	0.73	0.18	9.40	8.0	1.47	8	8	3.66	0.47
		ר	0.00	64.0	0.18	0.36	-0.17	-0.33	0.8	-0.8r	1.33	-0.57	0.19	0.73	0.18	09.0	8.0	99.0	800	1.63	8	-0.67
		M	0.0	0.3	0.18	0.24	-0.17	-0.56	0.63	-1.83	1.57	-1.22	0.19	64.0	0.18	94.0	8.0	0.45	0.63	0.61	8	-1-36
									A	Vertical Deflection	eflection	9	at Indicated	ted Gage								
							Total									ľ	Debound					
			D ₁ D ₂ D ₃ D ₄ D ₅	2	D ₃	đ	2	90	L _Q	8	60		e d	D2	D ₃	a	De	DK	D	DA	C	
																	1	,	1		1	
	-	ы	0.0E7	0. a.9	0.012	0.002	0.001	0.00	0.00	0.00	0.00		0.034	0.00	0.00	0.00	-0.00	0.00	000	0.00	-0.00	
		o	0.00	0.013	0.043	0.007	0.007	0.007	0.03	0.007	0.00		0.07	0.00	0.035	0.00	-0.00	0.00	0.00	0		
		m	-0.006	0.00	0.034	0.00	0.0T	0.005	0.012	0.007	9000		0.0	0.30	98	0.00	0.00	0.00	900		8	
		н	-0.00	0.007	0.080	0.0	0.0g	0.00	0.00		000		0.007	0.00	0.00	0.00	000	8	8		3	
		ר	-o.a.	0.00	0.013	0.0	0.033	0.00	0.00	0.00	0.00		9	8	8	4			3	3 3	3	
			000	***		-	3 7						3	1	3	3	2000	3	0.00	0.00	0000	
		4		3	0	0.00	0.0	0	0.001	0.0	o.0		0.00	o.0	90.0	8	0.035	0000	0.00	0.00	0.03	

2 .	Contirue	
le A-4 (c	le A-4 (c	

ı										Vertical	Pres.	Vertical Pressure net	Tradfosted Coll	0 00000	11.5							1
	Tond	1000			1	1	Tota	7		100		1 1 1 1	1	יבורכת ר			Rebounk	2				1
2	Point	tion	n.	2	-M	a.=	2	9	Ld	P8	40	210	a. T	P2	4	a. 3	2	9	P 7.	80	م	200
	H	•	0.0	0.24	0.0	0.12	0.0	0.23	٥. ن	0.30	0.36	0.0	0.00	o.24	0.0	0.12	8.0	0.79	0.32	0.50	0.52	5.0
		U	0.19	0.37	8.0	0.24	0.0	0.34	0.42	0.20	0.36	-0.28	0.19	0.37	0.0	0.24	0.0	8.0	0.53	0.1.0	0.52	0.47
		Q	0.19	0.24	00.0	0.24	0.00	0.57	0.42	0.10	0.26	-0.38	0.19	0.24	0.00	0.24	8.0	1.13	0.53	0.30	0.52	0.37
		g _a g	0.19	0.37	0.00	0.24 0.24	8.0	0.79	0.53	0.00	0.35	-0.47	0.19	0.37	0.00	0.24	0.00	1.35	9.0	0.30	0.61	0.29
		Ba,	0.28	64.0	0.00	0.24	0.0	1.08	0.63	0.10	0.44	0.00	0.28	64.0	0.0	0.24	8.0	1.58	0.74	0.30	0.70	0.7
		Ç*	0.19	64.0	3	0.24	0.0	1.13	0.74	0.0	0.61	-0.10	61.0	64.0	0.00	0.24	0.0	1.69	9.0	0.50	0.87	9.6
		nd	0.19	67.0	0.0	12.0	0.00	0.57	0.74	0.30	0.78	0.0	0.19	64.0	0.0	0.2	0.0	1.13	0.65	0.50	1.04	0.7
		н	0.19	64.0	0.0	o.24	0.17	n.º	0.74	0.41	96.0	-0.19	0.19	64.0	0.0	0.24	0.18	79.0	0.85	0.61	1.22	0.56
		ь,	0.19	0.37	8.0	0.4.0	2	-0.22	0.63	0.20	1.03	-0.38	0.19	0.37	0.0	0.24	8.0	0.34	0.7	0.40	1.3	0.37
		×	0.0	₹.0	0.09	0.36	0.17	-0-34	+0.12	-0.10	0.78	-0.56	0.0	0.24	0.0	0.36	0.18	0.23	+0.53	0.10	7.0	0.19
		ы	0.00	0.24	0.0	72.0	0.17	-0.45	0.45	-0.20	0.61	-0.56	0.0	0.24	0.09	0.24	0.18	0.11	0.53	0.0	0.87	0.19
		×	0.00	0.24	0.0	0.24	00.0	-0.45	0.32	-0.31	11.0	95.0-	0.00	0.24	0.0	0.24	0.00	n.0	0.13	-o-	0.70	0.19
		×	0.0	0.12	0.0	0.24	0.17	-0.56	٥. <u>ت</u>	-0.31	0.36	95.0-	0.00	0.12	0.0	0.24	0.18	8.0	0.32	T-0-	0.52	0.19
			8						A.	Vertical D	Deflection, in.	n, in.	at Indicated Gages	ted Gage	ug.	1						
							Total									0	Febound	pu				
			4	2	2	ď	50	90	$\mathcal{L}_{\mathbf{d}}$	8	60		I _Q	20	a	គឺ	2	90	La	80	6	
	H	m	0.008	0.009	0.00	0.001	0.00	0.006	0.001	0.000	0.00		0.00.5	0.007	-0.009	0.000	-0.061	0.005	0.000	-0.00T	-0.002	
		υ	0.00	0.015	0.00	0.00	0.003	0.00	0.003	00000	0.003		0.017	0.013	-0.007	0.000	-0.060	0.00	0.00	-0.00	-0.00	
		A	0.0	0.018	0.00	0.00	0.003		0.00	0.001	0.003		0.018	0.016	-0.005		-0.060	0.009	0.003	0.000	-0.00	
		(c)	0.011	0.082	0.000	0.00	0.003		9000	0.001	0.003		0.018	0.000	-0.001	0.00	-0.060	0.009	0.00	0.000	-0.0a	
		Ba .	0.008	0.019	0.029	0.003	0.00		0.01	0.00	0.003		0.015	0.017	0.018	0.00	-0.061	0.008	0.000	0.00	-0.0a	
		o	00.0	0.013	0.059	0.00	0.003	0.007	0.015	0.003	0.00		0.01	0.011	0.048	0.003	-0.060	0.006	0.014	0.00	0.000	
		æ	00000	0.00	0.049	5000	0.006	0.00	0.024	0.00	0.006		0.007	0.007	0.038	0.00	-0.057	0.00	0.013	0.003	0.00	
		н	-0.303	0.005	0.089	0.008	0.013	0.003	0.008	0.00	0.00		0.00	0.003	0.018		-0.050	0.002	0.00	0.003	900.0	
		כי	-0.004	0.00	030.0	0.00	0.043	0.000	0.005	0.00	0.017		0.003	0.00	0.009		-0.020	0.001	0.00	0.003	0.03	
		ы	-0.005	0.003	0.016	0.006	0.131	0.001	0.003	0.003	0.082		0.00	0.001	0.005	005	0.068	0.000	0.00	0.002	0.018	
		ы	-0.005	0.003	0.01	0.00	0.106	0.001	0.002	0.003	0.021		0.00	0.001	0.003	0.00	0.043	0.000	0.00	0.002	0.017	
		×	-0.005	0.003	0.013	0.00	0.088		0.000	0.003	0.019		0.002	0.001	0.00	0.003	0.00	0.000	0.00	0.00	0.005	
		Þ.	-0.006	0.003	0.012	0.003	0.059	0.001	0.000	0.005	0.013		0.001	0.001	0.001	0.000	900.0	0.000	0.000	0.00	0.00	

	or ₄					H	6 0.19		1	1	1 8	3 8	3 8	3 6		-
	9						8.0			o o		357		0.00		
	8	0.10	01.0	O. E.	130	170	0 2			88	1			0.00	0.0	-
	L _d	0.53	120	2	2	0	0.63			D ₇	100		800	000	0.00	1
	9	0.56	0.70	0.67	0.45	0.0	0.0			90	8		0.00	0.00	0.00	
	P S	0.0	0.0	00.0	0.00	0.00	0.00		9	2	8	000	0.013	0.00	0.034	,
	P.	0.12	70	0.10	0.5	0.24	0.24			G ^a	80	0.00	0.00	0.00	900.0	
1	3	0.00	0.0	0.0	0.0	0.0	0.0		١	D ₃	0.00	0.030	0.00	0.01	0.008	
cated Ce	60	0.24	0.24	0.2	0.24	0.24			Da Conges	D2	0.006	0.09	00.0	0.00	0.00	
Vertical Pressure, psi, at Indicated Celli	12	0.19	0.19	0.19	0.19	0.10	0.10		Toda Car	D,	0.00	0.00	0.003	0.00	0.00	
Tr. Pet	210	61.0	0.28	0.19	0.37	0.19	0.19		10. c 61							
1 706	00	9.36	0.52	0.70	0.87	0.87	0.78		7001100	6	0.007	0.00	0.000	0.015	0.023	
Vertic	8	n.0-	0.11	0.20	0.20	0.20	0.00		100	80	0.001	0.003	0.00	0.005	0.005	
	22	0.43	0.64	0.74	0.74 0	19.0	0.53	1	15.	^D 2	0.007	20.00	0.021	3.012	0.008	
	9	95.0	62.0	79.0	0.45	2.0	0.00		l	9	0.313	900.0	0.005	0.003	0.002	
Total	2	0.18	0.18	0.18	0.18	0.18	0.18		Total	P _S	0.002	0.00	0.002	0.010	0.023	
	0.7	.12	8	77	2	ź,	₹.			ď	0.002	0.00	900.0	0.007 0.010	0.007	
	2	8.0	60.0	800	80.0	0.0	0.0	-9		D ₃	0.00	0.037	0.027	0.012	900.0	
	20	0.24	0.24	P.0	0.24	0.24	· 5			20	0.016	0.008	0.00	0.002	0.001	-
	4.	61.0			0.19					r a	900.0	0.00	0.000	-0.001 0.002 0.012 0.	-0.002	
	tion	84	¢1	101	н	7	×				64	O	m	H	ы	
1	Point	-									rt					

(Continued)

										Vertic	al Fress	Vertical Fressure, psi, at Indicated	at Ind	Cated Co	3116	4						
Dec	н	-830					TOC										Rebon	pur				
Point	-1	tion	1,	2	a.e.	d.*	2	29	P7	PB	34	P10	"	A.CV	۳	ρ.**	2	P6	P	8	64	100
-		842	0.19	0.12	0.0	0.12	8.0		37.0	a.0	0.35	0.19	0.0	7	00.00	61.0	0	000	0 40	110		5
		o	0.10	0.24	0.0	0.12	00.0		0.63	6	0	97.0	8	9	8					1	3	
				1							0		3	200	3	7	3	5	0.03	1.0	0.53	0.19
		×	0.19	, v	8	0.12	8		0.63	a.0	0.70	0.00	0.0	0.36	0.0	0.12	8.0	0.55	0.63	0.0	0.70	8.0
		н	0.10	0.24	0.18	0.24	0.00	0.22	0.63	o.31	0.79	0.19	0.0	0.36	0.18	0.24	0.0	0.25	0.63	2.0	0.79	0.19
		7	01.0	0.12	0.12 0.09 0	0.24	0.17		0.53	o.3	0.88	0.0	0.00	d o	000	0.2	0.17	8.0	6.53	20	0.88	80.0
		×	0.10	0.12	0.00	0.24	0.24 0.17	8.0	0.44	0.21	02.0	0.00	0.0	2.0	0.0	2.2	0.17	8.0	0.11	0.10	0.70	0.00
									Ver	Vertical Deflection,	Tection		in., at Indicated Gage	ed Geges					ı		1	
							Tota										Rebound				-	
			2	200	e e	ca l	Š	90	L_{Q}	DB	60		er!	25	o.	ď	2	90	24	9 _Q	00	
4		BA2	0.00	0.011	0.004 0.011 0.006 0	0.001	0.001 0.006	0.017	0.008	0.000	0.00		0.00	0.012	0.00	0.00	0.00	0.00	0.00	0.0	-0.00	
		O	0.00	0.006	0.020	0.003	0.006	0.011	0.000	0.00	0.002		0.00	0.007	0.00	0.003	0.016	900.0	0.033	0.003	-0.03	
		æ	0.001	0.003	0.015	0.005	0.008	0.007	0.033	0.00	0.00		0.003	0.00	0.019	0.00	o.a.e	0.00	0.00	0.00	-0.001	
		н	0.000	0.001	0.006	0.005	0.014		0.00	0.006	0.011		0.00	0.00	0.000	0.00	0.00	0.00	0.003	0.00	0.0	
		43	-0.001	0.00	0.00	0.00	0.02	00.0	0.014	0.006	0.082		0.001	0.00	0.00	0.00	0.031	0.001	0.00	0.00	0.07	
		×	-0.001	-0.001	-0.00	0.00	0.022	0.003	0.01	0.005	0.033		0.001	000.0	0.00	0.00	0.032	0000	0.00	0.00	0.00	
																					-	

(Continue

			1							Vertica		Fure. Dat	Pressure, Dat. at Indicated Cell.	cated Ca	25.5							1
	Lond	Toops					101	7									heter	Pall				
NO	Polat	t on	24	4	-	4	PS	9 _e	P7	a [®]	8	10	a,rd	۳. دم	4	O_3	P	P ₆	P	a.	م	01,
0	н	M	60.0	0.12	0.00	0.00	0.17	0.22	0.42	-0.10	0.18	2.00	0.0	0.12	0.0	0.0	8.0	0.8	0.42	0.21	0.18	0.0
		U	60.0	0.24	0.0	0.12	0.17	0.34	0.42	0.11	0.35	8.0	0.00	0.2	0.00	0.12	8.0	0.34	0.42	00.0	5.3	8
		H	0.00	0.24	0.0	0.12	0.17	0.22	0.42	0.11	0.11	0.0	0.00	0.24°	0.0	0.12	8.0	0.55	0.42	8	0.44	0.00
		н	0.00	0.12	0.00	0.12	0.17	0.22	0.42	0.11	0.53	0.0	0.00	0.12	8.0	0.12	800	0.25	0.42	00.00	0.53	8
		ь	0.00	0.12	0.00	0.12	0.17	٥٠.	0.45	o.31	0.61	0.0	0.0	0.12	3.0	0.12	00.00	0.11	0.10	3	0.61	200
		×	0.00	0.12	0.12 0.09 0.12 0.34	0.12	0.34	0.0	0.45	0.21	0.53	0.0	0.00	0.12	0.0	0.12	0.17	0.0	0.42	0.10	0.53	8 .0
							10.		A	ertice	reriection	-	in. at Indicated Gag	ited Gag	8							
			a	20	D ₁ D ₂ D ₃ D ₁ D ₅	a ⁴	50	90	20	_D 8	o		a ^r	D2	D S	ηď	D ₅	90	L _Q	P _Q	O	
0	-	×	0.00	0.008	0.00	0.00	0.00	0.000	0.008	2,000	0.00		0.003	0.00	0.00	0.00	0.00	0.08	-0.00	0.00	-0.016	
		o	0.003	0.00	0.011	0.002	0.001	0.011	0.051	0.023	0.001		0.002	0.00	0.00	0.003	0.000	0.00	0.041	0.00	-0.015	
		×	0.002	0.002	0.008	00.0	0.00	0.007	0.042	0.006	0.00		0.000	0.003	0.002	0.00	0.00	0.00	0.032	0.00	-0.012	
		н	0.001	0.00	0.003	0.00	0.008	0.00	0.024	0.007	0.012		0000	0.001	0.007	0.00	0.013	0.00	0.00	0.00	0.00	
		ר	0.00	0.00	0.000	0.00	0.03	0.00	0.017	0.007	0.032		-0.00	0.00	0.00	00.00	0.018	0.00	0.007	0.00	0.006	
		×	0.000	-0.001	-0.002	0.003	0.001	0.003	0.013	0.005	0.081		-0.001	0.000	0.002	0.00	0.019	0.00	0.003	0000	0.065	

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										Verti	cal Pres	Vertical Pressure, psi.	at Indi	at Indicated Cells	elle							
100	Potet	tton	4	20	۳,	a.*	2 3	P6-	P7	80	6	P10	d.	4	4	a.*	Pebo	Pe Pe	24	8	0	P10
ជ	н	•	0.09	0.12	0.30	0.00	0.17	8.0	0.21	8.0	0.18	0.0	0.0	0.12	-0.09	0.0	0.00	8.0	8.0	0.0	0.18	0.19
		υ	0.00	0.12	0.0	0.00	0.17	n.º	ង.	0.0	0.18	0.0	0.0	0.12	-0.09	0.00	0.0	0.11	a.0	0.0	0.18	0.28
		Α	0.00	0.12	0.0	0.00	0.17	n.º	ត.	n.o-	0.18	0.00	0.0	0.12	-0.09	0.0	00.0	n.0	0.0	n.0-	0.18	61.0
		ы	0.09	0.12	8.0	0.0	0.17	n.º	0.32	0.00	0.19	0.0	0.0	0.12	-0.09	0.00	0.0	3.0	0.32	0.0	0.18	0.19
		Br _e	0.00	0.12	0.00	0.0	0.17	0.22	0.32	0.0	0.18	-0.10	0.0	0.12	-0.09	0.0	0.00	0.22	0.32	0.0	0.18	0.09
		v	0.00	0.12	0.0	0.12	0.17	0.22	0.42	0.00	0.26	-0.10	0.00	0.12	€0°0-	0.12	0.00	0.25	0.42	0.0	0.26	0.0
		æ	0.00	0.12	0.00	0.12	0.17	0.25	0.42	0.0	0.35	0.0	0.00	0.12	60.00	0.12	0.0	0.22	0.42	0.0	0.35	0.19
		н	0.00	0.12	0.00	0.12	0.17	n.0	0.42	0.0	0.35	0.0	0.00	0.12	-0.09	0.12	0.00	0.11	0.42	0.0	0.35	0.19
		נ	0.0	0.12	0.0	0.12	0.17	n.0	0.32	0.0	0.35	0.00	0.00	0.12	-0.09	0.12	0.0	0.11	0.32	0.0	0.35	0.19
		×	0.00	0.12	0.00	0.12	0.17	0.3	a.0	0.0	0.35	0.0	0.0	0.12	-0.09	0.12	0.00	0.00	0.2	00.00	0.35	0.19
		H	0.00	0.12	0.0	0.12	0.17	0.00	o.2	0.00	0.35	-0.10	0.00	0.12	0.00	0.12	0.00	00.0	0.2	0.00	0.35	0.0
		37.	0.00	0.12	0.00	0.12	0.17	0.0	a.º	0.0	0.35	0.00	0.00	0.12	0.00	0.12	0.00	0.0	o.2	0.00	0.35	0.19
		31 1	0.00	0.12	0.00	0.0	0.17	0.0	0.10	0.00	0.18	-0.10	0.0	0.12	0.00	0.00	0.00	0.0	0.10	0.0	0.18	0.09
												á				Ų						
							20.0		A	Vertical	Per ection	12:	at indicated Gages	ated Gag	8.8		- American					
			I D	20	G.	G T	2	90	70	D _B	Po		I G	D2	D 2	J.	2	P6	DZ	80	0	
1	н	•	0.002	40°°0	0.001	0.001	00000	0.008	0.000	0.001	-0.001		0.001	0.005	0.003	0.001	0.007	0.00	-0.004	0000	-0.057	
		υ	0.002	0.00	0.00	0.001	0 000	0.015	0.00	0.001	0.000		0.001	0.005	700.0	0.001	0.007	0.013	-0.002	0.000	-0.056	
		A	0.002	9000	0,002	0.001	00000	0.019	0.004	0.001	000.0		0.001	0.007	0.00	0.001	0.007	0.017	0.000	0000	960.0-	
		(k.)	0.003	0.006	00.00	0.001	0.000	0.00	0.007	0.002	0.000		0.002	0.007	0.005	0.001	0.007	0.00 o	0.003	0.001	-0.05	
		ħ.	0.00	0.00	0.000	0.002	0.000	0.018	0.023	0.00	-0.001		0.000	0.00	0.008	0.00	0.007	0.016	0.00	١.,	-0.057	
		O	0.002	0.003	0.008	0.003	0.001	0.012	0.049	0.00	0.000		0.001	0.00%	0.010	0.003	0.008	0.010	0.045	o	-0.056	
		tic	0.001	0.002	0.000	0.004	0.002	0.008	0.000	0.00	0.003		0.000	0.003	0.006	0.00	60000	0.006	0.035	0.00	-0.053	
		ы	0.001	0.000	0.003	0.004	0.005	0.003	0.022	0.007	0.012		0.000	0.000	0.005	0.004	0.012	0.003	0.08	0.005	-0.0th	
		7	0.001	00000	0.001	0.00	0.008	00.00	0.013	0.007	0.006		0.000	0.001	0.003	0.00	0.015	0.002	0.009	0.00	-0.050	
		×	0.001	-0.001	-0.001	0.003	0.009	0.00	0.009	0.005	0.127		0.000	0.000	0.00	0.003	0.00	0.002	0.00	0.004	0.072	
		ы	0.001	-0.001	-0.001	0.002	0.008	0.003	0.007	0.00	0.114		0.000	00000	0.001	0.002	0.015	0.001	0.003	0.003	0.058	
		x	00000	100.0-	-0.001	0.002	0.005	-0.016	0.025	0.004	0.099		-0.001	00000	0.001	0.002	0.03	-0.018	0.001	0.003	0.033	
		ĸ	0.000	-0.001	-0.002	100°C	0.002	0.003	0.005	0.003	0.057		-0.001	0.000	0.000	0.001	0.000	0.00	0.001	0.002	0.011	

Multiple. Heavy Gear Load Flexible Favement Test, Static Instrumentation Loading Data Item 4; Load Condition: 30 kips per Wheel, Single Wheel, 100 psi

1 1 2 2 2 2 2 2 2 2																		-	-				
0.577 0.52 0.54 0.59 0.59 0.50 0.40 0.40 0.43 0.51 1.00 0.33 0.40 0.40 0.40 0.40 0.40 0.40 0	8	Point	tion	r _d	20	4	a. 1	P.	3	7	P8	6.	P10	12	2	P	P	2	9 b	P	8	4	-
1.28 0.44 0.45	м	=	4	0.00	0.57	0.22	0.36	0.39	0.0	0.45	0.40	0.34	0.31	1.00	0.38	-3.05	₹.0	-0.78	8.0	0.91	0.10	0.43	0.5
1.52 0.44 0.45 0.45 0.49 0.40 1.14 0.15 0.45 0.45 1.15 0.45			M	00.00	0.95	0.22	0.36	0.29	0.18	0.68	0.30	20.3	0.21	8:1	0.76	-3.05	0.24	-0.88	0.18	1.14	0.00	0.43	0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			b	0.00	1.52	0.44	0.60	0.19	0.0	1.14	0.10	0.51	0.21	8.1	1.33	-2.83	0.48	96.0-	0.0	1.60	-0.20	09.0	0.1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			A	28.72	1.71	92.0	0.72	0.0	-0.18	1.37	0.50	09.0	0.21	29.72	1.52	-2 51	09.0	-0.88	-0.18	1.83	-0.30	69.0	0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			54	30.53	5.19	1.42	0.84	0.39	00.0	1.60	0.50	0.68	o.2	31.53	5.00	-1.95	0.72	-0.78	0.0	2.06	0.20	0.77	0.4
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			ji.	-0.80	2.67	02.6	1.07	0.68	00.00	1.60	0.50	0.86	0.21	0.20	2.48	6.43	6.0	67.0-	0.00	5.06	0.20	0.95	0.4
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			0	-0.80	2.28	21.79	1.31	1.56	0.0	1.26	0.90	1.03	0.51	0.20	5.00	18.52	1.19	0.39	0.0	1.72	09.0	1.12	0.
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			363	-0.80	1.33	9.91	1.55	5.18	-0.18	0.68	0.40	1.12	0.82	0.20	1.14	6.64	1.+3	4.01	-0.16	1.14	0.10	1.2	1.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			н	-0.80	1.7	41.1	1.43	8.41	-0.18	0.23	0.10	1.03	1.03	6.20	1.52	0.87	1.31	7.24	-0.18	69.0	-0.20	1.12	1.5
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			ר	-0.80	74.0	3.08	1.19	29.67	-0.18	0.00	00.00	0.86	0.82	0.20	0.28	-0.22	1.07	4.50	-0.18	97.0	-0.30	6.9	1.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			×	-0.80	0.38	2.83	.84	2.93	-0.18	-0.23	0.0	09.0	0.31	0.20	0.19	-0.14	0.72	1.76	-0.18	0.23	-0.30	69.0	0.9
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			ы	-0.80	0.28	2.83	0.72	2,15	-0.18	-0.23	-0.10	0.51	0.2	0.20	0.0	-0.44	09.0	0.9	-0.18	0.23	-0.40	09.0	0.1
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			×	-0.80	0.19	2.72	09.0	1.86	-0.18	-0.35	8.0	0.43	0.00	0.20	8.0	-0.55	0.148	69.0	-0.18	n.º	-0.30	0.52	0.8
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			25	-0.80	0.19	2.72	0.36	1.46	-0.18	-0.35	0.0	0.25	-0.10	0.20	0.0	-0.95	0.24	0.29	-0.18	٥.٣	0.30	0.34	9
b3 b4 b5 b6 b7 b8 b9 b1 b2 b2<								Total			-	1		TOTAL THORES	100 000			Febound				1	
0.000 0.000 <th< th=""><th></th><th></th><th></th><th>a d</th><th>25</th><th>D3</th><th>a a</th><th>50</th><th>90</th><th>Za</th><th>P_B</th><th>D_Q</th><th></th><th>D₁</th><th>D2</th><th>Da</th><th>4</th><th>35</th><th>90</th><th>D₂</th><th>80</th><th>00</th><th></th></th<>				a d	25	D3	a a	50	90	Za	P _B	D _Q		D ₁	D2	Da	4	35	90	D ₂	80	00	
0.001 0.000 0.000 0.001 0.001 0.000 0.00	1	H	¥	Sign	0.00	00000	00000	0000	0.001	0.001	0.000	0.000		0.008	0.00	0.000	0.00	0.00	0.00	0.001	0.000	0.001	
			ph.	8	0.003	0.001	0.000	0000	0.001	0.001	0.000	0.000		0.000	0.005	0.003	0.00	0.00	0.001	0.001	0.000	0.001	
0.001 0.002 0.002 0.002 0.002 0.000 0.00			υ	S	0.007	0.001	0.001	0.000	0.005	0.001	0000	0.000		0.010	0.007	0.003	0.003	0.000	900	0.001	0.000	0.001	
0.001 0.002 0.002 0.002 0.003 0.000 0.00			A	2	0.080	0.001	0.001	000	0.002	0.001	0000	0.000		0.010	0.008	0.303	0.003	0.005	0.00	0.00	0.000	0.001	
			663	D	0.008	0.001	0.001	0000	0.002	0.001	0000	0.000		0.009	0.00	0.003	0.003	0.002	0.00	0.001	0000	0.001	
0.001 0.003 <th< td=""><td></td><td></td><td>St.</td><td>MC</td><td>0.007</td><td>0.001</td><td>0.002</td><td>0.001</td><td>0.002</td><td>0.001</td><td>0.000</td><td>0000</td><td></td><td>0.009</td><td>0.007</td><td>0.003</td><td>0.00%</td><td>0.003</td><td>0.00</td><td>0.001</td><td>0000</td><td>100.0</td><td></td></th<>			St.	MC	0.007	0.001	0.002	0.001	0.002	0.001	0.000	0000		0.009	0.007	0.003	0.00%	0.003	0.00	0.001	0000	100.0	
0.001 0.004 0.002 0.001 0.001 0.000 0.000 0.001 0.001 0.002 0.001 0.002 0.003 0.003 0.003 0.003 0.004 0.001 0.000 0.000 0.001 0.001 0.002 0.001 0.002			o	20	0.003	0.001	0.003	0.001	0.001	0.001	00000	0.000		0.00	0.005	0.003	0.005	0.003	0.001	0.001	00000	0.001	
0.001 0.005 0.004 0.001 0.001 0.000 0.001 0.001 0.001 0.001 0.002 0.001 0.002 0.003 0.007 0.006 0.001 0.000 0.000 0.001 0.002 0.001 0.002			H	E	0.003	0.001	0.004	0.008	0.001	0.001	0000	0.000		0.011	0.003	0.003	0.00	0.004	0.001	0.001	0.000	0.001	
0.000 0.004 0.005 0.001 0.001 0.000 0.001 0.001 0.002 0.001 0.002 0.001 0.002 0.004 0.002 0.004 0.002 0.004 0.000			н	S	0.002	0.001	0.005	0.004	0.001	0.001	0000	0.001		0.014	0.00	0.003	0.00	0.006	0.00	0.001	0.000	0.00	
-0.001 0.002 0.007 0.001 0.001 0.000 0.001 0.000 0.001 0.002 0.001 0.002 0.004 0.007 0.001 0.000 0.000 0.000 0.001 0.000 0.000 0.000 0.001 0.002 0.000 0.001 0.002 0.000 0.001 0.002 0.000 0.000 0.001 0.002 0.000 0.001 0.002 0.000 0.001 0.002 0.000 0.001 0.002 0.000 0.000 0.000 0.000 0.001 0.002 0.000 0.000 0.001 0.002 0.000 0.000 0.000 0.000 0.000 0.000			b	8	0.001	0000	0.00	0.003	0.001	0.001	00000	0.001		0.019	0.001	0.000	0.006	0.007	0.00	0.001	0000	0.00	
-0.001 0.002 0.009 0.000 0.000 0.000 0.001 0.002 0.001 0.001 0.001 0.009 0.000			×	8	0.001	00000	0.00	0.005	0.001	0.001	0.000	0.001		0.023	0.001	0.00	0.00	0.007	0.001	0.001	0.000	0.00	
-0.001 0.001 0.004 0.000 0.000 0.000 0.001 0.000 0.001 0.000 0.001 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000			-3	20	0.001	-0.001	0.002	0.00	00000	00000	00000	0.001		0.022	0.001	0.001	0.004	0.007	00000	0.000	0.000	0.00	
-0.001 0.000 0.003 0.000 0.000 0.000 0.001 0.004 0.000 0.001 0.002 0.03 0.000 0.000 0.000			×	M	0.000	-0.001	0,001	0.00	0.00	00000	0000	0.001		0.000	0.000	0.001	0.003	0.000	00000	00000	00000	0.002	
			M	E	0.000	-0.001	0,000	0.003	00000	00000	00000	0.001		0.014	0000	0.001	0.002	0.03	00000	00000	0.00	0.00	

(1 of 11 sheets)

Note: MD - no good.

										Vertic	Press	Vertical Pressure, psi		Indicated Cell	2110							1
	De o	Local					30,	7									Keb	Rebound				
ROW	Point	tion	a,Fi	4	a.m	a. 3	2	P6	2	8	0	P10	4	P	4	u. 3	267	P6	4	e B	6	ę,
cv	H	9+3	00.0	1.90	0.33	0.72	0.20	0.00	2.18	0.10	09.0	0.20	00.0	1.90	2.29	0.72	0.30	-0.36	2.07	1.20	0.51	0.20
		jh _e	0.00	5.29	2.9	0.9	0.59	0.36	2.52	-0.30	0.95	0.20	0.00	2.29	2.90	0.95	69.0	00.00	2.41	0.80	9.86	0.20
		v	00.0	1.81	8.50	1.19	1.37	0.36	2.06	0.40	1.12	0.61	00.00	1.61	10.16	1.19	1.47	00.00	1.95	1.50	1.03	0.61
		×	00.00	1.14	2.51	1.43	3.82	95.0	1.49	00.0	1.29	1.23	00.00	1.14	14.47	1.43	3.92	0.00	1.38	1.10	1.20	1.23
		н	00.00	0.57	-0.87	1.43	98.9	0.36	0.91	-0.70	1.29	8.0	00.00	0.57	1.09	1.43	94.9	0.0	0.80	0.40	1.20	2.05
		M	00.00	0.19	0.19 -1.85	0.72	1.57	0.36	94.0	-1.20	0.77	0.82	0.00	61.0	0.11	0.72	1.67	0.00	0.35	-0.10	99.0	0.82
																ı						
									Ver	ertical le	flection	a in. a	t Indicat	ed Gages								
			1				1014							-			Pebound					
			24	2	a .	r n	G.	90	24	8	60		1	2	D3	D.	2	99	Z _Q	80	٥	
C)	м	[a]	0.008	0.010	0.002	0.001	0.000 0.010 0.002 0.001 0.001		0.000	0.000	0.000		0.007	0.011	0.00	0.000	0.002	0.003	0.001	0.000	0.001	
		She	0.008	0.008	0.003	0.003	0,002	0.002	0.000	0.000	0.000		0.007	0.009	0.003	0.00	0.003	0.002	0.001	0.000	0.00	
		U	0.00	0.000	0.003	0,005	0.002		00000	0.000	0.001		0.008	0.007	0.003	0,006	0.003	0.00	0.000	00000	0.000	
		¥	0.011	0.003	0.003	0.007	0.004	0.001	0.000	0.000	0.001		0.010	100.0	0.003	0.008	0.00	0.00	0.001	0.000	o.me	
		ы	0.015	0.002	0.002	0.006	0.006	0.001	0.000	0.00	0.001		0.014	0.003	0.000	600.3	0.007	0.001	0.001	0.000	0.005	
		×	0.027	0.000	0.001	0.005	000°C	0.000	0.000	0.000	0,002		0.006	0.001	0.001	900.0	0.010	0.000	0.001	00000	0.003	

	ı	1				4			Vert	Press	'ertical Pressure, psi	at Ind	icated Celli	ells							
Toca-	۵	1	a	9		101	1									Feb	Februard				1
tion 1	5	-1	2		-1	2		2	, TO	6	P10	2	2	4	4	PS	9	P-	89	40	10
₩ 0.00	0.0	0	1.7	0.76	0.72	0.30	0.18	2.52	0.00	0.68	0.20	00.00	1.71	1.74	5.72	0	0.18	2.17	8	89.0	16.0
P 0.00	0.0	0	7.8	1.52	8:0	0.59		2.98	1.40	0.9	0.30	00.0	1.90	d.50	5	1.27	00.00	2,53	08.0	9	1 1
0.0	0.0	ō	1.62	3.03	1.19	1.28		2.5	07.4	1.20	0.61	0.00	1.62	1.03	1.19	3.8	0.0	2.30	3.20	1.20	06.0
H 0.0	0.0	0	0.9	0.0	1,31	2.64		1.72	3.10	1.37	1.96	00.0	8.0	1.0	1.33	E-1	00.0	10.47	8	1.27	1.51
00.00	0.0		0.57	-0.55	1.19	3.82		1.03	1.60	1.37	3.69	00.0	0.57	0.43	1.19	1 4	0.00	93.0	0.40	10.45	200
к 00.00	0.0		0.19	-1.20	-1.20 0.72 0.69	0.69		0.58	1.10	0.R6	1.64	0.00	9.19	-0.55	0.72	1.37	00.0	0.23	-0.10	9.00	1.23
								Year	dare to all for	of least ton		Tradition.									
		П				Total			1		4	1 110000	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			Labour day					
2	Q	1	22	D	rs ²	ů,	90	20	Pa	P9		á	G.	2	a a	2	200	147	P ₉	60	
n.0	0.0	6	0.022	0.003	0.007 0.022 0.003 0.002 0.002	0.002	0.003	0.001	0.000	0.001		0.00	0.018	0.003	0.00	0.00	0.00	0,000	0.000	0.00	
0.0	0.0	6	0.017	0.003	0.00	0.002	0.003	0.001	0.000	0.001		0.005	0,043	0.003	0.000	0.00	0.00%	0,000	0.000	0.603	
0.0	0.0	8	0.013	0.004	0.00	0,003	0.002	0.001	0.000	0.000		0.000	0.000	0.00	0.008	0.005	0.003	0.00	0.000	0.001	
Н 0.0	0.0	010	0.00.9	0.303	0.000	0.005	0.001	0.001	0.000	0.002		0.0nB	0.005		0.011	0.001	0.00	0.003	0.00	0.00	
I 0.0	0	177	-0°004	0.002	0.011	0.008	0.000	0.00	0.000	0.003		0.015	0.003	0.000	0.013	0.010	0.00	0.003	0.00	0.003	
X 0.0	0	39	0.004	0.001	0.006	0.012	-0.001	0.000	0.000	0.003		0.340	00000	0,000	0,008	0.014	0.000	0.001	0.00	0 000	
																			1	000	

Table A-5(Continued)

1	9	29	17	#	8	51	143									
	Α,	9 -0.62	į	ľ		14.51		1		1 1	a	92	84	20	*	
	4	0.69	0.36	1.8	1.30	1.28	0.7			2	0.0	0.0	0.002	0.0	0.0	
	A. 60	-3.10	07.0-	5.11	2.01	0.0	-0.60			30	0.000	0.000	0.00	0.000	0.000	
	P7	2.29	2.8	2.52	1.49	0.91	0.22			23	0.00	0.00	0.00	0.003	0.001	
4.4.4	9	37.51	0.00	0.0	0.00	0.0	0.0			40	0.000	0.000	0.00	0.003	0.007	
Paper or	2	95.0	1.18	1.66	2.35	2.74	96.0		repound	ก้	0.00	0.00	0.005	0.008	0.012	
	27	0.72	6.0	1.07	67.7	1.07	0.72			a ^a	0.00%	0.000	0.010	0.025	0.028	
2	ه. س	1.09	1.12	1.53	0.77	0.32	6.2			2	0.003	0.00	6.000	0.00°	0.003	
ated Ce	22	1.52	1.71	1.33	0.86	75-0	62.0	d Gages		200	0.03	0.018	0.C12	0.007	0.00%	
Pressure, psi, at Indicated Cells	a,-1	0.00	0.00			0.00	0.0	in., at Indicated Gage		a.	0.000	0.00-0	600.0	0.000	-0-00T	
e pair	, ol	0.50	14.	7.0	.87	5.33	80	in. at			•	•	•	•	٠	
	6				1.47 2		2.86	ection,		o.	000010	0.002	0.001	0.002	0.003	
Vertical	es So	0.10	2.80		. ,	3.20		Cal Lec		89	000.0	0.000	0.000	000.	0.000	
I	P	2.64			1.84		75.0	Vert			0.41 0	0.302 0	0.002	0.001	0.001	
	۵,0				0.37		0.37 0			, s	0.000	0.005 0	0.304. 0	0.003 0	0.00	
Total	2	39 37	9 65	0 10	0 92.	15 0	39		1.64.	25	· 43 0	0 500	0 700	0 100	0.770	
		72 0.	8	20	19 1.	2 2	72 0.				00 500	000	.0 600	01 L	and c.	
	<u>a</u>	0	9	9 1.		2	0			ත්	0.0	35 0.0	0	55	× 0.0	
	P2 P3 P5	0.6	0.9	1.0	0.3	-0.2	-0.6			2	0.0	2.00	0.0	0.0	0.0	
	۵,۷	1.33	1.52	1.14	29.0	0.38	0.00			200	0.0	0.017	0.031	0.00	0.003	-
	a.	0.00	0.00	0.00	0.30	0.00	0.00 0.00 -0.65 0.72 0.39 0			P ₁ P ₂ P ₃ P ₁ P ₅	0.303	0.003	0.00	0.00	0.014	-
	t lon	ling	fh.	Ü	bi	H	×				h	ſο.	C)	ber	p.4	1
	Potne	-		٠.							p-4					
	Sov	•									.4					

			1				900	-		Vertic	a Press	Vertical Pressure, psi,	at Indi	at Indicated Cells	i							1
اج	Polat	tion	4	6.	D. Pr	27	2	9	P _Z	a. 60	⁷ C	P10	ard at	۳. د	۵.	Ω ₁ ^{−7}	\$ - S	200	P	80	Po	Pao
10	рđ	4	0.0	0.38	0.55	₹.0	0.39	8.0	0.57	0.00	0.34	0.20	00.00	0.48	0.22	0.36	0.58	-0.36	0.57	-1.61	# · 0	-0. H
		(A)	0.0	99.0	0.22	0.35	0.39	0.0	0.93	0.0	0.3	0.20	0.0	92.0	0.23	0.48	0.58	-0.36	16.0	-1.63	#.º	TE-0-
		U	0.0	0.86	77.0	0.48	0.39	0.72	1.60	00.00	0.51	0.20	00.00	800	0.44	0.50	0.58	÷0.36	1.60	-1.61	0.51	12.0-
		Ω	0.0	1.05	0.4	0.148	0.39	62 3	2.06	0.30	09.0	0.50	0.0	1.15	77.0	09.0	0.58	62 27	2.06	1.31	09.0	-0.3t
		ы	0.0	1.14	99.0	09.0	0.39	9. 12. 13.	2.75	0.20	69.0	0.50	0.00	1.2	93.0	0.72	0.50	90.50	2.73	-1.41	69.0	-0.3E
		Be .	0.00	1.14	0.77	0.72	0.59	0.72	3.21	3.01	1.03	0.43	0.00	1.24	0.77	0.8	0.78	0.30	3.2	1.40	1.03	07-0-
		(5	0.0	8.0	0.87	6.0	0.0	0.54	2.63	7.21	1.20	0.71	0.00	7.0	0.67	1.07	1.17	0.18	2.63	2.60	1.20	0.20
		æ	0.00	0.57	74.0	9.0	2.37	0.54	1.00	3.61	1.38	2.87	0.00	29.0	77.0	1.07	1.56	0.18	1.60	2.00	1.38	2.36
		н	0.0	0.38	0.22	9.0	1.37	0.54	1.03	1.71	1.38	5.53	0.0	0.48	0.22	1.37	1.56	0.10	1.03	0.10	1.38	5.00
		h	0.00	91.0	-0.11	0.75	0.0	0.36	15.0	1.01	1.20	4.51	0.00	0.29	-0.11		1.17	0.0	75.0	-0.63	1.20	00.1
		×	0.0	0.00	-0.21	0.13	0.39	0.36	0.22	1.01	0.80	2.29	0.00	0.10	0.21	09.0	0.58	0.00	0.22	-0.60	98.0	1.74
		H	0.00	00.00	-0.21	0.36	0.20	0.36	0.22	1.0	69.0	1.53	0.00	0.10	-0.2J	0.18	0.39	00.0	0.22	-0.60	69.0	3.1
		» :	0.00	0.00	-0.21	0.24	0.10	0.54	0.52	1.01	0.51	1.23	0.0	0.10	z.o-	0.36	0.29	0.18	0.22	-0.60	0.51	0.72
		je,	8.0	0.00	-0.2I	0.2	0.00	0.36	0.11	1.01	0.34	0.82	0.00	0.10	-0.21	98.0	0.19	0.0	u.0	-0.60	0.34	æ.°
			1																			
							201		Ver	tical De	Vertical Derlection	the at	in. at Indicated Gages	ed Gages							1	
			គ្នា	20	ď	ត្នា	e c	90	20	800	0 Q		r o	N	D ₃	a	D 2	29	22	99	00	
5	rH	~	0.001	0.008	0.001	0.003	0.001	0.00	0.00	0000	0.001		-0.109	0.012	-0.001	0.003	0.000	0.00	-0.002	00000	0.001	
		n	0.002	0.014	0.002	0.003	0.005	0.006	0.001	0.000	0.001		-0.108	0.018	0.000	6.0C3	0.001	900.0	-0.001	0.000	0.001	
		U	0.002	0.022	0.003	0.003	0.003	0.008	0.001	0.000	0.001		-0.108	0.026	0.001	0.003	0.002	0.008	-0.001	00000	0.001	
		¢)	0.003	0.026	0.003	0.003	0.003	0.000	0.001	0.00	0.001		-0.107	0.030	0.001	0.003	2000	600.0	-0.001	0.000	0.001	
		(n T	0.003	0.027	0.00	0.00	0.003	0.009	100.0	00000	0.001		-0.107	0.031	0.002	0.00	0.002	0.00	-0.001	00000	0.001	
		þ.	0.003	0.022	500°5	0.007	0.00	0.008	0.002	0.00	0.002		-0.107	0.026	0.00	0.007	0.003		00000	0.000	0.000	
		O	0.003	0.014	0.007	0.011	0.005	0.006	0.00	0.000	0.002		-0.107	0.018	0.005	0.011	0.00	0.005	0.000	00000	0.000	
		203	0.006	0.007	0.00	0.019	0.00	0.00	0.002	0.00	0.00		-0.10	0.011	0.00	610.0	0.007	0.00	00000	0.000	0.00	
		н	0.014	0.002	0.005	0.02	0.014	0.002	0.000	0.000	0.005		960.0-	0.00	0.003	0.004	0.013	0.005	0.000	00000	0.005	
		4	0.034	000.0	0.003	0.022	0.355	0.001	0.005	0000	0.007		-0.076	0.004	0.001	0.022	g 0.0	0.001	0.000	0.000	0.007	
		het	• 0.186	-0.001	0.003	0.015	0.00	0.00	0.003	0.00	0.007		920.0	0.003	0.00	0.015	0.024	0.000	0.00	00000	0.007	
		,Jø	0.177	-0.002	0.002	0.01	0.0	0.00	0.003	00000	0.007		0.067	0.002	00000	0.011	0.023	0,000	0.001	00000	100.0	
		Y.	0.159	-0.002	0.002	0.00	0.022	0.000	0.002	0.000	0.00		0.049	0.002	00000	0.000	0.021	0.000	0.000	00000	900.0	
		in.	0.130	-0.003	0.03	0.005	0.016	0.000	0.002	0.00	0.005		0.020	0.001	-0.001	0.005	0.015	00.00	0.00	0.000	0.005	
											(Continued)	med)								(5 0	(5 of 11 sheets)	(92

Table A-5 (Continued)

										Verti	cal Pes	Vertical Pressure, psi, at Indicated Cells	at Ind	Cated Ce	118							ı
	Poor	-8007			-		20.	7									Feb	Febound				
Row	Point	tion	2.4	200	m,	التم	۵.'\ ا	9	27	ag O	6	201	₽H 0,	P2	P.	a. 9	27	9	2	A. 80	40	7
9	н	fel)	0.0	19.0	0.33	0.1.8	0.10	-0.36	1.8	0.4.0	69.0	# · 0	02.3	8.0	0.22	0.72	0.39	-0.18	2.18	2.61	0.69	1.03
		B.	8.0	19.0	0.33	0.18	0.30	-0.18	2.41	0.80	0.00	0.43	0.20	8.0	8	0.72	0.59	0.0	2.75	3.8	0.86	1.13
		c	0.0	0.148	0.33	09.0	67.0	8.0	1.95	09.0	2.5	0.82	0.20	0.76	0.3	9.0	0.78	0.18	2.29	2.81	1,20	1.5
		bt	0.0	0.29	0.33	1.43	67.0	0.0	1.49	-0.71	1.20	3.	0.20	0.57	8	1.67	0.78	0.18	1.83	1.50	1.20	2.36
		н	-0.20	0.10	ដ	0.48	64.0	0.0	0.57	-1.41	1.20	2.77	0.00	0.38	0.0	0.72	0.78	0.18	0.91	0.80	1.20	64.€
		×	8	-0.09	-0.20 -0.09 0.11 0.24 0.	0.24	0.20	0.0	0.12	1.7	69.0	0.72	0.00	0.19	0.00	0.18	64.0	0.18	97.0	05.0	69.0	77.1
				İ								and the section to	100									
				*			Cotal							מים ומשלים			Febound					
			ar a	200	a.	దే	es"	200	20	82	O		a rd	av.	a a	a ^a	2	90	22	89	O.	
92	r4	(in)	0.003	0.062	0.303 0.062 0.007 0.003 0.003	0.003	0.003	8	0.00	0000	0.002		0.035	0.043	0.00	-0.006	-0.00	0.cm	0.00	0000	0.00	
		fis.	0.001	0.050	0.00	0.007	00.00	0.021	0.003	000-0	0.002		0.033	0.031	0.007	-0.002	-0.00	0.130	0.003	00000	0.00	,
		B	0.002	0.033	0.012	0.016	0.00	0.026	700.0	0000	0.003		0.034	0.014	0.009	0.007	-0.002	0.008	0.00	0.00	0.00g	
		æ	0.00	0.003	0.011	0.036	0.010	0.013	0.004	000.0	0.005		0.036	0.00	0.008	0.027	0.005	0.005	0.00	00000	0.005	
		1	0.010	0.016	0.009	0.059	0.021	0.000	0.304	00000	0.000		0.0.2	-0.008	0.00	0.050	0.013	0.001	0.00	0.000	9.009	
		bit.	0.013	0.01	0.00	0.031	0.045	0.007	0.002	00000	0.012		0.050	-0.008	0.00	0.00	0.037	0.00	0.00	0.00	0.00	

Continued

1, 1, 1, 1, 1, 1, 1, 1,		100	-	1				1.0	Las		vert	L Lie	vertical pressure, psi,		at indicated cells	6118		Feb	Febound				
0.29 0.11 0.24 0.12 0.24 0.10 0.19 0.19 0.19 0.29 0.29 0.29 0.29 0.29 0.29 0.29 0.2	No.	ē	10073	۵.۲	2	-	2	2	a.e	P _Z	80	A. C.	01	α,	24	D. P.	Δ.3	25	9	d.	8	9	27
0.29 0.11 0.24 0.28 0.20 0.20 1.29 0.29 0.24 0.25 0.22 0.23 0.20 0.24 0.20 0.29 0.29 0.20 0.20 0.20 0.20 0.20	-	-	•	8.0	0.3	п.°	0.24	0.10	0.18	0.80	0.10	0.34	0.20	8.0	0.36	0.00	0.36	0.10	0.18	1.36	0.40	0.51	0.61
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,			υ	0.0	0.29	0.11	0.24	0.10	0.00	5.8	0.30	0.3	0.20	3.20	0.38	0.0	0.36	0.10	0.00	1.49	09.0	0.51	0.61
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			ค	-0.20	0.38	n.º	0.24	0.20	8.0	1.33	0.30	0.43	0.30	0.0	74.0	0.00	0.36	0.20	0.0	1.72	09.0	09.0	9.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			6-1	-0.20	0.38	17.0	0.36	0.50	0.00	1.36	0.00	0.51	0.20	0.0	0.17	0.0	0.48	0.30	0.0	1.72	0.70	0.68	0.6
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			Ba,	8.0	0.38	11. 0	0.36	0.20	00.0	1.38	07.0	0.69	0.30	0.20	24.0	0.00	0.18	0.20	8.0	1.8	0.70	0.86	0.7
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			O	0.0	0.3	0.22	0.78	0.29	0.0	2.03	0.50	0.80	0.51	0.0	0.38	0.11	09.0	0.29	0.0	1.49	0.50	1.03	8.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			313	0.0	0.19	0.22	97.0	0.39	0.18	0.59	-0.10	0.8	0.71	0.0	0.28	0.11	0.0	0.39	0.18	0.15	0.20	1.03	1.12
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			₩	0.00	0.10	1.0	0.36	0.39	0.18	0.23	-0.10	0.77	0.82	0.0	0.19	0.0	0.18	0.39	0.18	69.0	0.20	8.0	23
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			P 3	-0.30	0.0	70.0	0.36	0.3	0.18	-0.11	-0.32	0.69	0.62	0.0	0.0	0.00	0.18	0.29	0.18	0.35	-0.0	98.0	1.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			×	-0.20	-0.09	11.0 -	0.24	0.20	0.18	-0.11	-0.30	54.0	0.20	0.0	0.0	0.0	0.36	0.20	0.18	0.35	00.00	09.0	3.0
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			ធ	0.00	60.0-	-0.11	0.24	0.20	0.18	-0.23	- 5-30	0.3	0.10	0.20	0.00	8.0	0.36	0.30	0.18	0.23	8.0	0.51	0.51
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			×	8.0	-0.09	1.0	JC . O	0.20	0.1	-0.23	•0.30	0.26	-0.11	0.20	0.0	0.0	0.36	0.20	0.18	0.23	00.0	0.43	0.30
Particular Par			×	0.0	0.0	7	0.30	0.0	0.18	-0-3	0.30	0.00	-0.23	0.3	0.00	80.0	0.12	8.0	0.8	0.12	0.00	8	0.50
Paris Pari								10207			Tiles.	-Dectio	-	at indice	ted Gage			Feboure					
0.001 0.002 0.003 <th< th=""><th></th><th></th><th></th><th>ι Ω</th><th>20</th><th>e e</th><th>ត់</th><th>Δ,</th><th>20</th><th>ด</th><th>98</th><th>.0</th><th></th><th>G</th><th>6</th><th>a^r</th><th>ವೆ</th><th>š</th><th>200</th><th>157</th><th>88</th><th>60</th><th></th></th<>				ι Ω	20	e e	ត់	Δ,	20	ด	98	.0		G	6	a ^r	ವೆ	š	200	157	88	60	
1.00 1.00	-	~	•	0.000	0.019		0.003	0.002	0.019	0.00	00000	0.002		0.000	-0.030	00000	-0.018	-0.005	0.012	0.000	0.000	-0.00	
0.109 0.005 0.005 0.003 <th< td=""><td></td><td></td><td>U</td><td>0.001</td><td></td><td></td><td>0.003</td><td></td><td>0.030</td><td>0.002</td><td>0.000</td><td>0.003</td><td></td><td>0.01</td><td>0.005</td><td>0.002</td><td>-0.018</td><td>-0.004</td><td>0.023</td><td>0.001</td><td>0.000</td><td>-0.003</td><td></td></th<>			U	0.001			0.003		0.030	0.002	0.000	0.003		0.01	0.005	0.002	-0.018	-0.004	0.023	0.001	0.000	-0.003	
0.1147 0.0007 0.0009 0.0009 0.0009 0.0001 0.0009 0.0001<			£1	0.001			0.005		0.034	0.00	0.000	0.003		0.011	0.000	0.63	0.008	7.00-0-	0.027	0.00	0.000	-0.003	
0.104 0.009 0.007 .009 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003			840	0.001		0.00	0.005		0.037	0.003	00000	0.003		0.01	0.008	0.005	-0.026	-0.024	0.030	0.00	0.000	-0.003	
0.006 0.002 0.012 0.012 0.010 <th< td=""><td></td><td></td><td>6.</td><td>0.00</td><td></td><td>0.009</td><td>0.007</td><td></td><td>0.032</td><td>0.00</td><td>0.000</td><td>0.00</td><td></td><td>0.012</td><td>0.055</td><td>0.007</td><td>-0.014</td><td>-0.014</td><td>0.025</td><td>0.003</td><td>0.000</td><td>-0.002</td><td></td></th<>			6.	0.00		0.009	0.007		0.032	0.00	0.000	0.00		0.012	0.055	0.007	-0.014	-0.014	0.025	0.003	0.000	-0.002	
0.0056 0.0011 0.0049 0.0012 0.0049 0.0014<			v	0.002		0.022	0.0.7		0.023	0.003	0.000	0.005		0.012	0.031	0.010	-0.004	-0.012	0.026	0.00	0.000	-0.001	
0.058 0.000 0.000 0.000 0.001 0.000 0.001 0.000 0.001 0.002 0.001 0.000 0.001 0.000			*C	0.00			0.00		0.016	5.00°	0.00	0.000		0.014	0.027	0.000	0.298	-0.007	0.00	700	0.000	0.003	
0.053 0.006 0.0071 -0.044 0.006 0.004 0.000 0.0022 0.0021 0.005 0.007 0.005 0.007 0.003 0.000 0.000 0.002 0.002 0.002 0.004 0.005 0.004 0.007 0.003 0.000 0.002 0.002 0.002 0.002 0.002 0.003 0.			ы	0.008			0.098		0.01	0.003	0.000	0.025		0.018	0.009	0.007	0.057	0.003	0.004	0.00	0.000	0.009	
0.051 0.00d 0.0d 0.0d 0.0d 0.00d 0.0			h 3	0.011			0.071		0.008	0.004	0.000	0.022		0.021	0.30	0.0%	0.050	0.027	0.001	0.003	0.000	0.026	
0.050 0.00d 0.039 0.050 0.000			×	0.012			0.047		90000	0.003	00000	0.00		-0.022	0.002	0.002	0.00	0.044	-0.00	0.00	00000	0.000	
0.049 0.003 0.025 0.035 0.005 0.000 0.008 0.000 0.018 0.000 0.013 0.000 0.001 0.005 0.027 -0.002 0.000 0.000 0.000 0.000 0.000			₁ 2	0.011			0.039		0.03	0.002	0.000	0.026		0.0	0.00	0.002	c.ae	0.043	-0.002	100.0	0.000	0.000	
0.049 0.003 0.026 0.038 0.005 0.001 0.000 0.018 0.013 0.000 0.001 0.007 0.021 0.002 0.000 0.000			×	0.000			0.033		0.005	0.002	00000	J90.0		0.019	0.000	0.001	0.012	0.037	-0.002	0.001	00000	0.008	
			F .	0.003			0.025		0.005	0.001	0.000	0.018		0.013	0.000	0.001	0.00	0.001	-0.002	0.000	0.000	0.075	

			1							Ver	Acc. Pre	Saure. P.	Vertica, Pressure, psi, at Indicated Cal	00000								
	1000	1000					6	7									4.5	-				
2	Potat	tion	a. 1	الأيم	۵.	aî."	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	a,c	4	a0	۵.	P.20	a, d	2	D ₄	0,3	PS	Pe	a.	a.	a,	P10
	H	(n)	0.00	0.28	0.11	0.2	0.10	8.0	1.03	0.40	0.52	0.30	00.0	0.36	0.00	0.36	0.10	-0.37	36.	9.69	0.0	17.0
		fh ₁	0.0	0.28	0.11	0.36	0.20	00.0	1.15	0.00	0,60	0.30	8.0	0.26	0.0	0.18	0.50	-0.37	1.38	09.0	0.69	0.13
		O	0.00	61.0	0.22	0.36	0.20	0.00	1.33	0.10	0.77	0.41	00.00	0.19	0.12	0.1.8	0.50	-0.37	3.8	0.30	38.0	0.62
		31	0.0	0.19	0.0	0.36	0.20	0.18	0.58	0.0	0.77	0.61	00.0	67.0	8.0	0.48	0.30	-0.19	8.0	8 0	38.0	0.60
		н	0.0	0.0	0.11	0.7	0.20	0.18	0.35	0.0	0.77	0.62	0.00	00.0	8.0	0.36		-0.19		0.50	98.0	8
		×	0.0	8.0	0.11	0.12	0.10	0.18	0.00	0.0	0.52	0.30	0.0	0.00	0.00	0.24		-0.19		0.50	0.63	0.51
										er to the	el.ec.10	10.00	Section in . at the sections	Sec Gage								
							200										Labourne					
			2	2,5	a	പ്	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.jo	a l	(40	0		ei*	200	6"	ล์	ď	.9	127	88	O	
	-4	b.	0.000	0.036	5.0	0.0	0.303	0.049	9.0	0.000	0.003		0.007	9:00	0.00	0.00	0.006	0.0.5	0.003	0.00	0.00	
		N.	0.003	0.018	0.000	0.007	0.00	0.0	9.3	0.0	0.0		0.008	0.0.8	0.006	0.007	0.003	C. 034	0.00	0.000	0.00	
		o	0.002	0.305	0.011	9.0	0.00	0. J3C	0.0	0.000	0.000		0.00		0.000	0.0	0.00	0.0	0.00	0.000	0.001	
		ber .	0.00	-0.3E	0.010	0.3	0.010	0.022	0.00°C	0.000	0.0.0		0.009		0.00	0.03L	0.00	0.015	0.005	0000	0.00	
		н	0.30	-0.326	J.C.	0.00	0.028	0.015	0.0	0.000	0.017		0.012	0.014	0.007	0.000	0.017	0.00	0.00	0000	0.0	
		Ħ	0.000	-0.021	0.00	0.0	0.043	0.010	0.00	0.000	0.03		0.016	0.0	0.003	0.00	0.00	0 00		8	000	

	22	ส.	2.0	o.3	0.51	0.62	0.21								
	90	0.60	09.0	0.69	0.77	0.77	0.43	1		20	-0.007	-0.00	00000	0.00.0	0.034
	80	0.20	0.30	0.10	0.00	0.0	0.10			Eg	0.000	0.000	0.000	0.000	0.000
	F7	1.03	1.03	35.0	69.0	0.16	0.23			L _Q	0.00	0.006	0.006	0.005	0.005
	P6	0.0	-0.19	0.0	00.00	0.0	0.0			90	0.036	0.019	900.0	0.001	0.00
	P ₅	8.0	0.00	0.10	0.20	0.30	0.00		hebound	ď	0.009	0.00	0.01	0.02	0.036
	27	. S.	0.2¢	× .0	0.36	6.0	0.24			aª.	0.005	0.001	0.033	0.044	C.004
1	40	0.00	0.00	0.0	0.0	0.00	0.0			63	0.008	0.009	900.0	0.000	0.003
Cated C	22	0.19	0.19	61.0	0.19	0.00	0.00	5000		30	0.035	0.023	0.005	.000	.004
at Ind	4	0.0	0.00	8.0	0.0	0.0	0.0	Yndl care		24	0.00	0.00	0.005	0.00e	0.010
ure, pet	10	a:	0.21	0.32	0.51	0.62	্য	120.00							
Vertical Pressure, psi, at Indicated Cella	٥٥	0.52	0.62	0.61	0.69	69.0	0.35	effection.		0	0.003	0.005	0.010	0.000	0.0.1
Verify 1	199	0.10	0.50	0.30	0.20	0.20	0.10	io:		B _G	0.000	0.000	0.000	0.000	00000
	P7	25.0	0.90	0.83	0.58	0.35	0.12	Ver		22	0.00€	0.00	0.00	0.006	
	9	3.0	61.5	0.00	0.00	0.00	0.00			9	0.051	0.034	0.023	0.016	0.011
Post	e ⁱ c		•		0.20	3.20	0.00		0.0	5	0.003	0.005	0.008	0.015	0.030
	a-1	0.24	0.24	0.24	0.36	0.24	0.00 0.00 0.24 0.00			ವ ²	0.00.0	0.022	0.024	0.035	0.ens
	۵,۳۱	0.00	00.00	00.00	00.0	00.00	0.0			5	0.007	0.008	0.00	0.00%	0.002
	2	61.0	0.19	C.19	0.19	0.00	0.0			50	.001	0.009	0.001	0.00%	0.010
	a, t	00.00		0.00	0.00	0.0	0.00			2	0.002	0.0%	0.003	0.00	0.008 -0.010 0.002 0.015 0.030
	Lion	jia)	fh ₄	U	22	1-4	345	1	- 1	,	Bu	O	32	ы	bd:
	Potat	p-4									g-4				
	ROM	6									0				

(9 of 11 sheets)

		10	0.10	0.2L	0.2	0.31	0.41	0.2									
		20	0.43	0.52	0.52	09.0	0.52	0.35			8	0.000	-0.005	-0.004	0.000	0.002	0.00
		es.	0.30	0.50	0.50	8.0	0.10	-0.10			30 00	0.000	00000	0.000	0.000	0.000	0.000
		P 2	69.0	69.0	69.0	97.0	0.23	0.00			D _T	0.000	C.00k	0.000	0.006	0.00	0.00
	t.nd	8	-0.37	0.00	0.00	0.00	0.00	0.00			99	0.m88	0.00	0.00	0.000	0.000	-0.003
	Kebo	W.	0.00	0.10	0.10	0.10	0.20	0.10		Febound	24	0.007	0.007	0.000	0.012	0.017	0.00
		a,	0.24	0.2	0.24	र ०	0.3	0.24			ನ್	0.008	0.011	0.015	0.023	0.026	0.016
24.55		0,67	17.0-	0.00	00.0	8.0	0.00	-0-11			a a	0.00	0.00	0.007	0.006	0.00%	0.002
dicated		2,04	0.19	61.0	0.19	60.0	0.09	00.0	ed Gages		22	0.033	0.028	0.000	C. C.	0.00	0.00
it at in		a.	00.00	0.0	0.0	0.00	0.0	80.0	at Indicated Gares		6	0.002	0.000	0.003	0.90	0.005	0.007
Stare, Fa		10	0.10	0.2	0.21	15.0	0.47	200	18. 07								
Sec. Tres		n _e	15.0	0.13	0.53	0.51	0.43	0.26	act ton		0	0.003	0.00	0.00	0.021	0.021	0.03
Ser		a ^{no}	0.20	0.10	0.10	-0.10	-0.20	-0.20	Vertical Le		, ap	000.0	0.000	0.000	0.000	0.000	0.000
		P	69.0	69.0	99.0	94.0	0.23	00.00	Ver.		5	0.394	0,000	o.ore	0.008	J.00*C	0.00%
		o, c	-0.37	3,30	0.00	0.00	00.00	00.00			12	0.138	() ()	0.0%	0.3		0 - 26-3
	Total	ni ^c	0.00	01.0	07.0	0.10	0.3	0.00 0.00 0.00 0.24 0.10		10:01	ď	0.001 0.021 0.005 0.003 0.002	0.072	100	0.007	7.022	0,000
		a, 2	0.24	0.24 0.24	2.24	0.26	0.24	0.24			á d	0.003	0.00%	0.000	0.013	0,023	0.011
		~	0.00	0.17	0.11	0.11	0.11	0.00			-	0.005	30.0	0.007	0.00%	7,005	0,000
		25	0.19	0.19	0.19	0.09	60.0	0.0			2	0.02	0.016	0,00R	0.001	-0.00k	.00.0
	1	a ⁻¹	00.00	00.00	00.0	00.0	0.00	0.0			5 ⁷⁴	0.001	0.00	0. 10	0.003	100.0	0.00
ľ		tton	8-1	No.	p m	200	ы	×	, ,		,	g=2	lin.	67	×	8-4	×
		Potne	el									14					
		Row	10									10					

Table A-5 (Concluded)

2	0.0	8.0	8.0	0.10	0.10	Ø.0	0.2	Ø.0	8.0	0.10	0.10	0.10	8.0															
8	0.17	0.17	0.26	0.33	0.35	0.35	0.43	o.33	0.35	· 3	0.17	0.17	8.0			9	-0.006	-0.006	-0.005	-0.005	-0.005	-0.00	0.000	0.002	0.000	0.043	0.042	
8	0.50	0.30	0.30	0.30	8	0.2	8.0	00.00	0.0	0.0	0.30	8.0	0.0			æ	0.000	0.000	0.000	00000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
1	0.33	94.0	0.50	0.58	0.58	0.58	0.35	0.23	0.12	0.12	0.00	0.00	0.0			4	0.000	0.00	0.000	0.003	0.00	0.00e	900 0	0.00	0.003	0.000	0.00	
اعم	9.0	0.00	0.0	0.18	0.0	0.0	8.0	0.18	0.0	0.0	0.0	0.00	0.16	İ		90	0.001	0.007	0.061	0.096	0.032	0.000	0.01	0.00	0.000	-C.002	-0.003	
	0.0	0.0	0.0	0.00	0.0	0.10	0.10	0.10	0.10	0.0	0.10	0.0	0.0		Febound	as a	0.006	0.007	0.007	0.007	0.007	0.008	0.001	0.005	0.00	6m.0	0.018	
4	0.12	27.0	0.12	0.2	0.2	0.24	0.3	2.0	2.0	0.12	0.12	0.0	8.0			.S*	0.007	0.007	0.007	0.008	0.00	0.013	0.017	0.000	0.007	0.012	0.00	
4	0.00	8.8	0.00	0.0	0.0	9.0	0.0	0.00	0.00	11.0-	17.0-	0.0	0.00			6	0.00	0.000	0.003	0.003	0.00	0.005	0.00	0.003	0.000	0.00	0.000	
2	0.00	0.0	80.0	0.19	61.0	0.19	0.0	0.0	0.00	0.00		0.00	0.0	Sec.		200	0.018	0.023	0.09	0.00	0.001	0.026	0.01	0.007	0.00	0.003	0.003	
4	-0.20	-0.20	-0.30	-0.20	0.50	0.50	0.0	-0.20	0.50	-0.20	0.30	0.00	0.30	Vertical Seffection, in. at Indicated Occasion		ก็	0.000	0.00	0.00	0.00	0.00	0.002	0.003	0.03	0.00	0.00	0.005	
9	9.0	0.00	0.0	0.10	0.10	2.0	2.0	0.21	0.21	0.10	0.10	0.10	0.0	4		•												
٥	0.17	0.17	92.0	0.35	0.35	0.35	0.43	0.35	0.35	0.36	0.17	0.17	0.00	Cotton		6	0.00	0.000	0.003	0.003	0.003	0.005	0.00.0	0.000	0.037	0.031	0.050	
	0.10	0.10	0.20	0.10	0.10	0.10	0.10	0.10	01.0	-0.10	-0.10	0.10	0.10	100		6	0.000	0.000	0.000	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
4	0.23	¥.0	97.0		94.0	9.40	62.0	o.u.	0.00	00.0	0.12	0.12	0.15	Ver	1 1	4	0.001	0.002	0.003	0.00	0.00	0.007	0.007	0.005	0.00	0.003	0.000	
0	0.0	0.0	0.00	0.18	0.00	0.00	8	0.18	0.0	8.0	00.0	00.00	0.18			\$0	0.023	0.031	0.103	0.140	0.00	0.073	0.038	6.0.0	0.044	0.042	0.041	
4	9.0	0.00	0.00	8.0	0.0	0.10	0.10	0.10	0.10	0.0	0.10	0.00	0.0		pre	.,,	0.001	0.000	0.00	0.00	0.00	5.003			0.013	0.034	0.03	
	21.0	o.12	0.12	0.24	0.24	0.24	0.24	0.2	o.24	0.12	0.12	0.00	0.00			5	0.002	0.002	0.00	0.003	0.003	0.000	0.02	0.035	0.012	0.007	0.00	
-1	9.0		0.00			0.00										<u>a</u>	0.001								0.000	0.001	0.000	
~	0.00	60.0	6.0	0.19	0.19	61.0	60.0					00.00				2	0.011	0.006	0.07	0.017	10.0	0.009	0.00	0.000	-0.00	0.00	3.0	
	0.0	0.0	90.0								0.00	0.30	8.0			e l	0.000						0.003	0.113	0.00	0.00	0.004	
1 1	•	υ	A	813	۵.	0	×	H	4	w	ы	×			, ,	•	•	U	۵	•	•	•	æ	5-4	ני	×	,a	
12	-																н											

wiltiple-sheel Heavy Gear Lad Flexible Pavement Test, Static Instrumentation Loading Data

Item 3; Load Condition: 30 hips per elect, Twin Tunden, 100 pai

Post 4

		20	0.18	0.0	00.0	0.18	0.00	0.00	0.00	. 80.	99.0-	-0.57	-0.0-	16.0	-0.75	-1.13																	
		٥	0.70	0.53	0.53	0.61	0.70	1.3	2.27	3.42	4.55	8	80.5	2.07		Ċ			9	0.002	0.002	0.000	0.002	0.00	0.002	0.002	0.003	0.005	0.007	0.009	0.009	0.008	0.007
		88	0.62	0.31	0.41	0.41	0.43	0.62	1.8	2.35	2.0	3.08	3.74	0.41	-0.30	-0.83			8	0.001	0.001	0.00	0.001	0.001	0.00	0.000	0.003	0.003	0.003	-0.002	0.000	0.00	0.001
		12	9.0	1.06	3.48	1.69	3.8	2.64	3-17	3.59	2.70	3-38	2.85	2.53	2.11	1.48			- P	-0.002	-0.003	-0.002	+0.303	+0.00L	300.0	0.006	0.008	0.005	-0.004	-0.002	+0.001	-0.00T	0.000
	nd	9	0.79	7.5	2.37	3.27	1.85	6.89	8.00	8.10	99.9	3.27	7.5	0.79	0.34	0.0			90	0.001	0.003	0.004	0.005	0.035	0.50	0.003	0.000	0.00	0.000	0.000	0.000	-0.00	-0.00
	Nebor	a ^{se}	-0.17	-0.17	-0.17	-0.17	-0.17	-0.17	-0.17	-0.17	-0-17	-0.17	-0.17	-0.17	-0.17	-0.17		Pebound	ด้	0.002	00000	-0.001	-0.003	-0.002	-0.00g	-0.076	-0.071	0.002	0.002	0.042	0.038	0.033	0.00%
		3	0.0	-0.12	-0.23	-0.12	0.00	0.48	17 18 19	2.73	4.0	8.	5.47	5+35	2.3	3.09			ត្ត	0.003	0.003	0.003	0.004	8.0	0.005	0.008	0.009	0.011	0.021	600.0	0.008	0.007	0.00
Cells		ger.	-0.3	0.25	-0.18	0.0	0.42	1.89	(.87	-10.13	7.2.71	12.71	88.5	6.53	3-17	2.50			62 63	0.000	0.00	00000	0.000	0.000	0.000	0.000	0.000	- 0.000	0.000	0.000	0.000	0.000	0.000
dice.ed		40	0.33	16.0	3.15	1.98	2.43	3.43	4.36	8:	5.23	19.4	3.89	3-53	8.8	8	Indicated Gare		E4	0.008	0.022	0.027	0.019	0.00	0.00	0.015	0.011	0.005	0.003	+0.00	0.000	0.000	-0.002
1. 0: Indi		ar4	-0.28	0.55	3-13	97.6	7.65	10.14	11.61	2.3	200	7	6	1.36	26.0	0.65	- Patron		12.4	0.031	0.0.5	0.071	0.0	0.072	0.275	0.000	0.038	0.00	-0.005	-0.002	-0.0m	-0.0mg	-0.010
Sure, ps		10	0.55	0.38	0.38	95.0	0.38	0.38	0.47	0.38	-0.2	61.0-	-0.56	-0.50	-0.37	0.0	9																
Cal Pres		0	8	0.86	0.88	0.0	8	1.66	2.62	6 m	8.	3.40	2.60	5.4.	4-73	3.32	101000000000000000000000000000000000000		C.	0.000	0.300	0.000	0.000	100.0-	0.00	0.000	0.00	0.303	0.005	0.00	0.007	0.005	0.000
Tert		<u>م</u>	8	0.72	0.82	0.62	80.0	1.8	2.24	2.3	2.4	3.4	2.14	0.8	0110	41,0-	Vertical P		ac)	2,700	0.000	2,000	0.00	0.000	0.000	0.00	0,002	0.002	0.002	-0.0C	0.001	0.000	0.000
		2	0.0	78.3	1.48	1.69	8	2.62	3-17	3.59	3.70	3.33	2.83	2.53	2.11	7.10			12	-201-	-1,70A	-0.00	200.0-	-0.001	0.0	0.003	0.003	0.000	-0.003	-0.003	-0.0nl	0.00	-0.005
	7	9	0.58	1,13											0.23				9:	0.000	0.000	0.003	0,00%	0.00	0.003	0.002	0.00	0.3	-0°00	-0.001	-0.00	-0.00	-0.002
	0.	a.	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	2,17	0.17	+0.1"	+0.17	-0-17	+0.17		10.01	2.5	0.003	2000	0.000	0.000	-0.30	0.000	-0-075	-0.00	0.013	0.023	0.03	0.039	0° m34	0.0
		27	0.83	0.71	0.0	0. T	0.83	1-32	5.3	3,5	10.07	5.45	5.30	5.35 5.15	2	3.90			rs 1	0.003	0.071	0.301	0.072	0.302	0.003	0.0	0.00	0.000	0.000	0.30	0.0	0.03	0.000
		n.**	-0.43	-0.43	-0.35																0.000	0.000								0.000		0.000	
		25	1.22	7.7	8:	2.44	2.8	3.90	10.0	8-4-8	5.45	3.30	96.4	20.7	3.42	2.47			22	0.00	0.000	7750	0.026	0.017	0.006	0.022	ംവെ	0.003	0.000	0.00	-0.003	-0.003	0.0
		d.	0.33	1.38	8.	9.8	ල ව	10.47	12.44	13.03	10,14	5.16	2	2.21	1.75	1.16			le i	0.028	0-032	0.048	0.05	0.061	0.042	0.047	0.00	0.00	-0.00	-0.015	-0.019	-0.021	0.023
		tion	~	en.	Ð	£4	8n7	b	d	*	p. 4	h3	æ	ωĴ	y	×				d	(E)	U	43	61	jn.	۲۹	tr	6-4	*3	arc	ы	> :	15.
	-	Polnt	-4																	p-4													

(Continued)

	0,00		-0.0%	0.73	-0.89	-0.85	-0.85	-0.75	-3.75	11.99	7.12	1.68	29.06	9.28	1.32	94.0																	
	04	1	0.78	0.70	3	1.40	1.92	3.15	4.72	6.12	6.82	95.9	18.4	4.11	3-32	1.92		0,	0.003	0.003	0.003	0.003	0.003	0.000	0.038	0.022	0.016	0.018	0.005	0.024	0.012	0.00	
	90		57.4	-1.63	-1.63	-3.43	-0.61	3.16	4.89	4.68	7.33	2.44	-0.10	-0.43	-0.20	-0.41		88	0.003	0.000	0.002	0.002	0.003	0.00	00.0	0.005	0.005	0.00	0.003	0.000	0 200	,	
	B.	7	07.1	1.58	2.32	2.0	3.00	3.80	23	- 33	3.69	2.93	2.11	1.79	1.48	0.84		D,	0.000	0.003	0.007	0.00.0	0.002	0.003	0.000	0.007	0.00	0.005	-0.001	0.000	00000	-0.00	
	Pag.			đ.	7.08	9.36	10.50	11.85	12.87	8.35	3.8	1.75	0.79	0.56	0.34	0.23		9 _Q	0.000	0,009	0.009	0.009	0.000	0.00	0.00	0.002	0.000	0.000	-0.001	-0.00	-0.001	-0.001	
	o.	9	3	2.08	2.06	5.06	2.06	2.08	1.9	17:57	2.60	80	3.69	+1.39	-0.35	-0.35		Pehotind De	0.008	0.005	0.005	0.006	0.007	0.012	0.022	0.034	0.048	0.055	0.050	0.046	0.000	0.00%	
	a,ª	1 90	200	8	0.60	0.83	1.07	3.00	a:	4.40	5.11	5.11	4.0	3.33	2.73	1.55		30	1.002	0.000	6,00	6	0.000	0.010	0.023	0.015	0.01	0.022	0.006	0.007	0.003	0.003	
Ce115	2,0	0		-0°M	0.17	0.77	1.89	8.76	11.69	10.40	16.07	7.40	1.72	0.77	0.35	-0.08		E 02	ن. ن. سکه	0-000	0.000	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0000	0.000	
at indicated	A, CV	î	1	N 19	2.5	3.16	3.77	4.50	8	6.4	4.38	3.23	2.56	2.8	1.58	0.9	ed Cage	50	0.000	0.007	0.033	0.031	0.009	8.0	0.025	0.000	0.00	0.002	0.000	-C.001	-0.001	-0.002	
1 at 12	a.	8		W.50	7.5	8.47	9.10	10.50	10.90	6.45	2.58	8	-1.39	0.18	0.00	-0.19	t Indies	GT	0.007	0.116	0.107	0.137	0.19	0.117	0.0%	0.033	0.031	0.003	-0.00	-0.005	-0.00£	-0.00	
Fare Da	O.F.	98		0.10	-0.26	-0.26	-0.38	-0.18	-0.13	12.56	7.69	5.73	29.63	3.8	. 88	1.13	155																
Vertical Pressure	ů,	0 60		10.0	2	1.57	5.00	3.32	6.9	8	8.	6.73	8.	28	0:	2.09	Teflection in.	e.	0.00	0.002	0.003	0.03	0.001	00000	00000	0.00	0.012	0.016	0.013	0.012	0.000	0.000	
Vert	(I)	6		0.0	rt 0	-0.51	# · o	8	3.8	5.50	33	3.36	3.62	7.52	0.72	0.52	Vertical	ar.	0.000	0.000	20000	0.000	0.00	0.003	0.00	0.00	0.00%	0.003	0.000	0.001	100°C	0.00	
	74	. 3	10.4	60.7	15 to 15 to	2.72	3.17	8	33	7.1	G.,	8.	2.53	1.90	1.59	6:0	2	7-	0.000	0,303	0.007	2.000	0.00	0.0	0.000	0.007	0.39k	0.00	-0.001	00000	000.0	-0.001	
	a 6.50	1 114	0	\$ (7.92	67.6	10.73	12.Cg	13.10	8.58	10.	8.	8	0.79	0.57	5.25		92	0.00	600.0	0.009	0.75	0.000	0.00	0.30%	0.002	0.000	0.000	-0.002	-0.003	-0.001	0.03	
4	σ,												57.98					0 44	0.000	0.274	C. 20%	3, 70%	0.00	C.717	38	0.032	0.046	93	0.048	0.044	0.038	0.00	
	Ω,	627.0	7	9	0	8.0	1.19	2.14	3.33	4.52	5.23	5.23	0) +4 + 2	W . T.	£2.	1.00		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1							, C.								
	۵,	8	96	0.50	0.00	1.46	2.53	57.6	12.39	11.09	20.76	27	2.68 2.41	2.20	7. F.	0.53		0	JUL "														
	۵.	3																25	0.022														
-	α, ···	85	1	9 6	*0.	9.8	9.6	11.00	11.52	ਹ ਂ	3 - 2 - 5	1.57	-0.63	0.1	9.56	0.37		n n	5.073	0.162	0.153	0.183	0.2kn	0.161	0.112	0.079	0.060	0.049	3.042	0.00	0.338	0.334	
	1004	,	a	a, e	د.	П	5-3	fits.	17	22	9-4	77	act	L	90	P.			a	gez	υ	(.)	513	BL:	O	30	p=4	P-3	Set:	1-3	¥	P5	
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(2 of 15 sheets)

Table A-6(Continued

11	0	0	40	90	0.1	el	9	0	Q ₁	0	0	0	4											1			
	17.	0.0	0.1	-0-8	0.0	2	-0.66	0.0+	0.0	60	1.6	0.0	7.9				0	0.1			~		~	•		0	
	0	0.88	2.63	11.1	5	6.12	6.21	1.66	4.61	3.68	6.47	6.20	4.81			00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.000	20.0	0.320	1000
4	æ	-1.52	4.4	3.50	2.45	4.89	3.6	0.51	37.2	1.48	6.54	3.36	0.81			89	0.001	0.002	5.003	0.003	0.003	0.003	0.017	-0.00	-5.00L	-0.00	AO. Or
6	12	2.00	3.38	3.80	8.8	3.59	2.03	2.85	3.91	3.91	2.20	8.8	2.12			20	0.003	0.006	0.008	0.000	0.003	0.001	0.006	420-0	0.01	0.007	0.003
pq.	2	3.6	6.63	11.17	200	70.4	1.58	14.33	15.91	12.52	2.27	2.5	3.12			36	0.000	0.00	0.003	0.00	0.000	-0.001	0.023	+0.004	-0.002	200.0	0.000
moque.	5	00.0	00.0	0.0	63.0	5.19	0.00	00.00	0.0	0.34	0.00	8.0	2.5			,	0.003	0.008	0.015	0.00%	0.034	0.042	0.003	0.093	0.035	0.047	0.05.5
	-2	97.0	3.78	3.00	1.40	5.13	5.58	80.0	2.97	3.68	12.7	12:0	3-32			ă*	0.000	0.007	0.010	0.022	0.022	0.000	0.0	0.025	O.OLL	5.mp	0.00
a		38	6.01	1.08	8.59	b.0%	9.70	1.63	6.50	6.87	60.7	5.50	1.03			£ 2	0.000			0.000				0.000			,
	6						3-65								Sages	22	0.023							0.025			
E)							85.14								Indicate	.5*	0.07										
	30						99.0								- B.	1 1					•	•			4	•	4
	0			·			6-47 -0		·			•			10 T	0.	000.0	300	8	0.007	600	120	5003	0.003	0.00A	C.OLL	m.B
77	1														Ten.								•				
n	3	1.0	E .	80.3	90	6-52	2	0.0	3.9	8	8.9	2.8	0-30		1-1cm	67) 80)	0.00		0.003			6.00	0.0	-0.010	0	0.0	-0.0
a	1	2.3	3.70	4-12	27	10.0	3-17	5.8	50.	9	3.59	8	2.2		A	H	^.03	0.010	2.010	0.00	0.00	0.003	0.016	20.0	3.023	0.000	0.003
9	9	2.2	10.50	12-74	B. B.	4.63	63 - 25	23	15.80	2.0	4	1.90	7.07			5.2	0.03	0.00	0.003	0.001	0.000	-0.001	600.0	-0.00	-0.022	-0.003	-0.034
0		0.13	0.18	C . 1 G	0.87	5+37	0.13	0.18	0.18	0+28	T:	(C)	m -1 -1			ı.	0.000	0.00%	0.012	0.022	20.0	0.039	50000	2:032	0.027	0.039	0.047
a	7	09.0	3+93	3.21	1.52	5.23	5-70	8.	5.07	3.53	ξ.; -2	17.72	25.50			d'	0.001	C.30M	0.011	0.013	0.013	0.387	C.30A	-0.302	-0.003	-0.003	-0.005
a.	-	3.28	3.37	13-24	10.65	5.92	1.85	3	6.79	6.4	13.02	5.33	8			۵				0°0				0,000			0.000
a	2	6.46	79.4	5 23	5-35	16.8	3.89 11.85	2.30	3	3.30	3 + +2	99.0	8::			2	0.023	0.027	0.011	0.006	0.303	0.000	₹60°C	0.000	0.000	0.312	7,014
10.		7.10	7.3	2,35	3.75	4.24	2.03	6.82	7-2-7	02.4	26.2	0.64	01.0			ڻ د د	. A			0.024				3,346		.0.0	0.722
-800	non	b1	5	×	ы	Ь	340	(hi)	£°	×	14	13	×	•	,	, ,	[a1	ť°	Br*	5-6	h ₂	×	Sent	ť.	25	F-4	*3
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2 3 6 2	2 3 6 2	1	1	1	2	9		1	ap.	0	130	5	25	er l). 10	24	26	22	80	0	22
E 5.90 2.31 0.51 0.59 0.00 10.84	2.31 0.51 0.59 0.00	0.59	0.59	0.59	0.00 10.84	10.86		5.00	-0.71	8	-0.57	5.53	1.82	0.00	8:0	8.0	10.01	1.79	-1.33	0.79	-0.29
3.90 6.01 1.56 0.00 15.13	3.90 6.01 1.56 0.00 15.13	6.01 1.56 0.00 15.13	6.01 1.56 0.00 15.13	.56 0.00 15.13	19.13	19.13		3.37	2.55	2.62	-0.33	87.78	3.41	5.50	1.42	0.00	14.90	3.26	1.93	2.36	-0.19
4.51 14.50 2.65 5.00	4.51 14.50 2.65 5.00	2.69 2.69 5.00	2.69 2.69 5.00	00.0	2.00 165	10 10 10 10 10 10 10 10 10 10 10 10 10 1		3.80	5.50	3	95.0-	9.40	8	14.09	2.61	0.00	16.35	3.69	1.86	3.76	-0.38
4.63 8.59 3.92 0.52	4.63 8.59 3.92 0.52	8-59 3-92 0.52	8-59 3-92 0.52	.98	0.52 13.55	13.55		3.80	20	2-42	2.07	6.54	4.20	8.08	3.48	64	13-32	3-59	3.66	5.16	10 10
4.14 17.67 4.51 10.23	4.14 17.67 4.51 10.23	17.67 4.51 10.23	17.67 4.51 10.23	.51 10.23	10.23 4.74	4.74		3.59	7.13	5.30	23.72	2.50	3-65	17.36	12.4	10.23	4.51	3.48	6.51	6.0	63.90
3-53 13.06 4.87 0.00	3-53 13.06 4.87 0.00	13.06 4.87 0.00	13.06 4.87 0.00	.97 0.00	0.00 2.2	13		3.25	8.3	100	0.28	1.13	8	12.55	£9.4	00.00	2.03	8.8	4.07	11	97.0
2.5C 0.430.17	2.5C 0.430.17	0.437 -0.17	0.437 -0.17		-0.17 190	190		SG: 1	0.32	2.7	-0.20	5.33	2.80	6	6.0	9.6	06.7	2.7.	1.32	1.75	· i . O3
3.54 2.23 2.13 -0.17	3.54 2.23 2.13 -0.17	2.23 2.13 -0.17	2.23 2.13 -0.17	-13 -0.17	-0.17 16.93	16.93		8	3.67	0	F4.0-	80	3.66	2.57	2.37	8	16.93	3	8.58	k.63	94.0-
3.5~ 2.40 2.85 -0.17	3.5~ 2.40 2.85 -0.17	2.50 2.65 0.17	2.50 2.65 0.17	-65 -0.17	-0.17 12.19	12-19		*.13	3	6.23	d.	8.00	3.66	P. Ca	3.09	0.0	12.19	8.1	5.39	6.2	-0.19
3.05 3.09 3.20 -0.27	3.05 3.09 3.20 -0.27	3.09 3.20 -0.17	3.09 3.20 -0.17	-0.17	-0.17 7.16	7.10		3-49	3.60	5.R2		2.3	5-17	(F) -B' + (F)	3.54	00.00	7.66	3.38	6.51	6.82	60.0
2.32 1.20 1.02 -0.17	2.32 1.20 1.02 -0.17	1.20 1.08 -0.17	1.20 1.08 -0.17	-0-17	-0.17 1.70	1.70		2.03	2.85	6.47	-1.33	0.37	2.44	1.54	3.35	0.00	1.70	2.7	3.76	6.47	-0.09
1.59 -0.17 2.52 -5.17	1.59 -0.17 2.52 -5.17	-0.17 2-51	-0.17 2-51	-0.17	-0.17 0.91	0.91		8	C.23	8.	-0.73	-0°C	1.72	-0.17	2.63	0.00	16.0	3.1	1.12	8.4	-0.38
					10.00			741	S Sesson		3,50	st indicat	en Gages								
Δ,	Δ,	Δ,	*:	2 8 E	. ·		9 1	4	8	0.00		ar	20	4	3	2.5	P.	22	8	0	
# 0.196 0.032 0.000 0.016 0.016 0.17	0.032 0.000 0.004 0.004	0.032 0.000 0.004 0.004	7,000 0,001. 0,001.	0.01	0.01	£ .		D. 308	0.000	0.000		E 444	20.0	0.000	0.003	0.001	0.00	0.007	0.00	-0.00%	
0.025 0.000 0.000 0.000	0.025 0.000 0.000 0.000	0.025 0.000 0.000 0.000	0.000 0.000 0.000	0.010	0.010	.00.		3. 30	0.003	0.00		0.132	Ğ.	0.000	0.009	0.007	D.0.0	0.005	0.003	-0.372	
0.01 0.00 0.314 v.019	0.01 0.00 0.314 v.019	0.01 0.00 0.314 v.019	0.300 0.314 1.029	670	670	A 0.0		0.027	0.0%	0.03		0.0	300	0.000	0.003	0.445	0.00	0.013	0.00	*0.0CI	
0.020 7.0m 0.026 C.M.	0.020 7.0m 0.026 C.M.	0.020 7.0m 0.026 C.M.	1,000 0,00 0,000 0,000	C. (723	C. (723	3.0%		0.00	2.78	01313		0.037	0.000	0.000	.045	2,030	0.002	500.0	0.00%	0.000	
3-305 3-700 0-026 7-34/	3-305 3-700 0-026 7-34/	3-305 3-700 0-026 7-34/	7.000 0.00 0.000	2.047	2.047	10010		0.00	0.3%	0.025		0.017	£ 3	0.000	.045	0.044	0.00	0.00	0.00	0.011	
0.003 0.000 0.004 0.047	0.003 0.000 0.004 0.047	0.003 0.000 0.004 0.047	0,000 0,024 0,047	0,087	0,087	3.36		0.3%	0.00	8		0.007	000	0.000	0.0	C. 36	98	0.003	0.004	0.00 E	
5. 4" 1,300 c. 110 1,000	5. 4" 1,300 c. 110 1,000	5. 4" 1,300 c. 110 1,000	7,300 c.7; 7,720	1.020	1.020	9.75		. 0:	Se C	+0.004		0.142	0.043	00.00	0.007	-0.007	0.025	0.006	0.00	-0.007	
0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.000 0.000 0.000	0.000 0.020 0.062	2,04.0	2,04.0	0.0%		33	0.3%	·0.03		0.000	300.0	0.000	0.017	0.025	0.007	0.007	0.007	*0.00	
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0.00 0.00 1.003 1.000	0.00 0.00 1.003 1.000	0.00 0.00 1.003 1.000	0,000 1,003 1,080	2.08c	2.08c	0.002		0.00%	3	0.034		5.00g	0.00	0.00	0.000	0.633	0.000	40°008	0.007	0.023	
200°C 020°D 000°C	200°C 020°D 000°C	200°C 020°D 000°C	200°C 020°D 000°C	J. Con	J. Con	0.00		5.003	0.005	0.0		0.000	0.63	0.000	0.027	0.00%	0.00	-0.00	0.00	0.01	
0.000 0.015 0.002 -	0.000 0.015 0.002 -	0.000 0.015 0.002 -	0.000 0.015 0.002 -	20000	20000	-0.00g		-0.00	0.305	0.0.0		40.055	0.002	n.300	0.012	0.005	0.000	-7,000	0.00	0.0	

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Table A-6

		10	8	0.00	0.86	000	0.78	89										
		A,	1.57	12.37	100	1,55	8	1.63				O	0.00%	0.026	0.00	0.035	2000	0.038
		8	2	8	8	A PO	8	,3.0				B _Q	0.00	0.00	0.000	0.00	2000	0.005
		F7	95.05	3.80	8	3.50	2	3-8				n 1	0.0	0.033	0.00	0.017	000	0.00
	nd	μ,ο	14.11	37,70	12.67	8,12	8.	8				56	0.026	0.006	0.00%	0.002	100.0	00.0
	Febound	D.	000	8	3	00.0	0.0	0.3			Febound	25	-0.010	0.012	0.039	0.058	0.073	0.081
		a,7	0.83	8	2.49	2.8	2.85	2.14				ď	0.00	0. 19	0.023	0.063	0.019	0.014
Sell's		Δ,	0.69	1.89	8	2.36	2-12	નુક ્ 0				4	000.0	0.000	0.000	0.000	0.00	0.000
dicated (2	2.14	3.29	3.41	2.92	2.29	17.1		ed Gazes		c c	0.048	0.025	0.015	0.007	0.00	0.002
1. at In		۵,۲	8	8	2.40	11.11	0.37	0.0		Indica		P ₁	0.136	0.03	0.039	0.025	0.017	0.013
sure re		10	0.0	60.0-	0.85	1.22	24.0	16.1		in. a								
Vertical Pressure, psi, at Indicated Cells		٥,	1.57	4-37	5.68	6.55	6.39	4.63		Vertical Deflection, in. at Indicated Gazes		60	0.003	0.01A	0.023	0-034	0.043	0.036
Vert		g;	0.51	86-	8	7.53	3.97	1.52		tical De		DB	0.00	900.0	0.009	0.008	0.007	0.005
		ρ.	-2.85	3.80	3.9	3.59	2.74	3.84	Ì	Ver		27	0-030	0.030	0.35	C.014	0.006	0.001
		00	14.34	16.93	13.10	8.35	2.03	1.13				90	0.015	0.007	0.00	0.001	0.00	-0.001
	Total	25	0.0	0.00	0.0	0.00	0.0	0.2	1		0.91	25	0.000 0.011 0.014	0.036	0.063	0.085	0.097	0.105
	6	2	0.71	1.78	2.37	2.73	0.86 2.73 0	2.05				o o	0.011	0.021	0.025	0.025	0.08	0.016
	,	, m	0.43	1.63	1.80	1.80	0.86	0.08				3	0.000	00000	0000	000-0	0.000	0.000
	£	2	2.14	3.29	3.41	5.35	5.29	1.7	7		ļ	2	0.050	0.027	0.017	0.00	9000	0.00
	a	,-1	3.87	3.7	2.2	0.92	0.13	-0.19				rt a	0.131	0.059	0.034	0.080	0.012	0.008
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										Ver	cal Pres	Vertical Pressure, net . at Indiated Cells	f. at Ind	1. ated	elle							1
	Town of	Tocal	1				Total							222			Febrund	pur				
BON	Point	tton	ч	2	m,	n. 1	a.c.	4	4	A.CO	6	P10	a,T	P 2	or C	a ^a	م د	94	L 4	14 80	d _O	10
2	н	~	0.55	0.73	-0.17	24.0	-0.17	0.23	0.85	-0.51	0.79	0.0	0.92	0.8	-0.17	t.0	0.00	0.23	0.74	0.30	0.79	1.13
		p)	1.10	0.98	-0.34	0.35	-0-17	0.13	1.06	19.0-	0.53	00.00	1.47	1.10	0.00	0.59	8.0	0.13	8.0	-0.36	0.53	1.13
		υ	2.03	1.22	-0.26	0.35	-0.17	3.16	1.37	-0.72	0.53	00.00	2.40	1.34	•0.c3	0.59	0.0	3.16	1.26	-0.20	0.53	1.13
		គ	5.76	1.47	-0.36	0.35	0.00	5.19	1.80	-0.81	0.70	0.0	3-13	1.59	90.0	0.59	-0.17	5.19	1.69	-0.10	0.70	1.13
		{+}	3.59	1.93	-0.17	24.0	0.0	11.29	2.0	-0.61	0.88	0.0	3.8	1.8	-0-17	0.77	+0.17	n.29	3.8	-0.30	0.89	1.13
		€×+	1-79	2.44	0.43	0.71	-0.17	14.45	2.75	-0.10	1.57	0.00	5.16	2.56	0.77	6.0	0.0	14.45	2.6	+0.81	1.57	1.13
		e	5.23	3.05	1.29	1.18	00.00	16.14	3.38	2.15	2.62	-0.10	5.62	3.17	1.63	1.42	0.17	न-्	(y e)	3.36	2.62	-1.03
		\$1.5	5.34	3.41	2.40	1.90	-0.17	17.16	3.91	3.97	1.20	-0.19	5.72	3.53	2.74	2.14		17.16	9.80	88	4.20	0.0
		н	3-35	3.54	2.23	2.61	-0.17	14.00	3-70	3.67	5.77	9.0	3.69	3.66	2.57	2.85		17.00	3.59	4.58	5.77	-0.19
		b	1.20	3-17	3.00	3.08	-0.17	8.81	3.70	5.50	9.9	-0.9ª	1.57	3.29	3.43	3.32		8.8	3.59	6.41	6.64	0.19
		act.	60.0	2.44	1.80	3.08	-0.17	2.03	2.85	3.67	.64	-1.27	94-0	2.56	2.14	3.32	00.00	2.03	2.74	4.58	19.9	60.0
		+1	-0.19	2.50	69.0	2.97	-0.17	1.47	2.64	1.63	6.12	-1.04	+0.18	2.32	1.03	র চ	0.0	1.47	2.53	2.54	6.12	60.0
		>:	-0.16	1.71	0.00	2.61	-0-17	1.13	2.22	0.61	5.83	-1.0	-0.09	1.63	0.34	2.85	8.0	7 3	7:17	1.52	5.00	60.0
		×	-0.55	1.8	-0.52	1.78	-0-17	0.68	1.59	-0.20	3.50	300	-0.18	1.34	-0.18	2.05	8.0	\$ •	3.18	0.7	3.50	0.19
														ĺ	ı							
									le.	rtical De	flection	Vertical Feflection, in., at Indicated Gages	t Indicat	ed Gages								
			ก์	ń	q	ค์	D-D-	D	Q	G	d			G	á	-	Fet mad	ć	c	E	ē	
				V	-	1	1	٥	1	0	0.		-	2		7		9,	27	500	0.	
5	r4	٧	0.020	0.05	0000	0.003	0.031	0.006	0.001	0.00	100.00		0.0.7	0.011	00000	007:5	0.00	0.007	-0.005	0.002	-0.00	
		m	0.046	0.027	0.00	0.003	0.024	0.010	-0.016	0.001	900.0		0.073	0.023	0.000	000.0	-0.003	0.01	-0.322	0.002	-0.005	
		υ	0.077	0.033	000-0	0.004	0.020	0.013	0.008	100-0	+0.00		0.104	0.034	0.000	0.000	-0.007	0.014	+0.012	0.002	-0.307	
		А	0.087	0.043	0.000	0.00	0.019	0.015	0.00	0.00	100.0		0.114	0.039	3.0	0.002	-0.008	0.016	-0.01h	0.002	-0.007	
		1+1	0.09	970.0	00000	0.005	0.019	0.015	710.0	900.0	+0.003		.122	0.042	0.00	0.003	-0.008	0.016	0.018	0.007	-0.006	
		βa ₄	0.113	0.048	0000	600.0	0.020	0.015	0.014	0.003	700.0		0.140	0.044	00000	0.000	-0.007	0.016	0.018	0.00	-0.007	
		t	0600	5 0 0	0.3	0.01 10.0	0.025	ಂ.ಬಾ	0.02	0.004	-0.005		0.117	C.037	0.000	0.011	-0.002	0.02	0.031	0.005	-0.005	
		hi	0.354	0.029	00000	0.018	0.037	0.008	0.020	0.006	0.011		0.081	0.065	0000	0.015	o.00.0	0.000	0.02	0.007	00000	
		Н	0.023	0.018	0000	0.023	0.058	0.004	0.016	0.007	0.019		0.050	4100	0.00	080	0.031	0.005	0.000	0.008	0,306	
		ר	0.00	0.012	0000	0.024	0.075	0.002	0.008	0.00	0.028		0.033	0.008	0.000	0.021	O. CAB	0.003	0.012	0.007	0-027	
		14	00.0	0.008	0000	0.021	0.048	0000	0.003	0.005	0.053		+0.023	0.00	0000	0.018	0.001	0.001	-0.007	0.006	0.042	
		₽ 3	600.0-	900-0	0000	0.019	0.094	000.0	0.002	0-00	0.046		+0.018	0.002	0.000	0.716	0.067	7.001	+0.006	0.005	0.035	
		3 :1	-0.01	0 002	0000	0.015	760.0	-0.001	-0.001	0.003	C.041		970-0+	0.001	0.000	0.013	2000	0000	-0.003	00.0	0.030	
		\$13	-0-0 <u>1</u>	00.0	0000	0.012	0.079	-0.001	-0.003	0.002	0.03₺		70.0-	0.00	0.000	600.0	0.052	00000	100.0-	0.003	0.023	

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1.05 -0.44 0.52 -0.18 2.67 0.57 0.25 0.48 0.18 0.50 0.50 0.52 0.09 1.56 1.34 0.17 0.48 0.50 0.52 0.09 1.56 1.34 0.17 0.48 0.50 0.52 0.09 1.56 1.34 0.17 0.48 0.48 0.50 0.50 0.60		To.	Loca					Total	17					4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	at times are	27727		Reto	ound				
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1.10 -0.11 0.24 0.18 1.18 1.18 -0.20 0.52 -0.50 1.15 1.18 -0.11 0.18 0.10 0.18 0.18 0.10 0.18 0.1	5		A A	2.40	0.73	-0.09	0.24	0.18	1.58	1.05	+0.41	0.52	+0.18	2.67	0.97	5.0	0.48	00.00	1.02	1.05	-0.81	0.70	-0.7
1.146 0.00 0.48 0.18 1.156 1.159 0.150 0.151 0.150 0.151 0.150			βΩ	1.3	1.10	-0.17	0.24	0.18	3.38	1.18	+0.30	0.52	40.09	1.56	1.34	+0.17	0.48	0.00	2.85	1.48	-0.92	0.70	-0.84
1.77 0.05 0.47 0.18 12.41 2.28 0.10 1.04 0.05 2.58 1.25 0.15 0.10			U	2.12	1.46	00.00	0.24	0.18	11.06	1.90	+0.20	0.87	40.09	5.39	1.70	0.34	97.0	0.00	10.50	3.8	-:.8	1.05	-0.8
1.55 0.25 0.47 0.18 13.54 2.74 0.41 1.57 0.09 3.22 2.19 0.50 0.71 0.00 12.99 2.74 0.71 0.10 1.15 0.00 14.11 0.10			A	2.58	1.71	60.00	74.0	0.18	12.41	2.35	07.0-	1.04	40.09	2.85	1.8	64.0	17.0	00.00	11.85	2.32	-1.32	1.22	-0.8
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			(a)	5.3	1.9	0.26	74.0	0.18	13.54	2.74	+0.41	1.57	+0.09	3.22	5.19	09.0	0.71	0.0	12.98	2.74	-0.81	1.75	-0.8
1.0 1.0			fa ₄	3.13	2.44	69.0	0.95	0.18	14.67	3.38	3.66	2.53	00.00	3.40	5.68	1.03	1.19	00.0	14.11	3.38	2.44	2.71	-0.93
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			O	2.58	2.68	1.37	1.42	0.18	15.35	3.59	5.29	3.84	-0.19	2.85	2.35	1.71	39.	00.00	14.79	3.59	4.07	4.00	-1.12
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			101	3.32	2.56	1.72	1.90	0.18	11.74	3.69	1.89	5.2h	5.24	3.59	2.80	5.06	2.14	0.0	11.16	3.69	3.67	5.42	# ·
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			*	0.55	2.19	0.86	2.14	0.18	3.16	3.06	8.3	5.94	2.62	0.82	2.43	1.20	2.38	0.0	2.60	3.08	7.03	6.12	1.69
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			75	0.00	1.83	0.52	2.14	0.18	5.30	2.74	67.4	5.77	1.31	96.0	2.07	0.86	2.38	0.00	47.4	2.74	3.8	5.8	0.38
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			24	-0.18	1.22	0.0	1.54	0.18	0.68	5.00	2.04	4.28	1.68	÷0.09	1.46	0.34	1.78	00.0	0.12	8.8	0.82	1.46	0.75
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			H	-0.18	1.10	0.0	1.42	0.18	0.68	1.69	1.63	3.49	8.24	60.0+	1.34	0.34	1.66	00.00	0.12	1.69	0.41	3.67	7.3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			×	12.0-	0.85	-0.09	1.19	0.52	+0.45	1.36	1.42	2.62	1.87	0.00	1.09	65.0	1.43	0.34	11.0-	1.38	0.20	2.80	6.0
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			ārs.	-0.37	67.0	21-0-	0.7	0.18	•0.22	18.0	1.22	1.48	1.50	-0.10	0.73	+0.17	8.0	0.0	-0-34	0.84	00.00	1.66	0.57
b₂ b				-						Ver	tical De	Clection	10.00	t. Indica	bed Gage							1	
b₂ b								Total			-	2000			200			Rebound				1	
0.034 0.000 -0.000 <td></td> <td></td> <td></td> <td>I a</td> <td>22</td> <td>23</td> <td>70</td> <td>50</td> <td>90</td> <td>D2</td> <td>28</td> <td>60</td> <td></td> <td>I D</td> <td>20</td> <td>E .</td> <td>d³</td> <td>De</td> <td>a D</td> <td>P7</td> <td>Ba</td> <td>60</td> <td></td>				I a	22	23	70	50	90	D2	28	60		I D	20	E .	d ³	De	a D	P7	Ba	60	
0.0054 0.0000<	5		A	0.00	0.038	00000	+0.002	-0.008	0.016	+0.005	0.001	0.003		0.013	0.032	00000	-6.00	-0.045	0.016	+0.006	0.000	0.00	
0.053 0.000 <th< td=""><td></td><td></td><td>A</td><td>0.147</td><td>0.054</td><td>00000</td><td>+0.003</td><td>-0.011</td><td>0.022</td><td>0.013</td><td>0.002</td><td>0.001</td><td></td><td>0.091</td><td>0.048</td><td>00000</td><td>100</td><td>-0.048</td><td>0.022</td><td>0.01</td><td>0.001</td><td>0.007</td><td></td></th<>			A	0.147	0.054	00000	+0.003	-0.011	0.022	0.013	0.002	0.001		0.091	0.048	00000	100	-0.048	0.022	0.01	0.001	0.007	
0.069 0.000 <th< td=""><td></td><td></td><td>t.</td><td>0.144</td><td>0.063</td><td>00000</td><td>0.006</td><td>-0.012</td><td>0.025</td><td>0.026</td><td>0.00</td><td>0.001</td><td></td><td>0.078</td><td>0.057</td><td>0.000</td><td>0.00</td><td>-0.049</td><td>0.00</td><td>0.027</td><td>0.003</td><td>0.007</td><td></td></th<>			t.	0.144	0.063	00000	0.006	-0.012	0.025	0.026	0.00	0.001		0.078	0.057	0.000	0.00	-0.049	0.00	0.027	0.003	0.007	
0.056 0.000 0.011 -0.009 0.024 0.026 0.000 0.116 0.026 0.000 0.116 0.029 0.000 0.116 0.029 0.000 0.116 0.029 0.000 0.116 0.024 0.000 0.000 0.117 0.044 0.000 0.000 0.017 0.018 0.000 0.000 0.017 0.000 <t< td=""><td></td><td></td><td>C</td><td>0.185</td><td>690.0</td><td>00000</td><td>0.006</td><td>-0.012</td><td>0.025</td><td>0.031</td><td>0.005</td><td>0.00</td><td></td><td>0.119</td><td>0.063</td><td>0.000</td><td>0.004</td><td>-0.049</td><td>0.025</td><td>0.032</td><td>0.004</td><td>0.007</td><td></td></t<>			C	0.185	690.0	00000	0.006	-0.012	0.025	0.031	0.005	0.00		0.119	0.063	0.000	0.004	-0.049	0.025	0.032	0.004	0.007	
0.056 0.000 0.018 0.001 0.017 <th< td=""><td></td><td></td><td>(n)</td><td>0.230</td><td>0.068</td><td>00000</td><td>0.011</td><td>-0.009</td><td>0.024</td><td>0.037</td><td>90000</td><td>0.002</td><td></td><td>0.164</td><td>0.062</td><td>00000</td><td>0.007</td><td>-0.046</td><td>0.02</td><td>0.038</td><td>0.005</td><td>0.008</td><td></td></th<>			(n)	0.230	0.068	00000	0.011	-0.009	0.024	0.037	90000	0.002		0.164	0.062	00000	0.007	-0.046	0.02	0.038	0.005	0.008	
0.039 0.000 0.024 0.03 0.031 0.035 0.031 0.031 0.037 0.035 0.031 0.031 0.031 0.032 0.031 0.031 0.031 0.031 0.031 0.031 0.031 0.031 0.031 0.032			Die.	0.165	0.056	0000	0.018	-0.001	0.173	0.044	0.000	0.007		0.099	0.050	00000	0.014	-0.038	0.173	0.045	0.008	0.003	
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0.016 0.000 0.031 0.115 0.003 0.045 0.046 0.000 0.000 0.003 0.003 0.046 0.046 0.000 0.000 0.003 0.003 0.046 0.003 0.000 0.003 0.003 0.000 0.003 <th< td=""><td></td><td></td><td>EC.</td><td>0.093</td><td>0.025</td><td>00000</td><td>0.030</td><td>0.085</td><td>0.007</td><td>0.032</td><td>0.013</td><td>0.031</td><td></td><td>0.027</td><td>0.019</td><td>0000</td><td>0.026</td><td>0.048</td><td>0.007</td><td>0.033</td><td>0.012</td><td>0.037</td><td></td></th<>			EC.	0.093	0.025	00000	0.030	0.085	0.007	0.032	0.013	0.031		0.027	0.019	0000	0.026	0.048	0.007	0.033	0.012	0.037	
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0.006 0.000 0.015 0.125 0.000 40.002 0.035 0.039 -0.004 0.002 0.003 0.039 0.004 0.002 0.002 0.004 0.000 0.004 0.003 0.004 0.004 0.005 0.004 0.005 0.004 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005			7	+0.063	0000	0.000	0.0.8	0.156	0.000	+0.004	0.007	0.046		-0.003	0.003	00000	0.014	0.119	0000	+0.005	0.006	0.059	
0.007 0.000 0.010 0.010 0.010 0.001 0.001 0.003 0.025 -0.001 0.001 0.000 0.000 0.000 0.000 0.000 0.000 0.000			×	+0.062	90000	0.000	0.015	0.125	00000	+0.002	0.005	0.039		-0.00	0.00	0.000	0.011	0.098	00000	+0.003	0.00%	0.045	
			H	190.0+	0.007	00000	0.010	0.087	-0.001	+0.001	0.003	0.025		-0.005	0.001	0.000	900.0	0.050	-0.00	+0.002	0.002	0.031	

										Vert	ical Pres	Vertical Pressure, psi, at Indicated	1 at Inc	Mcated	30,10							
	1000	Local	1				Tot	7			ŀ						Pehon	pur				
POS	Point	tion	Н	2	-	a.ª	2	9	4	80	0	P10	o, H	P2	(F	n. 2	^ب کو	P6	P7	BB	o o	210
9	~	(-1	1.0	1.46	-0.09	0.24	0.18	10.95	1.90	-0.30	0.70	60.00	2.11	1.70	6.0	80	0.0	10.39	8	-1.12	0.88	80.0
		o	3.23	5.19	0.52	0.83	0.18	14.33	3.17	2.44	2.18	60.0	3-50	2.43	38.0	1.07	0.0	13.77	3.17	8	2.36	.8.0
		2.	5.86	2.56	1.12	1.19	0.18	15.57	3.59	2.60	3.45	-0.10	3.13	2.80	3.46	1.43	0.0	15.0	3.57	4.38	3.67	-1.03
		н	1.66	5.68	1.80	1.66	0.18	12.64	3.80	4.38	5.37	1.31	1.93	2.35	2.14	8.1	0.00	12.08	3.80	3.16	200	0.38
		۲,	0.7	2.1	1.20	2.14	0.18	8:3	3.18	7-43	5.77	11.53	1.8	2.68	1.54	2.38	0.0	8.69	3.18	6.2	5.65	10.60
		×	0.19	1.9	09.0	2.14	0.18	5.03	2.85	5.50	5.77	62.0	97.0	2.19	\$ 0	2.38	0.0	3.47	2.86	2.28	5.8	-0.65
		ы	0.74	2.31	1.03	2.14	0.18	3.84	3.38	8.86	6.20	14.81	10	2.55	1.37	2.38	0.0	38	3.38	7.6	6.28	13.88
	8	(a)	2.12	1.46	0.17	0.16	8.0	9.37	2.43	-0.20	1.39	8.0	2.12	1.46	-0.3k	0.18	8.0	9.85	2.38	1.22	1.18	0.09
		C	1.73	1.9	1.72	0.9	0.00	9.93	3-17	0.92	3.14	-0-37	1.75	1.8	1.21	8	8	10.38	3.06	2.34	3.23	-0.26
		H	7:1	1.9	3.26	1.3	0.00	1.67	3.28	0.82	8.1	76.0-	1.1	1.8	.2.75	1.31	0.0	8.12	3.17	2.2	17.7	-0.85
		н	0.55	1.70	1.37	1.43	8.0	1.47	2.82	1.33	75-7	-1.12	0.55	1.70	98.0	1.43	0.0	1.92	2.74	2.73	4.63	-1.03
		7	0.28	1.2	98.0	1.43	0.35	0.22	2.25	-0.30	4.19	-1.12	0.28	1.2	0.35	1.43	0.35	0.67	2.11	1.12	4.20	-1.93
		×	61.0	16.0	0.77	1.19	0.30	-0.23	1.80	-1.42	3.3	-1-31	67.0	16.0	92.0	1.19	0.0	0.52	8	0.0	3.42	1.22
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							13th.								ш	П	Pebound					
			4	C.	4	70	25	30	1	80	0		r _I	2	E _Q	D ₁	50	26	22	84	ο.	
9	н	[a]	0.159	0.067	0.000	900.0	-0.03	0.00	0,005	0.003	00000		0.093	0.061	0000	0.005	0.050	0.00	9.00	00.0	3.0.0	
		O	0.182	0.061	0000	0.016	-0.00		0.043	0.008	0.00		911.0	0.055	0.000	0.012	0.01	0.00	0.0	0.007	0.001	
		H	0.175	0.122	00000	0.025	-0.01		0.042	0.000	0.013		0.109	0.116	0.000	0.008	90.0	0.0	0.043	0.009	0.00	
		н	0.038	0.028	00000		0.057	0.008	0.035	0.012	0.027		0.032	0.085	0.000	0.025	0.020	900.0	0.036	0.011	0.033	
		٠,	0.081	0.019	0.00		0.117	0.005	0.000	0.013	0.041		0.015	0.013	0.000	0.027	0.000	0.00	0.0	0.0.2	0.0.7	
		M	0.071	0.013	0000		0.121	0.002	0.010	0.011	0.052		0.003	0.007	0.000	0.024	0.084	0.002	0.011	0.010	0.050	
		ы	140.0	0.015	0000		0.135	0.003	0000	0.013	0.017		0.006	0.009	0.00	0.027	960.0	0.003	0.00	0.02	0.03	
	~	in)	3.052	0.070	0.00		0.003	0.044	0.08	0.00	0.018		0.065	990.0	0.0	0.006	0.006	0.0.0	6.659	0.006	900.0	
		o	0.016	0.039	0000		0.029	0.00	0.108	0.017	0.0.0		0.029	0.035	00000	0.02	0.000	₹ °	0.05	0.025	0.009	
		m	-0.001	0.024	0000		0.070	0.015	0.089	0.000	950.0		-0.012	0.000	0000	0.07	0.061		0.074	o.ore	0.0.2	
		ы	0.8	0.015	0.000		0.100	6,000	0.055	0.020	0.088		-0.002	0.011	00.00	0.028	0.091	0.005	0.0.0	0.018	0.03	
		13	-0.07	0.010			0.125	0.00	0.037	0.017	0.10		-0.00	0.006	0.000	0.00	0.116		0.00	0.015	0.081	
		ĸ	-0.02	0.00			0.140	00.00	0.004	0.013	0.135		-0.00E	0.004	0000	0.017	0.131	0,000	0.000	0.01	0.082	

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		0	0.7	0.97	0.0	0.36	8.0		Ì				0.0	0.7	0.97	5.33	0.36	0.0	5.59	1.16	1.45	0.79	800
		D	0.92	0.97	0.0	0.36	0.00			8 0.00		0.70	0.00	0.92	0.97	-0.51	0.36	0.00	3.16	1.37	1.42	0.79	0.0
		64	17	1.09	0.08	0.48	0.0		1.80	-		C.87	0.0	7.7	1.09	-0.43	0.48	0.00	8	1.69	1.32	8	0.09
		54	1.8	1.46	0.17	0.43	0.0		9 2.22	2 -0.10			0.00	1.8	1.46	-0.34	0.48	8.0	5.6	2.11	1.35	2.3	0.09
		0	5.10	1.70	J.34	4.0	0.35		Ġ			2.0	0.00	2.40	1.70	-0.17	0.71	0.35	10.38	2.7	1. A3	2.10	0.0
		11	1.8	1.9	1.11	0.98	8.0		3.06				61.0	1.8	1.9	09.0	6.0	0.00	10.61	8	2.17	3.00	-0.10
		H	200	1.98	3.43	1.19	8	9.148				3.8	0.84	1.20	8	2.90	1.15	00.00	6.6	3.00	2.14	3.93	0.73
		5	0.7	1.70	1.72	1.43	0.00		3.00			4.45 -	1.12	0.74	1.70	2	1.43	0000	4.32	8	2.3	4.54	-1.03
		M	0.37	1.16	1.03	1.43	5.03				_	4-37	1.12	0.37	1.46	0.52	1.43	5.03	1.0	(A)	£.73	4.46	-1.03
		1	91.0	1.2	0.96	1.43	0.0	100	1 2.22	22 -0.53		- 20-	1.22	61.0	1.21	0.35	1.43	0.0	95.0	0	16.31	17.77	-1-13
		×	61.0	0.37	0.77	1.19	0.0	-0.23	3 1.90	27-1-55		3.41	-1.31	0.19	0.97	9.50	1.19	0.00	+0.22	1.79	-0.30	3.50	1.2
		ĸ	0.0	0.73	69.0	8.0	0.00	•		Ţ,			1.12	0.00	0.73	0.18	8	0.00	0.0	1.8	-0.41	2.45	-1.03
		1											r y	di									
		1					Total.			Vertic	Vertical Deflection	-	in. at	in. at Indicated dages	allen pa			Februard					
		1 1	In In	25	23	¹ O	2	90	7d .	1	D'A I	o		ដ	20	D ₃	å	ď	90	120	8	o.	
7 3	r-4	g g	0.000	0.037	0000	0.00	0.00	0.026	26 0.015		0,002 0.	0.721		0.42	0.053	0,000	-0.00	-0,000	0.022	000.0	0,000	-3.003	
		b	0.000	0.053	00000	0.006	0.00		36 0.019		0.002 0.	0.018		0.053	670.0	0.000	-0.002	-0.007	0.032	0.00	0.000	-0.000	
		ρ	0.045	0.060	0.03	0,006		1 0.039			0.003 0.	. 710.		0.058	950.0	0.000	-0,000	-0.308	0.035	0.012	0.00	-0.007	
		562	0.050	990.0	00000	0.008					0.00%	0.000		0.063	0.0%	0.000	0.000	-0.308	0.038	0.037	0.000	-0.009	
) h	0.033	0.000	0.000	0.012		2 0.044	44 0.076		0.007	0.018		0.066	990.0	0.000	0.00	100.0	0.000	0.001	0.005	-0.006	
		0	0.042	0.061	0.00	0.00	100				0.011 0.	0.023		0.055	0.057	0.000	0.011	-0.001	0.034	0.075	0.00%	-0.00E	
		H	0.022	0.0	0000	0.00	0.08	3 0.027			0.025 0.	0.035		0.035	0.740	0.000	0.018	0.024	0.363	0.091	0.013	0.004	
		I	0.00	0.028	0.00	0.033	0.05	5 0.018	18 0.096		0.000	0.057		0.027	0.00%	800	2.025	0.046	0.01k	0.081	0.0.7	0.026	
		5	90.0	0.018	0.000	0.036	+0.092	2 0.01			0.020.0	0.082		•0.005	0.014	0.000	0.028	+0.081	0.007	0.050	0.018	0.058	
		N -	-0.015	0.012	00000	0.033		L 0.007			0.000	0.099		-0.000	0.008	0.000	0.3	0.105	0.003	0.026	0.016	0.375	
		¥ ia	-0.018	0.010	0.000	0.031		0000	-			0.106		-0.005	90000	0.000	0.023	0.12	0.000	0.028	0.025	0.082	
		×	-0.020	0.008	8	0.027		0.00			0.014 0.	0.108		-0.007	0.004	0.000	0.019	0.131	0.000	0.009	0.022	0.08	
		¥ ====================================	0.082	0.007	000.0	0.021						0.034		-0.000	0.003	0.000	0.033	0.103	-0.001	0.005	0.008	0.070	

200	- 8	200	2.30	9	0.28	92.0	9.0	0.45	0.38	0.10	0.10	0.10	0.10	0.10															
۵,							. 1				2.36 +		•	*		o.	0.055	950.0-	-0.055	0.033	0.043	0.000	0.0.2	0.099	0.105	0.152	0.137	0.135	0.057
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8	1.0	0 33	1	1	00.0	0.40	0.91	1.22	5	0.40	0.0	-0.37	-0.41	-0.51	rtical	28	0.00	0.00	0.00	0.01	0.0	0.8	0.027	0.0	0.02	0.0	0.0	0.0	0.0
P	1 %	1 177	1	9	1.8	2.32	2.53	2.6	2.32	1.90	1.47	1.26	1.05	0.63	Ve	2	0.036	0.083	0.106	0.120	0.137	0.158	0.132	0.094	0.051	0.035	0.029	0.026	0.020
26	35	3 6	(303	2.70	3.04	3.61	3.04	1.91	1.24	0.45	8.0	-0.12	-0.12	-0.23		90	0.051	0.001	0.38	0.063	0.052	0.035	0.083	0.015	0.00	0.008	0.007	0.005	0.00
P 5	8	8	3	8	00.00	0.18	0.18	0.00	0.18	0.18	0.35	0.18	0.35	0.35	30.00	5	-0.003	-0.003	-0.003	-0.005	+C.013	•0.031	0.087	0.131	0.143	0.186	0.163	0.137	0.00
P	0.10	3	0.0	₹.0	D.24	0.48	0.13	0.71	0.77	17.0	r.0	0.18	0.13	0.24		ď	0.004	90000	0.008	0.010	0.017	C.024	0.029	0.030	0.027	0.020	0.016	0.01	0.009
4. E	8	8	3	8	0.00	0.18	0.52	9.69	0.35	0.18	60.0	0.0	0.0	0.0		2	0.000	00000	0.000	00000	0000	0.000	0.000	00000	0.000	00000	00000	00000	0000
P2	200	200	3	96.0	800	1.23	1.34	1.22	1.22	96.0	0.73	64.0	64.0	0.3		D2	0.052	0.062	0.065	0.084	0.053	0.036	-0.055	0.015	0.000	0.00	0.007	0.005	0.00
d ₁	0.55	8	× ×	=	1.29	1.48	1.29	2.0	0.75	0.37	0.28	6.19	61.0	0.00		In Indian	0.030	0.037	0-037	0.036	0.027	0.016	100.0	0.002	-0.001	-6.002	-0.004	-0.00	SOC 0 .
Loca-	, a)	Ω	la]	(n ₄	o	Ħ	н	ם	M	Ы	×	373			д	U	Ο	(a)	t ₀	O	303	14	ы	aut	ы	×	R
Load	0																N												
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Į										1000	teal Pre	saure. rs	1 at Inc	at Indicated C	61.8							
	400						202	5									Febou	nd				
NO9.	Poli	10 12	n. f	2	p.	Cia T	P.	0,0	4	a.	n _e	01	p.	CV.	Ω ₄	and An	Sho Sho	sh,	F7	ac a.	O.	Fic
(0)	p4	(s)	8.1	0.73	0.00	0.24	00.00	2.18	1.16	-0.61	0.70	-0.27	0.83	0.35	0.00	0.25	0.0	3.3	1.50	-0.11	62.0	-0.19
		ŧ~	2.03	1.34	8	0.48	8.0	2.3	2.23	0.00	1.75	-0.47	± €	16	0.26	0.1.0	0.0	96.	2.54	8.5	1.00	-0.19
		31	1.57	3.46	0.78	Ę.0	0.00	3	2.7	0.51	2.53	-0.17	5.33 1.4	3.58	0.78	0.72	0.0	4.63	2.85	1.53	2.65	+0.19
		1.4	7::	1.46	1.03	800	00.00	2.82	2.7.	0.61	2.36	-0.57	0.92	1.58	1.03	96	0.00	3.39	2.95	2.03	5.4.5	45.00
		כי	F-0	1.2	1.03	1.07	00.0	1-35	2.53	0.62	3.67	72.0-	0.55	1.23	1.03	1.07	0.00	2.13	2.6	1.65	3.76	-0-19
		×	0.37	0.97	0.35	8.0	-0.17	0.22	8	-0.21	3.58	99.0-	0.18	1.09	0.35	8	-C.17	0.79	2.0	+0.Su	3.67	0.00
	8	[12]	0.93	0.73	0.17	0.2%	+0-17	5.49	1.58	0.0	0.87	00.00	0.83	0.7	0.08	0.12	-0.17	2-37	1.58	-0-30	0.00	0.00
		O	9.00	8.0	0.35	0.13	+0.17	2.37	2.11	1.53	1.83	00.00	0.55	0.08	98.0	0.30	-0.17	% %	2.11	1.23	1.92	00.0
		tr:	95.0	8.0	09.0	09.0	+0.17	1.70	2.11	1.83	2.27	00.00	97.0	0.09	0.51	0.18	-0.17	(C) (A) (-4	2.11	1.53	2.30	0.00
		j-4	0.37	98.0	0.35	09.0	-0-34	0.91	8	1.2	2.35	0.10	12.0	0.86	0.26	0.18	-0.00	0.79	1.90	0.9	2.45	0.19
		ы	0.28	0.73	0.35	0.77	0.34	0.57	1.58	0.81	2.18	1.03	0.18	0.3	0.2	0.59	0.0	0.45	1.58	0.51	2.27	1.12
		×	0.19	64.0	0.0	09.0	0.34	0.34	1.16	0.61	1.56	0.10	8.0	00	0.17	97.0	0.0	0.25	3.26	.0.31	1.75	0.19
				1			200		100	rtical I	eflection	n in a	at Indica	ed ince	Jió.							
			a ^{r4}	D2	G.	ជាំ	a a	26	P7	p _B	0		ω ⁻¹	22	C P	a a	3,1	9:3	20	ري ش	٥°.	
ത	7	(a)	0.340	0.062	00000	0.00	-0.012		0.063	0.00	-0.005		0.520	0.059	0.000	0.000	410.0-	0.040	0.058	0.000	0.00	
		Ľ)	0.025	0.054	00000	0.016	-0.00		0.10	0.003	0.015		0.043	0.051	0.000	0.014	-0.00	0.039	0.000	0.010	-0.003	
		iri	0.01	0.036	0.000	0.023	0.014		0.124	0.038	0.033		0.029	0.033	0.000	0.023	0.022	0.025	671.0	0.025	0.005	
		ы	-0.001	0.083	00000	0.028	0.053		0.108	0.022	0.09		+0.017	0.020	0.000	0.006	0.051	0.025	0.103	0.339	0.041	
		ы	-0.009	7.00°	0.000	0.030	-0.001	*	0.059	0.005	0.091		600°0÷	0.011	00000	0.02E	-0.003	-0.006	0.094	0.012	0.03	
		×	-0.140	0.000	0.000	0.027	0.114		0.037	0.020	0.10		+0.00	0.006	0.000	0.025	0.112	0.004	0.03	c.m.	0.088	
	CV	[n]	3	9.0.0	00000	0.007	0.000		0.112	0.010	-0.015		0.026	0.0.6	0.000	0.00	-0.003	0.063	0.10€	0.007	-0.07	
		U	0.00	0.022	0000	0.001	0.029		0.147	0.044	0.030		0.031	0.082	0.000	0.000	0.7.0	50000	0.143	0.0.1	0.028	
		111	0.005	0.013	0000	0.083	0.000	0.022	0.124	0.028	0.070		0.307	0.013	000.0	0.022	C. ^2	а, с,	0.120	0.005	6.056	
		ы	0.00	0.007	00000	0.024	0.059		0.073	0.029	0.113		0.306	0.007	00000	0.023	0.056	0.000	OF. 3	0.0	0.11	
		٠,	0.001	0.003	00000	0.020	0.072		0.168	0.025	0.132		0.003	0.003	0.000	0.00	0.00	0.00%	0.164	0.022	06	
		×	00000	0.00	00000	0.014	0.077		0.023	0.018	0.156		0.002	0.021	0.000	े व्याप	0.072	0,003	0.00 o	0.00	0.154	

									Vertical	ical Pre	ssure, ra	1 at Inc	deated C	sell's							
Irea-		1				Tota	7									sebound	pu				-
Point tion P1 P2	2	2		Δ,	0,	o. W	9	p.	9 9	0	P. I.O.	a. T	2	ρ,(7	n.if	Out.	sia _e	1.4	£.9		0.1
E 0.92 0.73	0.92 0.73	0.73		00.00	0.24	0.00	2.03	1.47	-0.11	0.61	-0.19	O. P.3	0.73	+0.17	36	-0.18	2.15	1.47	ec. 30	0.07	*O.20
6 1.48 1.22	1.48 1.22	1.23		0.18	0.36	0.00	3.61	2.33	0.30	1.40	-0.19	1.39	1.22	0.35	S	-0.18	3.73	2	0.71	3-66	0.0
H 1.29 1.34	1.29 1.34	1-3-		0.35	0.18	0.18	3.38	2.53	0.31	2.01	-0.19	1.20	1.34	0.52	09.	00.	3.50	2.53	200	2.2	96.0
1 0.83 1.22	0.83 1.22	1.22		0.78	0.7	0.00	2.25	54.2	1.22	2.62	-0.19	0.75	1.22	8	c.	-2.18	2.37	2 2	2.63	2.68	+0.26
J 0.55 1.22		1.2		0-43	0.77	0.00	1.12	2.32	1.01	2.97	-0.19	97.0	1.22	0.50	- B	-0.18	6.1	2.33	-7	2.23	PC. 24
K 0.37 0.98		0.98		0.18	0.83	0.18	0.55	2.11	1.63	2.39	-0.37	2.26	8	0.35	5.0	00.0	979	2.2	₹.	3 76	.0.10
8 0 7 0 8		0.86		0.0	0.23	-0.19	2.15	1.43	-0.51	0.38	-0.56	0.7	0.73	0.0	, E	-0.18	2.25	8077	-6.10	6	90.0
G 0.55 1.10		1.10		0.17	0.35	0.0	1.92	2.07	+0-72	1.73	0-1	0.55	0.97	1 100	• 1	8.0	3.6	2.cl	100	8	8
н 0.37 0.98		9		0.35	27.0	0.0	र -1	2.0	1.93	2.10	95-0-	0.37	9.0	3.35	0	00.0	70	2.07	- # #1	2.57	-0.8
I 0.28 0.86		0.86		0.35	C-47	0.00	98.0	1.80	0.77	2.27	-C-38	0.26	0.73	55.0	- H.	00*;	0.68	1.80	200	-7	95.0
J 0.18 0.96	0.18 0.96	0.96		0.3	0.47	0.17	0.45	1.18	0.20	2.03	7	0.16	0.73	ě,	. A	0.17	0.45	1,48	8.0	00 PT	1.13
19"0 60"0 X	0.09	19.0		-0.17	27.0	8.0	0.23	1.16	-0.10	1.57	0.56	0.00	97.0	-0.17	0.27	800	6	1.10	-0.51	1.74	S 5
						0.8			r foat r	eflectio	n fr. a	Indices	Indicated Jares			Laborated					
2 1 _a	2 12	2	1	e a	ค์	ဇ်	26	22	ac ac	C		e71	25	G.	152	52	90	27	1.9 60	00	
E 0.035 0.060		0.0	0	000.0	0.005	-0.003	0.759	0.072	0.006	-0.00		0.041	0.055	000	0.002	9.0.0-e	0.052	0.057	0.002	-0.056	
		0.0		0.000	0.016	0.010	0.055	0.131	0.05	-0.008		0.035	0.051	0.00	0.003	-0.039	0.000	0.116	0.01	-0.046	
		0.0	0	0.00	0.022	0.03	0.000	0.154	0.023	-0.260		0.005	0.035	0.000	0.00	0.0	C.035	0.139	0.00	-0.088	
I 0.00 0.006		0.0		0000	0.027	-0.061	0.006	0.143	0.026	-0.057		0.026	0.021	0.000	0.00	+0.012	0.0	0.128	0.002	0.03	
		0	~	0000	0.030	0.133	0.017	0.950	0.028	0.152		0.000	0.012	000.0	0.027	0.08	0.02	0.800	0.00%	0.096	
_	_	0	•	0000	0.028	0.135	0.011	0.058	0.006	0.151		0.006	2000	0.000	0.00	0.036	0.00	0.0.3	0.002	0.097	
E 0.037 0.036		0.03		0000	0.008	0.003	0.00	0.154	0.020	0.005		0.00	0.035	0.000	0.00	0000	0.09	0.10	0.000	-0.027	
G 0.00% 0.00		0.0	~	00000	0.017	0.00	0.033	0.191	0.00	0.042		0.021	0.017	0.000	0.015	0.016	0.033	0.143	0.00	0.000	
н о.019 о.010		0.00	-	00000	0.000	0.036	0.83	0.168	0.00	0.091		Court	5.00	0000	C.018	0-033	0.009	0.120	0.00	6.00	
1 0.016 0.00		0	10	000.0	0.000	0.019	0.017	0.122	0.030	0.129		0.003	3.00°	0.000	0.018	0.046	0.311	160.0	0.086	0.107	
J 0.024 0.002		0.0	O	0.00	0.027	0.059	0.012	0.085	0.026	0.158		100°	<i>(</i> * .	*			OUT.		5	0.136	
K 0.012 0.00		0.0	_	0000	0.013	0.058	0.00	0.058	0.020	0.17		10°C=	0.000	0.30	7.01.	0.055	0.003	0.000	0.0.0	0.155	

(Comment)

	3						Tot	7		Vert	ical Pre	Vertical Pressure, psi, of Indicated Cells	d of In	dicated (ells		Rebound	pro-				
3	i i	tton	4	2	-M	a.*	2	9	4	8	a. ^O	P 20	d.	2,0	a, (*)	A. 1	P.	29	P7	8	0.0	200
2	4	M	0.65	0.61	0.0	0.24	-0.17	1.47	1.16	2.0-	0.61	0.19	0.55	0.61	0.00	0,12	-0.17	1.3	1.16	-0.5	0.70	0.26
		o	20.1	98.0	0.17	0.36	-0-17	2.85	3.8	0.0	1.14	00.0	0.92	0.80	0.08	20.0	-0.17	2.70	8.1	-0.30	53	8.0
		æ	0.83	8.0	0.35	0.36	-0-17	5.60	2.11	0.61	64.1	0.00	0.73	0.9	0.26	0.24	-0-17	2.18	2.11	0.31	1.58	0.00
		н	0.65	0.9	0.35	09.0	-0.17	1.81	2.1.	1.83	2.18	00.0	0.55	98.0	0.36	0.48	-0.17	1.69	2.11	1.53	2.27	0.0
		'3	94.0	8.0	0.43	09.0	-0.17	1.13	1.9	1.42	2.36	0.00	0.3	0.98	0.34	0.18	-0.17	1.01	1.90	1.12	2.45	60.0
		×	0.10	6.73	0.35	17.0	-0.17	0.57	1.69	86.5	2.27	1.42	0.00	50.00	0.26	0.59	-0.17	0.45	1.69	0.62	4	1.50
	N	M	8.0	-0.37	-0.43	-0.1.8	-0.52	1.47	0.5	12.32	98.0	23.31	0.46	64.0+	60.0	00.00	-0.17	1.69	0.75	12.35	0.00	8
		o	0.0	0.53	-0.34	-0.24	-0.52	1.24	1.06	12.53	0.0	22.59	0.46	19.0	00.0	+0.24	-0.17	3.46	1.17	13.16	1.16	2,82
		bet	-0.18	0.8	-0.26	-0.24	-0.52	0.68	1.05	13.75	E-1	23.43	*0.28	+0.61	-0.08	-0.24	-0.17	0.9	1.17	14.38	1.83	3.66
		н	-0.18	-0.25	-0.26	-0.24	-0.35	0.35	0.8	12.30	1.40	21.93	+0.28	19.0*	*0.08	40.24	00.0	95.0	8.	11.9	1.32	2.16
		77	-0.28	-0.25	-0.36	-0.24	-0.35	0.30	6.6	11.30	1.22	21.18	+0.18	40.61	+0.06	-0.24	00.00	0.22	0.75	11.93	1.74	2.42
		ĸ	-0.37	64.0-	-0.34	-0.24	-0.35	¥9	0.21	11,30	0.38	20.99	60.04	+0-37	00.00	·C.24	00.00	7.0	0.32	11.93	1.40	2
									Ve	Tites] L	eflection.	100	to Tradition Case	Sed Gage								
							Total			1			The second secon				Status and		-			
			ď	22	03	á	50	90	D7	010	6		e ^r	E C	e d	o ^a	2	90	Dy	8	00	
10	н	61	0.028	0.045	0.000	0.003	-0.002	0.062	0.072	0.00	-0.018		0.000	0.045	0.000	0.002	-0.005	3.058	0,768	0.00	-0.020	
		o	0.019	0.039	00000		0.00	0.057	0.126	0.015	-0.007		0.02	0.039	0.000	0.011	0.001	0.053	0.122	0.002	-0.009	
		tes	0.012	0.027	0000			0.00	0.144	0.021	0.011		0.024	0.027	0.000	0.026	0.011	0.036	0.140	0.028	0.00	
		H	0.00	0.025	00000			0.08	0.133	0.027	10.0		0.006	0.025	0.000	0.023	0.030	0.021	0.129	0.024	0.552	
		+3	0.00	0.008	000-0	0.024		0.016	0.088	0.020	0.106		0.008	0.008	0.000	0.023	0.052	0.012	0.084	0.000	0.10	
		160	0.00	0.00	0000			0.000	0.048	0.006	0.12%		0.004	0.004	0.000	0.000	0.364	0.00%	0.044	0.023	0.122	
	N	м	0.012	0.000	00000			0.08	0.137	0.012	+0.003		0.027	0,026	0.000	0.00	0.007	0.060	0.107	0.020	-0.015	
		v	0000	0.013	0000			0.036	0.165	0.023	0.0.0		600.0	0.013	0.000	0.014	120.0	0.032	0.135	0.0	3.002	
		ht	0.000	0.007	0.000			0.083	0.154	0.020	0.098		0.005	0.007	0.000	0.017	0.036	0.019	0.124	0.026	0.09c	
		н	-0.002	0.004	0.000			0.016	0.103	0.0	0.135		+0.009	0.00%	0000-0	0.017	0,046	0.022	0.078	0.67	0.117	
		1-3	-0.003	0.001	00000	0.014	0.048	0.011	0.73	0.024	0.157		200,0+	0.001	0,000	0.01	0.054	0.007	0.043	0.000	0.139	
		×	-0.004	0.000	0.000			0.008	990.0	0.018	0.183		3.001	000,0	0,000	0.010	0.051	0.004	0.026	3.026	0.345	

										ert	ertical Pressure,		psi, at Indicated Cells	Micated	Cells							1
	Lond	100	-		6		Tot	10	6		6			6	6	,	Hebor	pur		4		
No.	Polat	tion	-	cu	.rl	2	2	9	7		6	10	2,54	N	(17)	2	2	2.0	4	20	0	20
ដ	-	m	0.18	0.37	0.00	0.00	0.0	0.34	0.0	-0.3	0.35	-0.19	6.18	0.2	0.00	0.0	0.0	0.34	300	-0.30	0.52	-0.47
		O	0.38	0.61	0.0	0.00	0.0	0.68	0.6	-0.61	11.0	-0.37	0.28	0.18	0.0	0.00	0,00	99 0	0.6	0.00	0.61	-0.65
		Ω	0.37	0.61	0.0	0.00	8.0	0.91	1.06	-0.41	0.53	-0.37	0.37	0.48	0.0	0.0	00.00	0.92	1.06	-0.20	0.74	-0.65
		M	0.46	0.61	0.0	10	0.00	1.13	1.16	-0.51	0.53	-0.37	0.46	0.48	0.00	11.0	0.00	1.13	1.16	0.0	0.70	-0.65
		By.	0.65	0.86	00.0	0.23	0.00	1.8	1.49	-0.51	0.79	-0.56	0.65	0.73	0.00	0.23	00.0	1.98	1.48	+0.10	800	-C.8.
		O	0.74	98.0	0.0	0.23	0.00	2.49	1.80	-0.41	1.22	-0.56	0.74	0.73	0.0	0.23	0.00	2.49	1.80	+0.20	1.39	-3.8t
		H	0.65	1.10	17.0	0.25	0.00	2.15	1.%	0.20	1.57	95.0	0.65	0.97	0.17	0.23	0.00	2.15	3.8	0.8	1.74	-C.8
		н	0.46	0.98	0.35	0.47	000	1.36	2.85	1.73	2.10	0.75	94.0	0.89	0.35	0.47	00.00	36	2.85	2.3	2.27	-1.03
		h	0.37	36.0	0.35	0.1	00.00	0.91	7.8	1.00	2.27	-0.75	0.37	0.85	2.35	6.47	0.00	0.91	3.8	1.63	2.44	-1.03
		×	0.18	98.0	9.5V	74.0	0.0	0.45	1.18	0.41	2.10	5.73	C.18	0.73	0.30	0.47	00.0	0.45	1.48	1.00	N.	19.60
		ы.	0.18	r,	0.1	0.47	0.17	0.45	1.37	0.10	1.92	1.4	0.18	1.58	+0.17	0	0.17	0.45	1.37	0.7	5.00	1.13
		×	0.0	19.0	+0.17	0.47	0.00	0.23	1.16	-0.10	1.66	24.0	0.09	0.18	27.0	0.47	00.00	0.23	1.16	13.0	1.83	67.0
		15	0.0	6.0	-0.17	0.23	00.00	0.12	0.85	-0.41	1.14	0.38	0.00	0.36	+0.17	0.23	0.00	0.12	8.0	0.20	1.3	0.10
									V.	Vertical Deflection	100000		at Tribon and Games	Case								
							Total							2			Rebrund				ĺ	
			D ₁	25	4	á	25	90	27	_D 8	27		្នា	25	D ₃	S.	24	(1 ²)	12	DB B	Po.	
Ħ	-	•	0.00	0.00	0.000	0.002	0.005	0.00	H. 042	-0.00			-0.003	0.00	0.000	0.000	0.012	D.C34	9000	-0.000	-0.014	
		U	0.01	0.030	0000	0.003	0.002	0.055	690.0	•0.003	•0.00		0.00	0.029	0.300	0.001	-0.0a	0.20	0.021	00.0	-0.016	
		a	0.00	0.034	0.000	0.003	0.002	0.062	0.08	100.00			0.033	0.033	0.000	0.001	0.001	0.056	960*0	00000	600°0-	
		M	660.	0.035	000.3	0.00	0.002	0.067	0.107	0.003	•0.003		9,000	0.034	0.000	0.000	0.001	0.061	0.059	0.000	570.0-	
		h	0.000	0.337	0000	0.007	0.00	0.07	0.148	0.00	+0.00		0.027	0.036	0.000	0.00	0.001	0.065	0.100	0.00	S.012	
		o	0.032	0.030	0000	0.011	0.007	0.061	0.170	0.0			0.433	0.029	00000	0.009	0.00	0.055	0.122	0.0	-0.00	
		200	0.00	0.021	0000	0.016	0.016	0.044	0.186	0.082			0.03	0.020	0.000	0.014	0.003	0.038	0.138	0.018	-0.0	
		н	0.00	0.01	0000	0.000	0.033	0.007	0.183	0.000	0.080		0.007	0.040	0.000	0.00	0.0	2.02	0.135	0.084	0.056	
		43	0.017	0.007	0.000	0.000	0.045	0.019	0.134	0.030	0.120		0.00	0.006	0000	0.018	् अह	0.023	0.086	0.026	0.098	
		×	0.0	0.003	0000	0.018	0.057	0.013	0.00	0.0	0.147		0.00	0000	0000	0.ME	0.054	0.307	0.047	5.00	0.125	
		ų	0.0	0.00	0.300	0.016	0.061	0.01	0.080	10	0.10		0.000	0.0	00000	0.0	0.056	0,005	0.032	0.021	0.144	
		×	0.012	0.00	0000	0.01	0.060	0.00	0.072	10 00	0.175		-0.001	0.0	0.000	0.014	D.C-7	0.00	0.104	2.01	0.153	
		R	0:01	0.00	0.00	0.00	0.06	0.00	0.001	0.015	1.147		-0.002	-0.00	0.00	0.000	0.0.3	0.002	0.03	0.011	0.12	
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Table A

							Total			Vert	ical Pre	Vertical Pressure, psi, at Indicated Cells	i, at In	dicated	Cells		100					
ROW	Potet	tion	4	2	4	a rd	P	PP 8	4	P P	4	P10	P.	P2	P.	Q.	P ₂	P6	4	8	20	P10
ជ	N	•	0.0	64.0	8.0	0.0	0.0	0.45	0.63	-0.20	0.36	-0.09	60.0	64.0	-0.17	0.0	0.0	0.34	0.74	0.0	11.0	9
		υ	0.18	0.37	40.0	0.0	0.00	0.79	0.63	01.0-	0.26	-0.09	0.18	0.37	-0.08	0.0	0.00	0.68	0.74	+0.10	0.14	+0.28
		A	0.18	64.0	60.04	0.00	0.0	1.0	0.84	-0.10	0.43	-0.09	0.18	64.0	-0.08	6.0	0.00	1.8	6.0	+0.10	0.61	+0.28
		M	0.18	64.0	0.0	0.00	0.0	2.13	0.95	-0.10	0.43	-0.09	0.18	64.0	-0.17	0.0	0.00	8.8	1.06	+0.10	0.61	40.28
		(A)	0.18	64.0	60.00	0.00	0.17	2.35	1.16	0.00	0.70	-0.09	0.18	64.0	-0.08	8.0	0.17	2.24	1.27	0.20	0.88	+0.28
		ø	0.18	19.0	60.0	0.0	0.00	1.0	1.26	0.20	9.0	-0.09	0.18	0.61	-0.08	9.0	0.0	1.90	1.37	0.40	1.14	40.28
		H	0.27	19.0	0.17	0.12	0.0	0.68	1.16	0.51	1.13	-0.09	0.27	0.61	0.0	0.12	8.3	0.57	1.27	4.0	1.3	+0.28
		н	0.27	64.0	0.17	0.12	0.0	0.45	1.03	0.20	1.13	~0.19	0.27	64.0	0.00	0.12	0.00	0.34	1.16	0.40	1.3	+0.18
		b	0.00	0.49	0.17	7,75	0.0	0.22	0.84	0.10	1.05	-0.37	0.00	64.0	0.0	0.12	0.0	0.11	6.0	0.30	1.23	0.0
		M	0.0	0.37	0.17	8.0	0.0	n.º	0.63	0.00	0.87	-0. 28	0.00	0.37	0.00	0.0	0.00	0.0	0.74	0.20	1.05	€0.00
		ы	0.0	0.24	0.17	0.12	0.00	0.11	0.63	9.00	0.70	-0.58	00.0	0.24	0.0	0.12	0.0	0.0	0.74	0.30	0.88	11.0+
		×	2.00	0.24	0.17	0.0	0.00	٥.11	0.45	0.00	0.52	-0.26	0.0	0.24	8.0	0.0	8.0	0.0	0.53	0.50	0.70	11.0+
		101	-0.10	0.24	0.0	0.00	0.0	n.º	o.2	0.0	0.35	-0.26	-0.10	0.2ª	-0.08	0.0	0.0	0.0	0.32	0.50	0.53	1.0
						,									•							
							Total		Ve	Vertical Deflection, in.	eflectio		at Indicated Gages	ted Gag			Rehomind					
			Z ^L	2	P ₃	ď	2	90	^D 2	80	6		ď	20	~	ď	2	90	²	80	P ₉	
7	c	M	0.00	0.017	0.00	0.001		0.051	0.031	0.002	-0.006		0.012			0.003	+0.009	0.049	0.00	0.003	-0.046	
		υ		0.00	0.000	0.002		0.059	0.075	0.00	-0.007		0.013			0.00	+0.008	0.057	0.070	0.00	-0.047	
		A		0.019	0.00	0.003		0.061	0.09	0.006	-0.006		0.012		0.000	0.005	÷0.009	0.059	0.089	0.007	-0.00	Ť
		M		0.017	0.00	0.005		0.060	0.106	600.0	-0.00		0.01	0.020	0.000	0.007	+0.010	0.058	0.101	0.010		
		04	0.005	0.013	0000	0.007	-0.001	0.050	0.124	0.014	+0°00+		0.008		0000	0.00	+0.013	0.048	0.119	0.025		+
		v		0.008	0.00	0.010		0.032	0.140	0.000	÷0.026		900.0	0.011	0.000	0.012	÷0.080	0.030	0.135	8.0	-0.01	
		H		0.003	0.000	0.011		0.019	0.110	0.024	0.102		0.004	900.0	0.000	0.013	+0.031	0.017	0.105	0.005	0.062	
		3-1		0000	0.00	0.01		0.012	0.067	0.024	0.143		+0.002	0.003	0.000	0.013	+0.039	0.010	0.062	0.00	0.103	
		r,	-0.002	-0.00	0000	0.00		0.008	0.038	0.020	0.151		+0.001	+0.002	0.000	0.011	40.0+	0.006	0.033	0.021	0.11	
		×	-0.002	-0.002	00000	0.00		0.005	0.018	0.014	0.199		+0.001	+0.001	0000	0.008	40.040	0.003	0.013	0.015	0.159	
		ы		-0.003	0.000	0.005		0.00	0.011	0.011	0.179		0.000	0.000	0.00	0.00	0.036	0.002	0.006	0.012	0.139	
		×		-0.003	0.000	0.003		0.003	0.012	0.008	0.148		0000	0.00	0.000	0.005	0.051	0.001	0.007	0.00	0.108	
		K		-0.003	0.00	0.001		0.003	0.00	0.004	0.102		0.000	00000	00000	0.003	0.020	0.00	0.00	0.00	0.062	

Table A-7
Multiple-wheel Heavy Gear Load Flexible Pavement Tert, Static Instrumentation Loading Lata

Item 4; Load Condition: 30 kips per Wheel, Twin Tanden, 100 psi

	3		ı				Total			Vert	CAL PTE	Vertical Pressure, psi, at Indicated Cells	I at Inc	Cated	Sel 18		Rebound	pu				
3	a H	100	4	P2	۳.	a. **	2	9 B	P ₇	a _o	40	P10	مرا	4	^م	P.	25	P6	4	8	۵	P10
п	-4	4	0.00	2.10	-0.10	1.20	0.00	0.0	1.72	-0.10	98.0	0.2	0.00	1.43	-0.87	09.0	-0.29	-0.18	1.72	0.80	0.78	0.31
		A	8.0	3.24	99.0	1.67	0.0	0.0	2.98	-0.30	1.12	0.00	0.00	2.57	-0.11	1.07	-0.29	-0.18	8.8	09.0	7.0	0.10
		U	0.0	7.86	5.62	2.15	0.39	-0.36	4.36	-0.9	1.55	ह-0	00.0	4.19	2.18	1.55	0.10	-0.54	4.36	0.00	1.47	0.3L
		Α	8.0	5.72	2.56	2.63	0.58	-0.36	4.93	-1.10	1.81	ন.	0.00	2.03	4.79	2.03	0.29	-0.54	4.93	-0.30	1.73	0.3
		M	0.0	6.39	8.92	3.11	0.97	-0.18	5.50	-0.80	2.15	o.2	0.0	5.62	9.15	2.51	99.0	-0.36	5.50	0.10	2.07	0.31
		٨,	0.0	7.3	13.51	¥.4	3.35	0.0	6.19	0.40	3.01	0.72	0.00	6.57	12.74	3.71	3.03	-0.18	6.19	1.30	2.93	0.82
		v	0.00	7.93	12.97	5.38	7.43	-0.36	5.85	-0.10	3.79	1.9	0.0	6.38	12.20	1.78	7.14	-0.57	5.98	0.80	3.72	8
		Ħ	0.0	5.72	18.63	6.10	10.17	-0.18	4.58	1.10	7-30	3.08	0.0	5.05	17.86	5.50	98.6	-0.36	35.	2.00	22.4	38
		H	0.0	3.62	#:π	6.10	n.73	-0.18	2.86	0.10	4.39	3.69	0.0	5.32	10.67	5.50	44.11	-0.36	2.86	1.00	 E	3.79
		4	0.0	2.148	74.4	5.50	13.a	-0.18	1.83	-1.70	3.36	4.3	0.00	1.81	3.70	8.7	12.72	-0.36	1.83	-0.80	3.88	4.41
		×	0.50	1.43	2.07	4.43	61.6	-0.18	0.91	-2.30	3.18	2.87	0.20	92.0	7.30	3-83	8.90	-0.36	0.91	-1.40	3.10	2.97
		ы	0.0	1.24	1.64	3.83	6.55	-0.18	0.57	-2.30	2.75	1.85	0.0	0.57	0.87	3.23	6.26	-0.36	0.57	-1.40	2.67	8
		×	0.0	1.14	1.45	3.23	4.50	-0.18	c.35	-2.49	2.54	1.13	0.00	6.47	0.65	2.63	12.7	-0.36	0.34	-1.59	2.16	1.23
		K	0.00	98.0	1.20	2.39	2,15	-0.36	0.0	-2.50	1.55	ন.	0.00	0.19	0.43	1.79	1.86	-0.54	0.00	9	1.47	0.31
									Ve	rtical De	flection	Vertical Deflection, in., at Indicated Gages	t Indicat	ed Gage	F.							
			D ₁	D2	P.	ď		90	70	P _B	Р		ι _σ	D2	L L	D	rebound D ₅	D6	57	28	a°	
_	٦	4	0.025	0.007	0.00	0.001	0.006	0.003	0.00	00.00	00.0		0.017	0.02	0.00	0000	0.013	0.008	0.001	0.000	0.00	
		p)	0.010	0.016	0.002	0.00	0.00	900.0	0.00	0.00	0.00		0.012	0.030	0.006	0.008	0.011	0.011	0.00	00000	0.00	
		b	0.006	0.028	0.003	0.002	0.003	0.00	0.001	0.00	-0.001		0.008	0.042	0.007	0.000	0.000	0.024	0.002	0.000	0.003	
		Q	90000	0.041	0.00	0.003	0.005	0.00	0.001	0000	-0.001		0.008	0.055	9000	0.011	0.30	0.015	0.002	0.000	0.003	
		ы	0.006	0.048	900.0	0.00	0.002	0.00	0.001	00000	-0.001		0.008	0.062	0.010	0.012	600.0	0.015	0.005	00000	0.003	
		(n ₀	0.007	0.035	0.007	600°0	0.003	0.009	0.005	0.00	-0.001		0.00	0.050	0.011	0.017	0.010	770.0	0.003	0.000	0.003	
		ซ	0.013	0.00	900.0	0.017	0.007	0.006	0.002	0.000	0.001		0.015	0.040	0.012	0.025	0.014	0.011	0.003	0.000	0.005	
		111	0.023	0.016	0.008	0.027	0.012	0.003	0.002	0000	0.002		0.025	0.030	0.012	0.035	0.019	0.008	0.003	0.000	0.005	
		+1	0.00	0.005	0.305	0.035	0.021	-0.00	0.005	0.000	0.00		0.042	0.019	0.00	0.043	0.026	0.00	0.003	0000	0.00	
		+3	0.054	-0.002	0.002	0.030	0.028	-0.002	0.001	0.000	900.0		0.056	0.012	0.006	0.038	0.035	0.003	0.002	0.000	0.010	
		×	990.0	-0.006	0000	0.022	0.033	-0.00	0.001	0.000	0.007		0.068	0.008	0.00	0.030	0.000	0.001	0.002	00000	0.011	
		Fia	0.071	-0.308	100.0-	0.017	0.033	-0.004	0.001	0.000	0.007		0.073	900.0	0.003	0.025	0.040	0.001	0.002	000.0	0.01	
		×	0.072	-0.010	-0.002	0.012	0.031	-0.005	0.000	0.000	900.0		0.074	0.00	0.002	0.020	0.038	0.000	0.001	0.000	0.010	
		275	0.000	0.01	-0.003	0.005	0.023	-0.005	0.00	0.000	0.00		0.062	0.003	0.001	0.013	0.030	0.000	0.001	00000	0.008	
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Row	ä	tion	a.rd	25	-F	o.	2	9	a.	8	20	P	e,	2	₂ m	9. 1	P5	P	P7	80	6	P10
-	œ	4	10.85	3.05	1.09	1.43	0.50	₩.96.06	3.90	-0.40	1.38	n.0	11.65	3.24	0.33	1.43	0.20	45.70	3.67	-1.40	1.12	-0.50
		4	0.81	4.58	2.61	1.91	67.0	9.10	5.73	-0.20	1.89	0.31	19.1	1.7	1.85	1.91	64.0	8.7	5.50	-1.20	1.63	0.0
		υ	14.0	5.92	14.16	2.87	1.37	3.09	7.34	3.81	2.76	0.62	1.21	6.10	13.40	2.87	1.37	2.73	1.1	2.81	2.50	0
		Α	19.68	6.59	18.19	3.47	2.16	\$.78	7.79	5.31	3.27	0.93	20.18	6.48	17.43	3.47	2.16	87.58	7.56	#	3 6	0.62
		M	23.30	64.9	16.77	3.83	3.33	114.16	8.00	5.1.1	3.70	1-44	24.10	6.68	16.01	3.43	3-33	113.80	7.79	14.4	3.11.	7
		Fi.	-0.60	6.10	15.68	5.08	7.83	0.91	7.57	5.m	1.82	17.7	0.20	6.29	14.92	5.00	7.83	0.55	7.3	7	7.56	4
		O	-0.60	84.4	23.96	5.50	10.08	0.73	2.62	1.2	5.3	98.9	0.20	19.4	23.20	5.50	10.08	0.37	5.39	2.9	5.08	9.9
		m	-0.60	2.86	11.33	5.36	n.35	6.73	3.67	15.4	5.34	7.07	0.20	3.05	10.57	5.36	11.35	0.37	3.44	3.33	5.08	9
		н	-0.60	1.43	3.48	45.4	12.72	45.0	2.18	1.0	47.4	8.51	0.20	1.62	2.72	45.4	12.72	0.18	1.8	0.0	87.4	ω
		ר	-0.60	0.58	1.74	3.47	7.83	0.36	1.14	0.0	3.79	5.84	0.20	11.0	96.0	3.47	7.83	0.0	0.91	-1.00	3.53	5
		M	-0.60	0.19	1.30	2.39	3.52	0.36	0.68	-0.10	2.76	2.57	0.20	0.38	0.54	2.39	3.52	0.0	0.45	-1.10	2.50	2
		អ	-0.60	0.19	1.30	1.91	2.45	0.36	94.0	-0.50	2.24	1.75	0.20	0.38	0.54	16.1	2.45	0.0	0.23	-1.20	1.98	7
		×	-0.60	0.19	1.19	1.55	1.57	9.36	₹.0	-0.10	1.89	1.13	0.20	0.38	0.43	1.55	1.57	8.0	1 .0	-1.10	1.63	0.5
		X	-0.60	0.0	1.19	6.0	0.88	0.36	89	-0.10	1.20	0.52	0.50	61.0	0.43	8.0	0.88	0.0	0.0	-1.10	\$0.0	2.0
																					· E	
							Total		×	rticel D	Vertical Deflection	n, in. ,	at Indica	ted Cage			Parker and				1	
			a ⁻¹	D2.	-F	ភ	2	9	10	80	6		ď	6	e ^m	4	2	9	$\mathcal{L}_{\mathbf{Q}}$	80	o a	
н	~	<	0.003	0.047	0.005	0.00	-0.004	970.0	0.002	0.000	0.001		-0.045	0.052	0.005	900.0	-0.007	0.018	0.001	000.0	0.00	
		A	00000	0.061	0.00	0.006	90000	0.021	0.003	0.000	0.001		-0.046	990.0	9000	0.008	0.003	0.023	0.00	00000	0.002	
		υ	-0.00	690.0	0.011	0.011	900.0	0.023	0.00t-	0.000	0.001	• •	-0.050	0.00	0.011	0.013	0.003	0.00	0.003	0.000	0.00	
		Ω	-0.002	0.070	0.013	0.016	0.307	0.08	0.00	0.000	0.001		-0.050	0.03	0.013	0.018	0.00	0.00	0.003	0000	0.002	
		ы	0.300	0.067	0.015	0.0	0.00	0.021	0.005	0000	0.00		-0.048	0.072	0.015	0.023	0.005	0.023	0.00	0.000	0.003	•
			0.00	0.052	0.017	0.036	0.016	0.015	0.003	0.000	0.00		-0.038	0.057	0.017	0.038	0.013	0.027	0.00	00000	0.00	
		o	0.00	0.036	0.016	0.049	0.027	0.00	0.005	0.000	0.008		-0.022	0.041	0.016	0.031	0.00L	0.012	0.00	0.000	0.00	
		×	0.065	0.00	0.013	0.058	0.0	C,000	0.00	0.00	0.012		0.017	0.005	0.013	0.060	0.038	0.007	0.004	0.000	0.013	
		н	0.130	0.00	0.00	0.056	0.055	0.00	0.00	0.000	0.016		0.082	0.015	0.009	0.058	0.052	0.00	0.00	0.000	0.0.7	٠
		*>	0.133	0.00	0.00	0.0	0.0	0000	0.00	0.000	0.018		0.085	6,000	0.006	9.000	0.059	0.002	0.003	0.000	0.00	P
		H	0.503	0000	0.003	0.00	0.059	-0.002	0.00	0000	0.016		0.155	0.00	0.003	0.031	950.0	0000	0.003	0.000	0.07	
		H	0.182	-0-03	0.00	9.0	0.054	-2.002	0.00	0.00	0.014		0.134	0.002	0.00	0.363	0.051	0.000	0.003	0.000	0.005	
		×	0.151	0.0	0.001	0.00.5	0.047	-0.003	c.003	0.000	0.012		0.103	0.001	0.00	n.017	0.044	-0.001	0.002	0.00	0.03	
		×	0.103	-0.003	0000	0.00	0.031	-0.403	8	0.000	0.007		0.055	0.000	0.00	0.008	0.028	-0.001	0.001	0.000	0.008	
			*	,																	,	20
				ŀ													4	1				٠
· ·		" post		1						1	(Continued)	(P)			,	ı		to our dynamics	sales estimates			-
																				0	of 15 abanes	-

Local	1				ē	19			100						Rebo	und				
tton	- L	20	-M	o.⁻→	4	94	7	8	2 0	10	L.	2		4	25	P6	. P.	8	6	10
ы	8.0	5.81	5.81 10.45 2.87 1.27	2.87	1.27	-0.18	6.42	8.0	2.50	0.51		5.72	9.15	2.73		-0.18	6.19	0.80	2.2	0.30
\$h	4.42	96.9	17.43	3.98	2.8	12.93	7.34	1.2	3.36	0.92		6.87	16.13	3.83			7.		3.10	
ဗ	0.20	98.9	13.9	8.8	-0.10	-0.18	7.2	3.41	£.4	2.97	9.0	6.77	12.6	8.3	-0.39	-0.18	6.9	র:	8	2.66
×	0.20	5.34	8.8	5.74	10.01	-0.18	5.73	5.61	₽.4	8.5		5.3	2.36	5.62			5.50		4.65	
н	0.30	3.33	15.03	5.74	3.1	-0.18	3.78	Z-7	2.8	5.74		3.24	13.73	5.62			3.55		17.1	
×	0.50	8	2.61	3.98	9.68	-0.18	1.37	8.0	3.62	5.43		8.0	1.31	3.83		-	1.1		3.36	
M	8.0	5.24	6.87	3.23	2.6	4.37	4.69	8.4	3.62	1.64		5.24	7.19	7.5			7.57		2,52	
h	0.00	7.3	92.9	3.98	5.68	8.0	7.16	4.40	4.65	14.41		8.3	7.08	3.83			7.34		F. 86	
v	8.0	3.62	10.57	4.3	7.34	97.0	5.62	5.72	5.8	94.9		3.62	10.89	4.19			5.50		5.16	
×	0.0	2.38	0.1	4.19	8.42	0.18	3.56	3.10	2.8	7.58		2.38	4.36	1.0.4			41.5		3.16	
H	0.0	1.23	0.23	3.47	8.90	0.18	1.9	0.30	4.56	8.61		1.33	0.54	3.35			1.83		1 12	
×	8.0	0.28	-0.87	3.8	2.45	0.18	69.0	-0.60	2.67	2.67		0.28	-0.55	8						

	P _Q	0.00	0.00	0.00	0.00	0.00	0.015	0.00	0.00	0.0	0.00	0.00	
	g G	0.00	000	0000	000	000.5	0.00	0000	0000	0000	0000	2	
	D _Z	0.003	00.0	0.00	0.00	0.00	0.003	0.00	0.00	0.00	0.00	9000	
	90	0.00		0.01									
Pebound	2	0.007		0.007									
	ď	0.02		0.029									
	D ₃	0.01	0.012	0.00 t	0.0L3	0.01	0.00	0.020	0.024	0.00	0.000	0.013	
8	25	990.0	0.061	6.0.0	0.035	0.083	900.0	0.091	0.074	0.052	0.032	0.017	ľ
	⁴	0.003		0.000									
	. 6 ₀ 8 ₀	0.000 0.001	0.000 0.001	0.000 0.003	0.000 0.006	0000 0000	0 000 0.014	0.000 0.003	0.000 0.007	0.000 0.012	0.000 0.019	0.000 0.026	
	7	0.003	0.00	0.00									
	90	0.017	0.0E	0.31	0.007	0.003	-0.00L	0.028	0.021	0.014	0.007	0.002	
iote.	4	0.004	0.006	o.@1	0.000	0.089	0.07	0.01	9.0	0.037	0.058	0.078	1000
	4	0.000	910.0	0.027	0.039	0.047	0.035	0.030	0.094	0.072	0.085	980.0	0 0
•	<u>.</u> -	0.011	0.012	0.014	0.a3	0.01	0.00	9.0	0.00	0.005	0.00	0.014	2000
4	2	0.055	0.050	0.038	0.00	0.A2	-0.003	0.08	0.067	0.045	0.00	0.00	ww 0
4	5	0.032	0.032	0.039 0.038 0.014 0.027	0.052	0.072	0.107	-0.00	9000	0.034	0.081	0.142	3 100
		(-)	p.	U	b:	н	×	ы	jh.	U	m	н	h

Table A-7 (Continued)

						E	1														
e e	tion tion	ο,	6.0	٥. س	an ^t	P5	P6	P7	88	P ₉	Plo	a. T	2	ъ. е.	a ^{a†}	P ₅	Pe Pe	a,	80	۵,	Plo
-	fel	0.0	92.4	7.52	2.39	0.97	0.0	6.19	2.80	2.35	0.31	0.0	4.76	7.41	2.27	0.88	-0.19	90.9	2.30	2.15	0.3
	Ģ,	13.26	5.81	13.62	3.35	2.11	125.64	7.45	5.31	3.36	1.13	13.26	5.81	13.51	3.23	2.35	25.45	7.34	5.3	3.19	1 2
	O	0.0	5.71	9.92	4.19	5.86	0.91	7.34	. 80	4.33	3.49	00.0	5.72	9.81	1.07	5.77	0.72	7.23	1.80	8	3.49
	hi	0.00	4.38	8.13	19.4	8.31	0.55	5.73	6.81	8.	5.74	0.0	4.38	21.79	4.55	8.52	0.36	5.62	6.81	1.82	5.74
	н	0.0	2.76	10.13	79.4	6.39	0.55	3.67	1.80	5.08	92.9	0.0	2.76	10.02	4.55	9.30	0.36	3.56	1.80	16.4	92.9
	hel.	0.0	92.0	0.77	3.35	ন.৪	0.55	1.36	80.0	3.70	92.9	0.0	92.0	99.0	3.23	8.12	0.36	1.15	00.00	3.53	92.9
2	\$a}	0.00	37.7	3.27	2.73	2.06	-0.19	8.15	3.70	3.61	1.64	-0.20	19.4	3.71	2.75	2.35	0.18	8.03	080	2.5	70.
	(h ₄	0.00	4.10	3.48	3.47	ਰ -	-0.37	7.80	7.00	4.82	4.92	-0.20	1.29	3.92	3-47	1.50	0.00	7.68	5.10	00	27.5
	O	-0.20	5.8	7.35	3-71	5.29	-0-37	5.74	5.40	5.34	92.9	04.0-	3.15	1.80	3.71	5.58	0.0	5.62	6.50	8.8	9.9
	tri	0.0	1.91	1.03	3.72	6.17	-0-37	3.56	3.20	5.34	7.89	-0.20	2.10	2.07	3.71	94.9	8.0	3.14	4.30	8	8
	н	0.00	0.8	-0.22	2.87	6.17	-0.19	2.07	0.20	4.73	8.81	-0.20	1.14	0.22	2.87	94.9	0.18	1.8	1.30	95.4	5
	ыd	0.00	0.10	-1-31	1.56	1.28	-0.19	69.0	-1.8	2.58	2.67	-0.20	0.29	-0.87	1.56	1.57	0.18	0.57	0.10	20.00	2.87
								100	The state of the s	2,000	1	100									
						Total			74.0	101000	1117	מה דוומדכמנים תשלפי	בבה כשאם			Dahousad				1	
		ď	22	D3	d Q	2	G ^O	70	D _B	60		$\mathbf{I}_{\mathbf{J}}$	D2	D ₃	ក្ន	D5	De	Z _Q	BB	0	
н	(m)	000.0	0.078	0.013	0.012	0.005	0.041	0.003	0.000	0.001		-0.023	0.082	0.012	0.011	0.00	0.031	0.003	0000	0.00	
	(a ₄	0.001	920.0	0.017	0.021	0.008	0.037	0.00	0000	0.002		-0.022	0.080	0.016	0.000	0.008	0.027	0.00	0000	0.003	
	O	0.012	0.063	0.000	0.037	0.014	0.031	0.005	0.000	0.005		-0.0H	290.0	0.019	0.036	0.014	0.021	0.00	00000	9000	
	H	0.032	0.043	0.00	0.054	0.026	0.00	0.005	0000	0.00		600.0	0.047	0.019	0.053	0.026	0.014	0.00	0000	0.000	
	н	0.057	0.026	0.017	0.06	0.042	0.019	0.005	00000	0.0		0.044	0.030	0.016	0.063	0.042	600.0	0.005	0000	0.01	
	×	0.162	0.005	0.008	0.055	0.066	0.012	0.004	0.000	3.022		0.139	0.009	0.007	0.054	0.068	0.002	0.00	00000	0.023	
C)	613	00000	0.134	0.029	0.039	0.015	0.052	0.00	00000	900.0		0.004	0.114	0.023	0.011	970-0-	0.047	0.007	0000	0.0%	
	fa ₄	0.011	0.108	0.035	0.075	0.025	0.040	0.011	00000	0.010		0.015	0.088	0.029	0.048	900.0-	0.035	0.009	0000	0.00	
	O	0.036	0.077	0.035	0.105	0.047	0.028	0.011	00000	0.018		0.000	0.057	0.029	0.077	910.0	0.023	0.000	0.000	0.024	
	Ħ	0.074	0.049	0.031	0.123	0.078	0.018	0.010	00000	0.027		0.078	0.029	5.005	0.095	0.047	0.013	0.008	00000	0.023	
	н	0.117	0.030	0.03	0.136	0.105	0.011	600.0	00000	0.037		0.121	0.010	0.017	0.108	0.075	0.006	0.007	0000	0.033	
	×	2.167	0.014	0.0	0.077	0.127	0.00	0.006	0.000	0.036		01	-0.006	0.005	0.049	960.0	-0.001	100°C	000.0	0.032	

							Total	1		Verti	cal Pres	Vertical Pressure, psi, at Indicated Cells	i, at In	dicated (ells		Lebound	1				
Point tion P1 P2 P3 P4 P5	P1 P2 P3 P4 P5	P1 P2 P3 P4 P5	P2 P3 P4 P5	P3 P4 P5	PL PS	25	1	9	4	80	do o	P 10	2,7-4	200	3	a, 7	15	P6	P	8	d.	01
2 E 0.00 3.82 2.61 2.51 1.76	2.51	2.51	2.51	2.51	2.51 1.76	1.76		19.49	7.80	5.60	3.79	1.2	0.0	3.82	3.37	2.63	2.15	19.30	7.57	2.30	3.71	8
3.63 2.61 3.11	3.63 2.61 3.11	3.63 2.61 3.11	2.61 3.11	2.61 3.11	3.11 3.03	3.03		0.19	7.80	5.40	4.65	4.7	0.0	3.63	3.37	3.23	3.42	0.0	7.57	8.4	4.57	4.7
2.67 2.18 3.35	2.67 2.18 3.35	2.67 2.18 3.35	2.18 3.35	2.18 3.35		3.91		0.19		7.7	5.3	98.9	0.0	2.67	2.9	3-47	4.30	0.0	5.73	6.3	5.17	98.9
н 0,00 1.72 1.09 3.11 4.40	1.72 1.09 3.11	1.72 1.09 3.11	1.09 3.11	1.09 3.11		7.40		0.37	3.67	1.80	5.34	8.09	0.30	1.72	1.85	3.23	4.79	0.18	3-44	3.40	5.26	8.09
0.00 2.63 3.91	0.96 0.00 2.63 3.91	0.96 0.00 2.63 3.91	0.00 2.63 3.91	0.00 2.63 3.91	3.91			0.19	5.06	1.70	7.56	9.15	8	96.0	92.0	2.75	4.30	0.0	1.83	0.30	4.18	9.12
-0.55 2.04 2.35	0.48 -0.55 2.04 2.35	0.48 -0.55 2.04 2.35	-0.55 2.04 2.35	-0.55 2.04 2.35	2.35		0	-19	1.26	1.00	3.62	6.25	8.0	97.0	0°2	2.16	2.74	0.0	1.03	-0.40	3.54	6.33
0.88	0.20 -0.76 1.44 0.88	0.20 -0.76 1.44 0.88	-0.76 1.44 0.88	1.44 0.88	0.88		o	61.0	0.80	0.80	2.50	2.87	0.0	0.20	0.0	1.56	1.27	8.0	0.57	09.0-	2.42	2.87
									Ver	tical De	Vertical Deflection.	5	at Indicated Gage	hed Games								
Total	Total	Total	Total	Total	Total	Total											Febound					
D ₁ D ₂ D ₃ D ₄ D ₅ D ₆	D ₁ D ₂ D ₃ D ₄ D ₅ D ₆	D ₁ D ₂ D ₃ D ₄ D ₅ D ₆	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	D3 D4 D5 D6	20 Ta) _Q 5 _Q	A	,,	20	80	6		e l	25	e E	ď,	22	90	D ₇	DB	Do	
0.156 0.035 0.046 0.014	0.156 0.035 0.046 0.014	0.156 0.035 0.046 0.014	0.035 0.046 0.014	0.046 0.014	0.014		0	0.049	0.011	00000	0.008		-0.005	0.128	0.033	0.028	0.001	0.056	0.012	0.00	0000	
0.117 0.041 0.091 0.025	0.117 0.041 0.091 0.025	0.117 0.041 0.091 0.025	0.041 0.091 0.025	0.091 0.025	0.025		0	0.038	0.013	0000	0.013		0.006	0.089	0.039	0.073	0.012	0.0.5	0.014	00000	0.004	
0.080 0.041 0.125	0.080 0.041 0.125 0.049	0.080 0.041 0.125 0.049	0.041 0.125 0.049	0.125 0.049	6,000		0	KC	0.013	00000	0.022		0.030	0.052	0.039	0.107	0.036	0.032	0.024	0.00	0.003	
	0.048 0.034 0.146 0.088	0.048 0.034 0.146 0.088	0.034 0.146 0.088	0.146 0.088	0.088		0.0	2	0.CL	0.000	0.034		0.079	0.020	0.032	0.128	0.075	0.00	0.012	0.000	0.035	
0.025 0.171	0.028 0.025 0.171 0.121	0.028 0.025 0.171 0.121	0.025 0.171 0.121	0.171 0.121	0.121		0	g	0.00	0.000	0.045		0.137	0.000	0.023	0.153	0.108	0.00	0.000	0.00	0.016	
0.016 0.016 0.137 0.140	0.016 0.016 0.137 0.140	0.016 0.016 0.137 0.140	0.016 0.137 0.140	0.137 0.140	0.140		0	-0.001	0.007	0.000	0.048		0.154	-0.012	0.014	ولد.0	0.127	0.006	0.008	00000	0.00	
0.0	0.009 0.02 0.091 0.144	0.009 0.02 0.091 0.144	0.01 0.091 0.144	0.091 0.144	0.144	•	0	경	-0.035	0.00	0.04		0.187	-0.019	0.008	0.073	0.131	0.003	-0.01	0.000	0.0	

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	Total	Too					Total			Vert	cal Pre	Vertical Pressure, psi	7	at Indicated	Cells		Febound	pur				
Row	Point	tion	L L	P	۳.	P.	PS	9	P7	8	P ₉	P10	P. 1	P2	<u>م</u>	ol T	P5	9	7	8	Pg	Pic
5	4	4	0.0	1.24	0.11	0.84	0.30	-0.37	1.95	-0.40	0.86	0.0	-0.20	1.43	0.55	0.84	65.0	00.0	1.83	0.70	0.52	0.20
		m	0.0	5.00	0.33	98.0	0.30	-0.37	3.22	-0.20	1.03	00.00	-0.20	2.19	0.77	96.0	65.0	0.0	3.10	8.0	69.0	0.2
		U	0.00	3.15	1.09	1.1	0.59	-0.19	5.39	0.30	1.72	0.2	-0.20	3.3	1.53	1.14	0.88	0.18	5.27	1.40	1.38	0.41
		a	0.0	3-43	1.31	1.56	69.0	-0.73	6.08	1.00	1.89	0.21	-0.20	3.62	1.75	1.56	96.0	-0.36	2.8	2.10	1.55	0.41
		le2	00.00	3.91	2.07	1.92	0.99	-0.55	6.77	2.10	2.32	0.41	-0.20	4.10	2.51	1.92	1.28	-0.18	6.65	3.20	1.98	0.6
		fis.	0.00	P. 148	3.27	2.51	1.77	0.0	7.92	3.70	3.27	1.23	-0.20	13.4	3.72	2.51	5.06	0.37	7.80	4.80	2.93	7.7
		o	8.0	4.19	3.27	3.23	3.82	-0.37	7.92	3.70	4.56	16.4	-0.20	4.38	3.77	3.23	1.11	0.00	7.80	4.80	4.22	4.5
		m	0.00	3∙34	1.36	3.71	5.19	-0-37	6.43	8.4	5.16	6.35	-0.20	3.53	4.80	3.7	5.48	0.0	6.31	6.00	4.82	6.9
		H	0.0	5.19	2.61	3.71	5.88	-0-37	2.3	4.20	5.45	7.38	-0.20	2.38	3.05	3.77	6.17	00.0	4.13	5.30	5.08	7.5
		h	0.0	1.14	0.22	3.35	95.9	-0.19	2.41	0.80	4.99	9.05	-0.20	1.33	99.0	3.35	6.85	0.18	5.29	1.90	4.65	9.8
		×	0.0	0.57	-0.76	2.63	4.41	0.00	1.50	-0.60	0.7	7.38	-0.20	0.76	-0.35	2.63	02.4	0.37	1.38	0.50	3.70	7.5
		ы	0.0	0.29	-1.09	2.27	3.0	-0.19	1.0	-0.80	3.53	5.12	-0.20	0.48	-0.65	2.27	3.32	0.18	0.92	0.30	3.19	5.3
		×	0.20	0.10	-1.09	1.80	1.87	-0.19	0.81	06.0-	2.92	3.49	0.00	0.29	-0.65	1.80	2.16	0.18	0.69	0.20	2.58	9.6
		22	0.20	60.0-	-1.31	1.20	0.50	-0.37	0.58	-1.00	5.06	44.1	0.0	0.10	-0.87	7.50	62.0	0.00	94.0	0.10	1.72	1.6
									Ve	Verifuel Deflection	Tank for		Thefas	2					1			
							Total			1	0		מי דוותר המרכם המינים	מבים השמים			Rehound					
			L _Q	D2	P3	E.b.	25	90	D2	P _B	0		r _o	D2	D3	70	2	90	22	Вд	, L	
5	п	٧	0.010		0.004	0.000	0.021	0.00	0.00	0.000	0.007	٠	0.014	0.000	-0.002	-0.018	0.00	0.014	0.000	0.000	0.003	
		A	0.00		0.006	0.00	0.017	0.028	3.003	00000	0.006		0.008	0.063	00000	-0.0m	-0.014	0.023	0.001	000.0	0.00	
		υ	-0.001		0.012	0.012	0.012	0.043	0.305	000.0	00.0		0.003	0.093	0.006	-0.016	-0.019	0.038	0.003	0000	0.000	
		A	-0.00		0.015	0.015	0.011	0.057	0.005	00000	0.00		0.000	0.103	0.009	-0.013	-3.020	0.052	0.003	0.000	0.000	
		\$43	-0.002		0.019	0.018	0.011	990.0	0.00	00000	0.00		0.000	0.110	0.013	-0.010	-0.020	0.061	0.00	00000	0.000	
		fa,	-0.001		0.026	0.032	0.013	0.054	0.008	00000	0.000		0.003	0.115	0.020	0.00	-0.018	0.000	0.006	00000	0.002	
		O	0.00		0.034	0.068	0,323	0.042	0.000	00000	0.010		0.014	0.093	0.028	0.000	900.0	0.037	0.008	0.000	0.006	
		H	0.000		0.035	0.095	0.039	0.032	0.01	0.00	0.015		0.030	0.067	0.029	0.067	0.008	0.027	0.009	00000	0.01	
		H	0.059		0.033	0.117	0.057	0.02	0.010	0.000	0.004		0.063	0.037	0.027	0.089	0.036	0.016	0.008	0000	0.000	
		Po	0.107		0.00	0.135	0.098	0.013	0000	0.000	C.034		0.111	910.0	0.019	0.107	290.0	900.0	0.007	0.000	0.030	
		84	0.133		0.018	0.123	0.120	0.007	0.008	0.00	0.000		0.137	0.002	0.012	0.095	0.089	0.002	0.006	0.000	0.036	
		ы	0.148		6.015	0.108	0.127	0.005	0.007	0.000	0.000		0.152	-0.000	00000	0.080	960.0	0.001	0.005	0.000	0.036	
		×	0.162	0.016	0.013	0.091	0.129	0.00	90000	0.000	0.038		0.166	-0.004	0.007	0.063	0.098	00000	0.004	0.000	0.034	
		m	0.141		0.00	0.058	0.114	0.003	0.005	00000	0.030		0.145	-0.008	0.003	0.030	0.083	-0.002	0.003	0.000	0.026	

										Vert	cal Pre	Vertical Pressure, psi, at Indicated Cells	d at In	dicated	Cells							П
Ros	Point	Location	12	.p2	P	P.	P ₅	Pe Pe	P	P8	Pg	P10	P.	P2	e.	4	P S	P6	P	P8	60	Pao
5	N	٧	0.0	1.53	0.32	1.32	0.0	य-४	3.2	0.70	1.12	0.20	0.00	1.62	0.43	1.1	0.20	23.148	3.33	0.50	1.12	0.20
		M	0.0	2.10	0.76	1.08	0.19	7.0	5.0	1.00	1.64	0.41	0.0	2.19	0.87	1.20	0.39	3.27	5.16	0.80	1.64	0.41
		υ	0.0	2.67	1.41	1.56	0.58	1.82	6.65	2.00	2.50	0.71	0.00	2.76	1.52	1.68	0.78	1.09	6.77	4.80	2.50	D.7
		Д	0.00	5.86	1.85	1.80	0.78	58.81	6.88	6.0n	2.85	1.00	0.00	5.62	1.96	1.92	0.98	58.08	7.00	5.81	2.85	8
		(a)	0.00	5.86	2-39	2.04	1.17	88.85	7.34	2.60	3.54	1.8	0.00	5.32	2.50	2.16	1.37	88.12	7.46	5.40	3.54	2.2
			0.0	2.58	2.72	2.51	2-15	0.91	6.99	5.60	1.40	4.7	0.0	2.67	2.83	2.63	2.35	0.18	7.11	5.40	017	17.7
		o	0.00	1.91	1.85	2.75	2.93	0.91	5.6	7.81	4.91	6.86	0.00	2.00	1.8	2.87	3-13	0.18	5.16	7.62	16.4	6.86
		H	0.00	1.15	0.98	2.63	3-13	0.73	3.2	4.40	16.4	7.89	0.00	1.24	1.09	2.72	3.33	00.00	3.33	2.30	1.9	7.89
		н	0.00	C. 58	0.32	2.27	2.54	5.73	1.72	1.40	2.3	9.12	0.00	19.0	0.43	2.39	2.74	0.00	1.8	1.20	4.22	9.12
		5	0.0	0.10	0.00	1.56	1.46	0.54	0.92	09.0	3.19	6.14	0.0	0.19	0.11	1.68	39.1	-0.19	1.0	0.40	3.19	6.14
		ad	0.0	60.0-	-0.53	1.03	0.58	0.73	0.34	0.40	2.33	3.07	8.0	0.0	-0.11	1.20	97.0	00.0	97.0	0.20	2.33	3.07
		ı	0.0	-0.19	-0.52	0.8	0.39	0.73	0.23	0.40	1.81	7.5	00.0	-0.10	17.0-	96.0	0.59	0.00	0.35	0.20	1.81	1.9
		×	0.00	-0.19	-0-33	0.60	0.10	0.73	0.23	0.40	1.47	1.33	0.00	-0.10	-0.22	0.72	0.30	00.0	0.35	0.20	1.47	1.33
		N	0.0	-0.28	-0.33	0.36	-0.20	96.0	0.0	0.30	0.87	19.0	0.0	-0.19	-0.22	0.48	0.30	-0.37	0.12	0.10	0.87	0.61
									Ve	Vertical Deflection	eflection	ţn.	at Indicated Gage	ted Gage	100			The second				
			L D	02	D ₃	ď	Total	90	7-3	DB	60		4	D2	23	ď	Febound D ₅	90	D_{7}	DB	20	
10	N	4	0.064	0.137	0.009	-0.001	0.007	0.054	0.005	00000	600.0		-0.009	0.099	0.007	-0.010	-0.003	0.063	0.00	00000	0.010	
		A	60000	0.186	0.018	0.003	0.003	0.072	0.00	00000	0.007		-0.064	0.148	0.00	-0.006	-0.007	0.001	90000	0000	90000	
		o	0.007	0.207	0.030	0.016	0.003	0.083	0.013	0.000	0.007		990.0-	0.169	0.028	100.00	-0.007	0.09	0.002	00000	0.008	
		J	0.008	0.242	0.036	0.005	0.00	0.083	0.015	0.000	0.008		-0.065	0.204	0.034	0.000	-0.006	0.092	0.00	0.000	600.0	
		ы	0.00	0.274	0.044	0.047	0.007	0.078	0.017	0000	0.000		-0.063	0.236	0.042	0.038	-0.003	0.087	0.000	00000	0.01	
		Jhr	0.021	0.198	0.00	0.106	0.022	0.061	0.019	0000	0.018		-0.052	0.160	0.048	0.097	0.012	0.070	0.018	0.000	0.019	
		O	0.232	0.111	0.050	0.151	0.053	0.039	0.019	0.000	0.030		0.159	0.103	0.048	0.142	0.043	0.048	0.018	0.000	0.031	
		h	0.098	0.10	0.044	0.177	0.099	0.022	0.017	0000	0.0.5		0.005	990.0	0.042	0.168	0.089	0.031	0.026	0000	9.0.0	
		н	0.209	0.082	0.032	0.204	0.174	0.010	0.015	00000	0.059		0.136	0.044	0.030	0.195	0.124	0.019	0.024	00000	090.0	
		P ₃	0.207	0.067	0.021	0.165	0.157		0.011	0.000	0.065		0.134	0.020	0.019	0.156	0.147	0.012	0.010	0.000	0.066	
		×	0.289	0.060	0.014	0.113	291.0		0.00	00000	0.062		0.26	0.022	0.012	0.10	0.157	0.008	0.008	0 000	0.053	
		ы	01285	0.058	0.011	0.090	0.159		0.007	0.000	0.057		0.212	0.000	0.009	0.081	0.149	0.006	90000	00000	0.058	
		×	0.238	0.056	0.000	0.069	0.142	-0.004	0.006	0.000	0.049		0.165	0.0.8	0.008	0.060	0.132	0.005	0.005	0.000	0.000	
		ts.	0.179	0.05	0.007	0.048	0.000	-0.005	0.00	0.000	0.033		0.106	0.016	0.005	0.039	0.089	0.004	0.003	00000	0.034	
											(Continued	(pend								()	(7 of 15 sheets)	1
																					0 7 70	ren and

Table A-7 (Continued)

										A	ertical	Pressur	Vertical Pressure, psi, at Indicated Cells	at Indi	cated Ce	112							
	Tony	1000					T	otel										Febound	pur				
Row	Potnt	tion	a.**	4	مهم	O.	4	4	Ld	89		۵,	P 10	4,4	20	مرا	Δ.	25	40	P		0.0	01,
9	r4	M	0.0	5.148	1.20	1.32	0.39		8 6.08			2.16 0.	0.61	0.00	2.57	1.31	3.5	0.50	-0.55	6.20	2.80	2.16	0.61
		fe _t	0.00	2.86	2.18	2.04	0.08		7.57						5.3	2.29	2.16	1.18	97.23	59.2	5.61	3.36	1.64
		O	0.0	2.67	2.9	2.39	1.96			_					2.76	3.05	2.51	5.8	0.36	7-34	5.81	41.4	3.89
		313	0.0	2.10	2.07	2.73	2.74		3 5-73						2.19	2.18	2.87	30.00	00.0	5.85	7.41	2.83	6.55
		н	0.0	1.34	1.20	2.63	3.13								1.43	1.31	2.75	3.33	0.18	3.67	8.4	5.00	7.68
		×	8.0	0.29	0.0	1.56	1.76	0.73	3 1.03	3 0.60		5 15 7.			0.39	u.º	1.68	8	0.0	1.15	0.40	3-45	7.07
	C	(a)	-0.80	1.62	5.29	1.20	0.59	•					·		1.91	1.64	1.44	0.78	-1.10	5.62	1.50	2.58	1.6
		fa _t	-0.80	1.43	3.92	1.44	1.07	•	1.82				•	0.80	1.72	3.27	1.68	1.36	-1.10	5.16	2.10	3.27	2.97
		o	0.00	1.24	2.07	1.92	1.8	0.00	3.79	9 1.60					1.53	1.42	2.16	2.15	00.00	4.13	2.50	50	4.41
		m	0.0	92.0	1.31	1.58	2.15	0.00	2.4]			3.88	18.4	0.0	1.05	99.0	1.92	2.34	00.00	2.73	0.80	8	5.12
		н	0.00	0.29	0.87	1.44		0.00	1.15	5 -0.80				0.00	0.58	0.22	1.68	1.76	0.0	1.49	-0.30	3.5	5.33
		×	0.20	0.00	0.65	0.72		0.00	0.12	2 -1.30				0.20	0.38	0.00	8.0	0.78	0.00	0.0	-0.70	1.6.	1.74
											1												
							Total			Vertica	1 Defle	Vertical Deflection, in.		at Indicated Gages	d Gages			Labranad					
			G.	20	P P	å	2	90) _Q	80	L¦	0.	ħ	a	02	D3	å	D _D	26	L_{Q}	5	200	
9	1	ge?	0.007	0.191	0.025			3 0.081	31 0.01			0.007	ř		0.153	0.023	-0.001	-0.007	060.0	0.010	0.000	0.008	
		Ba.	0.008	0.273	0.043					17 0.000		0.009	Ĭ		0.235	0.041	0.032	-0.005	0.088	0.016	0.000	0.000	
		C.	0.017	0.218	0.048			990.0 4				0.015	Ĭ		0.180	0.046	0.078	0.007	0.075	0.018	0.000	0.006	
		tr:	0.036	0.155		0.141		2 0.045	610.0 5			989	ĭ	0.037	0.117	6.0.0	0.132	0.032	0.054	0.018	0.000	0.027	
		н	0.081	0.111				920.0 6				0.042	9		0.073	0.044	0.160	0.079	0.035	0.004	00000	0.043	
		ĸ	0.509	0.067				0 0.003	3 0.011	000.00		790			0.029	0.020	0.166	0.150	0.012	0.000	0.000	0.058	
	N	(in)	0.010	0.505				411.0 6				018	Ĭ		6.219	0.000	0.018	-0.035	0.116	0.02	0.000	-0.001	
		B ₄	0.017	0.145					620.0 61			680	•		0.152	0.048	0.082	-0.019	0.0	0.02	00000	-0.003	
		O	0.032	0.088				0.08		_		670	9	0.000	0.105	0.050	0.133	0.016	960.0	0.0	0.000	0.017	
		tr:	0.056	0.050		0.203						620 0)	0.044	2.067	0.045	0,169	0.038	0.026	0.022	0.000	0.047	
		н	0.075	0.023	0.038	0.225	0.151	1 0.034	34 0.021	0000		501.0	,	0.063	0.00.0	0.030	0.191	0.107	0.00	0.017	0.000	0.073	
		×	0.00	0.002								1.210	9	0.082	0.019	0.00	0.000	0.140	-0.012	0.007	0.000	0.089	

					-															
	4	2	-	6.0	25	9	27	8	40	P10	a ⁻¹	20	4	P.	PS	P6	P7	88	6	4
-	0.0		0.22	0.60	0.50	-0.37	2.6	09.0	0.95	0.41	0.00	1.34	-0.43	9.0	0.39	-0.37	8	1.20	1.03	0.7
U	0.00		0.43	0.8	0.20	-0.37	3.79	1.00	1.38	0.41	0.0	1.72	-0.22	1.08	0.39	-0-37	1.13	1.60	1.46	0.7
0	0.6		0.65	8.0	0.30	-0.37	1.3	1.00	1.6	19.0	19.0	1.72	0.0	1.20	64.0	-0.37	1.59	1.60	1.72	0
*	3.62		92.0	1.08	0.39	-0.37	4.4	1.20	1.90	7.0	3.62	1.91	0.11	1.32	0.58	-0.37	38	1.80	1.8	0.1
•	4.8		1.52	1.20	64.0	-1.10	5.16	1.00	2.33	1.00	4.8	2.50	0.87	1.44	99.0	-1.10	5.50	1.60	2.41	1.3
0	-0.80	,	4.14	1.1	96.0	-1.10	\$:	1.30	3.05	2.2	-0.80	1.81	3.49	1.68	1.17	-1.10	5.28	8.1	3.10	2.5
M	-0.80		2.20	1.56	1.47	-0.92	3.79	1.60	3.54	3.48	-0.80	1.43	1.6	1.80	39.1	-0.99	4.13	2.20	3.62	3.7
H	0.0		1.52	1.80	2.25	0.0	2.6	0.50	3.97	19.7	8.0	1.15	0.87	2.04	2.44	0.00	2.98	1.10	8.4	4.9
7	9.0	0.48	1.09	1.56	1.86	9.0	1.49	-1.80	3.54	5.12	8.0	0.77	11.0	1.80	2.03	0.0	1.83	1.20	3.62	5.43
*	0.0		0.87	1.20	1.18	0.0	69.0	-1.00	2.85	3.79	0.00	0.38	0.22	1.14	1.37	0.00	1.09	0.40	2.93	4.1
ı	0.50		0.65	96.0	0.78	9.	0.35	-1.10	2.33	5.66	0.20	0.38	0.00	1.20	0.97	0.0	0.01	-0.50	2.41	2.9
*	0.20		0.65	0.72	0.78	8.0	0.12	-1.20	1.98	1.74	0.50	0.38	0.0	96.0	16.0	00.0	94.0	-0.60	2.06	2.0
	0.00		まい	0.48	0.20	0.0	17.0-	-1.40	1.21	19.0	0.0	0.10	70-	0.72	0.39	0.00	0.23	-0.80	1.29	6.0

				Total		A	rtical D	ertical Derlection, in.	n., at Indica	ed Gages			Rebound		l		1
r D	7 E 2 L	3	ď	ď	90	4	80	60	ar a	22	e G	ď	ď	200	D _Z	82	Do
0.01	0.093	0.00	0.00	0.00	0.094	0.007	0.00	0.016	0.00		0 00	-0.033	-c.035		0.003	000	-0.016
0.000	0.243	0.018	0.005	0.00	0.122	0.025	0000	0.013	-0.002	0.160	0.000	-0.029	-0.00	0.39	0.01	0.00	-0.00
0.00	0.157	0.023	0.008	0.003	0.131	0.013	0.000	0.012	-0.00	0.174	0.015	-0.026	-0.041	0.103	0.00	0.00	-0.000
0.007	0.171	0.030	0.03	0.005	0.140	0.017	0000	0.012	-0.005	0.188	0.022	-0.02	-0.042	0.112	0.03	0.00	-0.020
0.00	0.199	0.044	0.038	9000	0.146	0.063	0.00	0.00.5	-0.003	0.26	0.036	0.00	-0.038	0.118	0.009	0.00	-0.01
o.a5	0.158	0.034	0.000	0.00	0.125	0.028	0.00	90.0	0.003	0.175	0.046	0.066	-0.02L	0.097	0.00	0.000	-0.006
0.00	0.104	0.058	1.530	0.046	0.095 0.029	0.00	0,000	0.000 0.041	0.014	0.121	0.050	0.119 0.002	0.002	0.067	0.025	0000	0000 0000
C.046	0.059	0.053	0.190	9600	0.062	0.027	0000	0.070	0.034	0.076	0.045	0.156	0.052	D.C34	0.023	000.0	0.038
0.070	0.034	0.044	0.223	0.138	0.041	0.023	0.000	960.0	0.058	0.051	0.036	0.189	0.00	0.013	0.00	0.00	0.004
0.0	0.014	0.030	0.207	0.167	0.006	0.007	0000	911.0	0.072	0.031	0.022	0.173	0.123	-0.00	0.013	0.00	0.084
0.00	0.00	0.00	0.174	0.181	0.021	0.07	0.300	0.122	0.083	0.00	0.017	0.140	0.137	-0.007	0.00	0.000	0.000
0.00	0.00	0.020	0.140	0.184	0.008	0.012	0000	0.122	0.082	0.021	0.012	0.106	0.140	-0.00	900.0	0.000	0.000
0.00	-0.00	0.01	0.092	0.167	0.004	0.008	0000	0.109	0.067	0.016	900.0	0.058	0.123	-0.01h	0.00	0000	0.077

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(9 of 15 sheets)

							2	101		Ve	Vertical Pressure,		psi, at Indicated	ndicated	Cells		Debo	President				
8	of it	tion	4	4.0	a,m	a.	25	9	q.	P8	0.	Plo	P.	20	a.e	4	P	26	7	PB	40	P
1	cv		0.00	1.05	0.33	0.72		-0.18					0.00	98.0	0.33	0.72	0.20	-0.36	3.2	1.21	1.39	0.61
		U	0.0	1.15	99.0	96.0		-0.18					0.00	0.95	99.0	6.36	0.39	-0.36	3.90	1.41	1.72	0.7
		Q	0.00	1.24	0.87	96.0							0.00	1.3	0.87	96.0	65.0	-0.18	2.03	1.41	2.07	0.82
		M	0.0	1.15	0.98	1.08		0.0				0.61	0.00	8.0	96.0	1.08	0.59	-0.18	4.02	1.41	2.2	1.00
			0.0	1.15	1.3	1.20							0.0	0.08	1.32	1.20	69.0	00.00	3.67	1.8r	2.76	1.53
		v	8.0	98.0	6.76	1.20							0.00	19.0	92.0	1.20	1.27	00.0	2.73	1.11	2.93	2.3
		=	0.20	0.58	77.0	1.20							0.20	0.39	0.44	1.20	3.37	00.0	1.8	19.0	7 7 4 8	2.56
		н	p.4-	0.38	0.22	96.0		0.18	0.98			1.8	4.0	0.19	0.22	8.0	0.98	0.0	1.15	0.20	2.41	2.3
		יי	8.0	67.0	0.0	0.72			0.46				0.00	0.00	0.0	0.72	0.78	800	69.0	8.0	1.8	1.53
		M	0.0	0.00	0.0	0.48		0.18	0.12				0.0	-0.19	0.00	0.18	0.39	00.0	0.35	0.00	1.38	0.82
		.1	0.0	0.0	0.0	0.48			0.0	Ċ	0.9		0.0	-0.19	0.00	0.48	0.39	00.0	0.3	-0.10	1.12	0.61
		×	8.0	0.00	00.0	0.24	0.30	0.18	0.0	17.0-	0.69	0.0	0.0	-0.19	0.00	0.2	0.30	0.0	0.23	-0.10	98.0	0.41
		K	0.0	0.0	0.0	0.2		0.18	-0.11		0.35		0.0	-0.19	0.0	0.24	0.20	0.00	0.12	-0.10	0.52	0.41
										Vertical Deflection.	Deflects	1.2	in. at Indicated Gage	ted Gage	00						1	
							Total			0.00							Rebound					
			r o	D2	E D	ล้	50	90	- P7	P ₈	64		ď	D2	D3	á	25	90	DZ	Ba	60	
-	N	Ø	0.00	0.168	0.018	0.00		0.183	3 5.016	00000 9		10	0.009	0.127	0.01	0.02	-0.023	0.147	0.002	00000	-0.006	
		υ	0.00	0.201	0.032					9 0.000	0.006	10	0.00	0.160	0.028	-0.008	0.023	0.179	0.022	0.000	-0.085	
		Ω	0.00	0.231	0.037							6	0.000	0.190	0.033	0.002	-0.020	0.200	0.026	0.000	0.02	
		(A)	900.0	0.259	0.042							~	0.011		0.038	0.000	-0.01	0.232	0.031	0.000	-0.018	
		Be	0.00	0.189	0.048				9 0.038	8 0.000		-	0.005		0.042	0.077	-0.00	0.162	0.034	0.000	-0.00	
		ø	0.00	0.130	0.049							60	0.004		0.045	0.126	0.025	0.100	0.035	0000	0.027	
		þt	0.030	0.091	0.041						S 0.2	OI.	0.035	0.050	0.037	0.147	0.058	0.062	0.030	0.000	0.072	
		н	0.040	0.070	0.031					00000 9		64	0.045		0.027	0.179	0.101	0.039	0.002	00000	0.10	
		47	0.050	0.051	0.018	0,169	0.153	3 0.055	5 0.018	b 0.000	0.156	2	0.055	0.010	0.014	0.139	0.124	0.015	0.014	0.000	0.125	
		×	0.03	0.049	0.005				_	3 0.000		6	0.058	0.008	0.011	0.092	0.132	0.013	0.009	0000	0.128	
		н	0.049	0.05	0.012				_	1 0,000	1	0	0.054	0.00	0.008	0.065	0.123	0.000	0.007	00000	0.119	
		×	0.041	0.043	0.00			0.043				10	0.046	0.002	0.005	0.047	0.107	0.007	0.005	0.000	0.104	
		K	0.00	0.041	0.007				0.00	0.000	0.00	10	0.029	0.00	0.003	0.021	0.065	0.005	0.002	0.000	0.084	

(Continued

	Pag.	400					Tot	13		Vert	Ical Pre	Vertical Pressure, psi, at Indicated Cells	if at In	dicated (Sells		e H	100				11
HOW	Point	tion	~~	200	P ₃	Q,	2	Ch.	4	es.	6	P10	e d	2	0,01	A. 2	2	P	P	a)	20	P.20
80	н	(le3)	0.0	1.43	9.0	8.0	0.3	-0.37	4.12	09.0	1.63	0.41	8.0	1.53	0.76	1.20	0.39	-0.37	1,35	1.80	1.81	0.63
		ja,	0.0	1.52	1.31	1.20	0.59	-0.37	4.58	0.50	2.32	0.82	0.0	1.72	1.42	1.1	0.59	-0.37	2	1.70	2.50	8
		v	0.0	1.43	2.51	1.32	0.83	-0.18	1.47	0.60	2.8	17.1	0.00	1.53	2.62	1.56	0.38	-0.18	4.70	. 80	8	25.1
		Ħ	0.0	1.14	1.42	1.44	1.37	0.0	3.44	0.40	3.18	2.26	0.0	1.24	1.53	1.68	1.37	0.0	3.67	1.60	3.36	2,46
		н	0.00	0.76	£.0	1.4	1.66	0.18	2.17	-0.40	3.27	2.87	0.0	0.86	99.0	3.68	1.66	0.18	2.40	0.80	3.45	3.07
		×	0.0	0.0	0.1.	9.0	0.88	0.0	0.57	-1.10	2.23	5.03	8.0	0.19	0.22	1.08	0.68	0.00	0.80	0.10	2.41	8
	CV.	(e)	0.50	0.77	99.0	0.72	0.49	0.37	2.98	0.91	1.72	0.51	0.30	80.0	99.0	0.72	64.0	00.00	2.08	3,11	1.81	0.69
		ñ.	0.30	29.0	0.87	96.0	0.78	0.37	2.73	1.41	2.07	0.92	0.20	98.0	0.97	8	0.78	3	2	8	2.16	1.03
		O	0.30	0.148	44.0	96.0	0.98	0.37	2.07	4.0	2.33	1.23	0.20	29.0	77.0	800	98.0	80.0	2.07	2.91	2,12	2 4
		Ħ	0.20	0.19	0.33	8.0	1.07	0.37	1.36	0.20	2.15	1.7	0.30	0.38	0.33	0.0	1.07	3.0	8	2.10	200	193
		н	0.20	0.10	0.22	0.8	0.83	0.37	69.0	00.00	3.8	m = 4	0.20	0.39	9	80.0	0.88	00.0	9.0	2.50	8	1.54
		set.	0.00	-0.19	0.0	0.36	0.39	0.0	0.00	-c.30	800	0.41	00.00	00.0	0.0	0.36	0.39	-0.37	0.00	8	1.04	0.52
			į																			ĺ
									Ve	Vertical D	Deflection	in.	at Indica	ושמשני השו								
			c	D	C	-	1000	c	c	6	6		6	1	6		Personna					
				2	4	4	, i	9	7	8	0		2	2.0	Pa Pa	a ^a	2	90	24	1.8 8	DO	
00	н	šaž	0.00	0.196		0.016	00.00	0.158	0.028	00000	0.007		0.0	0.147	0.00	-0.00	-0.00	0.12%	0.00	0000	-0.003	
		Ba .	0.002	0.255		0.043	0000	0.194	0.027	0.000	0.012		0.027	0.206	0.038	0.00	0.001	0.160	0.0	0.000	000	
		ø	0.00	0.212		160.0	0.000	2.161	0.031	0.000	0.022		0.031	0.163	0.046	0.077	0.012	0.127	0.000	0000	0.00	
		ju;	0.00e	0.151		1.530	0.00	0.114	0 033	0.000	0.043		0.01	0.102	0.0.9	0.136	0.037	0.000	0.033	0.00	0.033	
		н	0.032	0.100	0.049	1.810	0.005	0.075	0.029	0.000	0.078		0.057	0.057	0.044	0.164	180.0	0.041	0.07	0.00	80.0	
		×	0.060	2.067		1.870	0.154	0.034	0.016	0.000	1.270		0.085	0.018	0.001	0.170	0.146	0000	0.014	0.000	0.17	
	(V	963	-0.012	0.138		0.007	-0.008	0.226	0.033	0.000	-0.005		0.03	0.140	0.036	0.000	0.021	0.215	0.035	0.000	0.00	
		Ba.	-0.006	0.098		0.074	0.00	0.164	0.037	0.000	0.012		0.011	0.100	0.041	0.087	0.023	0.153	0.039	00000	0.029	
		0	0.00	0.058		0.108	0.028	0.109	0.037	0.000	0.044		0.019	0.000	0.001	0.121	0.047	0.098	6:03	00000	0.001	
		3C	0.013	0.029		0.131	0.063	0.07	0.033	0.000	0.088		0.030	0.031	0.036	0.142	0.382	0.000	0.035	00000	0.105	
		Н	0.00	0.011		0.148	0.088	0.048	0.0	00000	611.0		0.041	0.013	0.006	0.161	0.107	0.037	0.027	0.000	0.136	
		×	0.086	-0.003		C.067	0.109	0.00	0.01	0000	0.116		0.043	-0.006	0.000	0.080	0.128	0.01	0.03	000	0 163	

	Plo		8	1.42	8	2.86	1.6	0.82	3.6	1.43	1.8	1.43	0.61													1		
	90	1.55	2.00	2.58	8	2.93	2.07	1.73	2.07	2.24	2.16	1.90	10.1		l	60	-0.08	-0.0	00°0-			0.118	-0.030	-0.014	0.019	0.000	0.100	
	8	1.41	1.41	1.	1.33	0.7	0.00	8.8	2.30	1.30	0.70	0.30	0.0			_B _Q	0000	0.000	0.000	0.000	00000	0.000	0000	00000	00000	0000	00000	
	PT	3.67	70.4	8	80.0	2.07	0.69	86.8	2.6	2.07	1.38	o.8	0.35			$L_{\mathbf{Q}}$	0.018	0.00	0.033	0.035	0.031	0.017	0.028	0.033	0.034	0.029	0.021	
pu	P-	-0.18	0.18	0.18	00.00	8.0	0.00	-0.54	-0.36	-0.36	-0.36	-0.36	0.0			D6	0.157	0.223	0.179	0.115	2.072	0.025	0	0.163	0.107	0.064	0.000	
Rebound	مين	0.39	0.59	0.78	1.18	1.37	0.78	6.29	64.0	69.0	0.78	0.59	0.50		Rehoused	57	.003	0.00	-0.008	0.006	0.057	0.118	900.0	0.003	0.021	0.051	0.074	
1	α, ²³	8.0	96.0	8	1.30	1.30	9.0	0.72	0.84	0.8	0.84	0.72	0.36	1		4	7000						0.005	0.055	0.080	0.100	0.107	
	۳.	44.0	0.87	1.3	0.87	44.0	0.11	0,43	0.54	0.43	0.43	0.22	0.0	ŀ		D ₃	0.022				0.041	0.mg			0.033	0.027	0.000	
	2	%.0	1.03	96.0	79.0	0.39	0.0	98.0	0.77	0.58	0.38	0.29	0.10	Gares		D2	0.137	0.509	0.164	0.101	090.0	0.017	0.101	0.078	0.048	0.022	0.007	
	P_1		00.0				á	0.00				00.0	80.0	at Indicated Gages		Į.						950.0					0.022	
	Pro							0.51				Ĭ	1	in. et				Ŭ	Ü	_			ĭ	ĭ	•	Ü	Ü	
	⁶						_	1.64 0.								్డా	80	0.00.0	0.022	670	060	149	0.012	929	061	2115	J.144	
	i													Vertical Deflection		l :	c.oc. 0.						0.000	Ü		0.000	0.000	
	8						•	1.20				9 -0.50	•	Vertica		8 _Q											Ĭ,	
	27			3.67		8 1.84	94.0 8				2 1.26		1 0.23			₂	33 0.022				28 0.035		5 0.033	71 0.038			920.0 84	
btal	9,6	00.00	0.00					0.37				0.55				90			1 0.215			7 0.061					2 0.04B	
	4	0.35	0.55					0.29	0.49						Total	2						3 0.147						
4	a7	0.8	%	1.20	1.20	1.20	8.0	0.72	0.84	8 0	0.8	0.72	0.36			ดี			0.053								0,115	
6	.m	7110	0.87	1.33	0.87	77.0	1.0	0.43	0.54	0.43	0.43	0.23	0.0			_E m						0.083						
•	, CV	1.15	1.24	1.15	98.0	0.58	0.19	0.86	0.77	0.58	0.38	0.29	0.10			20	0.178	0.250	0.205	0.142	0.101	0.058	0.00	0.075	0.045		0.00	
0	4	0.0	0.00	0.30	0.0	0.20	0.0	0.0	0.0	8	°.00	0.0	0.0			In Indian	0000	0.00	0.00	0.016	0.028	0	900.0	0.01	0.016	0.086	0.036	
Loca	tion	(a)	(a.	ø	DES	н	ж	m	(in	o	m	н	M				(sa)	Bu	O	ini	н	×	ы	(te	v	h	н	
Logg	Potnt	-1.						N									н						N					
	Row	0															0											

										Ver	Vertical Pressure,	essure, p	si at In	at Indicated Cell	Cells							1
3	Load Lo		9	0	,	•	Tot	1	-								Feb	ound				
2.1	비	lon	4	2,	4	4	12	9	17	8	2	201	4	4	4	4	25	P6	74	88		Plo
	-	M	0.50	0.77	-1.85	0.72	0.39	3.28	2.75	0.51	1.2	0.20	0.20	96.0	-1.85	0.72	0.39	2.91	2.73	2.7	1.30	0.2
		h	0.20	0.77	0.55	0.72	0.39	0.37	2.98	0.61	1.55	3.41	0.20	96.0	0.5%	0.72	0.39	0.00	2.98	2.81	1.6	0.52
		0	0.41	0.77	99.0	96.0	0.78	0.37	2.98	1.51	2.07	0.82	0.42	96.0	99.0	96.0	0.78	0.0	2.98	3.77	2.16	0.03
		H	0.41	0.58	99.0	9.0	96.0	0.37	2.18	0.81	2.15	1.23	0.41	11.0	99.0	8.0	96.0	8.0	2.18	8.6	2.24	1.4
		н	0.20	0.39	0.33	96.0	96.0	0.37	1.61	0.31	2.24	1.74	0.20	0.58	0.33	8.0	96.0	0.0	1.61	2.51	2.33	1.9
		×	0.20	00.0	11.0	09.0	69.0	0.37	0.35	-0.20	1.55	1.02	0.20	0.19		09.0	69.0	0.0	0.35	8.8	1.6	1.13
•	N	M	-0.20	29.0	0.32	0.48	0.20	-0.73	5.29	2.01	1.38	0.41	1.30	1.24	1.09	1.08	69.0	3.46	2.98	-8.31	1.89	8.0
			-1.00	0.10	-0.33	0.12	8.0	4.37	1.49	11.22	1.2	0.41	2.20	19.0	0.44	0.72	64.0	-0.18	2.18	0.0	1.72	8
		0		-0.09	-0.44	8.0	0.20	-4.55	0.98	11.12	1.36	0.72	0.0	94.0	0.33	09.0	69.0	-0.36	1.61	0.80	1.89	1.13
		H		-0.28	99.0-	8.0	0.20	4.73	94.0	1.22	1.30	8.0	0.0	0.29	11.0	09.0	69.0	-0.54	1.15	0.00	1.81	1.33
		н	ă.	-0.38	99.0-	0.0	0.10	-4.37	0.00	11.22	1.0	19.0	8.5	0.19	0.11	09.0	0.59	-0.18	69.0	0.0	1.55	8
		×	1.20	-0.57	11.0-	-0.24	-0.19	4.7	-0.57	21.11	0.35	0.00	8.0	0.0	0.0	0.36	0.30	-0.54	0.12	0.80	2.8	0.41
		11							Ve	rtical I	Vertical Deflection	-	in. at Indicated Gages	ted Gage							Î	
						1	Total	1000							Paragraph .		Rebound					
			7	25	m _D	7	2	90	La	80	6 _Q		ď	DS	P3	D.	ρ2	90	Zd	80	19	
	e i	T M	0.018	0.11B	0.00	-0.00	-0.015	0.186	0.021	0.000	-0.013		-0.0a		0.02	0.009	0.004	0.175	0.083	0.000	0.00	
		-	-0.0TS	0.138	0.031	0.018	-0.010	0.219	0.030				0.005		0.033	0.031	0.00	0.208	0.032	0.000	0.00	
		7		0.112	0.039	0.057	-0.00	0.184	0.036				0.008		0.040	0.070	0.018	0.173	0.036	0000	0.022	
		ш		0.068	0.000	0.10		0.122	0.042				0.017		0.042	0.114	0.039	0.111	0.0	00.00	0.031	
		н		0.037	0.036	0.122	0.052	0.082	0.034				0.00	0.039	0.038	0.135	0.071	0.07	0.036	0000	0.00	
		×	0.031	0.00	0.016	0.126		0.034	0.018				0.048		0.018	0.139	0.122	0.003	0.00	0.000	0.155	
	CV.	M		0.059	0.02	0.029		0.247	0.031				0.011		0.00	0.033	0.016	0.22	0.031	0.00	0.005	
		N ₁	m	0.043	0.027	0.047		0.185	0.035				0.014		0.028	0.055	0.00	0.163	0.035	00.00	0.00	
		o	0.011	0.082	0.00	0.061		0.129	0.035				0.017		0.006	0.070	0.038	0.107	0.035	0.000	0.03	
		ш	0.018	9000	0.021	0.074		0.093	0.031				0.024		0.022	0.083	0.058	0.071	0.031	0.00	0.00	
		H		-0.007	0.014	0.074		0.068	0.022				0.031		0.015	0.083	0.077	0.046	0.022	0.000	0.129	
		×	0.02th	970.0-	0.00	0.033		0.051	0.010				0.030		0.005	0.042	0.080	0.029	0.000	0000	9.149	

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	22	P									The second second								
1		1	P.	25	9	77	PB	19	710	<u>.</u>	P2	a.	O.T	ć,	9	7	PB B	a.	P10
	0.58	0.00	0.36		0.19	1.60	0.30	9.69	0.10	0.0	95.0	0.0	0.36	8.0	-0.72	1.72	1.10	0.78	0.41
141	0.77	0.11	84.0		0.00	2.18	0.40	0.95	0.10	0.00	0.77	0.11	0.48	0.00	-0.91	2.30	1.20	1.0	0.4.0
	0.77		0.48		18.39	2.41	0.50	1.38	0.10	0.00	0.77	0.11	0.48	0.0	17.48	2.53	1.30	1.47	0.41
144	0.77		09.0		20.94	2.64	09.0	1.2	0.20	0.00	0.77	0.22	0.60	0.20	20.03	2 76	1.40	1.30	0.51
141	0.86	O.43	0.72	0.30	0.37	2.87	0.90	1.55	14.0	0.00	98.0	0.43	0.72	0.20	-0.54	8.3	1.70	1.64	0.72
111	0.77		18.0		0.37	2.64	1.60	1.90	0.71	0.0	0.77	O.43	18°0	0.39	₩5.0-	2.76	2.40	1.99	1.0
111	29.0		0.84		0.55	5.06	0.80	2.15	1.12	0.00	19.0	0.43	0.84	0.59	-0.36	2.16	1.60	2.3	1.43
144	0.38		18.0		0.37	1.38	0.50	2.07	1.53	0.00	5.38	0.83	0.84	0.78	-0.54	1.50	1.00	5.16	1.8
LIM .	0.38		0.72		0.55	0.80	-0.40	1.81	1.33	8.0	0.38	0.22	0.72	0.59	-0.36	0.98	0.40	1.8	1.6
	0.19		0,0		6.73	94.0	-0.60	1.46	o.81	0.00	0.19	1.0	09.0	0.39	-0.18	0.58	0.20	1.55	1.12
111	0.19	1.0	94.0	0.39	6.73	₹.0	-0.60	1.29	0.51	0.0	0.19	0.11	97.0	0.39	-0.18	97.0	0.20	1.38	0.82
111	0.10		96.0	0.29	0.73	0.23	-0.60	1.12	0.41	0.0	0.10	0.11	0.36	0.29	-0.18	0.35	0.20	1.2	0.72
144	0.0	0.0	0.24	o.3	0.91	0.00	-0.80	69.0	01	0.00	0.00	0.00	0.24	0.20	0.00	0.12	0.00	0.78	0.41
						Ver	Vertical Deflection	flection	1 4	in., at Indicated Gages	ed Gages								
				fotal										Rebound					
	20	P3	ď	2	90	D2	80	60		ι _α	D2	D3	T _O	2	90	$L_{\rm G}$	80	60	
			9000	0.000	0.128	0.008	0000	0.00		-0.009	0.063	900.0	-0.002	-0.008	0.120	0.003	0.00	-0.033	
		0.140	0.007	9.000	0.169	0.01	0.000	0.006		-0.01	0.083	0.001	-0.00	-0.012	0.161	0.00	0.000	-0.036	
			0.00	900.0	0.184	0.018	0000	0.005		-0.0LO	0.092	0.014	0.000	-0.012	0.176	0.03	0.00	-0.037	
			0.015	90000	0.198	0.023	0.00	0.006		-0.00	0.099	0.018	0.007	-0.012	0.190	0.018	0.00	-0.036	
			0.028	0.00	0.222	0.031	0000	0.000		-0.008	0.102	0.00	0.020	-0.009	0.24	0.006	0.000	-0.032	
			0.054	0.017	0.188	0.037	0.000	0.00		-0.005	0.085	0.031	0.046	-0.001	0.180	0.032	000.0	-0.0mg	
			0.082	0.033	0.128	0.039	00000	0.051		0.000	0.056	0.033	0.074	0.015	0.120	0.034	00000	0.00	i
			0.10	0.000	0.084	0.035	0000	0.096		0.00	0.00)	0.029	0.093	0.042	0.076	0.030	0.000	0.054	
			٥. ٢١	0.085	0.055	0.028	00000	0.134		0.018	0.00	0.082	0.106	0.067	0.047	0.023	0.000	0.092	
A 0.000 -0			160.0	0.105	0.037	0.02	00000	0.160		0.046	0.000	0.014	0.089	0.084	0.00	0.00	0,000	0.118	
			0.080	0,106	0.031	0.017	0.000	0.16		0.000	-0.30	0.000	0.072	0.088	0.023	0.012	00000	0.126	
0- 640.0 M			₩0.0	0.106	0.027	0.01	00000	0.171		0.00	-0.006	0.008	0.056	0.088	0.00	0.00	0.000	0.129	
LP.			0.034	0.000	0.02	0000	00000	0.154		0.027	-0.00	0.005	0.026	0.072	0.03	0.00	0.000	0.112	

Table A-7 (Concluded)

1	္ဌါ	0.43	0.51	.51	15.	.51	8	.13	.82	0.61	#	Ħ.	5	0.31																
																ı	1 1	8	8	8	8	19	4.5	67	en.	25	37	8	77	
	o d	3.0	1.2	1.29	7.7	1.5	1.6	1.5	1.3	1.1	9.0	0.5	0.69	No.			6 _Q	-0.00	•								0.137			
	P _B	0.40	0.50	0.60	0.60	0.40	0.20	0.0	0.0	0.0	0.0	0.0	0.0	0.0			28	0.00	0.000	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0000	0.00	0.00	
	P	1.72	1.8	1.95	1.95	1.72	1.38	1.0	69.0	97.0	0.00	0.0	0.35	0.00			DZ	0.014	0.02	0.02	0.029	0.032	0.032	0.027	0.020	0.013	0.008	0.006	0.00	
nd	P - P	0.73	0.73	0.73	0.73	0.73	0.73	0.73	0.73	0.73	00.00	0.18	0.0	0.73			D6	0.133	0.155	0.191	0.23	0.140	0.089	0.048	0.028	0.150	10000	00.0	0.00	
Rebound	200	61.0	0.29	0.29	0.39	0.58	0.58	0.58	67.0	0.39	60.0	0.0	0.29	0.19		ebound	_D 2	0.000	0.010	0.011	0.013	0.020	0.030	0.047	0.058	0.065	0.051	0.053	0.046	
	G4	65.0	0.71	0.59	15.67	0.71	0.71	0.59	0.59	0.59	0.11	0.11	0.11	0.23	ı		ci di	910.0	0.021	0.026	0.032	9.00	0.058	0.067	790.0	0.051	0.037	0.024	0.018	
	<u>م</u>			1.74	•						0.11	0.00	0.0	0.22			ص ص	0.013	0.017	0.019	0.022	0.023	0.022	0.018	0.013	600.0	900.0	0.003	0.002	
	P2			- 19.0							•				Gazes		D2			0.074	0.000	950.0	0.000	0.025		0.010		.00.0	2000	
	P ₁			0.80											Indicated Gazes		D,		0.003				0.000				0.02			
	P10														1 2 2		1 1	0	0	0	0	o	0	0	0	0	0	0	0	
	a,	1.33	1.43				1.8				1.23	7	H	1.23	ion. ir			10	10	6 0	Q	9	CI.	_+	0	6			6	
	^д	-0-35	-0.17	-0.09	0.08	0.17	0.26	0.17	0.0	-0.36	-0.78	-0.86	-0.69	-1.12	eflect		6	0.00	0.00	0.00	0.0	0.0	0.052	0.0	0.120	0.139	0.144	0.13	0.119	
	PB	16.72	-15.62	16.52	16.52	16.72	-16.92	17.12	17.12	-17.12	-17.12	-17.12	-17.12	17.12	Vertical Deflection, in. at		ВВ	0000	0.000	0.000	00000	0.000	0.000	00000	000.0	0.000	0.000	00000	0.000	
	۲ .		- 25.0		1.03			0.12		- 94.0-	-0.92	-0.92	- 75.0-	-0.92	Ver		D7	0.015	0.022	0.026	0.030	0.033	0.033	0.028	0.021	0.014	0.009	0.007	0.005	
	9 _d	6.01	6.01	6.01	6.01	6.01	6.a	6.01			5.28	Ü	5.28	. 10.9	·		90	0.185	0.207	0.243	0.265	0.192	0.141	0.100	0.080	0.067	0.059	950.0	0.054	
Total	5 _d			96.0							92.0	69.0	96.0	88.		tal	25			0.003										
	P.			-0.36												ĭ	า๊ต			0.014										
	ا																			0.015 0										
	a,			-1.74											ı		Δ [']													
	20	0.76	0.86	0.86	0.86	0.76	0.76	0.57	0.18	0.38	0.19	0.38	0.19	0.38			22	0.0	0.051	0.057	0.05	0.03								
	4	1.80	2.21	1.80	1.80	8.8	1.80	1.80	1.80	1.80	7.8	1.00	5.00	1.80	1		ជី	0.002	000.0	0.001	0.002	0.00	0.007	0.013	0.017	0.019	0.018	0.013	0.008	
Toon	tion	Д	ပ	A	ial	D.	o	H	н	ы	純	ы	×	M				Д	O	A	(a)	₿e ₄	v	Ħ	н	מ	×	ы	×	
Tons	Point	N																C)												
	20	a																7												

P10 0.47 0.28 0.39 0.39 -0.09 -0.47 -1.12 -1.12 -1.12 -1.13

Table A-8

				Multi	iple-sheel	Heavy	Gear Load Flex Load Condition:	4	30 kins r	nt Test, per Abeel	Static Instrumentation Loading Date, Twin Tandem, 150 psi	Instrumen Tandem, 15	tation L	oading De	4				
								Vert	ical Pre	ssure, p	si, at Inc	Mested	Cells						
Loca-	1				Tot	is.									Febor	pun			
tion	4	₽	m	Δ. [±]	2	P6	P7	88	64	210	d I	P2	A.	o.3	2	9.	P	8	6
(a)	8.20	3.04	0.17	0.00	-0.35	4.63	2.01	1.33	1.22	74.0	7.46	2	0.43	0.12	0.00	12.1	1.80	D.31	0.87
fa,	11.15		1.55	0.00		99.9	2.75	1.73	1.75	0.28	10.41	14.	1.81	7.0	0.0	6.77	2.54	0.71	1.40
0	12.07		5.67	0.00		7.45	3.27	2.34	2.45	0.19	11.33	4.26	5.93	1.42	0.17	7.56	3.06	1.32	2.10
tet	12.90		7.6	0.0		8.13	3.80	3.06	3.85	0.38	12.16	4.9	16.6	3.09	00.0	8.24	3.59	8.0	3.50
н	ह-6		8.85	0.00		5.65	3.91	2.96	7.90	-0.09	8.47	5.15	9.11	4.39	0.17	5.76	3.70	1.9	4.55
5	62.7		12.55	0.00		2.9	3.59	5.96	5.60	-0.09	4.05	4.73	12.81	5.34	00.0	3.05	3.38	7.5	5.2
×	2.58		8.68	0.00		1.13	5.96	2.14	2.60	-0.47	1.8	3.78	\$ es	5.85	0.17	1.24	2.75	1.12	5.8
(a)	9.50	3.53	2.15	1.19		10.94	3.27	0.61	2.10	-0.65	9.04	3.65	1.1	8.0	1.2	9.93	3.06	-1.32	1.57
ía,	20.88		9.97	2.05		12.52	т. Т	4.89	3.50	-0.65	10.42	4.63	8.93	1.78	1.2	11.51	3.80	5.96	2.97
o	11.34		12.89	3.20		13.20	77.7	6.72	4.98	-0.84	10.88	5.11	11.85	2.96	1.2	12.19	4.23	1.79	4.45
æ	\$.9°		11.17	12.7		8.69	77.7	d .3	6.59	15.09	6.18	5.11	10.13	½.03	19.76	7.68	4.23	4.28	5.76
+ 1	3.05		17.14	7.99		7.40	7.01	8.96	7.17	2.60	2.59	4.63	16.40	4.75	1.56	3.39	3.80	7.03	6.64
ם	1.57		8.60	7.11		2.59	3.38	4.48	7.08	1.22	1.11	3.65	7.56	1.87	1.2	1.58	3.17	2.55	6.55
×	0.83		2.57	3.80		1.69	2.32	2.14	5.33	33.09	0.37	2°44	1.63	3-56	62.29	0.68	2.11	ย	7.80

Row Point

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	o,	0.002	0.00	0.003	1000	0.005	90000	0.007	0.003	0.007	0.000	0.013	0.017	0.03
	D _B	0.001	0.002	0.000	0.002	0.00					0.00		0.00	0.003
	$L_{\rm C}$	9000	0.007	0.008	0.007	0.005	0.003	0.002	0.013	0.025	0.013	0.009	900.0	0.003
	P.6	0.004	0.00	0.003	0.002	0.001	00000	0.000	900.0	90000	0.004	0.005	0.003	0000
Febound	25	0.001	0.005	0.004	0.007	0.013		0.034	0.008	0.012	0.018	0.028	0.038	0.043
	ñ	0.003	0.004	0.00	0.007	900.0	0.007	900.0	0.007	0.00	0.012	0.013	0.013	0.011
	D3	000°C	000-0	00000	0.000	00000		00000				0.000	00000	00000
	25	0.016	0.015	0.012	900.0	0.005	0.003	0.001	0.023	0.018	0.012	0.007	0.003	0.001
	ι _α	0.060	0.062	0.053	0.035	0°0	0.012	900.0	0.143	0.081	0.049	0.024	0.011	0.005
	60	-0.001	-0.001	0.000	T00.0+	0.002	0.003	0.004	0.001	0.003	0.005	600-0	0.013	0.014
	80	00000	0.001	0.001	0.001	0.001	100°0	0.001	0.002	0.002	0.003	0.003	0.003	0.002
	La	0.002	0.003	0.004	0.003	0.001	-0.001	-0.002	0.012	0.014	0.012	0.008	0.005	0.002
	90	0.003	0.003	0.002	0.001	00000	0.001	0.001	90000	0.004	0.002	0.000	0.001	-0.002
Total	2	0.000	0.001	0.003	0.005	0.012	0.018	0.033	0.003	0.007	0.013	0.023	0.033	0.038
	14	0.002	0.003	0.00	900.0	0.007	0.00	0.005	0.007	0.00	0.012	0.013	0.013	0.011
	2	000.0	00000	00000	00000	00000	00000	0000	00000	0.000	00000	0.000	00000	00000
	D ₁ D ₂ D ₃ D ₁ D ₅	0.014	0.013	0.010	0.00	0.003	0.001	-0.001	0.022	0.017	0.01	0.006	0.002	0000
	DI.	0.043	0.045	0.036	0.018	0.00	-0.005	-0.011	0.184	0.122	0.000	0.055	0.052	0.045

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Table A-8 (Continued)

				Tot	78									Hebo	bund		
اب	P2	a,e	ď,	25	9	P7	a.e	9	Plo	o.⊶	42	-M	Q.	25	9	P7	4. G3
-51	2.19	8.0	0.35	0.35	7.23	2-33	-1.33	1.0	95.0-	તં.	2.19	0.43	0.59	-0.17	7.23	3.8	-0.6
8	2.92	0.51	0.59	0.35	10.72	3.17	п	1.83	95.0-	5.71	2.92	\$0	0.83	-0.17	10.72	2.74	0.0
27.	3.65	1.63	1.18	0.35	07.11	8.4	2.34	3.14	-0.37	6.45	3.65	2.06	1.42	-0.17	04.11	4.59	8
-72	71.4	2.74	1.90	0.35	13.77	75-7	3.97	4.72	-0.56	6.45	41.4	3.17	2.14	-0.17	13.77	17-7	7.0
17	41-4	2.43	2.85	0.52	17.6	2.73	3.67	19.9	-1.50	3.87	71.4	2.86	3.09	00.0	7.6	4.32	4.36
7	3.78	3.60	3.32	0.52	1.85	77.7	6.01	7.51	-1.12	1.84	3.78	4.05	3.56	0.0	85	10 01	6.73
74	3.04	2.00	3.32	0.52	2.15	3.59	3.97	7.63	-1.50	1.47	3.04	2.49	3.56	0.0	2.15	3.16	29.7
17.	2.43	0.17	0.83	0.17	9.85	3.17	0.51	2.03	0.38	3.96	2.55	1.03	1.07	0.17	9.56	5.3	0.7
-59	2.35	09.0	1.07	0.0	11.40	3.91	4.99	3.15	0.38	41.4	3.04	1.46	1.31	0.0	10.84	3.69	5.09
8.	3.16	1.37	1.66	0.17	12.19	4.33	6.42	4.73	0.19	3.41	3.28	2.23	3.8	0.17	11.63	11.4	6.5
98	3.04	1.63	2.14	21.0	7.90	4.33	6.22	6.12	12.09	2.21	3.16	2.49	2.38	0.17	7.34	11.4	6.3%
3	2.92	0.86	2.37	0.0	29.15	3.91	74.6	6.82	5.63	1.19	3.04	1.72	2.61	0.0	28.59	3.69	9.57
8	2.07	0.17	2.2	%	1.92	3.07	4.79	1.7.9	2.34	0.55	2.19	1.03	2.50	8	1.36	2.85	8.4
28	1.16	-0.35	1.78	0.0	1.24	2.33	2.14	4.73	28.78	0.27	1.58	0.51	2.05	0.0	0.68	2.11	20
													1				

6.00

6.30 7.17 7.26 2.02 3.15 4.73 6.12 6.82 6.47

					-			- 44												
						Total			L'ILCAL D	er treat perfection, in., at indicated dages	at Indica	100 0000			ebound					
		D_1 D_2 D_3 D_4 D_5	D2	₀	J _L	PS	90	La	D ₈	60	a ^t	D2	D3	a d	25	90	2 _d	28	್ಟರ	
et	(a)	0.083	0.044	0.000	0.005	0.007	0.014	0.012	0.002	00000	0.111	0.039	000.0	0.002	0.000	0.015	0.014	0.003	-0.003	
	ß.	0.102	9.0.0	00000	0.008	0.008	0.014	0.020	0.003	0.001	0.130	0.041	0.00	0.005	0.001	0.005	0.022	0.00	-0.002	
	o	0.077	0.038	00000	0.013	0.014	0.010	0.028	0.005	0.004	0.105	0.033	0000	0.000	0.007	0.01	0.030	0.006	0.00	
	tot	0.044	0.028	0.000	0.018	0.023	0.007	0.024	0.006	900.0	0.072	0.023	00000	0.015	0.016	0.006	0.026	0.007	0.00	
	н	0.015	-0.021	00000	0.021	0.042	0.004	0.017	0.007	0.015	0.043	-0.026		0.028	0.035	0.00	0.019	0.008	0.012	
	43	0.001	0.012	00000	0.022	950.0	0.002	0.011	90000	0.024	0.029	0.007		0.019	0.049	0.003	0.013	0.007	0.021	
	aut.	-0.008	0.008	0.000	0.019	0.057	00000	0.005	0.005	0.044	0.020	0.003		9.000	090.0	0.00	0.007	0.006	0.041	
N	[a]	0.217	0.062	00000	0.012	0.005	0.021	0.000	0.007	0.004	0.148	0.055		0.008	-0.046	0.0	0.041	0.005	0.008	
	fe ₄	0.155	0.032	00000	0.019	0.012	0.017	0.047	60000	0.008	0.086	0.045		0.015	-0.038	0.007	0.048	0.008	0.02	
	v	0.115	0.036	00000	0.025	0.034	0.011	0.04	0.012	0.018	0.046	0.029	00000	0.02	-0-C17	0.00	0.045	0.011	0.002	
	122	0.092	120.0	00000	0.029	0.094	0.006	0.034	0.013	0.030	0.023	0.017		0.08	0.043	900.0	0.035	0.012	0.034	
	н	0.078	0.017	0.000	0.029	0.127	0.003	0.021	0.013	0.00	600.0	0.000	00000	0.025	0.076	0.003	0.022	0.012	9,000	
	63	0.00	0.012	00000	0.025	0.139	0.001	0.010	0.000	0.049	0.001	0.005		0.021	0.088	0.001	0.011	600.0	0.053	
	*	7700	0000	8	010	101	000	-	000	- 10 0							,	1	1	

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						400	1000		Vertical	ICE ITE	seure, pa	it, at Inc	at Indicated (Cells		Bahan	7				
 Potnt S		2	82	4	4	2	9	74	88	201	Pro l	2-1	4.0	24	4	P ₅	P P	P7	8	8	P
7	14	1.47	1.09	0.08	0.36	0.0	3.39	1.79	1.2	0.88	-0.66	1.38	1.2	69.0-	0.48	0.0	7.08	1.79	1.83	98.0	0.75
	(h ₁	2.2	1.16	0.17	0.48	0.0	4.97	2.35	0.82	1.49	-0.66	2.12	1.58	-0.60	09.0	0.00	5.6	2.32	1.43	1.57	0.7
	o	0.92	1.9	0.51	09.0	0.17	5.65	3.06	1.53	2.28	-0.84	58.0	2.07	-0.26	0.72	0.17	6.32	3.06	2.14	2.36	0.57
	þt.	2.12	1.98	1.37	96.0	0.00	5.87	3.48	2.14	3.50	-1.13	2.03	2.07	09.0	1.07	0.00	6.54	3.48	2.75	3.58	0.28
	н	1.47	1.9	4.12	1.31	0.17	3.95	3.59	2.04	4.38	-1.69	1.38	2.07	3.35	1.43	0.17	4.62	3.59	2.65	4.16	-0.28
	6	0.83	1.9	2.32	1.13	0.00	1.70	3.16	2.85	86.	-1.88	0.74	2.07	1.55	1.55	0.30	2.37	3.16	3.46	5.07	-0.47
	M	94.0	1.34	1.20	1.43	3.64	0.23	2.53	1.12	18.4	-2.2	0.37	1.46	0.43	1.55	3.64	0.90	2.65	1.73	4:89	₩.0-
cv	ы	177	1.22	91.0	0.36	0.17	3.04	2.12	-0.20	1.23	-0.28	1.38	1.34	0.18	0.48	0.17	3.61	2.12	1.43	1.57	0.38
	A	1.57	9m**	0.35	09.0	0.17	3.38	2.54	0.2	1.93	-0.19	1.48	1.58	0.35	0.72	0.17	3.95	2.54	1.84	2.27	0.47
	o	1.20	1.46	69.0	0.71	0.17	2.82	2.85	19.0	2.63	-0.15	1.11	1.58	69.0	0.83	0.17	3.39	2.85	2.2	2.97	0.47
	m	12.0	1.46	1.04	0.98	0.00	1.69	2.85	0.92	3.15	-0.19	9.0	1.58	1.04	1.07	00.0	2.26	2.85	2.55	3.49	0.47
	H	0.55	1.22	0.52	1.07	0.17	95.0	2.54	0.41	3.41	-0.28	94.0	1.34	0.52	1.19	0.17	1.13	2.54	2.04	3.75	0.38
	י	0.37	0.98	0.35	1.07	0.17	11.0	2.0	-0.30	3.06	99.0-	0.28	1.10	0.35	1.19	0.17	0.68	2.0	1.33	3.40	8.0
	M	0.28	0.73	0.18	0.83	0.17	-0.34	1.48	-0.81	2.10	-0.56	0.19	0.85	0.18	0.95	0.17	0.23	1.148	0.82	2.44	0.10
								Ve	rtical D	eflectio	Vertical Deflection, in., at indicated Gages	t Indica	ted Gage								
						Total				S 12 2 1 8	188				11.64	Rebound					
		o I	N	DJ	ď	50	90	La	80	60		I _Q	22	2	ď	25	90	4	80	60	
н	(a.)	0.00.5	0.004	0.000	0.005	-0.012	0.041	0.051	0.005	0.008		0.059	0.060	0.000	0.00	-0.002	0.037	0.034	0.00	-0.003	
	(he	0.049	0.00	0000	0.00	-0.010		0.076	0.008	0.00°		0.063	0.065	00000	0.007	0000	0.039	0.059	0.00	-0.00	
	O	0.0	0.059	00000	0.00	-0.004		980.0	0.008	0.a.6		0.050	0.055	00000	0.03	0000	0.032	694.0	0.005	0.005	
	H	0.015	0.040	0000	0.024	0.01	0.024	0.098	0.a6	0.030		0.029	0.036	00000	0.021	0.024	0.020	0.081	0.03	60.0	
	н	-0.001	0.026	00000	0.029	0.047		0.085	0.019	0.048		0.013	0.022	00000	0.026	0.057	0.012	0.068	0.00	0.037	
	7	-0.013	0.00	0000	2.031	0.083	0.00	0.055	0.000	0.069		0.00	0.012	0000	0.028	0.093	0.005	0.038	0.017	0.058	
	×	-0.020	0.0	00000	0.027	0.103	9000	0.032	0.017	0.084		-0.006	90000	0000	0.00	0.113	0.00	0.00.5	0.024	0.073	
N	(m)	0.00	0.072	0000	0.013	0.00	0.058	0.110	0.00	0.007		0.038	0.051	00000	0.007	-0.048	0.052	0.090	90000	-0.060	
	h	0.016	0.062	0.000	0.020	0.018	0.048	0.133	0.017	0.018		0.030	0.041	00000	0.014	-0.040	0.042	0.107	0.03	-0.049	
	0	0.006	0.00	0000	0.027	0.037	0.032	0.154	0.023	0.042		0.020	0.00	00000	0.021	-0.021	0.026	0.128	5.00 e	-0.05	
	ht	-0.001	0.36	0.000	0.031	0.093		0.129	0.006	0.108		0.013	0.015	0.000	0.005	0.035	9.000	0.103	0.022	0.041	
	н	-0.006	0.028	000	0.03			0.082	0.022	0.166		0.008	0.007	00000	0.005	0.03	900.0	950.0	0.018	0.099	
	7	-0.009	0.03	0000	0.028			0.054	0.023	0.171		0.005	0.004	0.000	0.022	0.085	0.00	0.028	0.019	0.104	
	×	-0.00	0.023	00000	0.02			0.037	0.018	0.220		0.00	0.00	0.000	0.00	0.131	0.002	0.011	0.00	0.153	

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						100	1			1 Tak	TCT LLE	Seure, pe	17 8 T	at Indicated Cells	Cetts							
Now	Point t	ton.	P ₁	P2	3	4	PS	94	4	88	00	P10	4	P	a.	d.	Z Z	P6	Py	84	0	of a
"			4	190	8	1	1	:	1 .	100	1 5	9.0	710	1	1 8	1 :	18	:	!	1 8	1	1
1	•	•		1 1	3	* .	17.5	7:-	7.5	01-0-	3.72	0.10	0.40	5:5	3.5	-0-15	3.0	3:	12.1	× 0-	0.70	-1.40
			0.05	c.	3	₹.0	8.0	1.8	1.38	0.10	0.78	0.10	9.65	0.85	0.0	-0.12	-0.17	8	1.59	-0.72	96.0	-1.40
		•	0.83	0.85	0.09	0.48	00.0	2.7	1.69	0.21	1.22	0.10	0.83	0.97	0.09	0.12	-0.17	5.59	1.90	-0.61	1.10	-1.40
		m	9.02	0.85	0.18	0.13	71.0	5.36	1.90	0.82	1.66	0.10	9.0	0.97	0.18	0.12	00.0	2.14	2.11	0.00	1.8	-1.40
		н	94.0	96.0	0.36	09.0	0.0	1.36	1.8	5.65	5.09	0.10	94.0	1.10	0.26	0.24	-0.17	1.24	2.11	1.83	2.27	1.40
		•	0.28	c.85	92.0	0.72	0-17	0.9	1.80	1.84	2.27	0.29	0.28	0.97	0.26	0.36	00.0	62.0	2.01	3.00	2.45	-1.2
		*	60.0	19.0	0.18	0.72	0.17	54.0	1.48	1.43	5.09	91.11	0.09	0.73	6.18	0.36	00.00	0.33	1.69	0.61	2.27	99.6
	c.		0.28	64.0	0.00	-0.12	-0-17	1.0	1.06	0.00	0.70	-0.09	0.28	67.0	0.00	0.12	0.00	1.01	1.16	0.10	0.87	0.75
			0.38	64.0	0.00	-0.12	-0.17	1.24	1.27	0.00	0.87	-0.09	0.28	67.0	0.0	0.12	00.00	1.24	1.37	0.10	1.0	0.75
		0	0.28	0.61	0.00	-0.12	0.00	1.0	1.148	0.40	1.14	-0.09	0.28	0.61	0.00	0.12	0.17	1.0	1.58	0.50	1.3	0.75
		#	0.19	0.61	60.0	0.00	0.00	0.56	1.48	19.0	1.40	0.0	61.0	19.0	60.0	0.24	0.17	95.0	1.58	0.7	1.57	0.84
		1	60.0	64.0	60.0	0.12	0.0	0.33	1.27	0.30	1.49	-0.37	60.0	64.0	0.00	0.36	0.17	0.33	1.37	0.10	1.66	0.47
		,	60.0	64.0	0.00	0.0	-0.17	0.8	1.06	0.20	1.31	-0.16	0.0	67.0	0.00	0.24	0.00	0.22	1.16	0.30	1.14	0.38
		×	60.0	0.24	60.0	0.00	-0-17	0.0	0.74	0.0	96.0	-0.65	60.0	0.24	60.0	0.24	0.00	0.11	0.84	0.10	1.13	61.0
					160		Total	-	-	reacen p	er lect 10	Vertical Deliection, in., at indicated Gages	t Indica	ted Gege			Rehound				1	
	V		2	D2	P P	ď	25	90	72	80	Po		24	C. W	E P	ď	2	90	74	P _B	60	
#	1		0.051	0.033	00000	0.002	-0.013		1	0.00	-0.020		0.040	0.003	0.000	0.003	0.005	0.059	0.062	0.001	-0.00	
			0.035	0.035	00000	0.005	-0.013		6.112	0.000	-0.013		0.00	0.00	0.000	900.0	0.005	950.0	0.103	0.007	0.001	
		0	0.028	0.029	00000	0.00	-0.008			0.015	-0.009		0.01	0.019	0.000	0.01	0.010	0.055	611.0	0.002	0.000	
		14	0.082	0.0LB	0.000	0.01	0.001	0.042		0.02	0.01		0.01	900.0	00000	0.015	0.019	0.037	0.136	0.00	0.030	
		н	0.017	0.00	00000	0.38	0.018		0.126	0.027	0.059		5.006	-0.001	0.00	0.00	0.036	0.021	0.117	0.024	0.078	
		h	0.013	0.00	0000	0.018	0.032			0.029	0.100		0.002	-0.006	0000	0.019	0.050	0.012	0.070	0.006	911.0	
		×	0.011	0.00	0.000	0.016	0.01			0.005	0.119		0000	-0.010	0.000	0.007	0.059	0.007	0.036	0.022	0.138	
	~	M	0.052	0.005	0000	0.02	0.00	0.087	0.105	0.027	-0.001		0.03	0.00	0.000	9000	0.013	0.000	0.099	0.012	-0.043	
			0.049	0.000	0000	0.00%	0.029			0.034	+0.010		0.000	0.019	00000	0.001	9.00	0.056	0.112	0.00	-0.032	
		e	9,000	0.014	0.000	0.029	0.037			0.041	0.033		0.007	0.013	0000	0.015	0.006	0.037	0.130	0.026	-0.009	
		=	0,043	0.008	0000	0.030	0.050			0.045	0.111		0.32	0.007	0.000	0.00	0.039	0.001	0.100	0.030	690.0	
			0.041	0.005	0.000	0.030	0.061			0.057	0.155		0.305	0.00%	00000	0.00	0.000	0.0	950.0	0.0.2	0.113	
			0.040	0.00	0000	0.027	990.0			0.000	0.168		0.00	0.001	0.000	0.013	0.055	0.006	0.027	0.00	0.126	
		×	0.040	0.00	0000	0.083	0.059			0.032	0.230		0.001	0000	0.000	0.009	0.048	0.003	0.01	0.017	0.188	

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Table A-9
Multiple-wheel Heavy Gear Load Flexible Pavesent Test, Static Instrumentation Loading Data
Item 4: Load Condition: 30 kips per Wheel, Twin Tander, 150 psi

			i							Vert	Vertical Pressure, psi	rure, ps.		at Indicated Cel	2115							
3	Point	tion	e ri	2	2,5	4	2	9	P7	88	20	P10	مرا	200	a.m	4	2	9	P	40	40	P10
н	H	8-3	0.0	8.9	8.50	3.11	1.17	-0.37	5.73	0.80	2.41	0.51	8.0	6.29	9.56		0.59	•	5.50	1.20	1.98	0.10
		h	0.0	7.72	13.51	4.43	3.8		6.54	2.41	3.27	0.92	0.00	7.05	14.27	3.59	2.6	-0.18	6.31	2.81	2.84	0.82
		O	00.0	7.53	12.09	5.50	7.53		6.42	1.70	41.4	5.5	0.00	98.9	12.85	9.4	6.9	-0.37	61.9	2.10	3.72	2.15
		Ħ	0.0	6.10	17.87	6.20	10.76		5.0	2.77	4.74	3.59	0.00	5.43	18.63	5.38	10.18	-0.37	평.	3.2	₹. ⁴	3.49
		н	0.0	4.29	4.1	6.34	12.03		3.55	2.01	4.82	4.00	0.0	3.62	12.20	5.50	11.45	-0.37	3.35	2.41	4.39	3.8
		רי	0.0	2.67	3.38	5.7	13.49		5.29	8.0	4.39	4.82	0.0	5.00	41.4	8.3	12.91	-0.37	2.06	0.40	3.96	4.72
		M	0.0	1.7	96.0	99.4	9.88		1.37	-0.60	3.70	3.79	0.0	1.0	1.74	3.82	9.30	-0.55	1.14	-0.20	3.27	3.69
	N	M	23.69	6.48	14.71	3.8	3.42		8.33	7.41	3.8	1.74	\$.09	6.57	15.03	8.6	4.30	70.46	7.56	4.10	3.64	1.23
			-0.40	6.39	15.03	5.0	7.73	g.0	8.25	6.91	2.00	4.7	0.0	6.18	13.29	8.	8.61	8.0	7.56	3.60	4.65	2.4
		O	-0.10	4.7	23.96	5.50	10.08		6.42	14.6	5.51	98.9	0.0	7.86	8.2	5.38	10.96	0.54	5.73	6.10	5.16	6.35
		M	-0.40	5.96	חיה	5.38	₽·1		4.36	6.11	2.60	7.88	0.0	3.05	9.37	5.26	12.52	0.54	3.67	2.80	5.3	7.37
		н	01.0-	1.62	41.4	7.66	12.81		2.73	3.21	2.00	9.11	9.0	1.7	5.40	4.54	13.69	0.54	5.06	-0.10	4.65	8.60
		יי	-0.40	98.0	2.61	3.59	7.8		1.83	2.40	6.1	6.55	8.0	0.95	0.87	3.47	8.80	0.54	1.14	-0.91	3.70	6.04
		×	-0.40	0.38	2.18	2.51	3.62		1.37	2.10	2.93	3.27	0.0	24.0	44.0	2.39	4.50	0.36	99.0	1.2	2.58	2.76
							Tata		Ve	Vertical Deflection	eflection	10.4	at Indicated Gage	ted Gare			Dahamad					
			o l	D2	33	Q	2	90	La	80	6		e l	20	e e	ď	5	90	4	80	0	
н	7	M	0.006	0.047	0.007	0.00	0.00	0.007	0.002	0.00	-0.00		0.029	0.056	0.00	0.004	0.013	0.ca6	0.00	0.00	0.007	
		p.	900.0	0.037	0.00	0.00		0.005	0.003	0.000	-0.00		0.031	0.046	5.013	0.00	0.01	0.01	0.003	0.000	0.007	
		o	0.024	0.027	0.011		0.005	0.000	0.003	0.000	0.000		0.037	0.036	0.004	0.027	o.as	0.0	0.003	0.000	9000	
		×	0.00	o.a.7	0.010	0.026	0.00	•	0.203	0.000	0.00		0.048	0.000	0.03	0.036	0.023	0.008	0.003	0.000	0.00	
		н	0.039	0.009	0.008	0.034	0.018		0.003	0.000	0.003		0.062	0.018	0.01	0.044	0.031	0.005	0.003	0.000	0.001	
		tg.	0.055	0.00	0.005	0.031	0.027		C.003	0.000	0.00		0.078	0.013	0.008	0.041	0.010	0.003	0.003	0.000	0.00	
	ĺ	M	0.068	-0.003	0.000	0.022	0.032		0.00	0.000	0.005		0.091	900.0	0.005	0.032	0.045	0.00	0.005	0.000	0.013	
	/ (V	7	0.024	0.051	0.00	0.004	0.00		0.005	0.000	0.00		-0.050	0.074	o.00	0.031	0.02	0.027	0.005	00000	0.008	
			0.00	0.039	0.000			0.000	0.005	0.000	0.004		-0.040	0.062	0.021	0.045	0.000	0.0	0.005	0.000	0.00	
		9	0.043	0.082	0.019	0.052		0.00	0.006	0.000	0.008		-0.02	0.045	0.000	0.059	0.031	0.005	0.006	0.000	0.0Th	
		×	0.000	0.008				-	0.005	0.000	0.012		0.006	0.031	o.a.6	0.067	0.046	0.000	0.00	0.000	o.ae	
		н	0.163	-0.002				1	0.005	0000	0.017		0.099	0.00	0.01	0.064	0.060	0.007	0.00	0.000	0.023	
		ר	0.164	-0.003		0.045		100.0-	0.00	0.000	0.017		0.100	0.00 t	900.0	0.052	0.068	0.00	0.00	0.000	0.003	
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| P7 | 5.51 | 6.08 | 5.85 | 4.148

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| P6 | -0.55 | -0.55 | -0.36 | -0.36

 | 0.00 | 0.0 | 0.00 | -0.18
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 | 0.138 | 0.114 | 0.081 | 0.055 | 0.034
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										Verti	Cal Pres	Vertical Pressure, psi, at Indicated Cells	st Ind	1cated C	1							1
ROS	N P	Lion	2	2	4	9,7	2	9	2	88	8	P10	a.	P	P ₃	4	I S	P6	4	80	6	or s
=	-		0.0	98.0	0.32	09.0	0.19	28.04	2.73	0.70	1.20	u.0	0.20	1.53	0.32	0.72	64.0	64.12	8.8	0.20	1.55	0.3L
		h	-0.50	6.0	64.0	0.72	0.29	37.14	2.86	1.10	1.63	0.62	0.00	1.62	0.43	0.8	65.0	36.59	3.09	09.0	1.98	0.62
		0	-0.20	0.10	0.54	3.72	61.0	-0.36	2.6	7.00	1.89	0.92	8.0	0.77	0.54	0.84	67.0	16.0-	2.87	6.51	2.2	0.92
		INT	-0.20	0.00	0.43	0.72	0.39	-0.36	5.06	2.90	2.06	7.7	0.00	19.0	0.43	₩°.0	69.0	16.0-	2.29	5.40	2.41	1.1
		н	-0.20	-0.29	0.32	0.72	67.0	-0.36	1.37	5.30	1.88	5.0	8.0	0.38	0.32	0.84		16.0-	1.60	1.80	2.33	5.02
		7	-0.20	-0.148	0.11	0.60	0.39	-0.36	69.0	5.10	1.72	1.7	0.0	0.19	n.º	0.72		-0.91	0.92	7.60	2.07	1.74
		×	-0.20	-0.57	n.º	0.36	0.19	-0.55	0.23	2.90	1.37	1.13	0.0	0.10	n.º	0.48	67.0	-1.10	94.0	1.40	1.72	1.13
	œ	м	0.00	0.148	0.2	0.36	0.50	-1.28	1.72	5.10	1.2	0.41	0.00	0.57	0.10	0.36	0.10	-0.18	1.98	0.70	1.29	0.51
		*	0.00	0.38	8	09.0	0.30	-1.38	1.49	1.80	1.38	0.62	0.00	0.17	-2.07	09.0	0.50	-0.18	1.72	0.40	1.16	0.72
		o	0.0	0.29	a .0	0.18	0.39	-1.28	1.15	1.50	1.38	0.82	0.0	0.38	0.10	0.148	0.29	-0.18	1.38	0.10	1.16	0.92
		101	8.0	0.19	7.0	0.36	0.39	-1.28	69.0	7.00	1.2	1.03	8.0	0.28	0.00	0.36	0.29	-0.18	8.0	0.30	1.29	1.13
		н	0.0	0.10	1. 0	0.36	0.30	-1.28	0.34	4.40	1.12	0.82	0.0	0.19	0.0	0.36	0.20	-0.18	0.57	0.0	1.20	0.92
		73	8.0	0.0	n.º	15	0.30	-1.28	0.1:	4.30	0.86	0.41	0.00	0.0	0.0	0.24	0.50	-0.18	±°0	-0.10	\$ 0	0.51
		×	0.00	-0.09	n.0	0.24	0.20	-1.28	0.00	4.30	0.52	o.2	00.00	8	0.0	0.24	0.10	-0.18	0.23	-0.10	09.0	o.32
									Ver	tical De	Mection	Vertical Deflection, in., at Indicated Gages	Indicat	ed Gages							Ì	
			ď	20	D	Dh	D	ρķ	2	DR	o		á	60.	Da	ď	De	De	D ₇	D _R	10	
1	,	,					1				1			90.0	1	1	1 8	1 3	1 8		13	
#	4	м	0.0	0.00	0.00	0.00	000	0.170	0.0	000	0.00		00.00	0.100	0.0	0.00	0.00	0.191	0.020	0.00	-0.00	
		h	0.00	0.082	0	0.00	0.00	0.201	o31	0.00	0.007		0.00	0.10	0.031	0.000	0.00	0.225	0.00	0.00	-0.001	
		ø	0.00	0.062	0.033	0.031	0.013	0.155	0.035	0.00	0.000		0.003	060.0	0.036	0.067	0.027	0.176	0.033	0000	0.012	
		Ħ	0.00	0.043	0.033	0.067	0.00	0.101	0.036	0000	0.048		0.00	0.07	0.036	0.063	0.042	0.122	0.034	00000	0.000	
		н	0.018	0.00	0.028	0.092	0.033	0.08	0.032	0.000	0.00		9.00	0.036	0.031	0.108	0.067	0.079	0.030	0.000	0.087	
		h	0.028	-0.01	0.019	0.105	0.079	0.029	0.024	0000	0.136		9000	0.017	0.005	0.118	0.093	0.050	0.022	00000	0.128	
		×	0.057	-0.021	0.0	0.082	0.093	0.025	0.017	000	0.158		0.055	0.007	0.014	0.098	0.107	960.0	0.015	00000	0.150	
	C)	84	0.00	c.036	0.018	0.018	0.00	0.244	0.029	0000	0.013		-0.078	9.0.0	-0.006	-0.098	0.018	0.164	-0.006	0000	-0.003	To see 2
		•	0.00	0.00	0.000	0.031	0.01	0.175	0.032	0.000	0.028		-0.075	0.034	-0.00	-0.085	0.00	0.095	-0.03	0.000	0.002	
		•	0.00	0.011	0.00	0.043	0.00	0.131	0.032	00000	0.034		10.0	0.01	-0.005	-0.073	0.035	0.051	-0.03	0.000	0.038	
		×	0.024	-0.002	0.0L	0.050	0.034	0.0	0.027	0.000	960.0		-0.066	2.00	-0.00	990.0-	0.048	0.024	-0.018	0000	0.080	
		н	9.018	-0.01	0000	0.045	0.017	0.073	0.00	0000	0.125		-0.062	B	-0.015	-0.071	0.061	-0.007	-0.026	00000	0.109	
		43	0.080	-0.0e	0.00	0.032	0.052	0.061	0.013	0.000	1110		-0.060	-0.016	-0.020	-0.084	900.0	-0.00	-0.032	0.000	0.128	
		×	0.110	-0.00	0.00	0.162	0.033	0.00	0.056	00000	6.179		0.030	-0.00	2.005	9.00	290.0	-0.001	0.0	0.000	0.163	
	And the second		Acres and															400	ALC: NO.			

Multiple-Wheel Heavy G.ar Load Flexible Pavement Test, Static Instrumentation Loading Data Item 3; Load Condition: 60 kips par Wheel, Twin Tanden, 200 psi

P8 P9 P1 P1 P2 P3 P4 P4 P4 P4 P4 P4 P4		3				K		Tota			Verc	vertical rressure, psi	sure, p		at Indicated Cell	1		Rebound	pg				1
1.53 0.30 0.00 0.00 9.00 9.79 9.70 0.27 0.27 0.27 0.10	8	Point	tion	4	25	<u>س</u>	0.7	2	P6	P7	88	201	P10	۵۲۰	2	3	4	2	9	P7	P8	6	P10
1.55 1.64 1.15 0.00 11.55 1.65 1.65 1.65 1.65 1.65 1.65 1.25 1.25 0.00 1.54 0.15		7	M	15.76	5.36	0.35	8.0	0.0	9.03	3.59	0.71	2.27	1	15.11	5.61	-1.54	6.42	0.0	10.61	4.0	1.22	1.3	1
9-04 13-14 1.77			p.	18.89	7.55	3.		0.00	11.51	.60	1.83	4.08	1	18.33	7.80	2.75	5.23	0.0	13.09	5.28	2.34	3.50	1
9.98 14.99 1.86 0.17 12.98 6.34 6.00 8.37 19.72 10.23 13.00 9.98 0.17 14.56 6.76 6.56 6.39 1.89 1.89 1.89 1.89 1.89 1.89 1.89 1.8			13	18.89	9.a	13.41		0.0	n.%	5.71	4.28	6.72	1	18.33	9.56	11.52	8.50	8.0	13.54	6.13	4.79	2.60	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			Ħ	20.37	9.98	18.90		-0.17	12.98	6.34	6.0a	8.57	t	19.72	10.23	17.00	8.8	-0.17	14.56	92.9	6.52	8.05	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			н	13.73	8.8	14.95		-0.35	8.01	5.23	5.09	10.23	1	13.08	10.23	13.06	10.45	-0.35	65.6	6.65	2.60	7.6	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			ר	6.36	9.01	n.n		-0.17	3.16	5.7	7.43	п. п.	ì	5.7	9.56	54.6	10.93	-0.17	表:	6.13	\$.	10.49	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			M	2.68	9.51	15.12		0.00	0.22	4.23	4.38	9.40	•	2.03	6.82	13.23	7.60	0.0	1.80	4.65	4.89	8.88	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		N	M	17.60	7.55	2.41		0.0	21.45	6.65	1.73	4.37	ŧ	17.51	8.15	1.72	2.37	3.81	22.01	6.65	-2.75	4.55	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			64	17.97	9.56	16.84		0.0	22.80	8.23	п.п	7.60	1	17.88	9.86	16.15	3.56	3.81	23.36	8.13	7.25	7.78	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			ø	19.65	10.23	23.63		0.0	24.38	8.87	15.68	10.49	ŀ	19.53	10.83	22.9	5.93	3.B	ある	8.87	11.30	10.67	1
S. 56 S. 1.5 S. 54 S. 1.4 S. 1.5 S.			m	13.17	10.23	15.64		4.51	17.50	8.76	12.22	12.85	ł	13.08	10.83	14.9	7.12	8.32	18.06	9.76	7.74	13.03	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			H	5.53	8.89	25.43		54.42	6.78	7.81	18.33	13.98	ı	5.14	64.6	24.74	7.12	58.23	7.34	7.80	13.85	14.16	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			ר	5.49	6.82	18.73		-2.43	2.7	6.34	13.44	13.37	1	2.40	7.42	18.04	8.07	1.38	3.27	6.34	8.96	13.55	ı
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			×	1.20	4.63	13.95		74.87	1.13	4.58	4.2	8.6	ŀ	1.1	5.33	13.26	5.93	78.68	1.69	4.58	₽.0-	10.14	•
D₂ D₃ D										Ver	T. Can	of each form	-1.	- Indian	Sad Carre						1	1	
D ₂ D ₃ D ₄ D ₅ D ₄ D ₅ D ₆ D ₇ D ₈ D ₉ D ₉ D ₁ D ₂ D ₁ D ₅ D ₁ D ₅ D ₁ D ₅ D ₁ D ₅ D ₁ D ₁ D ₂							Total	100				4	1	1000			Rebound				1		
				ι Γ	D2	D3	ħα	D2	90	P ₇	₈	6		a ^L	2	E _D	η _Q	2	90	P	80	of	
0.021 - 0.005 0.000 0.000 0.001 0.002 0.001 0.002 0.001 0.002 0.001 0.002 0.001 0.002 0.001 0.002 0.001 0.002 0.001 0.002 0.0		1	843	0.12	3.023	ı	0.005	0.000	0.003	00000	0.001	0.001		0.114	0.024	;	0.002	0.001	0.00	0.005	0.001	0.003	
0.001 - 0.007 0.000 0.000 0.000 0.010 0.000 0.0			14	0.128	0.021	ı	0.005	0.000	0.003	0.001	0.001	0.001		0.121	0.022	ı	0.005	0.001	0.00	0.006	0.001	0.003	
0.001 - 0.001 0.002 0.000 0.0146 0.012 - 0.010 0.004 0.014 0.002 0.0146 0.014 0.012 0.004			15	0.108	0.01	•	0.007	0.001	0.002	0.001	0.001	C.001		0.101	0.018	1	0.007	0.00	0.003	9000	0.001	0.003	
0.008 - 0.012 0.004 - 0.002 0.000 0.002 0.003 0.002 0.003 0.002 0.003 </td <td></td> <td></td> <td>200</td> <td>0.153</td> <td>0.011</td> <td>ı</td> <td>0.010</td> <td>0.003</td> <td>0.000</td> <td>0.001</td> <td>0.002</td> <td>0.001</td> <td></td> <td>941.0</td> <td>0.012</td> <td>ı</td> <td>0.00</td> <td>0.00</td> <td>0.001</td> <td>0.006</td> <td>0.002</td> <td>0.003</td> <td></td>			200	0.153	0.011	ı	0.010	0.003	0.000	0.001	0.002	0.001		941.0	0.012	ı	0.00	0.00	0.001	0.006	0.002	0.003	
0.003 - 0.012 0.011 -0.020 -0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.002 0.003 0.002 0.003 0.003 0.002 0.003 0			н	0.031	0.008	1	0.012	0.007	-0.001	-0.001	0.002	0.001		0.024	0.009	1	0.012	0.008	0000	0.00	0.00	0.003	
0.000 - 0.009 0.01 -0.009 0.01 0.000 -0.015 0.01 -0.015 0.015 0.01 -0.015 0.010 0.014 0.014 -0.007 0.014 0.001 0.			to 	0.009	0.003	1	0.012	0.011	-0.002	-0.003	0.002	0.002		0.002	0.00	1	0.012	0.012	-0.001	0.005	0.00	0.004	
0.56 — 0.12 0.000 0.005 0.000 0.0343 0.44 — 0.007 0.004 0.001 0.003 0.0447 — 0.002 0.004 0.004 0.004 0.004 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004			×	-0.008	0.000	ı	0.009	0.018	-0.002	-0.005	0.001	0.002		-0.015	0.001	1	600.0	0.019	-0.001	0.000	0.00	0.004	
0.047 - 0.048 0.004 0.0		N	M	0.622	95.0	1	0.12	0.001	0.00	0.005	0.003	0.000		0.343	0.44	ı	0.007	0.00	0.01	0.00	0.003	0.03	
0.036 0.025 0.006 0.005 0.000 0.				0.530	0.047	i	0.00	0.00	0.007	0.008	0.00	0.001		0.53	0.035	1	0.013	0.007	0.00	0.012	0.00	900.0	
0.024 0.030 0.017 0.001 0.004 0.005 0.005 0.0074 0.012 0.025 0.020 0.003 0.009 0.005			O	0.426	0.036	J	0.003	0.008	0.00	90000	0.005	0.003		0.147	0.004	1	0.000	0.01	900.0	0.000	0.005	0.008	
0.016 0.030 0.025 0.000 0.001 0.005 0.010 0.025 0.004 0.025 0.026 0.005			E	0.353	0.004	1	0.030	0.017	0.001	0.004	90000	9000		0.074	0.012	1	0.00	0.020	0.003	0.00	0.006	0.001	
0.002 0.027 0.029 -0.001 -0.002 0.004 0.012 -0.005 0.000 0.022 0.033 0.001 0.002 0.004 0.002 0.004 0.002 0.004 0.002 0.004 0.002 0.004 0.002 0.004			н	0.304	9000	1	0.030	0.005	0.000	0.001	0.005	0.010		0.005	0.00	i	0.025	0.026	0.005	0.00	0.005	0.00	
0.009 0.020 0.028 -0.002 -0.003 0.002 0.000 -0.003 0.003 0.015 0.031 0.000 0.001 0.002			י	0.273	0.012	1	0.027	0.030	-0.001	-0.002	0.00	0.012		-0.006	0.000	ı	0.022	0.033	0.001	0.00	0.00	0.017	
			×	0.257	0.00	1	0.000	0.028	-0.002	-0.003	0.002	0.00		-0.022	-0.003	ı	0.015	0.031	0.000	0.001	0.002	0.005	

-										Vert	Vertical Pressure, psi. at Indicated Cell	sture. p	si. at In	dicated	Cells				100000			
	Tond	Tores					To	143	Temperature of the second					1 5 D C 11 E			Rebo	pun				
8	뛢	tton	1.	P2	2	a. 7	PS	9	74	PB	64	P10	P1	25	P3	4	3	P6	$\frac{1}{L_{\mathbf{d}}}$	88	20	10
-	1	m	2.93	12.30	18.04	5.8	0.18	15.13	7.28	4.07	7.87	1	21.38	12.57	18.90	4.75	-0.17	15.35	7.28	7.9	7.69	1
		י	5.62	10.94	20.27	9.50	0.00		6.33	5.50	10.84	1	5.07	10.11	21.13	8.31	-0.35	3.83	6.33	9.37	39.01	
		×	2.58	8.16	13.06	9.50	0.35		7.86	1.63	9.23	:	2.03	7.43	33.92	8.31	0.00	1.35	7.86	5.50	9.03	1
S	d	84	8.18	4.00	-0.3₺	-1.19	69.0		4.6	-0.82	3.68	1	9.03	4.63	00.00	-1.19	0.00	16.14	4.43	-2.65	1.49	1
		h	m.06	5.97	0.00	1.19	0.69		6.55	0.61	3.50	1	11.61	6.58	0.34	1.19	9.0	25.12	6.34	-1.22	3.33	1
		O	11.25	7.43	4.12	1.19	0.52		8.44	8.15	6.55	1	11.80	8.04	94.4	1.19	-0.17	22.80	8.23	6.32	6.39	1
		H	12.17	8.65	7.22	8.1	0.35		9.50	11.40	10.49	1	12.72	9.56	7.56	1.90	-0.34	25.28	6.50	9.57	10.32	1
		H	7.56	8.40	4.8	3.56	0.35		9.50	10.96	13.46	1	8.11	9.0	5.15	3.56	-0.3₺	17.83	9.29	8.15	13.29	1
		מ	3.35	7.55	8.25	5.46	0.35		8.66	13.64	14.86	1	3.87	8.16	8.59	5.46	-0.34	7.56	8.45	11.81	14.69	1
		×	1.1	5.148	2.67	5.48 5.67 4.75	0.35		92.9	11.40	14.51	:	1.66	6.09	6.01	4.75	-0.34	2.85	6.55	9.57	14.34	1
									Ve	rtical D	Vertical Deflection,	į	at Indicated	ted Gage	8							
							Total		100 m					V		X	Rebound					
			10	2	P	ď	25	90	7	80	6		r L	20	E P	ď	25	9 ₀	D ₇	DB	P ₂	
4	н	m	-0.01 0.006	9000		0.0	0.005		0.001	0.002	-0.001		0.044	0.011	1	0.03	0.00	0.001	0.005	0.00	0.000	
		7	-0.076	-0.003		0.011	0.015		0.000	0.001	0.005		-0.021	0.002	1	0.013	0.015	-0.001	0.001	0.001	0.003	
		×	-0.093	-0.005	1	0.00	0.022		-0.002	0.001	0.003		-0.038	0.000	1	0.01	0.022	-0.001	-0.001	0.001	0.00	
5	a	M	0.316	m.º	1	0.00	0.003		0.010	0.005	0.000		0.308	9.078	1	-0.005	-0.006	0.0	0.011	0.001	0.000	
			0.378	0.118	1	0.017	0.003		0.014	0.004	0000		0.370	0.085	1	0.003	-0.006		0.015	0.003	00000	
		o	0.321	0.102	1	0.029	0.007		0.018	0.007	0.000		0.313	0.069	1	0.015	-0.002		0.00	900.0	0.005	
		E	0.207	0.074		0.042	0.00	0.00	0.016	0.00	0.006		0.199	0.041	1	0.028	0.010	600.0	0.017	9000	9000	
		н	0.133	0.054	1	0.051	0.036		0.012	0.00	0.012		0.125	0.02	1	0.037	0.027	0.005	0.013	0.00	0.002	
		5	0.08	0.042		0.054	0.048		0.007	0.00	0.021		9.00	600.0	1	0.040	0.039	0.002	0.00	0.00	0.02	
		×	0.052	0.033		0.048	0.057		0.003	0.00	0.035		0.0	0000	1	0.034	0.048	0000	00.0	0.00	0.035	

(Continued

3.68 12.68 13.03 13.03 12.57 12.52	2 1 2 1 8 8 8 8 8 4 4 8 8 8 8 8 8 8 8 8 8 8 8	1.43 19.35 19.35 17.11 17.11 17.10 1	8.6.0 9.0.0 9.0.0 9.0.0 9.0.0 9.0.0 9.0.0 9.0.0 9.0.0 9.0.0 9.0.0	22.35 6.76 23.48 8.45 23.48 8.45 25.28 9.08 25.76 7.65 2.34 6.02 2.34 7.90 2.40 2.40 2.40 2.40 2.40 2.40 2.40 2.4	22.35 6.76 23.48 8.45 25.28 9.06 25.28 9.06 25.76 7.66 2.94 6.02 11.58 4.22 7.90 5.92 4.29 7.22 6.68 4.03	-1.19 0.00 22.35 6.76 0.00 0.00 23.48 8.45 0.59 0.00 25.28 9.06 2.37 0.00 15.30 8.99 2.37 -0.17 5.76 7.66 1.19 -0.17 1.58 4.22 -2.37 0.00 5.42 3.38 -1.19 0.00 7.90 5.91 0.00 0.00 4.29 7.53 0.00 0.00 4.29 7.53 0.00 0.00 4.29 7.53	-0.35 -1.19 0.00 22.35 6.76 0.00 0.00 0.3.48 8.45 0.00 0.00 0.3.48 8.45 0.05 0.00 23.48 8.45 0.07 0.25 28 9.06 0.07 2.37 0.00 15.30 8.99 0.17 2.37 0.01 15.30 6.02 0.00 -2.37 0.00 5.42 3.38 0.00 0.00 1.29 7.33 0.00 0.00 1.29 7.33 0.00 0.00 0.08 1.00 0.35 0.00 0.00 0.08 1.00 0.35 0.00 0.00 0.06 1.20 0.35 0.00 0.00 0.06 0.08 1.00 0.35 0.00 0.00 0.00 0.06 0.00 0.00 0.00 0.0	1,63 -0.35 -1.19 0.00 22.35 6.76 5.72 0.00 0.00 0.00 23.48 8.45 6.09 0.51 0.59 0.00 25.28 9.06 5.97 0.85 2.37 0.00 15.30 8.97 1,99 0.17 2.37 -0.17 5.76 7.66 2.31 -0.86 1.19 -0.17 1.58 4.22 1.71 0.00 -2.37 0.00 5.42 3.38 2.68 0.18 -1.19 0.00 7.90 5.91 2.68 0.18 -1.19 0.00 7.90 5.91 1.4c 0.35 0.00 0.00 4.29 7.33 1.4c 0.35 0.00 0.00 0.00 4.29 7.33 0.181 0.029 -0.002 0.040 0.03	-0.35 -1.19 0.00 22.35 6.76 0.00 0.00 0.348 8.45 0.05 0.00 25.28 9.06 0.85 2.37 0.00 15.30 8.99 0.17 2.37 0.01 15.30 8.99 0.17 2.37 0.01 15.30 8.99 0.18 1.19 0.17 1.58 4.22 0.00 -2.37 0.00 5.42 3.38 0.18 -1.19 0.00 7.90 5.42 3.38 0.17 0.00 0.00 4.29 7.33 0.35 0.00 0.00 4.29 7.33 0.35 0.00 0.00 -0.68 4.00 0.03 0.00 0.00 0.00 0.00 0.00
7.00 13.68 13.68 14.28 15.77 17.52		8.45 8.99 8.90 8.00		" " " " " " " " " " " " " " " " " " " "		0.00 0.00 0.59 0.00 2.37 0.00 2.37 -0.17 1.19 -0.17 -2.37 0.00 -1.19 0.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.51 0.59 0.00 0.05 2.37 0.00 0.17 2.37 0.01 0.00 -2.37 0.00 0.18 -1.19 0.00 0.18 -1.19 0.00 0.15 0.00 0.00	5.72 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0	5.72 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0
9.97 13.68 13.68 13.69 15.77 1.57 17.52	19.35 17.11 23.22 12.02 4.39 -0.31 -2.44 -2.44	9.8 8.2 3.4 8.8 8.4 4.4 1 1 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1		~		2.37 0.00 2.37 -0.17 1.19 -0.17 1.19 -0.17 1.19 0.00 0.00 0.00 0.00 0.00	0.51 0.59 0.00 0.85 2.37 0.00 0.17 2.37 0.00 0.18 1.19 0.01 0.00 2.37 0.00 0.18 1.19 0.00 0.15 0.00 0.00 0.35 0.00 0.00	6.09 0.51 0.59 0.00 2 5.97 0.85 2.37 0.00 1 4.99 0.17 2.37 -0.17 2.31 -0.35 1.19 -0.17 1.71 0.00 -2.37 0.00 2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.44 0.35 0.00 0.00 1.44 0.35 0.00 0.00	6.09 0.51 0.59 0.00 2 5.97 0.65 2.37 0.00 1 3.78 -0.35 1.19 -0.17 2.31 -0.86 1.19 -0.17 1.71 0.00 -2.37 0.00 2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.45 0.35 0.00 0.00 1.45 0.35 0.00 0.00 0.181 - 0.029 -0.029
13.68 13.68 13.69 15.77 1.57 17.52	23.22 12.02 1.39 -0.31 -2.44 -2.44	8.8 2.7 2.7 2.4 2.7 4.4 5.6 6.6 6.6 7				2.37 0.00 2.37 -0.17 1.19 -0.17 1.19 -0.17 -2.37 0.00 0.00 0.00 0.00 0.00	0.85 2.37 0.00 0.17 2.37 -0.17 -0.35 1.19 -0.17 0.00 -2.37 0.00 0.18 -1.19 0.00 1.72 0.00 0.00 0.35 0.00 0.00	5.97 0.65 2.37 0.00 1 4.99 0.17 2.37 -0.17 2.31 -0.86 1.19 -0.17 1.71 0.00 -2.37 0.00 2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.145 0.35 0.00 0.00 1.25 0.3 0.00 0.00 1.25 0.3 0.00 0.00 1.25 0.3 0.00 0.00	5.97 0.65 2.37 0.00 1 4.99 0.17 2.37 -0.17 2.31 -0.86 1.19 -0.17 1.71 0.00 -2.37 0.00 2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.4c 0.35 0.00 0.00 1.4c 0.35 0.00 0.00 0.01 1.4c 0.35 0.00 0.00 0.01 1.4c 0.35 0.00 0.00
13.81 13.03 1.05 1.57 1.57 1.75 1.752 1.	23.22 12.02 4.39 -0.03 0.41 -2.44	8.6.0 8.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4	the state of the s			2.37 -0.17 1.19 -0.17 1.19 -0.17 -2.37 0.00 -1.19 0.00 0.00 0.00 0.00 0.00	0.17 2.37 -0.17 -0.35 1.19 -0.17 0.00 -2.37 0.00 0.18 -1.19 0.00 1.72 0.00 0.00 0.35 0.00 0.00	1.79 0.17 2.37 -0.17 3.78 -0.35 1.19 -0.17 2.31 -0.86 1.19 -0.17 1.71 0.00 -2.37 0.00 2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.145 0.35 0.00 0.00 1.25 0.35 0.00 0.00 0.181 0.029 -0.002	1.79 0.17 2.37 -0.17 3.78 -0.17 2.31 -0.85 1.19 -0.17 1.71 0.00 2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.45 0.35 0.00 0.00 1.45 0.35 0.00 0.00 0.00 0.181 - 0.029 -0.029 0.00 0.181 - 0.029 -0.029 0.00
13.03 1.57 1.57 1.57 1.752 1.552 1	12.02 4.89 -0.03 0.00 0.41 -2.44	8. 8. 8. 8. 8. 9. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.				1.19 -0.17 1.19 -0.17 -2.37 0.00 -1.19 0.00 0.00 0.00 0.00 0.00	-0.35 1.19 -0.17 -0.86 1.19 -0.17 0.00 -2.37 0.00 0.18 -1.19 0.00 1.72 0.00 0.00 0.35 0.00 0.00	3.78 -0.35 1.19 -0.17 2.31 -0.86 1.19 -0.17 1.71 0.00 -2.37 0.00 2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.45 0.35 0.00 0.00	3.78 -0.35 1.19 -0.17 2.31 -0.86 1.19 -0.17 1.71 0.00 -2.37 0.00 2.68 0.18 -1.19 0.00 1.4c 0.35 0.00 0.00
9.09 1.57 1.4.28 1.7.52 1.7.52 1.7.52	6.89 -0.01 0.00 0.41 -2.44 -2.44	3.3				1.19 -0.17 -2.37 0.00 -1.19 0.00 0.00 0.00 0.00 0.00	-0.86 1.19 -0.17 0.00 -2.37 0.00 0.18 -1.19 0.00 1.72 0.00 0.00 0.35 0.00 0.00	2.31 -0.36 1.19 -0.17 1.71 0.00 -2.37 0.00 2.68 0.18 -1.19 0.00 1.45 0.35 0.00 0.00 1.45 0.35 0.00 0.00	2.31 -0.36 1.19 -0.17 1.71 0.00 -2.37 0.00 2.68 0.18 -1.19 0.00 1.44 0.35 0.00 0.00
1.57 - 1.28 - 8.04 - 7.52 -	-0.81 0.00 0.41 -2.44 -2.44	3.38 5.91 7.52 4.01				-2.37 0.00 -1.19 0.00 0.00 0.00 0.00 0.00 D ₄ D ₅	0.00 -2.37 0.00 0.18 -1.19 0.00 1.72 0.00 0.00 0.35 0.00 0.00	2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.45 0.35 0.00 0.00 	2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.44 0.35 0.00 0.00 D ₂ D ₃ D ₄ D ₅ 0.181 - 0.029 -0.002
4.28 8.04 - 7.52 -	0.00 0.41 -2.44 -2.44	25.97 10.4 10.4				-1.19 0.00 0.00 0.00 0.00 0.00 D ₄ D ₅	0.18 -1.19 0.00 1.72 0.00 0.00 0.35 0.00 0.00	2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.40 0.35 0.00 0.00 	2.68 0.18 -1.19 0.00 2.68 1.72 0.00 0.00 1.145 0.35 0.00 0.00 -
8.04 -	0.41 -2.44 -2.44	4.00				0.00 0.00 0.00 0.00 D. D. D.	1.72 0.00 0.00 0.35 0.00 0.00 D ₃ D ₁ D ₅	2.68 1.72 0.00 0.00 1.4c 0.35 0.00 0.00 	2.68 1.72 0.00 0.00 1.44 0.35 0.00 0.00 -0
7.52	-2.44	p4				0.00 0.00 1 Total	0.35 0.00 0.00 Total	1.4c 0.35 0.00 0.00	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	D ₈	Λ 2		111	144 1	344 1	344	D ₂ D ₃ D ₄ D ₅ O ₅ O ₁₈₁ O ₅ O ₁₈₁ O ₅	D ₂ D ₃ D ₄ D ₅ O ₃
flection, in., at Indicated Gages	.	₂		' '	D ₅ D ₆	90 50 Ma	D3 D4 D5 D6	0.181 - 0.029 -0.002	0.181 - 0.029 -0.002
60								0.181 - 0.029 -0.002	0.181 - 0.029 -0.002
0.001					-0.002	-0.002	-0.002		0000
900.0					9000	9000	0.050 0.008	0.150 - 0.050 0.008	0.150
0.019					0.028	0.028	920.0 990.0	0.114 0.066 0.028	0.114 0.066 0.028
0.035		2			0.079	0.079	- 0.082 0.079	0.082 - 0.082 0.079	0.082 - 0.082 0.079
0.034			-		0.093	0.093	- 0.086 0.093	0.061 0.086 0.093	0.061 0.086 0.093
0.062		0.013			0.093	0.093	- 0.077 0.093	0.052 - 0.077 0.093	0.052 - 0.077 0.093
0.059		0.007			₹.°0	₹.°0	150.0 650.0 -	0.045 - 0.059 0.094	0.045 - 0.059 0.094
0.012	0.01	0.068			0.002		- 0.014 -0.002	0.203 0.014 -0.002	0.203 0.014 -0.002
0.027					0.007	0.007	- 0.056 0.007	0.186 - 0.056 0.007	0.186 - 0.056 0.007
0.139					0.091	0.091	160.0 860.0	0.108 - 0.098 0.091	0.108 - 0.098 0.091
0.23		۲.			0.109	0.109	- 0.085 0.109	0.072 0.085 0.109	0.072 0.085 0.109

200 - 100 X 100 - 100 M

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	Rebo	P5_
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	Tot	2
		ا حم
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Table A-11
Multiple-wheel Heavy Gear Load Flexible Pavement Tast, Static Instrumentation Loading Data

Item 4; Load Condition: 60 kips per Wheel, Twin Tandem, 200 psi

P _L P _S P _S P _T P _B P _S S-72 -0.5 ⁴ 11.12	F ₂ P ₃ P ₄ P ₅ P ₇	P ₃ P ₄ P ₅ P ₅ P ₇ 18.08 5.75 3.72 -0.54 11.12	P _L P _S P _S P _S P _T P _B P _S	P ₅ P ₅ P ₇ P ₈ 3.72 -0.5 ⁴ 11.12	P ₆ P ₇ P ₈ -0,54 11,12	P ₆ P ₇ P ₈ 0.54 11.12	88		1 -3	P 2 14	P1C	1.41	P2 11.63	P3 16.55	P. 6.46	P 5 F	P6	P7 11.01	80	64 16.7	P10
		1.00	12.96	26.58	7.42	8.61	2.74	12.27	1	5.69	2.76	1.3	12.58	25.03	8.13	919	3.10	12.16	1	6.29	2.56
0 1	,	80	12.58	19.17	9.33	17.61	0.19	02.11	1	7.2	7.89	0.1	12.20	17.6	10.04	15.46	0.55	11.59	:	7.84	1.69
z +		8.5	10.48 6 86	8.8	10.29	۲.2 د.3	-0.36	9.52	1	%-10 %-10	%. 1.8	1.8	10.10	38.32	8 :	19.56	8.0	9.41	:	8.70	10.86
4 5		09.0	3.62	6.32	8.62	2 4	9 9 9 9	4 6	: :	6.89	13.01	8 6	\$ ₹ • •	22.00	8.1	8 8	8 8	6.20	: 1	8.70	1.37
×		09.0	2.28	3.03	8.9	20.34	-0.72	2.18	1	69.5	10.86	0.80	96.1	1.52	7.65	18.19	-0.36	2.07		6.30	10.36
(a)	1	1.20	12.96	34.20	8.49	8.51	227.42	15.03	1	8.01	6.04	04.0-	13.34	32.58	8.97	8.31	227.60	15.03	ŀ	8.10	5.63
p.	ī	01.0-	12.39	29.19	10.76	18.00	3.83	14.45	1	10.25	14.24	0.40	12.77	27.67	11.24	17.80	tc.4	14.45	1	10.34	13.83
O	ī	0.80	9.15	04.94	n.₩8	22.50	3.10	10.55	1	п.и	18.54	0.00	9.53	44.88	78.11	22.30	3.28	10.55	1	2.3	18.13
25	ī	0.80	5.43	21.35	00.11	23.08	2.01	6.43	1	10.68	18.54	0.00	5.81	19.83	11.48	22.88	2.19	6.43	1	10.77	18.13
ы	•	-0.40	2.86	7.19	60.6	59.45	0.91	3.44	1	9.04	20.18	0.40	3.24	2.67	9.57	24.45	1.09	3.44	1	9.13	19.77
1	•	-0.80	1.33	3.70	6.46	12.91	0.37	1.49	1	6.72	12.40	0.00	1.71	2.18	8.9	12.71	0.55	1.49	ł	6.81	1.99
M	1	0.80	0.57	3.27	4.30	5.87	0.18	69.0	1	72-7	5.84	0.0	0.95	1.75	4.78	2.67	0.36	0.69	1	4.83	5.43
	*					Total		Yer	Tics.	Vertical Dellection	-1	in., at Indicated Gage	red Gage	90		Rebound		1			
	1 1	ا م	D2	n n	T _Q	D2	90	D7	PB	00		o l	20	₃	ជុំ	2	90	DZ	Ba	6 _Q	
ы		ı	0.043	0.014	0.005	0.002	0.005	-0.002	:	0.000		:	0.054	0.015	0.013	0.000	٥.01	6.008	1	0.003	
84		1	0.038	o.00	0.007	0.003	0.00	-0.001	1	00000		:	0.049	0.020	0.015	0.01	0.011	0.009	1	0.003	
v		:	0.086	80.0	0.014	0.007	0.002	-0.001	:	0.001		1	0.037	0.022	0.022	0.015	0.008	0.000	1	0.00	
200		ŀ	0.017	0.021	0.021	0.013	-0.001	-0.002	1	0.005		1	0.028	0.022	0.029	0.021	0.005	0.008	1	0.005	
н		ı	0.007	0.01	0.086	0.022	-0.003	-0.003	1	0.003		1	0.018	0.018	0.034	0.030	0.003	0.007	ı	900.0	
b		1	0.002	0.0L	0.083	0.035	-0.005	0.00	1	0.005		:	0.009	0.012	0.031	0.043	0.001	900.0	ł	0.008	
×,		1	-0.006	0.007	0.018	0.041	-0.005	-0.005	1	0.005		1	0.005	0.008	0.026	0.049	0.000	0.005	ı	0.008	
(a)		1	0.045	0.000	0.055	900.0	0.010	0.007	1	-0.001		1	650.0	0.035	0.020	-0.003	o.016	0.01	:	0.004	
Bq.		:	0.036	0.042	0.033	0.015	0.007	0.007	ı	0.002		1	0.060	0.037	0.031	900.0	0.013	0.011	ı	0.007	
ø		ı	0.019	0.040	0.0	0.028	0.003	900.0	:	0.004		;	0.043	0.035	0.042	0.00	600.0	0.010	ł	0.00	
121		1	0.003	0.033	0.049	0.053	-0.001	0.00	1	0.008		1	0.027	0.028	0.047	0.044	0.005	0.008	ı	0.013	
н		1	-0.008	0.025	0.049	0.075	-0.004	0.003	:	0.012		:	0.016	0.020	0.047	990.0	0.002	0.007	:	0.017	
5		1	₩0.0-	0.016	0.039	0.087	-0.005	0.000	1	0.012		1	0.010	0.01	0.037	0.078	0.001	0.004	1	0.017	
×		1	-0.0T	0.010	0.005	0.081	-0.005	100.0-	1	0.010		1	0.007	0.005	0.024	0.072	0.001	0.003	1	0.015	
																				S	
										(Continued	(De									0 00 1	Shanes a

								1000		Ver	tical Pr	essure, p	el, at In	at Indicated Cell	Cells		11. The second		Surface Street			200
	1						2	tel	100 mg 27 25 (4)		700			X 14		ANDINE	Rebo	pun				
8		1	4	2	ન	4	2	9	7	8	4	P10	P1	P2	3	PL	PS	94	$T_{\overline{d}}$	PB	6	014
-	-		-1.a	12.87	17.54		1.56	-0.72	11.24	1	4.48		0.40	12.68	19.50	6.22	1.17	-0.72	17.TE	1	4.82	0.82
		•	-1.a	14.49	26.58		8.21			1	6.55		0.40	14.30	28.54	60.6	7.82	1.10	12.50	1	6.89	3.08
		Ħ	-1.a	10.48	30.72		23.08	-0.36	8.72	1	8.79	11.06	0,40	10.29	32.68	12.32	55.69	-0.36	8.60	ı	9.13	36.01
5	٦	83	0.40	8.96	1.92		1.8			1	6.20		0.00	9.53	8.06	5.74	3.53	-1.09	15.83	1	6.03	0.61
		•	09.0	10.10	7.84		4.69			1	8.96		0.20	10.67	11.98	2.90	92.9	1.46	17.66	1	8.79	4.50
		0	09.0	8.6	5.78		9.98			1	11.00		0.20	10.48	8.92	9.33	11.55	-0.36	16.98	1	10.85	12.09
		H	0.40	7.62	10.13		14.03			1	12.57		0.0	8.19	14.21	10.29	15.65	-0.5₺	12.96	1	12.40	18.44
		н	0.40	4.57	5.0		14.28			1	12.75		0.00	5.14	9.15	10.05	15.85	-0.36	7.57	ı	12.58	19.05
		12	0.40	5.29	00.0		15.45			1	10.85		0.0	2.86	41.4	8.61	17.00	-0.36	3.90	1	10.68	2.2
		×	0.40	6.0	1.3	5.86	9.78			1	8.61		0.0	1.52	2.63	5.82	11.35	-0.36	1.84	1	8.44	15.78
															4				A transfer			
									2	ertical	Vertical Deflection		in. at Indicated Gage	ated Gag	86							
						-	TOTAL		1		-		-	-		4	Hebeund		-		1	
			4	2	H	a d	2	90	4	80	ا ا		ď	25	3	4	5	90	4	B	9	
н	7	м	1	0.054	0.014		•	10000	7 0.002	1	-0.001		:	0.069	0.018		0.008	0.000	0.00	:	0.000	
			1	0.043	0.CE	0.00	0.002		5 0.003	1	0.000	_	1	0.058		0.016	0.011	0.008	0.005	1	0.001	
		×	1	0.026					0.003	1	0.00	٥.	ľ	0.031		0.031	0.023	0.003	0.005	1	0.003	
~	7	M	1	0.135					0.010	1	0.001		1	0.046	-	-0.032	-0.039	0.052	0.009	1	0.001	
		i.	1	0.142				0.035	5 0.016	1	0.003	_	. 1	0.053	-	-0.010	-0.034	0.045	0.015	1	0.003	
		O	1	0.128					3 0.018	1	0.00	10	ı	0.039		0.00	-0.022	0.038	0.017	1	0.006	
		æ	1	0.099					9 0.013	1	0.012	6.	1	0.010		0.045	0.010	0.029	0.017	1	0.012	
		H	1	0.065					9 0.015	1	0.0	فيرر	1	-0.00th		0.054	0.070	0.019	0.01	1	0.021	
		17	1	0.03					-	1	0.03		1	-0.055		0.062	0.134	0.012	0.00	1	0.031	
		×	1	0.022				٠		1	0.034		:	-0.067	0.021	0.055	0.162	0.00	0.00	1	0.034	

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1										N.	rtical Pr	Vertical Pressure, psi.	bet, at It	at Indicated	Cells							
	3						To	Total									Hebo	bunk				
2	類	100	4	2	2	4	.5	P6	L _d	88	م	P10	P	2	~ 	4	2	P6	P7	PB	٩	P10
5	8	M	0.00	98.9	2.62	5.74	3.13	222.15	16.29	1	8.96		-2.01	7.24	2.62	6.22	3.9	222.15	16.52	1	9.30	7.35
			0.00	6.29	3.71	6.70	5.09	1	12.96	1	11.20	16.98	-2.01	19.9	3.71	7.18	5.87	1	13.19	1	11.54	16.78
		o	-0.80	4.76	2.83	7.18	6.45	1.83	п.36	1	12.23		-2.8I	5.14	2.83	7.66	7.24	1.83	11.59	1	12.57	21.39
		Ħ	-0.40	2.76	1.53	6.70	7.05	1.46	6.43	1	11.72		-2.41	3.14	1.53	m	7.83	97.1	99.9	١	12.06	22.11
		н	-0.20	1.52	0.87	5.74	6.17	1.10	3.44	1	66.6	Ü	-2.21	1.90	0.4	6.22	7.9	1.10	3.67	1	10.33	23.95
		4	-0.20	0.57	0.22	4.19	3-53	0.73	1.61	1	7.41		-2.2	0.95	0.22	19.4	4.3	0.73	1.84	1	7.75	15.14
		M	-0.20	0.00	0.2	2.63	1.37	0.37	69.0	1	2.00		-2.21	0.38	2.0	3.11	2.15	0.37	0.92	i	5.34	6.33
1	7	M	0.20	3.24	0.87	2.15	0.98	-1.46	11.12	1	4.65		0.00	1.0	0.98	3.23	1.57	-1.82	11.46	1	5.34	2.16
		0	0.00	3.24	3.92	3-47	2.35	1		1	8.10		-0.20	1.01	4.03	4.55	2.94	1	11.69	1	8.79	8.8
		н	-0.40	1.33	1.09	3.23	3.91	-1.10		1	8.70		-0.60	2.10	1.20	4.31	4.50	-1.46	5.73	1	9.39	12.30
		×	07.0-	0.00	0.44	1.79	1.76	-1.10		1	5.68		-0.60	0.77	0.55	2.87	2.35	94.1-	1.83	1	6.37	8.6
												1										
									2	Vertical	Deflection	lon, in.	at Indica	Indicated Gages	84		100					
			ι _α	D2	D3	δÎ	200	90	Fr	P _B	60		ι	22	E P	δ.	Peboung D ₅	D6	10	B _Q	60	
5	N	80	1	0.111	0.116	0.043	0.010			1	0.00	2	1	0.159		0.128	-0.057	0.076	0.027	1	0.00	
		p.	1	0.082				0.051	0.035	1	0.00.5	2	1	0.130	0.109	0.156	-0.043	0.062	0.032	1	0.000	
		o	ı	0.044						1	0.026	6	1	0.092		0.157	0.032	0.045	0.031	ı	0.023	
		H	1	0.001						1	0.045	6	1	0.049		0.157	0.143	0.007	0.06	1	0.044	
		н	1	-0.031						1	0.065	5	1	0.017		0.157	0.22h	0.017	0.018	ı	090.0	
		4	1	-0.053						1	0.07		•	-0.005		0.146	0.277	0.011	0.01	1	0.069	
		×	1	-0.066						1	0.07	0	1	-0.018		0.108	0.303	900.0	0.006	1	0.065	
1	п	M	1	0.162						1	0.00	2	1	0.182		0.015	-0.060	0.146	9.00%	1	-0.029	
		v	1	0.147						1	0.026	6	1	0.167		0.037	-0.027	0.123	0.050	1	-0.006	
		н	1	0.075	0.150	0.069				1	0.114		1	0.095		0.059	0.172	C. OLA	0.046	1	0.080	
		M	1	0.021						1	0.17	•	4	0.041		0.053	0.326	900.0	0.023	:	0.145	

International

	2	2.97	5.73	5.73	1.7	1.23	5.66	4.20	2.02	-0.62	0.41	0.20	-0.93																
	4	\$.5	7.49	5.5	3.10	3.36	1.82	4.82	3.27	1.20	1.72	1.03	-0.18		1	6	-0.042	0.053	0.196	0.237	-0.061	-0.m9	0.161	0.284	0.035	0.142	0.350	0.357	
	88	ı	1	1	1	1	1	1	1	1	1	1	1			80	ı	1	1	1	1	1	1	:	1	1	1	1	
	77	8.48	5.73	5.29	94.0	5.39	5.03	2.87	1.04	1.50	94.0	-0.91	-1.83			27	6,063	0.075	0.051	0.00	0.042	0.077	0.068	0.034	0.088	0.097	690.0	0.041	
Para cent	9	96.0	0.73	0.36	0.00	9.47	0.00	-0.36	-0.36	1	1	1	1			90	0.186	0.125	0.051	0.a9	0.127	0.121	0.071	0.00	0.260	0.240	0.19	0.169	
-	P	1.27	2.44	2.05	98.0	0.39	96.0	1.27	0.78	-0.39	-0.19	-0.39	-0.59		Rehound	2	450.0-	0.067	0.277	0.312	0.026	0.049	0.152	0.22	-0.000	0.027	9/0.0	0.072	
	4	2.40	2.87	2.16	96.9	1.31	1.55	1.31	0.83	· 0.24	. 21.0-	0.148	.0.72			c ^a										0.057			
27.	25	1.31	1.09	0.44	0.22	0.33	0.33	0.33	0.11	-2.07	-2.07	-2.07	-2.07			P3	901.0	0.128	0.074	0.028	690.0	0.099	0.000	0.038	0.039	0.039	0.01L	0.000	
Ceted C	2	2.58	1.72	0.77	3.43	1.53	1.33	0.77	61.0	-0.19	-0.39	-0.77	. 96.0-		20 000	20	0.289	0.200	0.099	0.057	0.238	0.177	0.067	0.015	-0.10I	-0.as7	-0.200	0.26	
et Ind	4	1.80	1.40	1.00	1.00	0.40	0.40	0.20	0.00	0.40	0.40	0.40	0.40	Total control from	7007	2	1	1	1	1	1	1		1	:	1	•		
ure, pai	la P	2.36	5.12	5.12	1.13	0.82	2.2	3.79	1.6	1.02	5.02	1.84	0.71	1															
al Press	2	5.34	6.89	5.34	2.50	2.58	10.4	10.4	2.49	2.41	2.93	2.24	1.03	1000	1000	8	0.005	0.110	0.253	0.30	0.000	0.042	0.222	0.345	0.002	611.0	0.297	0.334	
Vertic	84	1	1	1	1	1	1	1	1	1	1	1	:	Vanetant De Canting	1	80	1	1	1	1	1	1	1	1	1	1	1	1	
	17	8.00	5.27	1.83	0.00	4.58	4.24	5.06	0.23	3.22	2.18	0.81	n.º.	Version of		7	0.077	0.089	0.065	0.039	0.065	0.100	0.092	0.057	0.078	0.087	0.059	0.031	
	9	6.73	9.36	0.73	1.09	9.83	96.0	00.00	0.00	96.0	96.0	-0.36	. 96.0			90	0.283	0.222	0.148	917.0	0.189	0.183	0.133	0.088	0.125	0.105	0.059	0.034	
- Brok	27	1.18	73	i de								0.39	1014		Total	2	0.002	0.133	0.343	0.378	0.003	0.000	0.123	0.192	0.003	0.032	0.081	0.077	
	4	2.16	2.63	1.8	0.72	96.0	1.20	96.0	97.0	0.59	0.71	0.35	n.º			đ	0.089	0.161	0.162	0.090	0.0LL	0.118	0.157	0.132	0.033	0.078	0.000	0.017	
	-	1.20	96.0	0.33	n.º	44.0	0.44	0.44	0.22	0.11	n.0	n.º	n.º			5	0.130	0.148	0.00	0.048	0.061	0.09	0.062	0.030	0.045	0.045	0.000	0.003	
	20	2.39	1.53	0.58	3.24	1.34	1.14	0.58	0.0	0.77	0.57	0.19	0.00			2										-0.008			
	4	09.0	0.20	0.30	0.30	1.00	1.00	0.80	09.0	0.40	0.40	0.40	0.40			4	1	:	1	1	1	1	1	1	1		1		
	t Se		ó	н			•	н			0			,				0	-			0	н			0		.	
	NE E	~				1				~							~				1				N				
						#						1					7				#								

Table A-12 Multiple-Wheel Heavy Gear Load Flexible Pavement Test, Static Instrumentation Loading Data Item 3; Load Condition: 30 kips per Wheel, 6 Wheels, 100 psi

-										Vert	cal Pre	ssure. Ds	Vertical Pressure, psi. at Indicated Cells	icated C	ells							
	Tond				STATE OF		Tol	18.									Reby	Rebound				
è	Polint	tion	4	a:	3	P.	P5	P6	L _a	P8	P9	P10	a.		۳,	a ^t	75	P6	P	8	9	P10
1.63	1.62	84	8.3	5.50		5.61	0.87	9.36	17.77	0.10	2.89	-21.93	11.25	47.74	3.78	1.42	0.18	8.35	3.27	0.51	2.10	99.0
-	-	h	13.27	7.07		70.7	69.0	12.07	5.06	2.95	4.29	-22.12	12.54	6.2	9.88	2.0	0.0	11.06	4.22	3.36	3.50	74.0
1.83	162	0	13.08	7.67		5.46	69.0	13.54	5.49	2.03	5.77	22.49	12.35	6.81	9.6	4.27	0.00	12.53	4.65	2.4	8.4	0.0
		Ħ	8.75	7.90		7.0	69.0	10.15	5.70	3.36	7.08	-22.40	8.00	8.9	8-33	5.85	0.00	41.2	78.4	3.77	6.39	0.19
		H	4.2	7.19		7.84	69.0	8	5.27	6.72	8.13	-22.59	3.51	6.33	10.91	6.65	0.00	3.95	4.43	7.13	4.7	9.0
		h	2.30	5.93		7.96	69.0	5.70	4.43	3.05	8.13		1.57	8.4	5.8	6.77	0.00	1.69	3.59	3.46	7.34	-0.18
		×	1.47	4.51		6.65	69.0	1.80	3.58	0.30	6.73		0.74	3.65	1.63	5.46	0.0	0.79	2.74	0.7	2.5	0.28
-	н	M	0.98	2.56	0.17	3.56	0.60	1.12	2.2	-0.31	3.50		0.19	1.70	0.26	2.37	0.0	0.11	1.37	0.10	2.7	0.10
			0			- 3																
									V	Vertical I	Deflect1	on in.	Deflection, in., at Indicated Gages	ted Gage				100				
							Total										Rebound	_				
			L _D	22	a a	T _G	2	9	4	P8	o _Q		ď	e ^c	2	4	25	99	r _d	æ	60	
1 & 3	182	M	0.113		0.00	0.00	0.002	0.003	0.00	0.001	0.001		0.129			9.006	0.028	0.00		0.00	0.002	
н	H	h	0.081	0.00	0.000	0.00	0.006	0.002	Ĭ	0.001	0.001	100	0.097	0.022	0.037	0.009	0.032	0.003	0.004	0.00	0.00	
		U	0.050		0.035			0.00		0.002	0.002		0.066			0.012	0.037	0.00		0.003	0.003	
		H	0.00		0.027			0000	0.003	0.002	0.003		0.042			0.014	0.044	0.00	0.003	0.003	0.00	
		н	0.008		0.03			0.000	Ĭ	0.002	0.00		0.00			0.00.5	0.054	0.001		0.003	0.005	
		'n	0.00		0.00			0.00		0.00	0.00		0.316			0.03	0.062	0.00		0.00	0.13	
		×	-0.006		-0.0d			0.002	Ĭ	0.00	0.005		0.00			0.00	0.063	0.003	00000	0.002	900.0	
-	1	IR	0.100		-0.005			0.00	0.003	0.000	5.001		0.006			0.004	0.039		0.003	0.001	0.00	

							-			Vert	Ce Pres	sure, pei	s at Ind	Icated C	110			STATE OF THE PERSON				
	7	100			-	1	2	3									Rebo	pun				1
3	Potest Potest	1100	4	2	4	4	4	9,	4	8	201	10	4	P2	P3	a. 1	3	P6	7	84	0	100
1,3,5	2,1,2		11.24	18:4	3.44	1.67	0.0	11.29	2.1	2.73	2.Ro	0.65	8.6	1.87	5.06	1.67	4.16	1:1	:	1 50	150	1 :
	5 2 5		13.08	6.00	13.49	2.85	0.0	12.53	5.17	7.74	4.37	0.56	11.70	80.9	12.11	4	71. 17	19 61	1 %	* 5	20.5	7
	2,1,2		14.19	6.82	11.86	4.36	0.0	13.21	5.8	6.82	6.30	0.47	12.80	6.83	10 18	8	71. 1		3 6	3.01	¥	d :
		m	8.84	6.82	11.95	5.59	30.00	8.70	5.8	7.00	7.69	27.18	7.55	6.80	10.57	2 50	74. 19	43.69	2.50	0.0	1 :	9:1
		н	1.3	6.21	19.25	6.65	-2.77	3.95	5.38	9.57	8.57	3.47	8.8	6.21	17.87	6.65	30	3.83	2	2 2	7.7	Z.Z.
		17	2.39	2.00	9.97	6.83	-2.43	1.70	4.43	5.39	8.39	5.06	1.10	8.8	8.50	6.80	2.5		7.50	2.30	S S S	0 0
		M	1.47	3.66	3.8	5.59	70.02	99.0	3.38	2.14	6.56	2.18	0.18	3.06	1.63	5.50	74.18	2 4		3 :	7 9	10.2-
	2 4 2	*	1.0	1.83	1.01 1.83 1.21 2.50 -4.16	2.50	-4.16	0.12	1.8	1.42	2.97	2.62	-0.28	1.83	-0.17	2.50	8	8 8	1.75	-2.65	8.3	- S. S.
									Vei	tical D	Llection	n. in. e	at Indicat	Ped Gare								
							Total					Service and					Debruma				1	
			러	20	씍	4	2	90	70	8	00		ď	20	9	ď	202	90	D7	08	og	
1,3,5	2,1,2		0.226	0.047	0000	0.000 0.000	0.00		900.0	0.00	-0.00		0.153	0.043	0000	0.007	-0.09	0.01	0.36	8	180	
٠	5 7 5		0.165	0.041	0.00	0.004	0.025		0.00	0.003	-0.002		0.09	0.037	0.000	0.00	-0.0at	0.00	0.00	0.00	900	
	2,1,2	o	0.122	0.030	0.00	0.0g	0.028		0.00	0.00	0.00	,	0.049	0.00	00000	0.07	-0.00	9000	0.016	0.00	0.00	
		Œ	0.093	o.m9	0.00	0.063	0.044		9000	0.00	0.00		0.000	0.015	0.000	0.021	0.005	0.00	0.013	900	0.00	
		н	0.076	0.013	0.000	0.00	0.062	0000	0.002	0.00	0.008		0.003	600.0	0.000	0.003	0.033	0.003	0.00	9000	900	
		ר	0.066	0.00	0.000	0.002	0.0		-0.002	0.00	0.010		-0.007	0.005	0.000	0.00	0.065	0.002	*0.00	0.00	0.00	
		M	0.001	0.001	0.00	0.617	0.153		-0.004	0.003	0.010		-0.012	0.003	0.000	0.015	0.124	0.003	0.003	0.00	900	
	0 8		0.057	0.006	0.00	0.00	0.083	0.00	-0.00	0.001	0.001		-0.016	0.002	0.000	0.00	0.054	0.003	0.003	0.000	o.a9	

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Table A12 (Continued)

									Verti	Cel Pres	Vertical Pressure, psi, at Indicated Cells	et Ind	Ceted C	alle			l				
		13/				Tot	1									Febound	pur				
No. Point	at the		P2	A.	ď	25	P6	PZ	PB	8	Plo	F. 1	P	P3	Ω,-3	a,	P6	2	8	6	10
546 14	2	7.19		1.03	1.07	0.17	13:11	4.22	0.91	2.62	0.19	69.9	3.41	1.20	0.35	-0.8,	æ.u	3.37	2.2		25.41
5 1	•	म.न		3.09	2.73		13.09	6.02	-17.02	8	-22.87	10.78	2.6	3.28	2.01	0.0	12.87	5.17	6.72		67
546 14	8	13.09		3.52	3.80		13.54	6.65	-18.54	06.9	-24.37	12.53	5.8	3.69	3.06	0.00	13.32	5.80	5.80	6.47	0.85
	=	8.30		8.01	8:		8.92	6.65	-18.23	3.39	-25.12	1/1	5.97	8.2	12.21	0.0	8.69	5.80	6.11	7.96	0.10
	H	3.97	3.53	16.58	8.8		4.17	6.23	-17.01	9.36	-25.31	3-41	3.6	16.75	5.22	0.00	3.95	5.38	7.33	8.83	60.0
	ט	2.03		8.76	6.65		1.80	5.17	-20.07	8.91	25.31	1.47	4.51	8.93	5.93	0.0	1.58	4.30	12.4	8.16	-0.09
	M	1.39		1.89	5.59		0.0	4.12	-23.22	7.16	-25.40	0.73	3.29	2.06	18.4	3.16	0.68	3.27	1.12	6.73	-0.18
5 1		0.93		0.17	2.73		0.22	2.43	-24.14	3.14	-25.12	0.37	1.58	0.34	2.0	0.0	0.0	1.58	0.30	2.7	0.10
								Λ	Vertical D	Deflection.	n. in.	in. at indicated Gages	ted Gage	15							
						Total										Pebound		ŭ			
		D ₁	20	D ₃	റ്	2	90	$\mathcal{L}_{\mathbf{Q}}$	8 _C	30		D	2	D	70	50	90	74	θα	00	
54614	2 2	0.089	9 0.065 0.000 0.03	0.000	0.013	0.007	0.020	0.016	0.002	0.001		0.134	0.057	0.000	0.008	-0.006	0.021	0.017	0.005	0.022	
5 1	•	0.06	1 0.057	0.109	0.023	0.021	0.019	0.031	900.0	0.00		0.108	0.00	0.093	0.018	0.00	0.020	0.032	0.00	0.025	
5 4 5 1 4	2 6	0.02	0.000	0.00	0.028	0.044	0.01	0.035	0.007	0.01		0.073	0.032	0.000	0.023	0.031	0.022	0.036	0.007	0.032	
	E	0.00	920.0	0.108	0.035	0.076	0.008	0.032	0.01	0.019		0.047	0.020	0.092	0.030	0.063	0.009	0.033	0.01	0.000	
	H	-0.01	3 0.018	00000	0.035	0.097	0.003	0.017	0.010	0.028		0.027	0.00	0000	0.030	0.03	0.004	0.018	0.00	0.00	
	ט	-0.02	3 0.012	0.000	0.031	0.128	0.001	0.00	0.00	0.037		0.017	0.00	0.000	0.006	्मः	0.002	0.010	0.009	0.09	
	ĸ	-0.03	10.00	0.029	0.085	0.166	0.001	0.006		. 0.039		0.012	0.003	0.013	0.02	0.153	0.00	0.007	0.007	0.000	
5 1		-0.03	0000	0.019	0.013	0.081	0000	0.00	0.00	0.016		0.00	0.001	0.003	0.008	0.068	0.001	0.00	0.003	0.037	

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1.66 1.67 1.66 1.66 1.66 1.66 1.67 1.66 1.66 1.66 1.66 1.66 1.66 1.66 1.66 1.66 1.66 1.67 1.66 1.67 1.61 1.67< | E 4.33 3.07 0.34 0.77 10.72 4.00 2.55 2.77 0.09 1.1.9 3.17 0.43 1.13 0.00 12.52 4.00 7.54 4.1.9 7.34 3.17 0.09 7.34 3.17 0.09 7.34 3.17 0.09 7.34 3.17 0.09 7.34 3.17 0.09 7.34 3.17 0.09 7.34 3.17 0.09 7.34 3.17 0.09 7.34 3.17 0.09 7.34 3.17 0.09 9.13 4.36 1.06 0.07 1.01 0.09 7.34 7.35 0.09 9.13 4.36 1.05 2.36 0.00 1.05 0.00 1.01 0.09 0.00 0.00 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 <t< td=""><td>E 4.33 3.0° 0.34 0.77 1.0° 1.0° 19 19 19 19 19 19 19 19 19 19 19 19 0.00 19 75 49 79 49 75 41 0.09 79 19 19 0.00 1410 59 41 09 19 19 19 0.00 1410 59 49 19 19 0.00 09 79 49 19 19 09 09 19 79 41 09 19 19 19 19 19 19 19 79 41 09 19 09 11 09 11 09 11 09 11 09 11 09 11 09 11 09 11 09 11 09 11 09</td><td>E 4.33 3.05 0.34 0.77 1.04 0.05 1.14 0.09 7.34 3.17 0.43 1.19 0.00 9.93 4.00 F 6.82 3.78 0.77 1.18 0.00 12.52 4.66 7.34 4.13 0.09 7.34 3.47 0.04 1.37 0.05 1.77 0.00 9.13 4.36 0.06 1.60 0.00 1.10 0.09 7.34 1.37 0.06 1.06 0.00 1.10 0.09 7.34 1.37 0.09 0.06 1.00 0.00 1.10 0.09 7.34 1.37 1.36 1.40 0.00 1.10 0.09 9.13 1.20 1.00 0.00</td></t<> <td>E 8-33 3-30 0-34 0-77 1-30 1-30 0-35 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 1-15 0-16 0-16 1-15 1-15 1-15 0-16 1-15 0-16 1-15 1-15 1-15 0-16 1-15 1-16 1-</td> | E 4.33 3.0° 0.34 0.77 1.0° 1.0° 19 19 19 19 19 19 19 19 19 19 19 19 0.00 19 75 49 79 49 75 41 0.09 79 19 19 0.00 1410 59 41 09 19 19 19 0.00 1410 59 49 19 19 0.00 09 79 49 19 19 09 09 19 79 41 09 19 19 19 19 19 19 19 79 41 09 19 09 11 09 11 09 11 09 11 09 11 09 11 09 11 09 11 09 11 09 11 09 | E 4.33 3.05 0.34 0.77 1.04 0.05 1.14 0.09 7.34 3.17 0.43 1.19 0.00 9.93 4.00 F 6.82 3.78 0.77 1.18 0.00 12.52 4.66 7.34 4.13 0.09 7.34 3.47 0.04 1.37 0.05 1.77 0.00 9.13 4.36 0.06 1.60 0.00 1.10 0.09 7.34 1.37 0.06 1.06 0.00 1.10 0.09 7.34 1.37 0.09 0.06 1.00 0.00 1.10 0.09 7.34 1.37 1.36 1.40 0.00 1.10 0.09 9.13 1.20 1.00 0.00 | E 8-33 3-30 0-34 0-77 1-30 1-30 0-35 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 0-15 1-15 1-15 0-16 0-16 1-15 1-15 1-15 0-16 1-15 0-16 1-15 1-15 1-15 0-16 1-15 1-16 1- |

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							I			Verti	al Pres	Vertical Pressure, Daf. at Indicated Cells	at Indi	cated Ce	115							1
	1000	Tone					Tot	1									Rebound	PE				
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64	1 4 2	鱼		2.07	2.07 -0.68	0.36	0.36 -0.18	99.9	3.27	-0.41	3.7	-0.09	3.13	2.19	0.17	0.72	0.0	4.0	3-48	1.8	5.09	2.44
٢	4	ja,		2.68	-0.34	12.0	%	10.16	4.12	0.50	3.15	-0.09	41.4	2.80	0.51	1.07	0.13	\$.6	4.33	1.93	3.35	2.14
6 7	1 & 2	U		3.0	-0.08	1.07	-2.18	13.20	4.65	0.20	4.55	-1.22	4.51	3.16	7.3	1.43	0.0	12.98	7.86	1.63	4.72	1.3
		×		3.16	0.52	1.78	9.0	9.14	7.86	3.05	\$.9	-2.16	3.13	3.38	1.37	2.14	0.18	8.8	5.07	94.4	n.9	0.37
		н		3.04	9.9	2 14	-0.18	4.40	74.7	6.98	6.99	-2.34	1.93	3.16	1.80	2.50	0.00	4.18	4.65	8.35	7.16	61.0
		ь		2.43	0.43	2.37	0.0	1.92	3.59	3.36	7.36	-5.63	1.20	2.55	1.28	2.73	91.0	1.70	3.80	62.7	7.43	-0.10
		×	-0.18	1.82	1.0-	5.08	0.00	1.01	2.75	₽.o-	5.68	3.28	0.83	1.9	99.0	2.38	0.18	0.79	2.96	1.22	5.82	5.8
						\\	i		Ve	Vertical De	Deflection	1 4	in., at Indicated Gages	ed Gages								
							Total									24	Rebound					
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6 4	1 4 2	M	0.000	0.072	0.072 0.000 0.017 0.009	0.017	0.009	0.059	0.072	0.01	0.00		0.00	690.0	000.0	0.01	0.027	0.055	0.062	0.007	-0.01	
7	п	ía,	0.000	0.061	0000	0.028	0.026	0.050	0.091	0.018	0.022		0.000	0.058	0.00	0.022	0.044	0.046	0.081	0.004	0.002	
4 9	1 \$ 2	O	0.00	0.0	000.00	0.037	0.052	960.0	0.114	0.024	0.044		0.00	0.041	0.00	0.031	0.000	0.032	0.10	0.000	0.00	
		b:	0.000	0.007	0.000	0.044	0.093	0.023	0.09	0.00	0.080		0.00	0.084	0.00	0.038	नाः	0.019	0.08	90.0	0.060	
		н	0.000	0.018	0.065	0.047	0.109	0.017	0.064	0.032	0.106		0.000	0.0.	0.062	0.041	0.127	o.a3	0.054	0.028	0.0B2	
		h	000°C	C.01	0.034	0.043	0.132	-	0.039	0.030	0.138		0.000	0.009	0.031	0.037	0.150	0.007	0.009	0.026	977.0	
		×	0.000	0.00	0.000	0.031	0.140	900.0	0.022	0.03	0.189		0.00	0.003	0.00	0.00	0.158	0.00	0.a2	0.018	0.169	

					100					Verti	al Pres	sure. psi	at Indicated	cated Co	1118							100 N 100 N
							Tot	7	100								Rebor	pun		SHALL COLUMN		
Row	S E	1 2 2	4	4	4	4	٠ <u>٠</u>	P6	4	8	P9	110	4	A.0	 	о	25	9	$\frac{\mathcal{I}_{\mathbf{d}}}{\mathbf{d}}$	P ₈	64	P10
1,9,11	2,1,2	(a)	1.47	1.59	0.17	0.18		3.50	2.64	0.0	1.22	0.00	1.47	1.7	0.00	0.148	-0.17	4.17	2.85	1.23	1.7	9.0
7.7	2,2		1.66	1.83	0.17	0.72		5.87	3.17	0.20	5.00	-0.10	1.66	1.9	0.0	0.72	-0.17	6.5₺	3.38	1.43	2.62	0.16
1.9,1	2,1,2	0	1.66	2.01	0.17	0.83		8.13	3.69	0.20	3.05	00.00	1.66	2.19	0.00	0.83	-07	8.00	3.90	1.43	3.58	0.28
		×	1.20	2.07	0.17	1.07		5.87	3.80	2.03	4.19	-0.19	1.20	2.19	0.00	1.07	0.00	6.54	₽.4	3.26	4.72	0.0
		н	0.74	2.07	0.3	1.43		2.71	3.59	2.60	5.24	-0.28	0.74	2.19	0.17	1.43	0.00	3.38	3.80	6.83	5.77	8.0
		מ	94.0	1.7	0.17	1.43		1.00	2.96	2.13	5.33	-0.38	94.0	1.83	0.00	1.43	0.00	1.69	3.17	3.36	5.86	-0.10
		M	0.37	1:3	0.17	1.19		₩.0	2.35	0.50	4.37	-0.19	0.37	1.46	0.00	1.19	0.0	1.13	2.53	1.43	6.4	0.09
7411	2 \$ 2	×	4.0	98.0	0.17	0.83	0.35	0.0	1.16	-0.61	1.74	-0.19	0.74	1.10	0.0	0.83	0.0	19.0	1.37	0.62	2.27	0.09
																					1	
							Total		A	rtical D	Deflection	5	at Indicated Gas	red Cage			Rebound				1	
			4	2	<u>م</u>	ď	2	90	7	80	8		ď	20	3	Ta a	2	90	D7	80	29	
1,6,1		M	660.3	0.076	0.110	0.017	0.00			0.017	0.00		0.105	0.069	0.088	0.012	-0.084	0.064	0.087	0.01	-0.077	
7,	2,2	۵.	0.075	0.066	0.127	0.08	0.021			0.08	0.024		0.081	0.059	0.105	0.021	-0.071	2.055	0.096	0.00	-0.062	
7,9,11		O	0.047	0.046	0.157	0.035	0.055			0.032	0.060		0.053	0.039	0.135	0.030	-0.037	0.037	0.m	0.00	-0.006	
		H	0.00	0.030	0.132	0.043	0.160			0.038	0.176		0.031	0.023	0.110	0.038	0.068	0.082	0.090	0.032	0.000	
		H	0.014	0.00	0.061	0.045	0.167			0.040	0.190		0.020	0.012	0.059	0.000	0.075	0.012	0.054	0.034	0.104	
		מ	0.007	0.007 0.013	0.048 0.039	0.039	0.193	0.012	0.041	0.035	0.509		0.013	900.0	0.00	0.034	0.101	0.006	0.027	0.00	0.123	
		×	0.005	0.00	0.033	0.031	0.249			0.028	0.261		0.01	0.002	0.011	0.006	0.157	0.003	0.024	0.022	0.175	
7 8 13	2 4 2		0.00	0.007	0.00	0.016	0.116			0.015	0.157		0.008	0000	0000	0.01	0.054	00000	0.003	0.00	0.07	

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Table

										Vert	cal Pres	seure. Ds	Vertical Pressure, ust, at Indicate Cell	frate Ce	11:							1
	Lond	7	į				Tot	7									Rebound	pur				
RCW	Point	tion	a,rt	۳.	~m	a.	25	8	P7	P8	٠,	20	٠,	42	4	d,	4	9	4	8	4	200
ជ	H	(m)	0.10	0.85	1.37	92.0		1.58	8.8	-0.81	96.0	-0.09	1.5-	0.85	-0.69	0.12	0.00	2.93	2.00	1.63	1.10	0.10
		fle	0.19	0.97	1.37	0.36		2.49	2.53	-0.61	1.48	0.00	-2.05	0.97	-0.69	0.12	0.0	3.84	2.53	1.83	1.8	0.19
		U	1.93	1.2	1.54	09.0		3.8	2.85	-0.40	2.10	0.0	-0.36	1.2	-0.52	0.36	0.0	1.29	2.8	2.0	2.5	0.19
		Ħ	1.73	1.2	1.54	0.60		2.03	5.3	0.0	2.77	0.00	94.0-	1.21	-0.52	0.36	0.0	3.38	5.62	2.₩	3.15	0.19
		н	1.57	1.21	1.71	17.0		0.68	2.74	0.41	3.41	60.0	-0.64	1.21	-0.35	6.47	0.0	2.03	2.74	2.8	3.85	0.38
		7	1.48	0.97	1.63	0.71	0.0	-0.22	2.32	-0.40	3.41	-0.09	-0.73	0.97	-0.43	6.47	0.0	1.13	2.35	70.2	3.85	0.10
		×	1.66	0.85	1.54	0.71		-0.67	1.9	-1.a	2.71	0.0	-0.55	0.85	-0.52	0.47	0.0	0.68	1.90	1.43	3.15	0.19
		K	2.58	0.73	1.54	0.48		-0.79	1.03	-1.42	1.13	0.0	0.37	0.73	-0.52	0.24	0.00	0.56	1.05	1.00	1.57	0.19
									Ve	rtical 1	Vertical Deflection,		in. at Indicated Gages	ted Gage	8							
			6			-	10201										Rebound					
			1 L	2	m	o ^a	4	9	D2	80	್ಷ		art.	20		คื	3	90	$L_{\rm Q}$	80	o	
#	н	M	0.032	0.062	0.059	0.012	0.006	0.073	0.096	0.017	0.010		0.055	090.0	0.054	0.010	0.00	0.068	0.089	0.012	0.00	
		(b.,	0.025	0.054	0.093	0.020	0.024	0.062	0.108	0.027	0.328		0.048	0.052	0.088	0.018	0.043	0.057	0.10	0.00	0.047	
		U	0.013	0.037	0.121	0.028	0.030	0.044	0.119	0.035	0.058		0.036	0.035	0.126		0.049	0.039	0.112	0.030	0.077	
		æ	0.003	0.024	0.LL	0.033	0.045	0.030	0.105	0.00	0.099		0.006	0.022	0.106	0.031	0.06	0.0	0.095	0.035	0.118	
		ы	-0.005	0.015	0.060	0.036	990.0	0.018	0.062	0.041	0.123		0.018	0.013	0.055	0.034	0.085	0.013	0.055	0.036	0.142	
		43	-0.009	0.00	0.034	0.033	0.098	0.01	0.037	0.036	0.145		0.01	0.007	0.029	0.031	0.117	9000	0.030	0.031	0.16	
		×	-0.010 0.007 0.021 0.025 0.142	0.007	0.021	0.005	0.142	0.008	0.023	0.028	0.159		0.013	0.005	0.016	0.023	0.161	0.003	0.016	0.003	0.178	
		×	-0.011	0.00	0000	0.01	0.048	0.00	0.00	0.013	0.067		0.02	0.00	00.0	0000	0.067	0000	0.00	0.00	0.066	

(Continued)

Table A-13
Multiple-Wheel Heavy Gear Load Flexible Pavement Test, Static Instrumentation Loading Data
Item 4; Load Condition: 30 kips per Wheel, 6 Wheels, 100 psi

1		1						Total	7		24		tel treesing there has	at indicated Cell	וכבי רבו ר	6118		Debound	7				
7.91 10.45 5.7^{4} 6.35 1.09 8.48 3.01 4.22 1.7^{4} 0.00 7.52 11.54 0.39 0.48 0.31 0.31 0.31 0.39 0.39 0.31 0.39 0	Row	Point	tion	4 A	۳.		a. 1	2	9	P7	PB	20	P10	27	4	a,**		24	94	74	PB	a o	P ₂ or
7.63 10.34 6.94 10.07 0.00 8.71 4.01 5.17 3.69 0.00 7.34 11.43 5.82 14.27 7.65 11.54 -0.18 6.99 6.41 6.93 5.02 0.00 5.53 15.36 3.82 6.75 7.65 12.51 -36.42 4.82 3.91 6.12 6.66 0.00 3.53 15.36 1.28 -0.22 5.28 8.21 0.00 1.97 0.00 1.97 0.00 1.97 0.00 1.97 0.00 1.97 0.00 0.97 0.00 0.97 0.00 1.97 0.00 1.97 0.00 1.97 0.00 1.97 0.00 0.97 0.00 0.97 0.00 0.97 0.00 0.97 0.00 0.97 0.00 0.97 0.00 0.97 0.00 0.97 0.00 0.00		1 % 2	(a)	0.0	7.9	10.45	5.7	6.35	1.09	8.48	3.8	22.	1.7	0.00	7.62	11.54	5.3	2.8	1.09	8.6	3.41	8:	1.6
5.8e 14.27 7.65 11.54 -0.18 6.99 6.41 6.03 5.02 0.00 5.53 15.36 3.8e 6.77 7.65 12.51 -36.42 4.8e 3.9g 6.12 6.66 0.00 3.53 7.8h 2.29 1.52 6.70 13.10 0.00 1.9g 0.00 1.4h 6.66 0.00 2.61 1.24 -0.22 5.26 8.2g 0.00 1.37 -0.40 3.4h 6.66 0.00 2.61 0.86 -0.88 3.83 4.10 0.00 1.37 -0.40 3.4h 3.28 0.00 2.61 0.86 -0.89 3.83 4.10 0.00 0.37 -0.40 3.4h 3.28 0.00 2.61 0.86 -0.89 3.83 4.10 0.00 0.37 -0.40 3.4h 3.28 0.00 2.61 0.84 -1.09 1.32 0.00 0.36 0.40 0.0			fin,	0.0	7.63	10.34	\$.9	10.01	00.0	8.71	10-1	5.27	3.69	0000	7.34	11.43	94.9	89.6	00.0	8.3	17.7	2.00	3.59
3.82 6.75 7.65 12.51 -36.42 4.82 3.94 6.12 6.66 0.00 3.53 7.84 2.29 1.52 6.70 13.10 0.00 3.24 1.01 5.60 8.71 0.00 2.00 2.61 1.24 -0.22 5.26 8.21 0.00 1.37 -0.40 3.45 3.28 0.00 0.57 -0.21 0.08 3.83 4.10 0.00 1.37 -0.40 3.45 3.28 0.00 0.57 -0.21 0.08 1.91 0.00 1.37 -0.40 3.45 3.28 0.00 0.57 -0.21 0.08 0.08 0.09 0.09 0.09 0.09 0.09 0.09			O	0.0	5.85	14.27	7.65	1.54 1.54	-0.18	6.9	6.41	6.03	5.00	0.0	5.53	15.36	7.17	11.15	-0.18	6.53	6.8	5.86	8
2.29 1.52 6.70 13.10 0.00 3.21 1.01 5.60 8.71 0.00 2.61 1.24 0.02 5.26 8.21 0.00 1.97 0.00 1.48 6.66 0.00 0.99 0.97 0.97 0.86 0.89 3.83 4.10 0.00 1.37 0.040 3.45 3.28 0.00 0.57 0.21 0.48 1.09 1.91 0.00 1.37 0.040 3.45 3.28 0.00 0.57 0.21 0.00 0.44 0.012 0.00 0.97 0.00 0.99 0.00 0.99 0.00 0.00			Ħ	0.0	3.85	6.75	2.65	15.51	-36.42	4.82	3.9	6.12	99.9	0.0	3.53	7.84	7.17	12.12	-36.42	4.36	4.31	8.8	6.56
1.24 -0.22 5.26 8.21 0.00 1.95 0.00 1,18 6.66 0.00 0.95 0.87 0.87 0.86 0.86 0.89 3.83 4.10 0.00 1.37 0.040 3.45 3.28 0.00 0.57 0.21 0.42 0.48 1.03 1.91 0.07 0.00 0.92 0.050 1.72 0.72 0.00 0.57 0.21 0.00 0.44 0.012 0.00 0.00 0.00 0.00 0.00 0.00 0.0			н	0.0	5.29	1.52	6.70	13.10	0.0	3.8	1.01	2.60	8.7	0.0	8.8	2.61	6.22	12.51	0.00	2.3	1.4.1	5.43	8.6
0.86 -0.88 3.83 4.10 0.00 1.37 -0.40 3.45 3.28 0.00 0.57 +0.21 0.48 -1.09 1.91 0.07 0.09 0.57 -0.50 1.72 0.72 0.00 0.19 0.00 0.48 -1.09 1.91 0.07 0.00 0.92 -0.50 1.72 0.72 0.00 0.19 0.00 0.044 0.012 0.012 0.003 0.002 0.003 0.000 0.004 0.003 0.002 0.003 0.000 0.004 0.003 0.004 0.007	4	н	י	0.00	1.2	-0.22	5.26	8.2	0.00	1.9	0.0	84.4	99.9	0.0	0.95	+0.87	1.78	7.32	00.0	1.49	0.10	#:·	6.56
0.148 -1.09 1.91 0.97 0.00 0.92 -0.50 1.72 0.72 0.00 0.19 0.00 Description Perfection Perfection Inc. at Indicated Gages Perfection Indicated Gages Perfection Inc. at Indicated Gages Perfection Indicated Gages Perfection Indicated Gages Perfection Indicated Gages Perfection Indicated Gages Perfection Indicated Gages Perfection Indicated Gages Perfection Indicated Gages Perfection Perfection Indicated Gages Perfection	-B	1 & 2	×	0.0	98.0	-0.88	3.83	4.10	0.00	1.37	-0.40	3.45	3.28	0.00	0.57	a. ♀	3.35	3.72	0.00	6.0	8.0	8	77.6
D ₂ D ₃ D ₄ D ₅ D ₆ D ₇ D ₈ D ₉ D ₉ D ₁ D ₁ D ₂ D ₃ -	н	×	0.0	84.0	-1.09	1.92	0.97	0.0	0.92	-0.50	1.72	0.72	00.0	0.19	0.0	1.43	0.58	0.0	91.0	-0.10	1.55	0.6	
D2 D3 D4 Total D7 D8 D9 D1 D2 D3 0.034 0.032 0.033 0.002 0.003 0.002 0.003 0.002 0.003 0.002 0.003 0.002 0.003 0.002 0.003 0.002 0.003 0.002 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>Ve</td> <td>rtical D</td> <td>eflection</td> <td>n. in</td> <td>LIndica</td> <td>Ped Gage</td> <td>u</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>										Ve	rtical D	eflection	n. in	LIndica	Ped Gage	u							
D2 D3 D4 D5 D6 D7 D8 D9 D1 D2 D3 0.034 0.032 0.002 0.003 0.002 0.003 0.000 0.003 0.002 0.003 0.000 0.003 0.002 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004								Total								Ш		Febound					
0.032 -0.004 0.012 0.003 0.002 0.003 0.000 0.003 0.002 0.003 0.002 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.003				L ₁	D2	Eq.	ď	DS	90	2	Ва	ဝိ		D	20	Da	⁷ C	ďζ	26	DZ	BB	0	
0.032 -0.004 0.017 0.006 0.000 0.004 0.000 0.004 0.006 0.008 0.008 -0.003 0.004 0.007 0.004 0.007 0.004 0.007 0.004 0.007 0.005 0.004 0.007 0.005 0.004 0.007 0.005 0.004 0.007 0.005 0.004 0.007 0.005 0.004 0.007 0.005 0.007 0.005 0.007 0.005 0.007 0.005 0.007 0.00		1 \$ 2	ы	0.008	0.044	0.012	0.000	0.003		0.303		0.003		0.021	960.0	0.013	0.089	0.015	0.00	0.003	0.000	0.003	
0.012 0.016 0.026 0.013 -0.003 0.004 0.000 0.005 0.042 0.054 0.017 0.006 0.017 0.006 0.017 0.006 0.017 0.006 0.017 0.006 0.017 0.012 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.007 0.005			jk ₄		0.032	100.0-		9000		0.00		0.00		0.028	0.08	-0.003	0.036	0.018	0.008	0.00	0000	0.00	
-0.006 0.014 0.039 0.021 -0.006 0.004 0.000 0.007 0.006 0.046 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.005 0.006 0.009 0.00			O	0.029	0.012	0.016			•	0.00		0.005		0.042	0.06	0.07	0.045	0.00	40.00	0.00	0.000	0.00	
-0.018 0.010 0.051 0.031 -0.006 0.003 0.000 0.008 0.079 0.094 0.011 -0.025 0.007 0.031 0.032 0.005 0.009 0.003 0.005 0.005 0.009 0.001 0.005 0.007 0.0			Ħ	0.047	-0.006	0.01			•	0.004	0000	0.007		0.060	0.046	0.015	0.058	0.033	+0.002		0000	0.007	
-0.025 0.006 0.040 0.045 -0.004 0.003 0.000 0.009 0.111 -0.025 0.007 0.025 0.007 0.025 0.007 0.025 0.007 0.025 0.007 0.0			н	990.0	-0.018	0.00			•	0.003	0000	0.008		6.00	0.034	0.01	0.070	0.043	40.002	0.003	00000	90000	
0.029 0.003 0.023 0.052 0.001 0.004 0.000 0.008 0.068 -0.029 0.004	п	r 4	5	0.098	-0.025	0.006			•	0.003	0.000	0.00		नः ॰	-0.025	0.007	0.059	0.057	+0.00t		0000	0.00	
0.031 0.001 0.000 0.000 0.000 0.000 0.000	4 3	1 & 2	×		0.00	0.003				0.00	0000	0.008		0.068	-0.029	0.00	0.042	0.064	0.009	0.00	00000	0.008	
2000 2000 0.003 0.003 0.003 0.003 0.003	н	П	×	0.00	0.031	0.001			0.005	0.003	0.00	0.003		0.083	0.02	0.002	0.00	0.037	0.013	0.003	0000	0.003	

Table A-14Continued

						100 000				Vert	cal Pres	soure, pe	1. of Inc	icated C	1							
	-	Tanna .					101	1									Rebo	und				
8	Poten	tion	4	P2	4	4	2	P6	7	88	۳.	a Pa	<u>م</u> ر	42	4	4.3	24	4	4	88	20	22
1,3,5	2,1,2		17.98	-7-53	14.81		5.87	28.77	9.63	6.2	3.26	3.59	+27.43	48.15	11.65	6.10	5.58	33.51	10.09	-16.42	5.51	8.4
			0.30		15.68			0.36	9.41	6.51	6.38	94.9	+0.52	4.96	12.52	2.06	9.39	5.10	18.6	-16.12	6.63	6.87
		B	-0.20		74.00	7.17		96.0	7.23	8.01	7.24	8.30	+0.52	+6.15	3.3	7.89	11.06	5.10	7.69	-14.62	7.49	8.7
		H	-0.20		12.85			0.36	4.82	4.7	7.34	8.9	+0.52	4.15	69.6	7.78	12.62	7.10	5.28	-17.92	7.49	9.33
		н	-0.20		5.0			0.36	2.87	1.7	6.46	10.05	+0.52	+2.53	1.85	6.82	14.19	5.10	3.33	-20.92	6.71	34.01
	2 4 2	5	0.30		3.05			0.36	1.72	1.91	5.17	6.87	+0.52	1.58	-0.11	5.50	8.7	5.10	2.18	-20.72	5.42	7.28
	2,1,2	16	-0.60		1.96			8.4	94.0	2.53	3.62	3.18	+0.12	+0.53	-1.20	3.59	3.92	-0.18	0.98	-1.10	3.87	3.59
1.65	2 4 2	*	-0.60	-0.47	1.74			7.35	7.0	21.43	1.38	0.11	+0.12	+0.15	-1.42	1.55	0.30	-0.18	6.3	-1.20	1.63	0.52
									S	of feel B	of fact (5	of Indian	tod George							1	
							Total										Rebound				1	
			4	D2	4	ď	2	90	70	80	6		ď	22	4	ď	25	90	건	80	2	
1,3,5	2,1,2		0.01						0.006	0000	-0.002		-0.104		100		-0.009		0.005	00000	0.008	
			0.086						0.007	0.000	0.00		-0.089			0.006	0.001		9000	00000	0.0	
		v	0.056						0.008	0.000	0.004		-0.059			0.048	0.00		0.007	0.000	0.0g	
			0.19	o.H	0.031	0.111	0.058	-0.007	0.00	0.000	0.009		0.076		0.028	0.08	0.040	40.000	0.00	0.000	0.00	
		н	0.226					•	0.00	0.000	o.al		0.111			0.131	0.066		0.008	0.000	0.004	
	2 6 2	7	0.226					•	0.007	0.000	0.a6		9.11			0.110	0.093	•	0.006	0.000	0.006	
	2,1,2	×	0.303						0.007	0.000	0.016		0.188			0.073	0.113		0.006	00000	0.006	
145	2 4 2	R	0.181					•	0.00	0.000	0.004		0.066	0.007	0.003	0.005	0.060		0.003	00000	0.01	

						100		The state of the state of		Vert	cal Pres	sure, ps.	1, at Ind	Cated C	2113							1
ľ	100	Local	1	-			2	133		01 15 M K 2	7 25 25 5						Rebo	pun				
ıls	Polat	tion	,,	2	4	2	4	29	77	88	29	P10	4-1	72	a.	a.	P5	20	4	PB	۵,	910
9	162	м	1.8	6.67	3.70	4.42	4.42 3.43		9.86	3.60	5.51	3.59	2.41	7.43	6.43	5.38	1.2	4.74	10.55	-13.22	5.69	1.7
		•	0.00	98.9	∄ .¤	5.50	5.97		69.63	3.00	6.80	7.07	09.0	7.62	14.17	6.34	6.75	5.10	10.32	-13.92	8.98	8.29
		0	0.0	5.15	25.22	6.22	7.63		4.7	3.8	7.58	8.40	09.0	8.8	8.8	7.06	8.41	5.10	8.03	-13.00	7.76	9.52
		Ħ	0.0	3.24	69.6	2.8	10.08	-5.47	4.12	21.82	7.15	8.40	09.0	8.4	12.42	6.82	10.86	0.0	4.8	8.4	7.33	9.52
		н	-0.60	1.14	0.2	99.1	12.91		1.95	18.12	6.28	9.22	0.00	1.90	2.8	5.50	13.69	0.00	2.6	1.8	91.9	10.34
	-	7	-0.40	0.19	-1.53	3.35	7.63		0.68	17.62	4.9	5.6	•0.20	8.0	41.20	4.19	8.41	0.0	1.37	0.70	5.00	6.76
		×	-0.40	-0.19	-1.8	2.15	2.9		0.0	17.12	3.14	5.03	40.20	-0.57	12.0+	2.99	3.72	0.00	0.69	0.30	3.62	3.17
		×	0.40	-0.57	-6.40 -0.57 -2.18	94.0	-0.09		-0.58	16.92	1.29	-0.51	40.20	0.19	+0.55	1.32	69.0-	0.00	₩.0	0.0	1.47	19.0
									4	1											1	
							Total			1	ארו דפוני וידור	2 TH. 5	at Indica	200			De la constant				1	
			ď	2	ď	ದೆ	ą,	90	27	D8	9		I _Q	D2	-F	ď	2	90	74	B _C	60	
9	1 & 2	54	0.00	0.203	0.04	0.060	0.016				0.00		6.379	0.305	0.038	0.031	2.00 t	0.086		0.000	0.00	
			0.00	0.150	0.051	0.105	0.105 0.032	0.045	0.0	0000	0.006		0.095	0.149	0.045	0.076	0.002	0.07	0.013	0.000	0.00	
		o	0.049	0.103	0.053	0.131	0.062			0.000			611.0	0.102	0.047	0.100	0.032	0.054		0000	0.01	
		m	0.074	990.0	0.048	0.16	0.09						0.143	0.065	0.042	0.135	630.0	0.039		0.000	3.027	
		н	0.098	0.038	0.035	0.200	0.135						191.0	0.037	0.029	0.177	0.105	0.027		0.000	0.039	
	н	ר	0.116	0.00	0.024	0.172	0.161	•					0.185	0.00	0.018	0.143	0.131	€0.022		0.00	0.051	
		×	0.119	0.016	0.016	0.113	0.176						0.188	0.005	0.00	0.084	941.0	€0.339		0.00	0.057	
		×	0.00	0.0	0.00	0.054	0.103	2					0.093	0.000	0.003	0.00	0.073	+0.016		0.000	0.031	

Continued)

		-								Vertic	Pres	sure, ps.	psi, at Indicated Celli	dested C	ells							
2	3	1					Total		Marie S								Behy	Praise				1
2	開	8	4	4	4	2	P6	!	74	8	م	or L	4.4	20	4	4	25	P6	P	Pe	8	or a
	-	M 0.0	0.00 4.6	7 2.5					_	1.61	4.82	3.08	0.0	5.15	3.15	74.0	2.2	87.78	9.40	3.80	1.65	2.67
		.0		6.2				0.9E		7.7	6.20	95.9	0.00	5.E	6.85	4.19	3.13	0.37	9.63	8.4	6.03	6.15
		0 0		12.5					1	0.8r	6.80	8.20	00.0	1.18	13.18	79.4	0.59	0.19	7.56	7.10	6.72	7.70
		H 0.1		8. 5.4						1.1	7.06	9.63	00.00	2.96	6.10	99.4	7.63	0.19	4.58	3.40	6.80	0.20
		I 0.1		3 1.6						3.51	6.39	71.17	8.0	1.8	2.28	4.19	86.6	0.0	2.7	-0.30	6.12	10.76
		J. 0.1		7 0.2						2.30	8.4	8.20	0.81	1.05	0.87	3.35	6.85	-0.18	1.37	-1.41	4.8	7.70
		M 0.0		0.29 -0.22	2 2.15	5 2.84				1.90	3.62	3.8	0.00	0.77	0.43	2.39	3.33	-0.18	99.0	E	3.45	3.49
					-				Ver	1			100									
						Tot	-1				-	1	1	100			Eshoumed				1	
		a l	P. 1	P3	d ³	a ^c	9	9	2	80	20		ar a	25	er Pa	ď	4	100	70	P _B	60	
		E 0.0	a7 0.2	0.a7 0.273 0.052 0.075 0.a8	52 0.0	75 0.0	18 0.		0.022	0000	0.00		-0.130	0.193	0.0		-0.027	0.167	0.017	0.000	-0.013	
		F 0.0	331 0.2	16 0.0	1.0 13	13 O.C	38 0.	0.183 0		00000	0.017		-0.116	0.136	0.03	0.106	-0.007	0.121	0.02	0000	100.0	
		0.0	258 0.1	64 0.0	53 O.I	74 0.0	75 0.		0.028	00000	0.031		-0.089	0.084	0.055		0.030	0.080	0.023	0.000	0.00	
		H 0.5	229 0.1	19 0.0	55 0.3	m 0.1	33 0.			0.000	0.055		0.072	0.039	0.047		0.088	0.044	0.023	00.00	0.034	
		I 0.	253 0.0	0.0 99	12 0.2	26 0.1	51 0.			00000	0.076		0.106	0.02	0.034		917.0	0.00	0.018	0000	0.05	
		J 0.1	26 0.0	72 0.0	28 0.1	20 0.11	0 98			00000	0.100		0.109	-0.008	0.000		0.141	0.012	0.012	0.000	0.081	
		K 0	0.0	62 0.00	18 0.15	77 0.1	0 4			0.00	STI. O		0	400	Owo				1			

										Ver*1	cal Pres	sure, ps	L at Ind	icated C	ells							
	Poor	Local	-				10	193		Total Carlette		Section Section 2		400	THE PARTY	120 November 21	Rebo	und	0.0000			
Box	Polut	tton	4	4	ard Ma	a. T	2	9	P7	8	Pg	P10	P	72	P3	ď	3	9	P7	88	0	S
64	1.62	ы	0.20	3.05	9.65	2.15	62.2	69.68+	8.00	0.30	3.96	1.95	0.20	3.43	2.29	2.39	1.76	-40.42	8.37	2.14	1.2	2.3
			0.0	3.05	1.08	2.73		-0.37	8.37	3.40	5.17	3.80	0.0	3.43	2.72	2.99	2.35	•0.36	8.72	5.01	5.43	4.10
		o	0.00	2.48	1.30	3.11		-0.37	69.9	7.41	* 5	5.23	00.0	2.86	2.94	3.35	3-13	40.36	7.00	8.06	6.20	5.53
		Ħ	0.00	1.62	10.32	3.11		-0.37	4.12	3.60	6.03	69.2	0.00	5.00	1.96	3.35	17.7	+0.36	1.47	5.2	6.39	7.99
		н	0.0	0.98	11.0-	2.2		-0.55	5.29	-0.30	5.34	10.56	0.0	1.33	1.20	2.99	4.50	-0.18	2.64	17.71	5.60	10.86
1	п	,	0.0	0.38	-0.99	2.15		-0.37	1.03	-1.31	4.13	2.48	00.00	0.76	9.0	2.39	3.13	96.0	1.38	+0.30	4.39	7.78
6 .	1 6 2	×	0.00	61.0	-1.30	1.55		-0.37	0.45	1.1-	3.01	3.59	0.00	0.57	44.0	1.79	1.76	96.04	0.80	-0.10	3.27	36.5
							Total			1 222	מיזיבר רדים	The Alles	TO THE PERSON	ובים הפנים			Rebound				1	
			12	D2	2	ď	2	90	70	80	0		ar ar	22	E 23	a ²	25	90	72	د .	20	
6.9	162	84	0.00	0.002 0.179 0	0.058	0.00	0.016		0.032	0.000	0.01		0.059	0.230	0.052	0.063	-0.002	0.208	0.029	00000	-0.012	
			0.014	0.125	0.068				0.038	0.000	0.033		0.07	0.176	0.062	0.135	0.023	0.156	0.035	0.000	0.007	
		o	0.030	0.07	0.000				0.039	0.000	0.000		0.087	0.122	0.00	0.166	0.062	0.108	960.0	00000	0.034	
		H	0.055	0.023	0.000				0.035	00000	0.101		0.112	0.07	0.054	0.194	0.118	0.062	0.332	0.000	0.075	
		н	0.076	-0.006	0.045			0.040	0.029	00000	0.129		0.133	0.045	0.039	0.218	0.151	0.035	0.006	00000	0.103	
	-	יי	0.106	-0.023	0.029				0.021	00000	0.153		0.163	0.028	0.023	0.177	0.174	0.02	0.018	0.000	0.127	
6 4	1.6.2	×	0.177	-0.033	0.00				0.00	00000	0.19		0.234	0.018	0.013	0.113	0.181	0.03	0.03	00000	0.105	
-	н	×	0.049	-0.038	0.00				0.007	00000	0.102		0.106	+0.013	0.00	0.039	0.097	900.0	0.00	00000	0.376	

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esta vente la pr

7.9,11 2,1,2 E 0.00 1.62 0.54 1.44 7.9,11 2,1,2 E 0.00 1.62 0.55 1.67 7.11 2 & 2 J 0.00 0.36 0.43 1.67 7.11 2 & 2 J 0.00 0.39 0.21 0.96 7.9,11 2,1,2 K 0.00 0.39 0.10 0.72 7.9,11 2,1,2 E 0.001 0.327 0.054 0.070 7.9,11 2,1,2 E 0.001 0.327 0.056 0.195 7.9,11 2,1,2 E 0.008 0.25 0.065 0.146 7.9,11 2,1,2 K 0.098 0.134 0.059 0.227 7.9,11 2,1,2 K 0.098 0.134 0.059 0.227 7.9,11 2,1,2 K 0.098 0.134 0.059 0.227 7.9,11 2,1,2 K 0.035 0.106 0.054 7.9,11 2,1,2 K 0.035 0.106 0.054 7.9,11 2,1,2 K 0.135 0.065 0.140					Total		Vert	TCST LLCS	sure, ps.	vertical Pressure, psi, at indicated Celli	Toured o	2112							
24,2 E 0.00 1.62 0.55 5 0.00 1.62 0.65 8 0.00 1.24 0.65 24,2 J 0.00 0.36 0.23 24,2 M 0.00 0.39 0.22 21,2 E 0.001 0.327 0.05 5 0.00 0.39 0.10 24,2 M 0.00 0.39 0.00 24,2 J 0.00 0.30 0.05 24,2 M 0.00 0.30 0.00 24,2 J 0.00 0.00 24,2 J 0.00 0.00 24,2 J 0.00 0.00 24,2 J 0.00 0.00 24,2 J 0.00 0.00 25,2 J 0.00 26,2 0.07 26,2 0.07 26,2 0.07 26,0 0.00	4 1	2	4	3	94	P	80	6	710	4	2	4	4	P S	9.	2	89	0,0	20
2 & 2 & 2 & 0.00 1.24 0.65 G 0.00 1.24 0.65 H 0.00 0.36 0.43 2 & 2 J 0.00 0.39 0.21 2 & 2 J 0.00 0.39 0.22 2 & 2 J 0.00 0.39 0.24 0.059 2 & 2 J 0.00 0.39 0.11 0.045 2 & 2 J 0.00 0.35 0.05 0.00 2 & 2 J 0.00 0.00 0.00 0.00 0.00 2 & 2 J 0.00 0.00 0.00 0.00 0.00 0.00 0		62 0.	54 1.1	प ० च				3.0	1.03	0.0	1.7	0.33	7.1	0.40	0.36	6.65	3.41	3.4	1.1
2 & 2 & 3 & 0.00 1.24 0.65 H 0.00 0.86 0.43 2 & 2 J 0.00 0.39 0.21 2 & 2 J 0.00 0.39 0.21 2 & 2 J 0.00 0.39 0.21 2 & 2 J 0.00 0.39 0.20 2 & 2 J 0.00 0.39 0.00 1 0.00 0.30 0.30 0.00 2 & 2 J 0.00 0.30 0.34 2 & 2 J 0.00 0.37 0.05 2 & 2 J 0.00 0.37 0.05 2 & 2 J 0.00 0.37 0.05 2 & 2 J 0.00 0.37 0.05 2 & 2 J 0.00 0.00 3 & 0.00 0.00 3 & 0.00 0.00 4 & 0.00 0.00 5 & 0.		62 0.	65 1.4	57 0.5		6.19	3.31	3.79	1.85	0.00	1.7	44.0	1.67	0.59	00.00	6.88	5.2	4.20	2.26
2 & 2 J 0.00 0.96 0.43 2 & 2 J 0.00 0.57 0.21 2 & 2 J 0.00 0.39 0.21 2 & 2 J 0.00 0.39 0.21 2 & 2 J 0.00 0.39 0.20 2 & 2 J 0.00 0.39 0.20 2 & 2 J 0.00 0.39 0.250 0.05 3 0.00 0.250 0.05 4 0.00 0.250 0.05 5 0.00 0.39 0.34 0.05 5 0.00 0.39 0.34 0.05 5 0.00 0.33 0.06 5 0.00 0.03 0.03 5 2 & 2 J 0.06 6 0.05 0.07 7 0.06 7		3t 0.	55 1.	T.0 12		18.4 8	2.8	4.39	2.87	00.00	1.33	44.0	1.91	0.79	€0.00	5.50	6.9	4.82	3.28
2 & 2 & 3 0.00 0.57 0.21 2 & 2 & 2 & 3 0.00 0.38 0.21 2 & 2 & 2 & 3 0.00 0.38 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.1		96 0.	43 1.4	6.0 75	8 0.36	5.98	1.91	4.39	5.13	00.00	8.0	0.22	1.67	0.98	0.18	3.67	2.81	4.82	5.54
2 & 2		57 0.	2 1.4	8.0 75	8 0.36		0.10	2.9	7.07	00.0	99.0	0.0	1.67	0.88	0.18	2.41	2.00	1.148	7.148
242 N 0.00 0.29 0.21 242 N 0.00 0.38 0.10 21,2 E 0.001 0.327 0.05 7 0.008 0.250 0.06 6 0.020 0.183 0.06 1 0.059 0.111 0.045 242 J 0.084 0.095 0.009 245 J 0.062 0.079 0.008		38 0.	2 1.	32 0.5	9 0.36	0.80	-0.60	3.18	26.1	00.00	0.47	8.0	1.32	0.59	0.18	1.49	2.50	3.61	5.33
2.1,2 E 0.001 0.327 0.054 2,1,2 E 0.001 0.327 0.054 7 0.008 0.250 0.065 6 0.020 0.183 0.066 H 0.039 0.113 0.045 2.1,2 K 0.135 0.065 0.009		29 0.	2 O.	36 0.2	0 0.36	4E.0 3	-0.90	2.15	2.38	0.0	0.38	0.0	96.0	0.20	0.18	1.03	2.80	2.58	2.67
2,1,2 E 0.001 0.327 0.054 F 0.008 0.250 0.055 G 0.020 0.183 0.068 H 0.038 0.134 0.059 I 0.059 0.111 0.045 2,1,2 K 0.135 0.055 0.008		38 0.	10 0.	72 0.00	0 0.36	ď	-1.30	6.0	0.31	0.0	74.0	-0-11	0.72	0.00	0.18	69.0	3.10	1.37	0.72
2,1,2 E 0.001 0.327 0.054 F 0.008 0.250 0.065 G 0.020 0.183 0.068 H 0.038 0.134 0.059 2,1,2 K 0.135 0.065 0.038 2,1,2 K 0.135 0.065 0.008																			
2,1,2 E 0.001 0.327 0.054 F 0.008 0.250 0.065 G 0.020 0.183 0.068 H 0.038 0.134 0.059 2,1,2 K 0.135 0.085 0.038 2,5,2 M 0.062 0.079 0.008				-			Vertice	Der Pectio	n, in.	at Indicated Gages	ted Gage	60							
2,1,2 E 0.001 0.327 0.054 2,1,2 E 0.000 0.327 0.054 G 0.020 0.139 0.059 H 0.039 0.134 0.059 2,8,2 J 0.084 0.095 0.029 2,1,2 K 0.135 0.065 0.018		ľ	1	135	7	١								Repoun!					
2,1,2 E 0.001 0.327 0.054 F 0.006 0.250 0.065 G 0.020 0.183 0.068 H 0.039 0.134 0.059 I 0.059 0.111 0.045 2,1,2 K 0.135 0.055 0.038 2,1,2 K 0.135 0.055 0.038	2	2	3	7	99	22	8	D _Q		ដ	D2	E D	70	25	D6.	L _Q	P ₈	o _Q	
7 0.006 0.250 0.065 G 0.020 0.183 0.068 H 0.039 0.134 0.059 I 0.059 0.111 0.045 23.2 J 0.084 0.095 0.029 23.2 K 0.135 0.095 0.008		327 0.		070 0.015	15 0.280	30 0.041	0000	0.018		+0.011	0.228	0.049	0.031	-0.018	0.20	0.036	0.000	-0.012	
2 6 0.020 0.183 0.068 H 0.038 0.134 0.059 2 8 2 J 0.084 0.095 0.029 2 4 2 J 0.084 0.095 0.029 2 4 2 2 M 0.062 0.079 0.008		250 0.		0.0	34 0.216	200 9	0000	0.042		0. ULB	0.151	090.0	0.107	0.001	0.146	0.0.2	00000	0.012	
1 0.039 0.134 0.059 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 &		183 0.		133 C.O		56 0.047	00000	180.0		0.030	0.084	0.063	0.144	0.042	0.086	0.042	0000	0.054	
2 & 2 & 3 & 0.084 0.095 0.029 2.1,2 K 0.135 0.085 0.029 2.1,2 K 0.135 0.085 0.018		134 0.		227 0.1	30 0.110	0.042	00000	0.132		0.048	0.035	0.054	0.188	0.097	0.000	0.037	0.000	0.102	
2 & 2 3 0.084 0.095 0.029 2,1,2 K 0.135 0.085 0.018 2 & 2 M 0.062 0.079 0.008		n 0.		261 0.1	-	5 0.034	00000	0.156		0.00	0.012		0.222	0.126	0.00	0.029	0.0	921	
2,1,2 K 0.135 0.085 0.018		000		25 0.1	890.0 68	38 0.025	00000	0.177		0.094	-0.004	0.024	0.176	0,156	-0.002	0.020	0.0	1117	
2 5 2 N 0.062 0.079 0.008		0 (a)		140 0.2		8 0.018		0.180		0.145	0.014	0.013	0.101	0.170	-0.012	0.03	0.000	0.150	
		000		750 0.1	19 0.051	0.008	0000	0.109		0.072	-0.020	0.003	0.025	0.086	-0.00	0.003	00000	0.079	

Table A13 (Concluded)

										Ver	Vertical Pressure		Ed. at Indicated Celli	dicated	Cella						-	1
	2						To	tal				4					Reband	Pon				
Pov	Potnt	tron	4	o, C)	a.m	a ¹	5	9	P7	P _B	67	P10	ard a	2	4"	A.T	2	P _C	P7	PB	90	2
я	H	fall	8.0	1.24	2.29		0.79	-0.18	3.67	0.10	2.15	0.41	0.0	8.0	80.0	9.0	0.10	-0.18	36.4	2,10	2.41	8
		βų	0.00	1.15	2.51		0.96	00.0	3.67	0.50	2.67	1.00	0.00	98.0	8	96.0	0.50	80.0	9	2.50	8	1.43
		o	0.00	96.0	2.51		0.98	0.00	2.8	0.20	3.00	1.43	0.00	29.0	0.23	8	0.30	8.0	3.67	8	2.3	1
		br;	0.0	0.86	5.29	1.08	1.08	80.0	2.8	-0.60	3.8	2.15	0.00	0.57	0.00	٥. ٢٠	0.39	8.0	2.73	1.60	98	2.56
		н	0.00	29.0	2.01		96.0	c.18	1.03	-1.30	2.67	2.56	0.0	0.38	-0.82	8.0	8	0.18	1.72	0.80	8	6
		ט	0.00	19.0	1.75		62.0	0.00	94.0	-1.40	2.2	1.9	0.00	0.38	-0.54	0.72	0.10	0.0	1.15	0,60	2,50	
		×	0.0	0.77	1.64		69.0	8	0.23	-1.60	1.64	8.0	00.00	0.48	-0.65	0.72	0.0	00.0	8	0.40	8.1	3 2
									-	Vertical	Serlecti	Serlection, in. at Indicated Gages	at Indica	ated Gag	6.8						1	
				-			Total										Rebound	4				
			24	2	2	70	5	99	7	Ba	6		ď	25	e G	ล้	2	90	₂	80	0	
ជ	-	េ	-0.006	0.206	0.041	0.037	0.00	0.185	0.043	0000	0.016		10.0	0.237	0.000	0.03	-0.008	0.20	0.038	0.00	20.00	
		Bra	-0.001	0.129	0.051	0.072	0.02	0.130	0.048	0.00	0.042		610.0+	0,160	0.00	6.058	0.007	0.165	0.043	0		
		U	0.00	0.07	0.055	0.104	0.065	0.074	0.04	0.00	0.088		0.00	6.100	0.05	0.090	0.03	0.100	0.013	0.00	0.087	
		þri	0.012	0.035	0.048	0.147	0.074	0.036	0.0	0.00	0.125		0.032	990.0	0.047	0.133	0.000	0.0	0.038	000	0.00	
		н	120.0	0.027 0.010 0.034 0.208 0.	0.034	0.208	0.107	0.00	0.03	0.000	0.137		0.047	0.041	0.033	0.19	0.093	0.039	0.00	0000	2,106	
		ы	0.040	-0.005	0.020	0.168	0.142	-0.02 t	0.02	0.000	0.179		0.050	÷0.026	0.039	0.154	0.128	0.0	0.00	0.00	0.148	
		×	0.049	0.00	7000	0.11:	0.16	-0.052	0.017	0.00	0.183		0.000	0.00	0.013	0.00	0.150	8 0	6	8	0 36 0	

Table A-14
Multiple-sheet Heavy Gear Load Flexible Pavement Test, Static Instrumentation Loading Data
Item 3; Load Condition: 30 kips per Sheel, 12 Sheels, 100 psi

	91	21:1	1.12	1.22	1.12	1.12	1.12	1.12	\$.0	95.0	0.26	0.75	.0.33	-0.19	0.00																
	۵	0.35	62.0	1.57	2.10	2.62	3.76	8.3	8.5	95.9	6.64	5.77	5.07	94.4	3.67		D	0	0.000	90.00	0.00	0.005	-0.00e	-0.002	00000	0.001	0.003	0.00%	0.0C5	0.00	2.00%
	8	1.12	1:8	1.53	1.73	2.04	3.36	2.85	1.38	6.92	3.87	1.00	0.30	0.30	0.43		200	o	0.000	•		•	•	•			5.003				
	P7									77.00							D	'									0.002				
	26	1.6															D,	1									6.003				
	P Seboun																D.										0.037				
	4								•	6.77 =	•	·	•	Ť			á	1									0.012				
2	4																4	•	•	•							0.020			0.03	•
ated Cel	67									5.85 10						Gages		•									0.011 0				
at Indicated	a ^r									3.41 5						Indicated Gages		1									0.030 0				
pet																es in	14.3		Ü	ď	0	Ü	C	0	0	0	0	Ö	0	0	0
ressure	P10															lon in	1	è	0	8	CV	2	CV	c)	0	7	(4)	J.	45	8	a ²
tical P	20	0.52	9.0	1.7	2.27	2.79	3.93	5.03	n-9	6.73	.1.9	5	χ, u	4.63	3.8	Pellect	u e		0.0	-0.002	•	•	•	•			0.003				
Ver	o _{sto}	-0.30	-0.10	0.21	17.0	0.72	2.0	2.53	3.0	5.60	2.55	-0.30	-1.02	-1.02	16.0-	ertical De	o _G	'	•	-0.001	0.300	0.300	0.00	0.001	0.001	0.001	0.00	0.001	0.001	0.70	C.001
	a.	1.27	1.69	2.53	8.8	3-17	3.80	4.12	点 说	25.23	3-69	3.38	3.33	3.38	3.48	â	D		0.000	0.000	0.30	0.002	0.002	0.003	0.003	0.002	0.002	0.001	0.001	0.00	0.003
	200	1.81	3-73	3	7.34	8	7.6	m.06	8.24	07.4	2.36	2.03	5.73	3.52	12. 5		ď		0.302	0.003	0.00	0.32	0.00	0.003	0.003	0.002	0.003	0.00%	J. 2	0.006	0.00
	9. 20.	8.0	8.0	8.0	0.17	0.0	8.0	-0.18	-0.35	-0.35	-0.35	-0.35	-0.35	-0.35	0.0		อ เก	-	00.00	000°0	0.00	0.002	0.00	0.008	0.014	0.023	0.033	0.0.5	0.045	0.043	0.038
	O.S	0.47								5.22							á	,	000.0	0.00	0.003	0.00	0*002	0.007	0.010	0.013	0.014	0.003	0.011	0.011	0.010
	a.m	0.17				3.8	9.76	8.59	8.42	10.48	5.93	1.89	1.03	0.51	0.51		Ġ	·	0.004	0.008	0.015	0.018	0.022	0.030	0.036	0,030	0.082	0.016	0.015	0.015	910.0
	200	1.58	2.31							5.1.8							5	,	0.015	2.02	0.028	0.030	0.030	0.028	0.023	0.019	0.018	0.080	0.024	0.00%	0.029
	مرا	8.3	2.30							4.52					65.6		5,	1									0.057				0.101
'	tion	*	A	ů	Д) T	N N	ม อ	22	н	h)	×	٠- م	×	R	#.I	X.	1	*	m	U	i)	61	la,	0	IX.	ы	1-3	M	ы	> :
	Point L	٠ ط				1 \$ 2	м	142					н						-4				5 5	7	F 2					н	
	8	4				E 3	а.	6.4					-						м				£ 3	pul	(F)					+4	

(1 of 11 sheets)

(Continued)

1 1 2 2 1 2 2 2 3 4 4 4 4 4 4 4 4 4											Ver	toal Pre	Vertical Pressure, psi, at Indicated Cells	si, at In	dicated	Cells							
Table Tabl		9		ı				Tot	3			Ī						Kebor	pan				
14.2 E 10.32 4.87 6.58 10.55 6.00 0.00 1.33 2.80 0.00 10.14 4.87 3.35 2.37 -0.17 9.82 3.80 0.00 10.14 2.00 0.00 10.14 2.00 3.30 2.31 0.00 3.31 0.00 0.00 1.30 0.00 11.01 0.00 0.00	8			4	20	P.	7	P5	P6	2.2	80	20	P10	a. 1	a ^C	4	Q.	2	9.	P _T	89	20	P10
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	-2 -8		D-3	10.32	4.87	6.3	2.05	0.0	9.70	3.80	1.33	2.80	0.0	10.14	78.4	3.33	2.37	-0.17	9.82	3.80	0.61	2.62	-0.56
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			U	19.11	6.58	10.65	6.3	2.80	12.19	5.07	62.7	5.68	0.00	11.43	6.58	16.6	5.10	1,.63	₩.c.	5.07	3.57	5.50	-0.47
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			Ħ	7.56	6.58	10.05	5.95	10.57	8.69	5.07	5.60	6.82	8.8	7.38	6.59	9.37	6.17	10.40	8.8	5.07	4.38	49.9	B. 3
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$			н	3.78	6.33	11.60	6.30	0.00		6.	8.15	7.52	93.0	3.60	6.33	13.92	6.65	-0.17	4.18	20.1	6.33	あた	0.10
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			ь	2.39	2.60	8.24	6.42	0.00		4-43	68	7-43	0.75	2.2	5.60	7.56	6.77	-0.17	2.37	4.43	3.46	50	0.19
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			het.	5.9	18.4	2.40	5.23	3-91		25.12	1.22	6.12	12.00	2.77	1.87	1.72	5.58	3.6	2.3	25.12	0.00	3.5	#. H
D ₂ D ₃ D ₄ D ₅ D ₄ D ₅ D ₁ D ₂ D ₃ D ₄ D ₅ D ₅ D ₅ D ₇ D ₅ D ₇ D ₅ D ₇ <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>1</td><td>C [colon</td><td>of Jacob</td><td></td><td>Total Ca</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>										1	C [colon	of Jacob		Total Ca									
D₂ D₃								Total										Febound					
0.037 0.030 0.007 0.006 0.006 0.006 0.007 0.001 -0.004 0.0143 0.032 0.002 0.004 0.006 0.006 0.006 0.004 0.006 0.004 0.006 0.004 0.002 0.002 0.004 0.004 0.002 0.004 0.004 0.002 0.004 0.00				T ₁	20	٩	ď	25	29	D ₂	P _B	00		d d	25	ก็	ď	3		D7	80	8	
0.022 0.039 0.014 0.020 0.004 0.005 0.005 0.002 -0.001 0.070 0.022 0.031 0.011 0.018 0.004 0.006 0.002	-2	4	(14)	0.157		0.030	0.007	0.00		0.00	0.001	-0.00		0.143	0.032	0.002	0.00	0.00	0.006	0.006	0.00	0.00	
0.022 0.050 0.017 0.032 0.004 0.006 0.002 40.001 0.041 0.015 0.012 0.014 0.036 0.004 0.007 0.002 0.002 0.002 0.003 0.004 0.000 0.004 0.000 0.004 0.000 0.004 0.000 0.004 0.000 0.004 0.000 0.002 0.002 0.003 0.004 0.000 0.000			v	0.09		0.059	0.014	0.000		0.007	0.00	-0.001		0.00	0.082	0.051	0.01	0.018	0.00	0.008	0.000	0.00	
0.021 0.034 0.018 0.045 0.004 0.0004 0.002 40.004 0.0041 0.016 0.026 0.015 0.043 0.004 0.005 0.0004 0.0002 0.002 0.004 0.0005 0.004 0.0002 0.002 0.002 0.003			घ	0.061		0.050	0.017	0.032		0.000	0.002	+0.001		0.0.7	0.017	0.042	0.024	0.030	0.00	0.007	0.00	0.007	
0.023 0.027 0.017 0.060 0.005 0.003 0.002 +0.006 0.049 0.018 0.019 0.014 0.056 0.005 0.004 0.002 0.002 0.002 0.002 0.003 0.010 0.003 0.010 0.003 0.010 0.003 0.010 0.003 0.010 0.003 0.010 0.003 0.010 0.003 0.010 0.003 0.010 0.003 0.010 0.003 0.010 0.003 0.010			14	3.055		0.034	0.018	0.0.5		0.004	0.002	00.00		0.041	0.016	0.000	0.005	0.043	0.00	0.00	0.00	0.00	
0.028 0.024 0.015 0.079 0.008 0.003 0.001 -0.306 0.087 0.023 0.016 0.012 0.067 0.004 0.004 0.001			מ	0.063		0.027	0.017	0.000		0.003	0.002	+0.006		0.00	0.018	0.00	0.014	0.056	0.00	0.00	0.00	0.012	
			×	0.101		0.004	0.025	0.0.9		0.003	0.001	-0.305		0.087	0.003		5.002	0.067	0.008	0.00	0.001	0.012	

Table Alk (Continued)

Point tion 2 & 2 & 2 2 & 1,2 & 2 2,1,2 & 3 2,1,2 & 4 2,1,2 & 4 3,1,2 & 4 3,1,2 & 4 3,1,3 & 4 3,1	P1 2.58	d			300	1									Rebound	pun	THE PERSON NAMED IN		
4	2.58	2		O.	2	P ₆	4	P3	Δ,	P10	a, -1	2	۳,	a, 3	25	94	P7	eg.	8
	-	1.70	0.0	0.12	0.00	2.18	1.40	0.00	0.61	0.00	1.48	77.77	\$ 0	0.35	20.27	2.2	1.48	-0.41	6.88
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7-53	2.55	0.17	0.48	0.00	5.42	2.11	-0.30	96.0	60.0-	4.43	2.31	-0.86	D.0	20.27	5.19	2.11	-0.61	1.23
	9.21	3.65	0.78	0.8	0.00	9.56	5.3	0.10	1.74	-0.19	8.11	3.41	-0.25	1.18	20.27	9.03	5.9	₩.0-	2.0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6.6	98	1.55	1.19	00.00	10.39	3.38	o.3	2.27	60.0	8.83	4.02	0.52	1.42	20.27	10.16	3.38	-0.10	2.54
0 Q 0 H P M A M M M	10.32	-8	3.98	1.67	00.00	10.84	1. ca	1.73	2.97	0.00	10.22	4.63	2.92	1.90	20.27	19.01	1.00 th	1.32	3.24
0 H H H H H K K	11.89	5.84	12.03	2.97	00.00	11.97	4.0	5.70	4.28	800	11.79	5.60	11.00	3.20	20.27	17.11	3.4	5.29	4.55
図 H P3 M C4 M (c) (d)	12.53	6.45	10.83	2.38	0.0	12.64	5.28	69*+	3.8	-0.38	12.43	6.21	2.80	4.51	20.27	12.41	5.28	4.28	6.2
의 3E to be ef to 이 하	8.39	6.82	11.00	5.47	10.10	8.81	2.38	1.89	6.9	8.25	8.19	6.58	8.97	5.70	66.37	8.58	5.38	4.1.8	7.34
C) 36 24 36 16	1.03	6.33	16.67	į.	-12.82	90.7	2.01	7.13	7.60	1.87	3.95	60.9	15.6	6.53	7.45	3.83	5.0	6.72	7.87
60 63 E 16	2.76	2.60	₹.8		-12.13	5.36	4.54	3.67	7.83	1.50	5.66	5.36	7.91	6.65	8.14	2.03	4.5	8.	7.70
o x x	5.8	8.4	2.58		17.17	2.36	7.2	0.41	6.20	24.18	2.85	4.7	1.55	5.46	62.04	2.03	4.22	0.00	6.47
X H	1.05	88.4	1.55		19.11	3.39	10.4	-0.20	5.14	4.50	3.8	4.63	0.52	4.7	98.0	3.16	4.0	-0.61	5.7
is	5.72	18.4	1.03	3.92	20.79	5.19	10.4	-0.51	4.54	0.0	2.61	1.63	0.00	4-15	-0.52	7.98	p.7	-0.92	4.81
	9.21	2.11	1.03		30.15	9.14	4.22	-0.41	3.58	1.87	1.6	18.4	0.00	3.32	-0.18	8.92	4.22	-0.82	3.85
					Total		ve	Vertical Deflection,	flection	111.	at Indicated Cage	red Gage			a de la constante de la consta				
	or or	20	2	ď	25	90	L _Q	D ₈	2		or or	20	D3	and a	DS	90	P7	P _B	40
1.2 A	0.165	0.005	0.009	0.001	0.000	900.0	0.001	000.0	-0.00		0.043	0.0	-0.009	-0.003	-0.000	0.006			0.004
60	991.0	0.036	0.017	0.003	0.001	900.0	0.000	0.00	-0.00		0.044	0.022	-0.00	-0.00	-0.419	0.008			0.004
U	0.172	9.00	0.028	0.000	0.003	0.010	0.00	0.02	-0.002		0.050	0.032	0.010	0.001	-0.01	0.000			0.00
Q	0.27	0.051	0.034	0.007	0.0	0.000	9000	0.002	-0.002		0.095	0.037	0.00	0.003	-0.116	0.000	0.00		0.004
2,1,2	0.261	0.03	0.042	0.00	0.007	0.00	0.008	0.002	-0.002		0.139	0.039	0.024	0.00	-0.03	0.000			0.004
4 2 4 5	0.192	0.048	130.0	0.013	0.015	0.009	0.000	0.003	0000		0.070	0.034	0.043	0.009	-0.005	0.039			0.006
2,1,2 G	0.147	0.038	0.086	0.018	0.027	0.007	0.01	0.005	0.003		0.00	0.00	0.068	0.014	0.007	0.007			0.009
ber	0.120	0.031	0.073	0.00	0.042	0.006	0.009	0.006	0.00		-0.0ve	0.017	0.055	o.one	0.022	90000			0,012
Ħ	0.114	0. 330	0.049	0.004	0.000	0.00€	900.0	90000	0.010		-0.008	0.016	0.031	0.000	0.40	0.006	900.0	0.006	0.026
Nj.	0.12	0.132	0.038	0.023	0.086	0.007	0.004	0.005	0.01		0.001	0.018	0.000	0.0	2.066	0.07	0.006	0.005	0.020
M	0.24	0.039	0.034	0.019	0.131	0.000	0.004	0.005	0.015		0.092	0.00	0.00	0.00.5	0.111	0000	0.006	0.005	0.0
. 42 L	0.23	0.042	0.035	0.018	0.114	0.01	0.00	0.004	0.014		0.131	0.028	C.317	0.014	0.00	0.00	0.006	0.004	0.000
*	0.222	0.047	0.037	0.007	0.097	0.012	0.005	0.004	5.03		0.100	0.033	0.00	0.03	0.077	0.002	0.07	0.004	0.00
m	0.213	0.052	0.045	970.0	0.074	0.013	0.007	0.00	0.009		0.091	0.038	0.027	0.012	0.054	0.013	0.009	0.004	0.005

										Vert	ical Pre	sture. De	Vertical Pressure, psi, at Indicated Cella	Mested	lells.							İ
	Pag.	Local					0.	1			7.4						Febound	pun				
ROS	Polut	tron	4	4	P .	P	15	P	P7	P _B	P. P.	P10	4	2	مام	a-#	45	P6	2	8	a.	OT A
2 & 4	2 \$ 1	BN	8.84 4.14 2.14 1.55 0.00	71.4	2.14	1.55	0.0	10.72	7.07	1.33	2.97	60.0	8.29	77.2	2.75	1.67	0.18	10.83	4.01	2.86	3.14	2.53
		O	12.25	5.84	4.9	3.92	0.00	n.85	5.49	3.87	6.03	-1.50	11.70	5.8	7.05	70.1	0.18	11.96	5.49	5.40	6.20	7.0
		æ	8.11	5.97	8.76	1.99	0	8.24	5.49	3.87	7.17	-2.07	7.56	5.97	9.37	5.11	1.22	8.35	5.49	5.40	7.34	0.37
		F4	8	3.5	14.51	2.6	-0.35	90.4	5. 13	5.40	7.87	-2.35	3.50	5.8	15.12	6.08	-0.17	4.17	5.28	6.93	8.0	0.0
		٠,	64 ,	5.11	8.33	5.18	-0.35	2.14	1.85	2.65	7.69	-2.44	ab	5.11	\$.8	5.30	-0.17	5.3	4.85	4.18	7.86	00.00
		Set.	2.58	4.63	1.53	5.33	1.73	2.14	4.22	-0-01	6.39	-3.00	2.03	4.63	2.24	5.35	1.91	5.3	4.23	0.72	97.9	-0.56
									Ve	Vertical Da	effection	1, in	Deflection, in. at Indicated Gages	ed Gages	1							
							Total										Бероила				1	
			L D	20	en a	ద	23 20 Eq	90	La	80	0		ď	D2	or or	ลี	2	26	4	89	Do	
4 6	2 4 1	(m)	0.121	0.057	0.052	177.0	0.008	0.016	0.012	0.003	0.001		0.138	0.03	0.00	0.00	-0.034	0.015	0.01	90.0	0.007	
		O	0.055	0.041	0.104	0.02	0.035		0.082	0.007	0.007		0.072	0.027	0.080	0.017	-0.007	0.00.0	0.021	0.006	0.03	
		×	0.032	0.034	0.000	0.028	0.057	0.000	0.019	0.000	0.013		0.049	0.000	950.0	0.021	0.015	0.008	0.018	0.007	0.00	
		н	0.008	0.035	0.061	0.031	0.078	0.00	0.014	600.0	0.020		0.00	0.018	0.037	0.004	0.036	0.008	0.013	0.00	0.006	
		د.	0.000	0.036	0.046	0.029	0.108	0.010	0.00	0.006	0.00		0.057	0.022	0.025	0.005	0.0%	0.000	0.00	0.007	0.031	
		M	0.088	0.045	0.042	0.025	0.185	0.013	0.009	0.007	0.026		0.105	0.031	0.020	0.018	0.143	0.012	900.0	0.006	0.034	

Continued

Table Alk (Continued)

						-				1				1								
							101	7		Ver	17071	essure b	4	et indicated Cells	Series		hebor	pun				1
NO.	Point	tion	a.	P2	۵,۳	a.*	a.s	9	2	89	6	P	a.**	62	2.	A. 3	2	8 P	P7	20	0	20
80	н	4	1.85	1.46	-0.18	0.12	-0.17	2.85	1.48	-0.20	0.52	0.0	1.75	1.16	0.00	0.00	0.00	2.18	1.69	0.82	6.70	0.65
		M	3.51	59	00.0	0.36	0.0	3.6	2.10	-0.20	0.9	0.0	3.41	2.19	0.18	0.2	0.17	5.30	2.31	0.82	1.14	0.56
		U	5-17	8	6.0	0.72	0.00	9.37	2.98	-0.20	1.74	-0.09	5.07	2.92	64.0	09.0	0.17	30.6	3.16	0.86	8:	0.47
		Ω	6.27	3.65	1.03	1.07	00.00	10.83	3.59	0.41	2.11	0.0	6.17	3.65	1.2	6.0	0.17	10.49	3.80	1.43	2.62	95.0
9 \$ 6	1 \$ 2	ы	7.58	4.14	1.20	1.55	0.0	11.17	1.4	1.63	3.28	0.00	7.18	41.4	1.38	1.43	0.17	10.83	32	2.65	3-36	94.0
in.	н	Bı,	9.68	18.4	5.66	5.36	00.0	12.08	85	4.18	4.28	0.00	9.58	1.87	2.84	2.14	0.17	7.11	5.06	2.50	4.46	0.56
9 \$ 5	1 2 2	9	11.62	5.148	3.36	3.33	-0.17	12.75	5.38	3.97	3.50	-0.38	11.52	5.48	3.44	3.21	0.00	12.41	5.59	8:3	6.12	0.18
		æ	7.56	5.8	2.8		-0.17	8.69	5.49	4.48	7.16	-0.17	2.16	5.84	8.08	4.28	00.0	8.35	5.70	5.50	7.34	8.0
		ы	69.0	2.50	15.98	2.47	-0.35	7.07	8.58	5.81	7.95	-0.56	3.59	5.60	16.16	5.35	-0.18	90.4	5.49	6.83	8.13	8.0
		ы	2.03	8.	8.93	8.5	0.0	2.10	1.6	2.85	7.86	-0.73	1.93	8	9.11	5.85	0.17	2.14	1.85	3.87	8.0	-0.19
		×	2.12	4.38	-0.00		20.62	2.148	1.22	-0.51	6.39	0.0	2.8	4.38	0.00	8.3	20.79	2.14	4.43	0.51	6.47	-0.36
80	H	,1	2.58	3	1.03	4.52	-24.09	3.72	10.4	-1.8	5.59	-0.75	2.148	8	1.2	07.4	-23.98	3.38	7.3	00.00	5.77	-0.19
		7.	3.69	41.4	0.51		-0.17	5.3	70.7	-1.22	4.63	99.0-	3.59	41.4	69.0	3.57	0.00	5.41	4.22	-0.20	8	-0.10
		315	5.53	5.33	0.34		0.00	9.1.8	1.22	-1.22	3.67	-0.47	5.43	1.38	0.52	2.85	0.17	9.14	4.43	-0.20	3.85	0.0
									1												1	
							Total		2	er ar can	ertical lellection	10.	at Indicated Gage	2000	9		Labourne				1	
			គ្នា	25	D	ದೆ	25	90	40	60	o O		ดี	200	e e	ณ์	2	90	27	89	000	
80	-4	<	0.000	0.042	0.08	0.00	0.000	0.013				_	0.099	0.022	0.00	-0.005	-0.00	600.0	-0.002	-0.00	0.038	
		A	0.113	0.057	0.032	0.00	0.001	0.019					0.122	0.037	0.000	-0.003	-0.002	0.005	0.00	-0.0m	5.008	
		ı	0.127	690.0	0.017	0.007	0.003	0.023	0.012	0.003	0.000		0.136	0.00	0.00	0.000	-0.00	0.00	900.0	0.00	0.008	
		Q	0.139	0.075	0.059	0.011	0.007	0.005				,	0.148	0.055	0.037	0.00	0.003	0.082	0.0	0.00	0.000	
2 4 6	1.52	843	0.144	0.077	0.083	0.015	0.01	0.027					0.153	0.057	0.061	0.008	0.307	0.023	0.005	0.003	0.00	
10	н	ě.	0.119	0.070	0.098	0.021	0.022	0.00					0.126	0.050	0.076	0.001	0.018	0.000	0.023	0.005	0.025	
2 4 6	1.6.2	69	0.075	0.055	0.123	0.029	0.045	0.019					0.085	0.035	0.101	0.022	0.041	0.015	0.033	0.008	0.00	
		tic:	0.050	0.045	0.106	0.035	0.078	0.015				61	0.059	0.005	0.084	0.028	0.074	0.011	0.000	0.00.0	0.030	
		н	0.044	0.043	0.0%	0.038	0.100	0.01			0.032	6.	0.03	0.023	0.047	0.031	0.097	0.000	0.018	0.001	0.0.0	
		5	0.058	0.048	0.052	0.035	0.128	0.025				•	0.067	0.028	0.030	0.028	0.124	0.011	0.012	0.011	0.000	
		ĸ	0.103	0.061	0.047	0.030	0.161	0.00					0.112	0.041	0.005	0.023	0.157	0.025	0.000	600.0	0.055	
80	н	ы	0.121	0.068	0.049	0.028	0.143	0.022					0.130	0.0.8	0.007	0.02	0-139	0.018	0.000	0.008	0.052	
		×	0.130	0.07	0.058	0.00	0.115	0.00		0.00	0.039	•	0.139	0.034	0.036	0.000	0.111	030.0	0.012	0.007	0.047	
		*	921.0	0.082	0.00	8	0.083	0.00					0.147	0.062	988	O. CO. R.	0 00	100	o me	200	Ser C	

		2 -3.09	JE								ដ	8	4		2
	17	2.62								100	-0.021				
	8	1.3	3.16	4.16	7.03	2.55	-0.61			Ba	0.00	0.02	0.016		0.018
	2	P.4	5.38	5.59	5.27	1.7	4.32			4	0.ag	0.065	0.056		0.032
1	9	9.8	12.30	8.6	3.8	1.80	1.58			200	0.035	0.000	0.00.5		0.0
4	2	0.0	-0.52	0.00	0.00	0.00	1.2		Dahamad	25	-0.630	-0.009	0.097		0.10
	2.0	0.9	2.61	3.20	4.03	1.51	1.03			2	0.007				
3	4	0.35	1.38	19.4	16.6	18.4	1.72			2	0.078	0.137	0.005		0.00
Ceted C	2	3.17	4.39	4.63	4.51	8.4	3.66			20	0.062	0.335	0.006		0000
	12	1.23	7.73	#. S	2.57	1.16	1.28	124	-	ď	0.137	0.000	900.0		0.0
ure, per	22	0.0	0.28	3.62	2.62	3.65	3.37	5					i		- A
	8		M				Wit:	lect for		20	0.005	0.006	0.033	. 200	100.0
Vertic		1.83						100		80					
	7-							Very		27	0.038				
	Ι.	19.01								90					
Total	25	27%		A.			1.2		btel		0.110				
	23						3.8			a a	9.00	.mg7 0	10.0	1	
	-4						1.72	40.75		24	0.10 0.018	051.	901		3 30
	2						3.66		100	25	000	.052	.ch3 c	042	-
	-1	.42	8.	.53	92	.65	1.47 3			2 Ta	.266	.149 0	, IZI.	115	-
	a a a		0 7	H 5	1 2	7	× 1	1			0	0	0		*
1		-													
			٠												

ontinued

1										Vert	or Pre	Wertical Pressure, pst. at Indicated Cella	t. at in	Steared (1000								
	peo.	- Boor					0.	7									hebound	nd		,			
Rose	Poźnt	tion	1	2	2	a, g	24	a _a	ρ,	a, 10	o.	0	Ar t	p.	۵.	a-3	12	9.	20	200	0.	F.0	
t ~	Ħ	ø	0.83	1.22	-0.50	0.12	0.0	3.6	5.79	-0.20	0.70	-0.19	99*1	1.34	0.17	0.35	0.00	2.8	2.0	1.22	0.79	2.62	
		0	1.18	1.58	-0.51	0.36	0.00	16.4	2.53	-0.30	1.22	0.00	2.3	1.70	-0.35	0.59	0.0	8.4	2.73	1.22	1.31	2.81	
		Ω	1.85	1.8	-0.51	0.36	0.0	2.59	5.8	-0.30	1.57	-0.19	2.68	2.07	0.35	0.59	0.00	5.87	2.27	1.12	1.66	2.62	
4 2	1 \$ 2	м	2.40	2.31	-0.51	0.18	0.0	7.00	3+37	-0.30	2.0	-0.19	3.23	2.43	0.35	E.0	0.0	6.89	3.59	1.23	2.10	2.62	
_	r4	ß.	3-32	2.80	0.3	0.8	0.00	3.93	3	0.51	3.25	60.0	4.15	2.92	09.0	1.07	8.0	9.95	1.23	1.93	3.5	2.72	
6 \$ 2	1 \$ 2	U	3-50	3-03	60.0	1.3	0.17	12.75	3.5	0.61		-1.03	4.33	3.17	8.	1.54	0.17	12.64	98.1	2.03	4.72	1.78	
		×	2.40	3.29	0.52	8:1	0.17	9-37	17.	2.65	5.77	-2.15	3.23	3.5	3.38	2.13	0.17	9.36	16.4	4.37	5.86	93.0	
		н	1.20	3-17	1.03	2.0	0.0	4.63	19.4	7-13	6-73	-2.25	2.03	3.29	1.89	2.49	0.00	1.52	98.4	8.55	6.82	9.50	
		ь	0.65	2.8	0.34	2.50	0.00	2.37	7.7	3.26	7.08	-1.87	1.18	0	1.20	2.73	0.00	3	4-33	4.68	7.17	8.0	
		×	95.0	2.68	-0-17	2.26	3.0	2.03	3.80	0.00	5.86	67.6	1.39	2.80	59.0	5.49	0.0	3.8	8	1.42	5.9	12.00	
r-	н	ü	0.74	2.56	-0-3-	2.00	0.00	2.37	3.58	-0.51	9.16	-0.37	1.57	2.68	0.52	2.25	0.00	2.8	3.80	0.91	5.3	2.14	
		3 7.	0.05	2.56	-0.51	1.90	0.00	3.16	3.58	1.8	4.28	2.0	1.73	3.68	0.35	2.13	0.00	3.03	3.80	0.40	75. 17	2.0	
		sr.	4.48	2.68	-3,51	1.55	0.0	5.08	16	-1.8	3.42	-2.3	2.3	2.80	0.35	1.78	0.00	16.	3.80	0.40	3.50	0.56	
							-		A.	Vertical Peffection	"Cection	n in a	. Indica.	ted Once.									
			o o	25	e a	ca l	2	29	e ·	Ba	0		9	22	D3	d'	D 5	80	27	80	0		
4	н	æ	550.0	0.070	0.046	0.005	0.001	0.031	0.031	0.00	0.001		0.108	0.050	0.030	-0.00	0.022	0.033	0.009	-0.00	-0.02		
		U	0.082	0.082			0.004	0.052	0.038	0.007	0.003		0.131	0.052	0.057	0.003	0.025	0.044	0.036	-0.001	-0.010		
		Ω	0.163	0.086			0.007	0.067	0.070	0.010	0.005		0.152	0.0%	0.083	0.007	0.028	0.049	0.048	0.002	-0.006		
6 4 2	1 4 2	(m)	0.126	0.0			0.012	0.0	0.076	0.013	0.00		0.175	0.0%	0.091	0.01	0.033	0.051	0.054	0.00	-0.003		
1	н	ĝa,	0.088	0.0			0.027	0.061	0.00	0.00	0.000		0.137	0.057	0.101	0.001	0.048	0.043	0.068	0.01	0.007		
6 5 4	1 6 2	U	0.043	0.060			0.057	0.0.8	0.113	0.00	0.0.3		0.002	0.000	0.115	0.031	0.078	0.030	0.091	0.00	0.030		
		æ	0.00	0.00			0.03	0.000	0.098	0.032	0.072		0.06	0.030	0.093	0.037	0.117	0.022	9.000	0.004	0.059		
		6-4	0.009	0.148			0.117	0.038	0.067	0.034	0.0		0.058	0.028	0.056	0.040	0.138	0.000	0.045	0.000	0.081		
		ь	0.005	0.057			0.140	0.044	0.050	0.032	r.124		0.084	0.037	0.035	960-0	0.161	0.000	0.008	0.324	0.111		
		ĸ	0.033	3.072			0.149	0.055	0.045	0.028	0.164		0.082	0.052	0.032	0.030	0.170	0.037	0.003	0.000	C-151		
7	ρſ	ы	0.043	0.00			0.135	0.0%0	0.047	0.00	0.153		0.092	0.050	0.036	0.027	0.156	0.0.2	0.00	0.008	0.140		
		5	0.051	0.085	0.053	0.032	0.113	0.055	0.032	0.00	0.129		0.100	0.005	0.047	0.00	0.134	0.047	0.030	0.017	911.0		
		×	0.067	0.09			0.075	0.072	0.075	0.024	0.005		0.116	0.072	0.080	0.00	0.00	0.34	0.033	0.016	0.000		

										Vert	Cal Pre	seure. De	if. at In	Meated	cille							1
	Long	Too.					Tot	7									Rebon	pun				-
Nos	Polat	£100	2	20	4	a. 1	2	9	4	80	م	P10	4	4	a.	200	24	9	2-1	8	0	2
10	1.6.2	м	1.7		-0.43		0.0	5.65	2.9	0.2	2.10	0.00	2.31	2.07	0.00	0.7	4.0	5.53	3.16	-0.51	1.8	-1.9
		o	5.39		0.0		0.00	11.39	8	0.61	1.20	-0.19	2.95	2.68	0.43	1.30	0.34	11.17	1.2	-0.11	8:	-2.16
		×	1.66		0.36		0.0	7.68	27.7	4.38	5.42	-0.19	2.25	2.8	0.78	3.66	46.0	7.56	4.43	3.66	5.2	-2.16
		н	8.0		0.43		0.00	3.8	1.0	8.86	6.39	-0.28	1.48	2.80	6.9	1.8	ある	3.72	4.2	8.14	6.11	-2.25
		7	0.6		3.26		0.0	2.3	3.69	4.18	74.	1.50	1.20	2.68	0.78	2.13	0.34	2.14	3.8	3.46	6.8	-0.47
		×	3.0		2.19 -0.09	1.67	0.0	1.8	3.37	1.43	5.42	30.56	1.20	2.43	0.43	8:	0.34	1.80	3.58	D.7	5.8	26.59
									4												1	
							Total			-	200		T ASSESSED	200			Kehmind				1	
			o I	25	ď	ล์	2	90	D7	£3	60		ď	en En	a P	2	2	94	27	80	204	
1 10 1	1.62	14	6.26	0.07	0.00	6.216 0.074 0.097 0.020 0.03	0.03	0.0	0.061	0.00	0.001		0.161	0.063	0.062	0.00	-0.028	0.054	0.067	0.007	-0.029	
		O	0.115	0.00	0.132	0.039	0.005	0.043	0.115	0.00	0.00		0.000	0.039	52.27	0.000	0.00	0.033	0.10	0.00	0.00	
		pr.	0.00	0.00	0.105	0.046	0.16	0.035	0.093	0.035	0.120		0.035	0.009	0.000	0.036	0.105	0.00	0.079	0.007	0.00	
		н	0.0	0.00	0.069	0.048	0.158	0.035	0.061	0.038	0.134		0.000	0.009	0.054	0.038	0.117	0.00	0.07	0.030	0.0	
		7	0.088	0.050	0.049	0.045	0.183	0.043	0.00	0.035	0.159		0.033	0.039	0.034	0.035	0.142	0.033	0.031	0.007	0.119	
		×	0.100	0.005	0.01	0.039	0.20	950.0	0.0.2	0.031	0.309		0.045	0.0%	0.032	0.000	0.169	0.00	0.028	0.023	0.169	

Continued

Table Alt (Continued

										Vert	ical Pre	Vertical Pressure, psi, at Indicated Cells	it, at In	dice ted (Sells.							1
Row	Point	Lion	ai 4	200	2	42	75	9	P ₂	8	A.	P. 20	4	F2	4	a a	P Rebox	Pe Pe	7	8	40	2
141	2 8 2	m	0.95	0.97	00.0	0.23	0.17	1.58	1.47	-0.20	0.52	-0.19	0.7	0.97	0.00	0.23	0.0	1.80	1.58	0.82	10.0	1.3
		O	62-1	2.5	0.00	0.35	0.17	2.49	7.2	-0.50	0.87	-0.10	7	1.22	0.00	0.35	0.0	2.7	2.25	0.82	1.22	1.40
		Q	1.47	3.46	0.00	0.47	0.17	3.38	2.45	-0.20	1.23	-0.19	8:1	1.16	0.0	0.47	0.0	3.50	2.53	0.82	1.57	1.2
	2,1,2	68.	1.66	1.58	00.00	0.47	0.17	3.8	2.7	-0.20	1.39	-0.19	1.16	1.58	0.0	0.47	0.0	4.17	2.85	0.82	1.74	1.2
7.11	2,2	(n	2.03	8:	80.0	4.0	0.17	6.95	3-34	0.11	8.8	-0.10	1.9	1.9	60.5	0.72	0.0	6.77	3.48	1.23	2.6	1-40
	2,1,2	Ö	2.33	2.19	0.17	8.0	0.17	9.69	3.80	0.41	3.50	-0.10	1.0	8.19	0.17	8.0	0.0	8.92	3.92	1.43	3.7	1.40
		90	1.66	2.31	0.34	1.16	0.17	6-55	8	1.8	15.3	-0.10	1.46	2.31	0.34	1.18	8.0	6.77	4.0	2.86	4.72	1.10
		н	1.30	19	0.34	1.50	0.17	3.39	3.80	5.30	5.24	-0.19	1.00	2.19	0.34	27	0.0	3.61	3.91	6.32	5.59	1.3
		by.	800	61.2	0.34	1.6	0.17	1.7	3.58	2.24	5.42	-0.73	0.74	2.19	20.0	1.66	00.00	1.8	3.69	3.8	5.7	0.7
		×	7.00	1.8	0.17	1.42	0.35	3.47	3.16	-0.20	1.54	-1.50	0.83	8	0.17	1.42	0.18	1.69	3.27	0.82	4.89	0.30
7 6 23	2 8 2	ы	1.11	1.8	0.17	1.42	0.17	1.58	8	-0.30	3	-1.69	0.93	2.8	0.17	1.42	0.0	1.80	3-17	0.72	4.37	-0.19
		×	1.38	200	0.17	1.18	0.17	1.90	8	-0.61	2	1.72	1.30	2.07	0.17	1.18	0.0	2.14	3-17	0.41	3.67	-0.18
		m	B. 1	2.19	0.0	1.18	0.17	8.	3.16	-0.81	2.62	1.32	7.66	2.19	0.00	1.18	0.0	3.16	3.27	2.0	2.97	0.18
							Total	-		Trees !	enection.	Vertical Leffection in. at Indicated Gares	t Indica	ted Oace			Sehmand					
			ā"	25	e e	Car.	2	9	D2	(A)	o G		a rd	20	B3	D. B.	a a	26	PZ	28	0	
1811	2 4 2	m	0.045	0.08	0.041	0.005	0.001	0.064	0.045	0.005	0.00		0.053	0.043	0.00	-0.00	-0.077	0.043	0.027	-0.003	-0.05h	
		0	0.08	0.077	0.080	0.000		0.074	0.082	0.00	0.003		0.072	950.0	0.049	0.003	-0.075	0.053	0.054	0.00	-0.052	
		ρ	0.088	0.083	0.10	0.003		0.078	0.009	0.013	0.00		0.00	0.062	0.000	0.007	-0.072	0.057	0.07	5.005	-0.00	
7.9.11	2.1.5	949	0.103	0.084	0.10	a.o.e		0.00	0.103	9000	0.009		0.11	0.063	0.075	0.000	-0.069	0.058	0.175	0.008	90.0-	
.41	2.5	dia.	0.07	0-573	0.12	0.02		0.068	0.112	0.02	0.024		0.082	0.052	0.00	0.000	-0.054	0.047	0.084	0.016	-0.031	
	2,1,2	0	0.040	0.056	0.140	0.035		0.053	0.128	0.033	0.056		0.048	0.035	0.118	0.009	-0.000	0.032	0.100	0.00	0.00	
		80	0.020	0.046	0.126	0.041		0.044	0.109	0.038	0.143		0.030	0.00	0.097	0.035	0.082	0.023	0.081	0.030	0.088	
		н	0.014	0.043	0.080	0.044		0.043	0.073	0.040	0.160		0.022	0.022	0.049	0.038	0.00	0.002	0.045	0.032	0.105	
		13	0.016	0.050	0.057	0.040		0.081	0.054	0.037	0.171		0.00%	0.000	0.00	460	0.110	0.030	0.00	0.00	917.0	
		×	0.006	0.065	0.053	0.034		0.085	0.051	0.031	0.22		0.034	0.044	0.022	0.028	0.174	0.045	0.023	0.023	991.0	
181	2 2	ы	0.031	0.07	0,055	0.021		0.07	0.053	0.030	0.20		0.039	0.050	0.004	0.00	0.146	0.050	0.005	0.022	0.149	
		×	0.038	0.078	0,066	0.020		0.077	0.005	0.028	0.165		0.066	0.057	0.035	0.023	0.100	0.056	0.037	0.000	0.110	
		200	0.058	0.088	0.108	0.027		0.06%	0.104	0.027	0.118		990.0	0.067	0.077	0.02	0.053	0.063	0.076	0.00	0.063	

		P10	9.0	0.93	0.93	2.0	0.16	80.0												
		a.O	1.57	15	8	#. ·	8.	28.4		-	0	0.00	0.07	0.120	0.110	0.157	0.172			
		B	2.7	2.3	5.8	1.07	2.55	1.38			P8	0.001	0.008	0.033	0.034	0.031	0.00%			
		d.	2.54	3.38	3.59	3.59	3.26	2.96			27	0.087	0.105	3.0Ac	0.000	0.033	0.031			
	20	9	3.50	6.32	4.7	2.60	1.58	1.35			50	0.063	0.037	0.000	0.000	0.037	0.052			
	Sebou	مرم	0.17	0.37	523	0.17	0.17	0.17		Februard	â	0.000	0.0%	0.000	911.0	0.150	0.18	,		
		α,	74.0	0.71	8.0	1.16	1.18	1.18			ដ	0.022	0.009	0.034	0.037	0.033	0.007			
ells		Α,"	0.0	0.0	0.17	0.36	0.30	0.0			ค์	0.000	0.123	0.00	0.052	0.031	0.027			
icated (2,0	2.3	- B	E9:	1.83	£9.1	1.70	ed Gaze		22	0.003	0.037	0.027	0.00	0.031	0.043			
Vertical Pressure, psi, at Indicated		7.24	0.92	1.10	0.92	3	0.55	3 .0	in. at indicated Gaze		a°	0.007	0.051	0.039	0.034	0.036	0.043			
Sure, per		07	60.0	0.18	0.18	6.0	62.0	99.0-												
ca. Pres	Ī	40	1.39	3.06	30.00	£9.5	2.80	8	Taffection.		0	3.01	0.0%	0.107	0.127	0.144	0.159			
Verts		ano An	20.0	0.1.0	1.1	2.13	0.61	-0.72	Vertical Le		e00	0.727	0.034	0.039	0.000	0.037	0.031			
		17	2.54	3-38	3.59	3.59	3.38	·8.	i de		La	0.095	0.113	0.02	0.058	0.041	0.039			
		0,6	3.27	60.3	15:07	2.37	1.35	1.12			50	0.073	0.047	0.039	0.038	0.007	0.1.2			
	0	a.tr		0.35						C. C.	a	0.009	0.047	6.000	0.100	0.131	0.169			
		n, I	74.0	LL.0	8.	1.18	1.13	1.13			ದೆ	0.005	0.033	0.038	0.041	0.037	0.031 0.159			
		a.m	0.52	0.52	0.60	69.0	69.0	1.58 0.52			ດ້	0.072 0.081	0.134	0.110	0.063	0.012	0.038			
		n. Cv	1.10	1.7	7.7	7.7	1.71	1.58			20	0.072	0.066	0.036	0.034	0.000	0.052			
	4	n,	0.56	1.7.0	0.56	0.28	0.19	0.20			ດ້	0.061	0.025	0.03	0.008	070.0	0.017			
	Local	tion	18	v	85	P4	7	×				6.1	U	325	1-4	وم	ж			
	201	Point	2 4 7									2 \$ 1								
		Ros	4 10									10								

Table Alk (Concluded)

		1						1100	211	Spire, ps	Vertical Pressure, psi, at Indicated Celli-	Cated	9							
tion P1 P2 P3 P3	P2 P3 P3	a.	£*		25	P P	L _d	8	0	20	a.**	40	4	a.**	T S	94	2	Pe	8	210
0.19 0.61 1.20 0.36	1.30		0.36		0.35	0.68	1.27	-0.51	0	0.00	95.0	0.73	8.0	0.2	0.00	1.13	1.27	19.0	0.62	01.
0.73	0.73		0.36		0.35	1.47	1.69	-0.30	0.79	0.0	0.56	0.0	-0.09	0.2	0.0	3.5	1.69	0.82	0.97	0.10
0.55 1.03	0.55 1.03	_	0.36		0.35	1.81	8	-0.30	8	-0.10	0.65	0.97	-0.17	0.2	0.0	2.3	1.90	0.82	1.14	9.0
0.85 1.03	0.85 1.03	_	0.36		0.35	2.37	2.12	-0.30	1.22	0.0	0.7	0.97	-0.17	0.2	0.00	2.82	2.12	0.82	1.40	0.10
1.10 1.03	1.10 1.03	_	0.48		0.35	3.27	2.6	-0.10	1.7	0.0	20	1.22	-0-17	0.36	0.0	3.72	2.6	1.00	1.93	0.0
1.34 1.03	1.34 1.03	_	0.60		0.35	3.8	8.8	0.0	2.45	0.18	0.74	1.16	-0.17	0.18	0.0	1.10	8.8	1.22	2.63	0.3
1.34 1.11	1.34 1.11		0.0		0.3	8.0	3.17	0.61	3.23	0.0	0.65	1.16	60.0	0.72	0.0	3.39	3.17	1.73	3.42	0.19
1.30	1.30	e,	0.84		0.35	1.69	3.07	8	3.76	0.18	0.45	1.5	0.0	0.72	0.0	2.14	3.07	2.04	3.8	0.26
1.34 1.20	1.34 1.20		0.8		0.35	1.00	9.9	J. 0	3.8	0.0	0.16	1.16	0.00	0.72	800	1.47	2.85	1.43	4.00	0.19
0.37 1.34 1.11 0.84	1.34 1.11		. S.		0.35	0.79	2.64	-0.51	3.32	000	0.74	1.16	0.0	0.72	8.0	7.3	2.6	0.6	3.50	0.10
1.03	1.34 1.03		0.84		0.35	0.79	2.5	0.7	2.97	00.00	0.83	1.46	-0.17	0.72	800	1.24	2.54	0.51	3-15	0.10
1.3	1.34 1.03		0.84		0.3	1.00	2.54	-0.81	2.53	0.0	1.1	1.16	-0.17	0.72	0.0	1.47	2.54	0.41	2.7	0.19
11.58 1.11	11.58 1.11		*8°°		0.35	1.58	2.3	16.0-	2.18	0.0	1.85	1.70	-0.39	0.72	0.0	2.03	2.73	0.31	2.36	0.1
				-			Ver	ricel D	nection	Vertical Leffection, in. at indicated Deges	t Indice	ted Gage								
2 2 2 1 _d	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	ď	1	De	9	L _G	8	6		á	8	e	ď	Pebound	99	27	a _Q	00	
0.049 0.025 0.004	0.049 0.025 0.004	0.025 0.004	0.00		-0.001		9.0.0	0.00	0.00		0.057	0.038	0.024	0.00	-0.006	0.031	0.00	-0.00	0.003	
0.046 0.008	0.063 0.046 0.008	0.046 0.008	0.008		0,000	0.081	A C	1000	0.00		0.050	0.052	0.035	0.00	-0.00	0.062	0.067	0.00	0.007	
0.069 0.055	0.069 0.055	0.055		-	0.00	0.005	0.098	0.01	0.007		0.055	0.058	0.04	0.007		0.066	0.00	0.007	0.009	
0.069 0.063	0.069 0.063	0.063		-	0.007	0.083	0.103	0.03	0.02		0.057	0.058	0.052	0.00		0.064	0.005	0.0	0.0k	
0.000	0.000	0.091		-	0.017	0.072	0.112	0.00	0.026		0.000	0.00	0.080	0.00 B		0.053	0.00	0.000	0.00	
0.044 0.132	0.044 0.132	0.132			0.039	0.055	0.125	0.036	0.00		0.035	6.033	0.12	0.026	0.034	0.036	0.107	0.00	0.066	
0.035 0.108	0.035 0.108	0.108			0.001	0.045	0.10	0.042	0.112		0.026	0.00	0.097	0.032	0.056	0.00	0.086	0.035	٥٠.	
0.032 0.061	0.032 0.061	0.061			0.00	0.045	0.116	0.043	0.138		0.022	0.0	0.000	0.334	0.005	0.00	0.09	0.036	0,140	
0.03	0.036 0.043	0.03			0.125	0.053	0.000	0.039	0.156		0.00	0.00	0.032	0.032	0.120	0.034	0.032	0.032	0.158	
0.045 0.037	0.045 0.037	0.037			0.189	0.070	0.047	0.033	0.167		0.030	0.034	0.00	0.00	0.184	0.031	0.00	0.006	691.0	
0.023 0.051 0.038 0.026	0.051 0.038	0.038			091-0	0.077	0.05	0.031	0.154		0.034	0.000	0.007	0.023	0.155	0.058	0.033	0.00	0.156	
0.044	0.057 0.044	0.044				0.083	0.065	0.00	0.128		0.039	0.046	0.033	0.02	0.120	0.00	0.047	0.002	0.130	
3.057 0.050	3.057 0.050	0.000		_	0.0	0.00	0.00	0.00	0.00		0.049	0.056	0.049	0.000	0.081	0.00	0.078	0.00	0.090	

Multiple-sheel Heavy Gear Load Maxible Pavement Test, Static Instrumentation loading Data Intiple-sheel Heavy Gear Load Condition: 30 Mags per Weel, 12 Wheels, 100 psi Table A-15

			i							Vert	al Press	pire, pal	Vertical Pressure, pai, at Indicated Cells	ಂತಿಸಿಕಾರೆ ೧೯	11.5							
3		-100	c				To	7									kebonno	ınd				
Pos	Point	tion		2		.4	2	i.e	t-	(C)	o.	CT	D. 0 4	O.	ye (v	ide T	2	9	d.	a, 00)	0,	20
4	**	Y	-0.20	60.4	*	3.	0.40	0.0	4-13	8.0	1.47	0.20	-0.30	67.7	2.83	2.27	0.10	0.73	10.4	-0.70	1.55	0.30
		m	0.0	5.82	6.54	2.88	2.98	-0.37	5.80	-0.10	2.16	0.41	0.0	5.92	7.43	3.23	0.68	00.0	5.68	-0.80	2.2	0.41
		ย	0.00	6.1.8	12.20	3-83	2.55	0.19	6.63	8.8	2.93	0.82	0.00	6.58	13.07	4.18	2.3	0.19	92.9	2.70	3.61	0.82
		Ω	-0.20	6.76	12.09	4-31	以完	1.09	7-34	2.60	3.36	1.23	-0.50	98.9	35.5	99.4	3.62	97.0	7.22	3°30	3.5	1.23
1 8 3 1	5 3	(lad	-0.20	6.36	10.24	5.03	5.77	0.36	7.69	2.60	3.88	.4	-0.50	3	11.11	5.38	5.47	0.73	7.57	3.30	8.	1.8
		Br _a	00.0	6.57	10.68	5.87	9.00	-0.37	9	3.50	15-4	3.26	8.0	6.67	11.55	6.22	8.70	3.0	7.34	4.30	4.65	3.26
		U	8.0	5.24	13.73	6.23	10.38	-0.37	6.31	8.5	. 7	4.30	0.00	3000	34.60	95-9	9.78	0.00	61.9	5.70	2.3	4.30
		×	0.00	3-71	7.42	6.23	20.0	-0.37	4.72	3.00	5.20	5.53	0.00	3.00	B.26	6.58	30.05	0.00	4.59	3.70	5.3	5.53
		ы	0.0	2.30	Ŝ	5.73	11.15	-0.37	3.79	0.60	5.30	6.86	0.00	8.	2.83	6.10	10.05	0.0	3.67	1.30	8	98.9
pd	e-4	64	0.00	5	0.33	5.03	7.1	-0.37	3.67	-0.20	3	5-12	8.0	3.15	1.20	5.38	2.14	0.0	3.55	0.50	7.1	4.12
1 6 3 1	2 4 5	w:	00.0	8.4	7.0	4.55	3.8	00.0	4.59	-0.4)	-1-1-	2.56	00.5	4.19	1.32	86.4	3.62	0.37	74.4	0.30	4.20	2.56
-4	~		00.00	8:3	2.6	#. 	ती. ट.	-0.19	5.39	-0.50	8	d.	0.0	4.03	3.51	7.66	2.54	0.19	5.27	0.10	4.13	1.87
).	0.00	3.62	3.60	64.4	2.35	-0.55	5.85	-0.50	3	1.43	0.0	5.72	14.47	27.3	3.	-0.18	5.73	0.20	4.13	1.43
		æ.	00.00	6.57	10.16	64.4	2.45	-0.55	7.30	2:1	1.33	1.02	0.00	6.67	11.33	5.14	2.15	-0.18	6.86	8.1	4.30	3.5
							Ì		8	Vertical Defiects	Tection.	9 In.	at Indicated Care	ad Carre								
			6	c		6	10.	10		6	6				4		Febrund	pu				
			2.4	0	377	5.7	24	4	2	ar.	0		1	2	9 1	is a	2	.e	22	100 A	0	
p=4	e4	~	-0.00 g	0.031	-0.019	-0.090	0.00	0,305	-0.01	0.000	0.002		-0.023	0.0%	0.000	0.001	-0.002	0.00	0.00	0.000	0.000	
		ø0	-0.007	0.045	-0.01-	-0.0MB	-0.001	0.008	-0.013	?	0.000		-0.012	0.000	0.003	0.003	-0.00-	2.005	0.001	0.000	-0.0nl	
		υ	-0.00	0.045	-0.013	-0.0B3	0.003	0.00%	-0.012	0.000	0.000		-0.000	0.00	0.00%	0.mg	-0.003	0.00	0.000	0.000	-0.001	
		A	-0.002	0.062	-0.012	-0.780	0.002	0.010	-0.012	0.000	0.000		-0.007	0.077	0.007	0.511	0.000	0.00	0.00	0.000	-0.001	
143 1	2 4 3	fisk	0.00%	0.00	-0.010	-7.03	0,004	0.0	-0.012	0.000	0.000		-0.003	0.077	600.0	0.016	0.000	0.00	0.00%	0.000	-0.001	
		ji.	0.015	0.00	-0.00R	-0.00	0.010	0.00	-0.023	00000	0.001		0.010	0.365	0.011	0.00	0.008	0.00%	0.103	0.000	0.000	
		U	0.031	960.0	-0.cm	-0.08	0.117	2.03	-0.023	0.000	0.003		0.00	0.031	0.011	0.033	0.015	0.003	0.0.3	00000	0.000	
		200	0.055	0.025	. 3. O. 19	-0.0le	0.020	0.00	-0.022	0.000	0.005		0.000	0.040	0.010	0.045	0.025	0.000	0.003	00%	0.0%	
		1-4	0.077	0.022	-0.011	-0.038	0.03	2.007	10.0-	0.300	0.007		0.072	0.037	0.008	0.053	0.037	0.00	0.003	0.000	0.000	
pel	p-4	2	0000	0.027	-0.032	-0.045	0.049	0.013	-0.011	0.000	0.009		0.00	0.042	0.007	0.0w.	5.047	0.00.0	0.003	0.000	0.078	
1 2 3 1	5 4	¥	C-133	0.037	-6.2	-0.057	0.033	0.021	-0.01	0.000	0.000		0.136	0.002	2.007	0.034	0.053	0.018	0.003	0.000	0.008	
~	r-4	ы	0.131	0.043	-0.011	-0.73	0.052	80.0	-0.01	0.000	0.006		0.12	0.058	0.008	0.026	0.050	0.023	5.003	0.000	0.007	
		7	0.115	640.0	-0.011	-0.3%	0.040	0.030	-0.010	0.000	0.007		0.110	0.03	0.005	0.025	0.00	1000	0.00	0.000	0,776	
		per .	0.003	0.000	-1.009	0.40	0.038	7.032	-0.00	0.00	0.00		0.078	0.075	0.030	0.092	0.036	0.000	0.005	0.000	0.005	
											(Continued)	med)								T)	(1 of 12 sheets)	(ale

Table A. T. Const.

										4 4 4	ca. Pres	bertical Presents, pais at indicated (ells	at nd	Cated	6118							
	[00]	Loca					0	- 0									Febound	pun				
ACA.	Point	57	P-1	7	0,7	3	a _s tr	25	De la	.do	. O.	0,7	2°4	C2 32	gg.	-3 h	5	9g	12	7.00 .00	a	1 1
4 €	2 4 7	94.	S	7.3	15.91	5.00	4.89	75.01	8.49	6.31	10.00	2.15	8	7.53	13.84	5.3.	64.4	74.47	6.37	1.60	4.30	0
		Bu	0.00	6.96	13.8	3	9.20	0.72	8.37	6.11	15.00	8.3	0.00	8	12.71	97.9	8.80	0.18	8.23	4.40	5.34	-
		Ü	00.00	5.43	21.36	6.93	10.47	0.54	6.88	a.8	16.54	6.33	0.0	5.62	19.29	7.17	10.01	0.00	6.79	6.40	6.03	
		35	0.00	3.42	10.24	6.31	21.55	0. L	4.93	16.4	16.71	1.5	0.00	3.83	8.17	7.0	11.15	0.18	4.81	3.20	6.20	-
		b-d.	0.00	2.3	2.75 3.72	6.22	12.23	0.54	3.79	::	15.19	8.40	0.00	8:8	1.64	6.46	11.83	0.0	3.67	0.40	5.68	
		Ja.	5.62	3	2.18	4.7	8	No.39	;	60	50.53	2.97	5.62	5:	0.11	2.00	3.61	26.95	65.4	-0.70	2.3	
											rate : Sellection	6 . In	in- at indicated Gares	300								
				-			10161										Reh	Rebound				4
			of *	Q CY	a"	ດ້	ດ້	101	4	1.9	13 G		.:-	2	e e	ag ^a	25	99	17	3	3	
7 5 6	1 6 2	St.	0.010	0.10	6.725	3.025	0.03	0.010	0.003	0.000	-0.001		-c.cz6	0.10	0.013	0.009	-0.003	0.021	0.00%	0.000	0.00	69
		lo.	0.027	0.0	0.028	0.034	0.01	0.007	0.0%	0.000	0.001		0.001	0.087	0.016	0.002	0.000	0.018	0.005	0.000	0.003	- 853
		12	0.0%0	C	0.000	0.047	0.33	D. ON.	0.00%	0.000	0.003		0.03	0.0%	0.018	0.035	0.016	0.015	0.005	0.000	0.0	40
		×	0.103	0.0	0.018	0.0.0		0.001	3	0.000	0.30		0.0	0.047	0.016	0.053	0.031	0.012	7.005	0.000	0.009	60
		6-4	0.128		0.042 0.025	0.000	0.05	0.001	0.003	000.0	0.010		0.135	0.043	0.03	0.078	0.048	0.012	0.004	0.000	0.012	- iOM
		ler.	0.13		0.00 7.052 7.057 0.053	196 6	0.053	0.013	2,303	0,000	0.35		0.158	0.0	0.00	0.045	0.00	000	0 000	0000	0 00	

Table Als (Contimed)

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		-	30.08		1.32	1.79	0.29	74.12	5.16	0.20	2.73	0.30	45.33	8.4	0.00	1.67	-0.10	73.74	5.16	0.00	1.55	0.50
1,100 1,10	1,100 6,38 16,77 1,39 2,48 0,37 6,48 3,48	and .			5.01	2.53	0.88	0.13	8.9	2.50	2.59	0.53	7.83	5.43	3.70	2.51	67.0	-0.19	86.9	1.30	2.41	6.51
13.05 5.66 17.21 17.21 17.21 17.22 17.24 17.25 17.24 17.25 17.24 17.25	13.05 5.66 17.21 1.15 3.12 24.34 3.56 4.31 3.16 27.35 7.14 13.15 5.56 4.31 3.15 5.66 7.14 13.15 5.16 5	C			16.77	3.8	8	0.37	8.18	5.20	3.72	2	8.03	29.0	15.46	3.63	1.66	8.0	6.48	2.00	8,0	3.12
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13.56 1.35 22.11 6.82 10.27 0.135 1.38 5.24 6.72 1.31 0.28 5.45 2.45 5.45 2.45 5.4	11-166 1-13 22-111 6-18 10-27 0-13 1-18 5-12 1-19 0-18 5-13 0-18 1-19 0-18 5-13 0-18 5-13 0-18 5-13 0-18 5-13 0-18 5-13 0-18 5-13 0-18 5-13 0-18 5-13 0-18 5-13 0-18 5-13 0-18 5-13 0-18 5-13 0-18 0-18 5-13 0-18 0-18 0-18 0-18 0-18 0-18 0-18 0-18	B ₄			13.07	6.20	3.70	0.37	8.83	8.	5.5	5-73	0.80	7.14	2.2	8.0	F.31	00.0	8.83	4.70	5.77	5.73
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13.46 2.67 2.01 2.14 13.15 0.37 3.14 2.04 5.24 6.24 0.05 2.04 2.05 1.25 1.25 0.05 2.04	13146 2.67 2.04 1312 0.31 3.78 0.40 6.38 8.88 1.00 2.99 1.39 6.62 12.71 0.00 3.78 0.80 1.31 0.20 3.78 0.20	2			9.80	8.0	11.83	0.29	*.93	000	5.61	3.8	0.80	8.	6.49	6.82	33.44	-0.19	4.93	3.10	6.63	8
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1.0 kg 1.5 kg 1	10-84 1.58 1.59 1.50	۵,	-13.66		0.76	5.38	0.31	0.00	3.78	03.0-	2.6	6.24	0.80	2.8	-0.55	5.38	8.2	-0.37	3-78	-0.80	5.42	6.14
10.04 1.58 1.58 1.58 1.56 2.16 5.94 6.15 6.15 6.15 1.58 2.13 6.15	10.04 4.15 1.1	34,	19.6		0.55	8	4.20	24.45	5.6	-0.70	2.00	8.0	24.30	8.	-0.66	32	3.82	12.87	30:00	-0.30	4.82	3.07
1,11, 1,15 1,15 1,10	14-14-6 6-28 1-14-0 5-15 1-14-0 1-14	ы	10.8		1.52	3000	2.6	26.65	6.19	-0.40	4.83	2.0	25.30	380.4	0.23	1.54	6	59.54	6.19	-0.60	4.65	1.6
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	11.1.16 6.25 11.1.10 5.02 2.05 0.00 3.37 1.10 5.07 1.00 6.57 11.20 1.10	7			3.70	80-7	2.03	2.55	gr. o	0.50	4.83	5.53	0.00	E * * 2	2.39	.5.5	3:6	2.18	8:3	0.40	4.65	1.23
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Part Part	3%	-14.46		14.60	5.08	5.03	00.00	3.37	99.	5.17	1.08	0.0	6.14	13.20	8.	1.66	-0.37	8.37	1.40	8: 3	8:8
3. b 5. 5. 6. 5. 6. 5. 6. </td <td> 1, </td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>Ver</td> <td>. Torr</td> <td>:Dection</td> <td>10.</td> <td>. naice</td> <td>ed 345e</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td></td>	1,								Ver	. Torr	:Dection	10.	. naice	ed 345e							-	
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	×	0.0	3.15	3.15 -0.14		7.50	-0.72	4.93	-1.60	5.17	3.18	0.00	3.34	69.0	93.	7.2	0.19	7.93	0.41	5.17	3.28
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	EE:	0.160	0.00	0 0.045	0.242	0.00	0.020	6.323	00000	0.019		0.148	0.035	0.029	0.121	0.051	0.024	0.010	0000	0.016	
	н	0.19	3 0.08	2 0.041	0.286	0.098	0.019	0.021	0.000	0.027		0.181	0.027	0.021	0.165	0.079	C-023	9000	0000	0.026	
	×	0.22	H 0.11	1 0.037	0.25	0.130	0.029	0.020	0.000	0.034		0.217	0.056	0.017	0.00	0.111	0.033	0.007	0.000	0.033	

							é			Vertic	al Press	Vertical Pressure, psi	at Indi	at Indrated Cells	118							
2	Soint Point	tion t	۵.	P2	-F	4	25	9 _d	Q.	Δ,	۵۰	P. 10	24	۵,	a,	n-I	1.5 February	- Pag	2	on on	C.	O P1
2	н	*	0.0	2.86	0.08	1.43	0.20	0.00	5.27	0.61	1.63	0.30	0.0	3.14	1.09	1.55	0.39	0.18	5.27	2.51	1.63	0-30
		A	0.0	10-4	1.41	2.15	0.59	-0.55	7.11	1 41	2.11	0.61	00.00	2.29	\$ " • 1	2.27	0.73	-0.37	7.11	(F)	2.41	0.61
		U	8.0	5.34	3.27	3.11	1.37	-7:37	8.71	1.21	3.62	1.23	0.0	5.62	3.50	3.23	1.56	-0.19	8.71	6.23	3.62	3.23
		A	5.42	5.63	3.92	3.59	2.15	-0-37	9.17	5.01	4-31	7.	5.12	16.5	8.	3.71	2.34	-0.19	5.17	6.91	2.33	3,
9	1 \$ 2	(a)	10.0	6.39	71.7	4.30	3-13	-0-37	9.63	4.41	66.7	3.17	10.04	F 37	74.4	4.12	5.3	-0.19	5.63	6.31	66-7	4.17
		ĵa,	0.0	6.39	10.67	5.26	5.28	-0.37	9.17	1.07	6.19	6.33	00.00	29.9	00.11	5.38	2-7-5	-0.19	9.17	5.91	6.19	6.2
		Ö	0.00	5.95	22.87	5.86	7.24	-0.37	7.22	5.11	6.98	7.89	0.0	5.33	22.20	8.	7.43	-0.19	7.22	7.01	6.98	7-89
		H	8.0	3.43	11.33	5.98	86.6	-0.18	5.0	3.2	7.06	8.40	8.0	3.71	11.68	6.10	10.17	0.30	4	5.11	7.06	00 01
		н	0.00	2.39	2.83	5.50	12.91	-0.18	3.67	-0.20	6.54	9.55	0.0	2.67	5:10	5.62	13.10	00.0	3.67	1.70	2.5	9.22
5	н	43	00.00	5.29	0.97	2.78	8.25	-0.37	3.67	1.20	5.68	-2 -1 9	?	2.57	1.20	8	17.80	-0.19	3.67	0.70	5.68	6.24
9 8	12 13	×	00.0	8.8	0.65	10.1	3.62	-0-37	5.27	8	66.7	2.87	0.0	3.24	85.	4.19	3.81	-0.19	5.27	06.0	66-7	2.87
2	М	ы	0.00	3.62	0.76	10.4	5-4-5	-0.37	6.30	-0.40	1.82	1-7-	0.00	86.5	3	07.7	2.64	-0.19	6.30	1.50	4.82	1.77
		×	0.0	2	1.31	3.95	1.76	-0-37	7.22	0.61	7.82	1.23	00.0	671-7	1.0	70.4	1.95	-0.10	7.22	2.5	1.82	1.23
		17	0.00	5-34	3.70	7.30	1.57	-0.55	8.71	3.41	2.17	21.1	00.0	5.62	1. C3	27.7	2.76	(A) (A)	8.71	5.31	5.17	25.
																٠						
							Total		÷.	rtical De	flection	Pertical Deflection, in., at Indicated Gages	Indicat	ed Gages			barrada.					
			r G	20	Da	T _G	DS	1	L _Q	Pa	e e		$^{D}_{1}$	20	(⁷)	a ^z	ď		. ;	*30 ao	0	
2	н	*	-0.005	0.101	0.014	0.003	-0.002	0.034	0.004	00000	0.002		C. 324	0.006	0.000	-0. 333	0.080	0.050	0.002	000.3	-0.007	
		ø	-0.00-	0.127	0.022	0.011	000.0		0.00	0.000	-0.002		0.025	0.122	0.008	0.00	0.026	0.000	0.30E	0,000	-0.007	
		O	0.001	0.158	0.034	0.028	0.004		0.010	00000	000.0		0.030	0.153	0.020	-0.008	-0.022	0.0%	0.038	0.000	-0.50	
		A	0.005	0.193	0.042	0.045	0.008		0.012	0.000	0.001		0.031	0.188	0.026	0.000	0.018	0.073	0.010	0.000	-0.00	
5	1 \$ 2	[6]	0.011	0.213	0.048	0.066	0.013	0.074	0.014	00000	0.003		0.0.0	0.206	0.034	0.030	- 0.013	0.075	0.012	0.000	-0.005	
		ßı,	0.031	0.156	0.055	0.119	0.029		0.017	0.000	600.0		0.000	0.151	140°0	0.830	0.003	0.053	0.015	0.000	9.00%	
		15	0.084	0.103	0.057	0.152	0.056		0.017	000.0	0.017		0.093	960.0	0.43	3.116	0.030	0.0.7	0.015	0.000	0.012	
		ini	0.112	0.073	0.052	0.182	0.088		0.016	0.000	0.026		0.141	0.068	200	0.146	.000	0.036	0.014	0.000	0.021	
		н	0.150	0.062	0.0	0.527	0.118		0.013	0.000	0.037		0.179	0.057	0.025	0.191	0.092	0.031	0.01	0.000	0.032	
2	e4	ט	0.175	0.077	0.035	0.194	0.146		0.011	0.000	0.040		2.204	0.072	0.022	0.158	0.120	C-035	0.009	0000-0	0.00%	
9	1 4 2	×	0.190	o.n5	0.035	0.137	0.157	0.044	0.009	0.000	0.05		0.219	0.110	0.021	0.101	0.131	0.045	0.007	0.000	0.000	
10	н	ы	5.176	0.132	0.037	711-0	0.151		0.011	0.000	0.052		0.205	0.127	0.023	0.078	0.125	0.03	0.000	0000	0.047	
		×	0.148	0.143	0.040	0.098	0.137		0.01	0000-0	0.048		0.177	0.138	0.026	0.33	77.	1000	0.009	0000:0	0.043	
		12	960.0	0.162	0.046	0.087	0.105		0.013	0.000	0.037		0.165	0.157	0.032	0.062	0.079	222	0.011	0.000	2.0.0	
											-											

2. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	
6.82 6.92 6.92 7.73	2.003 2.003 4.00.0 2.003 2.003 2.003 2.003 2.003
3.60 6.81 1.00 1.00	L'8 0.000 0.000 0.000 0.000 0.000
8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	0.00% 0.00% 0.013 0.016 0.016
111.61 0.18 0.18 0.18	0.143
7.72 C	0.012 0.030 0.030 0.030
25.5 20.5 20.5 20.5 20.6 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	0.032 0.032 0.118 0.118 0.158
2.61 7.4, 13.50 5.20 1.63	0.043 0.043 0.043 0.023 0.023
5.2. 5.3. 4.4.8 3.2. 2.18 2.18	2 0.170 0.170 0.052 0.021 0.031 0.031
P ₁ 0.20 0.20 0.20 0.20 0.20 0.20	1. Indica -0.0% -0.0% -0.0% 0.077 0.110
Partical Pressure, psi, 1 Indicated Calls Partical Pa	Description In. at Indicated Gross Description 0.1 0.2 1 0.000 0.008 0.006 0.000 0.018 0.006 0.104 0.000 0.021 0.052 0.052 0.000 0.049 0.010 0.014 0.000 0.058 0.110 0.014 1 0.000 0.094 0.199 0.130
F. 1.74 6.03 6.89 6.37 6.37 6.37	2.008 0.018 0.031 0.039 0.038
7.91 7.71 11.12 7.31 3.31 2.71	DB DB 0.000
7.3 9.06 7.34 5.04 3.67 4.81	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
112.52 11.09 11.09 11.09 0.07 67.91	0.195 0.145 0.110 0.089 0.082 0.082
2.75 2.75 2.74 6.94 9.39	Detal D ₅ 0.017 0.039 0.017 0.117
P ₃ P ₄ 2.29 3.35 7.08 4.19 13.18 4.66 5.88 4.78 1.31 4.42 0.01 3.35	23 E ₁ 0.019 -0.035 0.027 0.025 0.029 0.051 0.024 0.073 0.015 0.038
2.29 7.08 13.18 5.88 1.31 0.01	0.019 0.027 0.027 0.029 0.015 0.005
2.57 4.67 4.67 3.81 2.57 1.81 1.81	0.256 0.190 0.138 0.107 0.107 0.216
9.50 0.00 0.20 0.20 0.20	0.017 0.047 0.207 0.207 0.205
Talon Edon	ध भ स स स
Point 1	н
8 9	v

							1	1		Verci	AL Pres	Sure, per	out 18	Deres C	877		Baker	,				1
Row	Point a	tion tion	I La	2	F 3	d'	25	9	17	P8	40	P10	4	20	A.	P. P.	Pe Pe	Pe	P	88	00	Plo
1	1	M	00.00	1.81	-0.04	1.32	-0.20	-0.91	5.39	0.20	2.07	0.41	0.00	2.28	1.09	1.1	64.0	-0.55	5.50	8:1	2.41	19.0
		S	0.00	2.58	0.30	1.91	0.20	0.73	7.00	0.50	3.00	1.03	0.0	3.05	1.53	2.03	68.0	3.09	7.11	2.20	3.36	1.23
		Q	6.63	2.36	0.33	2.15	0.59	40.79	7.57	0.30	3.53	1.1	6.63	3.43	1.86	2.27	1.28	41.15	7.68	2.00	3.87	1 64
7 8 9	1 8 2	(m)	0.00	2.86	0.44	2.39	0.78	55.72	8.03	0.30	4.8	5.8	0.0	3-33	1.97	2.51	1.47	\$6.08	8.1	5.00	4.39	2.2
		fh.	0.00	5.98	96.0	2.99	1.56	-0.18	8.14	3.00	2.00	3.79	00.0	3.43	2.51	3.11	2.2	0.18	8.3	4.70	5.34	3.99
		O	0.00	2.48	1.09	3-35	2.35	-0.18	6.54	7.31	69.5	5-33	0.00	2.9	2.62	3.47	3.04	0.18	6.65	10.6	6.03	5.53
		H	0.00	1.81	0.22	3-35	3.13	-0.18	4.59	3.70	5.86	7.58	0.00	2.28	1.73	3.47	3.82	0.18	4.70	5.40	6.20	7.78
		н	0.00	1.34	-0.65	3.12	3.52	-0.18	3.21	-0.10	5.43	10.25	0.00	1.81	0.88	3-23	12.4	0.18	3.32	1.60	5.77	10.45
1	1	ח	00.00	1.15	-0.87	2.87	2-35	-0.36	2.98	-1.30	47.4	7.89	0.00	1.62	99.0	5.99	3.0	00.00	3.09	09.0	5.08	7.89
7 4 9	1 & 2	M	00.00	1.53	-0.87	2.51	96.0	-0.55	4.00	-0.80	41.4	3.49	0.00	2.00	99.0	2.63	1.67	-0.19	4.13	0.9	P.148	3.69
-	н	ы	00.00	1.72	-0.87	2-39	0.59	-0.73	1.70	-0.70	3.8	2.26	0.00	5.19	99.0	2.51	1.28	-0-37	18.4	1.00	4.30	2.46
		×	0.0	2.10	-0.65	2.51	0.29	-0.73	5.39	-0.30	3.88	1.64	00.3	2.57	0.88	2.63	96.0	-0.37	5.50	1.40	4.22	1.8
		315	0.00	2.67	-0-33	2.63	0.20	-0.73	6.88	0.50	4.10	1.23	0.00	3.14	1.20	2.73	0.89	-0.37	6.93	2.20	4.48	3.43
					7																	
							1000		Ve	Vertical Deflection	Dection	1n.	at Indicated	ed Care	10							
			6	c	c	d	10201	c	4	c	-		6	c	c	-	eponno	-		4	1	
			4	2	4	3	2	9	2	œ	0		24	C	er G	3	2	9	2	8	60	
-	н	•	-0.00	991.0	0.035	0.013	-0.001	0.153	0.000	0.300	-0.001		0.058	0.205	0.023	-0.013	-0.024	0.128	0.000	00000	-0.029	
		U	-0.003	0.171	0.052	0.039		0.185	0.030	0000	0.00		0.062	0.230	0.000	0.013	-0.018	0.160	6.019	00000	-0.024	
		a	00000	0.210	0.061	0.063		0.218	0.036	00000	0.000		0.065	0.249	0.049	0.037	0.012	0.193	0.025	0.000	-0.020	
7 4 9	1 & 2	[k]	0.004	0.213	0.00	0.092		0.234	0.001	0000	0.013		0.069	0.252	0.056	0.066	-0.006	0.209	-0.010	00000	-0.315	
		p _q	0.020	741.0	0.077	0.172		0.169	0.048	00000	0.031		0.085	0.186	0.065	0.146	0.018	0.144	0.037	00000	0.003	
		O	0.040	0.088	0.079	0.212		0.117	0.051	00000	0.057		0.105	0.127	290.0	0.186	0.058	260.0	0.0.0	0.000	0.020	
		te	0.064	0.000	0.070	0.241		0.087	970.0	00000	0.089		0.129	0.089	0.058	0.215	0.107	0.052	0.035	00000	0.061	
		н	0.093	0.043	0.055	0.272		0.078	0.038	00000	0.118		0.158	0.082	0.043	0.246	0.145	0.053	0.007	0.000	0.000	
1	per	4	0.129	0.068	0.045	0.230		0.09	0.032	0.000	0.142		0.194	0.107	0.033	0.204	0.172	690.0	0.001	00000	0.11	
1 29	1 4 2	×	0.203	0.141	0.044	0.152		0.142	0.031	00000	0.153		5.268	0.190	0.032	0.126	0.179	0.117	0.000	0000	0.125	
1	7	ы	0.186	0.164	9700	0.126		0.159	0.032	0.000	0.11.8		0.251	0.203	0.034	0.100	0.170	0.134	0.021	00000	0.120	
		×	0.143	0.176	0.050	0.137		0.170	0.03	00000	0.136		0.208	0.215	0.038	0.081	0.151	0.145	.003	00000	0.108	
		35	0.073	0.191	0.062	0.000		0.191	0.041	00000	0.104		0.138	0.230	0.050	0.069	0.106	0.166	0.030	00000	0.076	

(8 of 11 sheets)

Table A15(Continued)

										Verti	nal Pres	Vertical Pressure, ref. at		Transmitted for	1130							
	Tond	1000					-	Total									Pehor	hound				1
NOW.	Point	tion	4	P2	م	d. 2	35	P6	P7	PB	o,	Pro	pet He	20	a,(*	-3 See	D. C	9	P7	" ac	P.	10
8 % 10	H 5	(m)	00.00	2.33	0.55	1.79	67.0	93.95	7.57	1.50	6,7	1.64	0.00	2.67	1.31	2.03	90.0	93.59	7.46	0.80	3.97	38.
		€a.e	0.00	2.38	8	2.27	0.08	1.09	7.57	07.7	7.56	2.87	2.30	2.67	1.9.E	2.53	1 1	0.73	7.46	3.60	47.74	3.07
		e	0.00	5.00	0.98	2.51	1.56	0.91	6.08	8.81	5.15	4.31	0.00	2.30	1.7	5.3	2.15	0.55	5.37	8.01	5.34	1.52
		bt	0.0	1.52	7,47	2.51	5.02	0.73	4.36	7.80	5.34	92.9	0.00	1.81	1.20	2.73	2.54	0.37	80	4.00	5.52	6.9
		н	0.0	1.14	0.8	2.39	2.15	0.73	3.21	1.60	76.7	9-33	0.00	1.43	92.0	2.63	2.6	0.37	3.20	0.80	5.8	60.00
		345	00.0	1.33	-0.21	2.03	69.0	0.36	3.67	1.20	3.96	3.49	0.0	1.62	0.55	2.27	1.18	9.0	3.56	0,40	41.4	3.69
									Ver	tical De	- Tection	Vertical Deflection, in., at Indicated Gages	t Indicat	ed Gages	-							
							Total									of.	ebound					
			I _G	D2	23	Dr	25	9 _a	Lg	DB	Do		D.	202	r ₂	దే	De.	26	27	Ba	0	
8 & 10	4 4	\$e3	0.00	0.274	0.0.6	0.07	0.016	0.270	0.036	0.000	0.01		-0.037	0.252	0.042	0.057	0.001	0.226	0.030	0.000	0.000	
		fkq	0.006	0.222	0.03	0.130	0.034	0.219	0.0.2	0.000	C.031		.0.027	002.0	0.040	0.113	0.029	0.176	0.036	000	0.006	
		U	0.033	0.161	960.0	0.165		0.163	0.045	0.00	0.062		-0.100	0.139	0.052	0.148	0.000	c.121	0.039	0.000	0.043	
		112	0.052	0.128	0.050	0.190		0.134	0.041		8		0.000	0.100	0.0	0.173	0.10	0.092	0.035	0.000	0.061	
		н	0.077	0.118	0.039	0.221	0.155	0.125	0.033	0.000	0.125		C.034	0.00	0.035	0.20	0.140	0.084	0.028	0.000	0.110	
		act	0.252	3.226	0.032	0.126		0.218	0.020	0.000	0.145		0.200	0.204	0.008	0.111	0,166	0.176	83.	0.000	0.130	

Table A15 (Continued)

1										Vert	cal Pres	aure, psi	at ind	Cated Co	2115							
	Tons	Torse					64	otal									Febo	pun				
Row	Point	tion	۵,	۵.	-m	۵.,	2	9	7	89	۵	P.10	۵,7	d.	a,	side play	2	a.	F	ec .	من	P.
7 \$ 11	5 4 2	m	0.0	1.43	0.98	0.9	0.49	-0.18	3.79	0.10	1.55	0.20	00.00	1.43	0.22	1.08	0.39	0.0	1.36	2.41	3.80	0.6
		U	8.0	1.72	1.20	1.2	0.59	-0.36	4.93	0.80	2.42	0.61	3.0	1.72	77.0	1.32	0.39	-0.18	5.50	2.83	2.76	1.0
		A	0.00	1.81	8	1.32	69.0	0.00	5.39	0.80	2.57	0.9	0.0	1.81	0.11	1.44	0.49	0.18	8.	2.81	3.0	1.3
π'6'2	2,1,2	[n]	8.0	1.9	92.0	1.58	0.58	0.55	6.42	1.71	3-36	1.23	0.0	2.30	1.09	1.68	0.68	0.0	6.54	1.61	3.44	17.1
		(to	0.0	1.81	0.98	1.91	0.88	0.18	6.12	3.91	4.22	2.3	0.0	1.91	1.31	1.93	96.0	-0-37	5-54	3.81	4.30	2.46
		O	8.0	1.62	8.0	2.15	1.17	0.18	5.33	5.91	72-7	3.48	0.00	1.72	1.32	2.15	1.27	-0.37	5.51	5.81	4.82	3.6
		31;	0.0	1.23	0.54	2.15	1.46	0.36	3.90	3.11		5.53	0.00	1.33	0.87	2.15	1.56	-0.19	8.4	3.01	16.4	5.6
		н	0.00	1.0	0.35	2.03	1.37	0.18	2.98	1.21	1.57	7.37	8.0	1.14	0.65	2.03	1.17	-0.37	3.10	1.11	4.65	7.58
		7	8.0	1.0	0.10	1.91	0.98	0.18	2.75	0.71	3.99	5.12	0.0	1.14	0.43	1.91	1.08	37	2.87	0.61	10.4	5.3
		×	0.0	1.33	0.10	1.80	0.58	0.18	3.21	0.71	3.53	2.87	0.00	1.43	0.43	1.80	93.0	-0.37	3-33	0.61	3.61	3.0
187	2 \$ 2	ы	0.0	1.53	٥ چ	1.68	69.0	-0.36	3.33	-0.50	3.10	1.6	0.0	1.53	0.22	1.80	0.49	0.18	3.90	1.51	3.44	8.0
		×	8.0	1.91	1.09	1.58	0.59	-0.35	20.4	-0.50	3.10	1.12	8.0	1.81	0.33	1.80	0.39	-0.18	65.4	1.81	3.54	1.5
		×	0.00	2.10	1.42	1.91	0.59	-0.36	5.16	00.00	3.28	0.82	0.00	2.10	99.0	2.03	0.39	-0.18	5-73	2.01	3.62	1.2
						-			5	Vertical Pa	Total and then	ţ	1 Tr. 46 C.	60		İ					1	
							Total										ebour d				-	
			r _Q	20	3	ล้	d a	99	DZ	Da	0		4	29	a ^r	ดี	es.	90	22	80 2	2	
7411	2 \$ 2	A	-0.008	0.213	0.023	0.008	-0.003	0.192	0.021	0.000	0.000		0.010	0.00	0.01	-0.006	-0.031	0.104	0.011	0.000	-0.05	
		U	-0.00	0.257	0.038	980	0.003	0.219	0.033	0.000	0.00		0.03	0.108	0.020	-0.008	-0.005	0.131	0.003	0.00	-0.021	
		n	-0.00	0.308	0.0	0.00	0.98	0.244	0.038	0.000	0.010		0.014	0.159	0.035	0.00	-0.022	0.156	0.026	0.00	-0.027	
7,9,11	2,1,2	(a)	0.00	0.252	0.049	690.0	0.014	0.26	0.041	0.000	0.015		-0.021	0.209	0.0.8	950.0	0.008	0.174	0.039	0000	0.01	
		(in _e	0.014	0.169	0.058	0.135	0.037	0.152	2.0.0	0.000	0.039		110.0-	0.126	0.057	0.122	0.03	0.110	0.045	0.000	5.035	
		o	0.00	0.116	0.059	0.164	0.074	0.105	0.018	0.000	0.07		0.005	0.073	0.058	0.151	0.06	0.063	0.0.6	0.000	0.070	
		201	0.044	0.005	2.052	0.193	0.116	0.075	0.043	0.000	0.109		0.019	0.042	0.051	0.130	0.110	0.033	0.041	0.000	0.105	
		н	0.065	9.0.0	0.041	0.227	0.145	0.059	0.035	0.000	0.133		0.000	0.033	0.0.0	0.21	0.139	0.007	0.033	0.000	0.129	
		ы	0.00	0.00	0.042	0.131	0.172	0.098	0.028	0.000	0.151		0.071	0.053	0.041	0.168	0.166	950.0	0.0	0.000	0.147	
		×	0.139	0.173	0.031	0.127	0.180	0.174	0.028	0.000	0.153		0.114	0.130	0.030	0.11k	0.174	0.132	900.0	0.000	0.149	
7411	2 \$ 2	ы	0.101	0.285	0.035	0.110	0.174	0.240	0.033	0.000	0.151		0.119	0.136	0.006	920.0	0.146	0.152	0.023	0.00	0.126	
		×	0.031	0.280	0.038	0.005	0.155	0.236	0.035	0.000	-136		0.099	0.131	0.029	0.058	jar.c	0.148	0.005	0.000	0.100	
		F .	0.043	0.313	0.050	0.080	0.108	0.251	0.045	0.000	0.00		0.001	0.164	0.041	970.0	0.080	0.163	0.035	0.000	0.072	

										Vertical	2	ressure, poi	at Ind	cated C	:11:							
	Lond	Loca-	0	Q	-	6		otal									Rebou	and				
Nov	100	tion	:	63		2	rich ich	20	7	80	6,	or pri	a, ^{ct}	F2	g,	n-2	giri Ba	200	D.	P8 .	D,	230
3 4 10	2 & 1	Sed	-0.20	1.62	1.52	1.30	0.88	-0.55	5.16	1.2	28.0	1,03	00.00	8 8.0	0 13		02.0	70.0	1		1	
		ß	000		. 63	11.		1				0	3	7.70	0.483	77.5	0.04	9,00	0.50	10.	3.00	3.400
		te		1.03	F-03	1	0	-0.37	5.28	1.81	3.6	1.6	0.0	2.43	0.5	2.44	69.0	-0.18	5.62	4.61	3.69	8
		0		1.34	1.63	88	12.27	00.00	97	2.21	8	2.46	0.00	To The	0.54	0,0	90	0.30	Bo	1		100
		tet	-C-20	1.14	-	60	1.27	0.0	10 6	6	1 00	8	8	3				7	30.00	1	2000	10.2
			8		1				1	41.0	5	2	3	1.04	0.35	100	0	0.19	3.55	3.51	23.4	4.32
		4		5	1.35	8	1.27	0.00	2.41	-0.30	3.79	8.	800	0.95	0.55	1.68	0.00	0.30	2,78	03 6	200	6 6 2
		×	-0.20	1.33	1-33	4	0.78	0.0	2.6	-0.80	3.01	26.	00.00	8	8	1 77	0 10	0,00	900	200	10.0	2.23
																	2	NA.	200	00.7	3-18	8.8
						1																
						-			Ve	rtical D	Vertical Deflection, in.,	-	at Indicated Gages	ed Gages							1	
					-		Coral									1	aponno				-	
			4	2	ar.	T _I	o"	90	ا ا	88	000		្ន	S A	E S	ď	Sa	90	Dy	(A)	200	
& 10 S	1 4 1	44	-0.002	0.169	0.046	0.056	0.01	9,158	0.045	0.000	0.018		0.034	0.218	0.043	Aco. o	0.03	00.0	O COMPS	1	1	
		fa,	0.00	0.113	0.053	0.100	0.007	0.119	0.083	0.00	950		2	200	0			100	25000	30.0	53.5	
		c	200	0	2000	000					2000		2	0.100	0.0	0000	0.0	0.158	0.043	0.000	0.023	
		3 }	-	6000	0000	1010	50.0		0.0	0000	C. 774		0.050	0.108	0.051	911.0	0.0	0.111	0.045	0.000	0.059	
		71		0000	0.050	0.176	0.100	-	0.047	3,0	0.126		0.000	0.00	0.045	0.158	0.00	0.079	0.030	0.000	0.100	
		ы	0.045	0.014	0.039	0.217	0.014 0.039 0.217 0.131	0.035	0.038	0.000	0.143		0.081	0.00	0.034	0.190	0.121	0.07	0.030	0.000	0.158	
		M	0.074	0.075	0.030	0.112	0.168	0.122	0.032	0000	7.157		0.1.0	3.124	0.00	0.00%	0 36.R	0.363	- word		21.0	
													-	-	-	10000	うくせき	TOTAL	2000	35.0	O. Lake	

(Crats

Table A15(Concluded)

										Verri	nal Press	Vereinal Pressure: Total	at Indicated Cells	Cated C	118							1
							F	Total									Febru	pur				
8	Point	tion	ا ا	P2	4	4	o _f C	94 25	7	о 80	0	O Liu	۵,۲	20	7.	2,7	مرد	9g	E-	, ap	20	20
-	7	•	0.20	6.0	2.01	0.72	0.79	61.0	5.36	0.50	1.29	0.10	0.00	92.0	0.33	0.72	0.20	0.37	3.21	1.50	1.46	0.6
		ပ	0.50	1.15	1.96	9.0	0.88	-0.18	3-55	0.50	1.81	0.32	0.00	8.0	0.22	2.0	0.53	9.0	3.90	1.80	1.98	0.82
		a	8.0	1	1.96	96.0	0.98	•	10.4	0.80	2.15	0.51	-0.20	8.0	0.55	8.0	50.0	8.0	4-36	2.10	8.3	8:
		(A)	8.0	1.2	1.9	800	0.98	-0.13	4.24	3.1	2.32	0.61	-0.20	1.63	0.55	8	0.39	0.00	4.59	2.30	6*	1.12
		See.	0.50	1.2	1.96	1.30	1.18	0.00	12.4	1.40	2.93	1.23	00.00	1.03	0.55	1.20	65.0	91.0	4.59	2.70	e é	1.7
		0	0.20	1.14	1.96	1.32	1.27	0.19	3.55	1.40	3.27	1.87	0.30	8.0	0.22	1.32	800	0.37	3.8	2.70	4.E	2.30
		25	0.20	8.0	1.85	1.32	1.37	0.19	2.63	09.0	3.36	2.56	00.00	0.76	0.11	1.32	0.78	0.37	24	8.1	3.53	3.07
		н	0.00	8.0	1.74	2.3	1.37	0.19	1.9	0.10	3.19	3.07	-0.30	0.76	0.0	1.3	0.78	0.37	2.29	1.40	3-36	3.58
		13	0.00	1.05	1.74	1.20	1.13	0.19	8	-0.10	2.8	2.35	-0.20	0.86	00.00	1:3	0.59	0.37	2.30	1.30	3.0	2.86
		×	0.00	1.34	1.85	1.20	0.08	0.19	2.29	-0.50	2.67	1.33	-0.20	2.25	0.11	1.20	0.39	0.37	2.6	1.10	2.8	1.84
		ы	0.0	1.53	1.96	1.32	0.38	0.19	2.03	0.00	2.50	1.00	-0.20	1.34	0.22	1.32	0.29	0.37	5.98	1.30	2.67	1.53
		×	0.20	1.72	2.18	1.32	62.0	0.19	3.09	0.10	2.50	0.71	8.0	1.53	0.44	1.32	0.20	0.37	3.14	1.10	2.67	1.8
		>:	0.00	1.91	2.61	1.56	0.98	-0.18	3.78	0.10	2.67	19.0	-0.20	1.72	0.87	1.56	0.39	0.00	1.13	1.70	2.8	1.12
									Ve	tion! le	Vertical Seffection,	l In.	t Indicat	Indicated Gares								
							Total									-	ebound					
			e ^{rt}	2	a.	2	50	39	La	89	c a		ດີ	25	64	10	ŭ.	92	4	66	0	
-	н	•	-0.009	0.102	0.017	0.005	-0.003	0.176	0.023	0.000	0.000	* ,	0.013	0.103	C.01	00000	-0.000	0.132	0.005	0.000	-0.018	
		O	-0.008	0.141	0.028	0.015	0.000	0.197	0.035	0.000	0.00		0.014	0.142	0.005	0.010	-0.006	0.203	0.007	000 0	-0.02h	
		c		2000	, w	*	300	0.00	0.00	0	0000		7000		000	0	0	0000	0	0.0	0000	

							-	TICKET	tection in-	TEL TROPECE	C 600 C							
					Total									hebound				
	es es	2	<u>م</u>	Sa.	⁵ a ⁷ e ⁶ a ² a ⁷ a	29	70	80	o o	ດີ	2	C.	ď	est.	26	ra r	8	30
•	-0.009	0.100	0.017	0.005	-0.003	0.176	0.083	0.000	0.000	0.013	0.103	2.01	00000	0.000 -0.000	0.132	0.005	0.000 -0.018	-0.018
ņ	-0.008	0.141	0.028	0.025	0.000	.197	0.035	0.000	0.004	0.014	0.142	0.005	0.010	-0.006	0.203	0.007	000	-0.02 h
Ω	-0.00	0.205	0.034	0.026	0.00	.23	0.042	0.000	0.000	0.016	0.20	0.031	0.001	200.0-	0.219	0.03	0.000	-0.03
(m)	-0.005	0.248	0.041	0.039	0.007	.214	0.043	0.000	0.016	0.017	0.249	0.038	750.0	0.001	0.220	0.040	00000	-0.002
jh,	0.000	0.170	0.048	0.071	0.002	3.144	0.95	00000	0.00	0.002	0.171	0.04	20.0	0.016	0.170	0.046	0.000	0.00
U	0.008	0.116	0.00	0.100	0.045	3112	0.055	0.000	0.076	0.030	0.117	0.0L?	0.00	0.039	0.118	0.047	000.0	0.058
202	0.000	0.082	0.045	0.152	0.079	3.076	0.0.9	0.000	0.118	0.042	0.063	0.0.2	0.147	0.073	0.082	0.041	0.00	0.10
н	0.034	0.000	0.034	0.20	0.111	.m.	0.040	0.03	0.147	0.056	0.07	0.031	0.190	0.10	0.07	0.032	0.000	3
1 79	0.049	0.079	0.007	0.167	0.141	0.100	0.033	00000	0.165	0.073	0.080	.00	0.152	0.135	0.100	0.025	0.000	0.1.7
345	0.057	0.104	0.003	0.109	0.157	0.159	0.032	0.000	0.166	5.079	0.10	0.022	0.10%	0.151	57.00	28.0	0.000	0.346
ы	0.034	0.118	0.026	0.085	0.152	.183	0.033	0.000	0.158	3.376	0.119	0.003	080.0	0.146	0.189	0.005	0.000	24. 25
> :	0.01	0.131	0.00	0.068	0.134	.193	0.036	0.000 0.140	0.140	6.0.3	0.132	0.026	0.063	0.128	0.100	920.0	0.000	0.122
y.	0.031	0.157	0.035	0.058	0.101	206	0.0	0.000	0.100	0.053	6-11-9	0.032	0.03	0.00%	0.212	6.036	0.000	0

Table 4-16

Paltiple-Wheel Heav, Jear Load Flexible Pavement Test, Dynami: Instrumentation Loading Data

Item 3; Load Condition: 30 kips, Single Wheel, 100 psi

		Miles Inches			Ve	rtical Pr	ressure, p	si, at Indica	sted Cells					
		For	ruard, Av	g Speed -	3.40 mph				. Be	verse, Av		2.90 mph		
Row	Position	Location		P2		-	15	Position	Location	1,	P ₂	P3	P4	15
5	0	184	-1.61	-0.14	-2.10	et .24	**	0	128	**	0.03	**	0.02	**
	1	168	44.1	-0.15	-2.12	-0.23	**	1	10E	0.05	0.06	**	0.02	**
		148	k1, 00	-0.10	-2.12	+0.25	**	5.1	BE	1011-1511	. 08	**	0.02	
		128	-1.60	-0.38	-2.10	-0.24	**		6E	1 50	743	**	0.03	
		TCE	-1.75	-0.07	-2.10	-0.23	**	19.0	4E	0,46	0 19	0.05	0.06	
		ØE .	-1.65	-0.05	-2.10	-0.22			2E	0.46	0.24	0.02	0.10	
	100	68	+1.50	0.01	-2.20	-0.20	**	100	A	0.40	0.33	0.46	0.18	**
		4E	-1-35	0.08	-2.05	-0.16	**	100	В .	0.52	0.43	0.14	0.22	**
		28	-1.45	0.13	-1.90	-0.11	**		C D	1.10	0.56	0.38	0.25	
		A	-1.95	0.22	-1.62	0.00	**		D	1.73	0.58	0.38	0.26	**
		В	-1.50	0.29	-1.88	-0.02	**		E	7.8	0.87	0.38	0.30	
	-34	c	-1.04	0.46	-2.06	0.02	**		F	·. 0	2.22	0.06	0.40	**
		D	-0.60	0.53	-2.08	0.03	**		0	Eu. 6	1.36	1.99	0.72	**
	1 4	*	-0.32	0.67	-2.08	0.07	**	100	h	2.15	1.45	11.04	1.38	
	1000		4.36	0.95	-1.92	U.16	*		1	0.60	1.26	13.30	5.06	**
		G	7.36	1.26	-1.30	0.40	**	1	3		1.00	2.80	2.14	5.90
	- 1	H	4.26	1.39	4.52	0.63	**	- 1	K	-0.22	0.70	0.50	1.54	67.40
	- 1	1	1.48	1.35	15.00	1.54	**	- 1	1	-0.28	0.99	0.18	1.25	1.10
	- 1	3	0.52	1.15	6.16	2.11	1.20	- 1	M	·O.34	0.48	0.05	1.01	**
	- 1	К	0.20	0.76	1.18	1.68	68,60	- 1	D.	-0.38	0.32	-0.14	0.60	**
	- 1	L	0.08	0.65	0.56	1.42	2.80	- 1	28	-0.38	0.17	+0.20	0.29	**
	- 1	M	0.06	0.50	0.36	1.10	0.20	- 1	land.	-0.36	0.08	-0.22	0.13	44
	- 1	N	0.04	0.35	0.14	0.66	**	•	68	-0.36	0.03	-0.22	0.05	**
		29	**	0.20	0.08	0.32	**		8×	•0.36	-	-0.25	0.02	**
		44	**	0.11	0.06	0.17	**	1 "N	100	-0, 5	**	-0.25	**	***
		6₩	**	0.08	0.05	9.98	**	1	128	-0.36	**	-0.26	**	
		a.	**	0.04	0.02	0.04		- 1	1346	-0.36	**	-0.30	**	**
		LOW	**	0.03	**	0.02		i	169	-0.36	No.	-0.30	**	**
		129		0.01			**	1	±8#	*0. 36	**	-0.30	**	**
		148	**	**	**	**	**	- 1	236	-0.36	**	≈0. 08	**	**
								1	224	-0.36		-0-26	**	**
								1	S- had	-0.36	**	-0.26	(811)	***
									268	-0.36		-0.26	~ *	**

(1 of 6 sheets)

Table Af (Contirued)

			rward, Ave		2 20 see	relead by	ARRINA' D	i at Indie	oted Cells	erse.	d Broad a	2.10 mil		
							-						Z ₀	100
Row	Position	laustica	6	7	-8	-9	10	Fosition.	Local lon	-		8	-9	10
4	Hone	128	-0.75		-1.50	-0.10	-1.50	0	176	**	0.20	••		
		106	-0.70	**	-1.50	-0.10	-1.50		Le	**	0.30	••	**	••
	Date of E	88	-0.50		-1.50	-0.10	-1.50	14.5	6E	0.25	3438		••	ne
	3210 00025	GE LE	-0.40	0.10	-1.50	**	-1.50		14E 2E	0.55	0.40	**		
	A 14		-0.25	0.10	-1.50	••	-1.50	2. 11.00			100			
		2E	-0.50	0.12	-1.50	**	-1.50	(y	A	0.40	0.4	0.30	0.10	••
		A	-0.40	0.24	-1,40	0.10	-1.50			1.90	0.50	0.30	0.20	••
			-0.50	0.40	-1.50 -1.50	0.20	-1.50 -1.50	1	D	1.35	0.70	0.28	0.30	-
		D		0.64	-1.50	0.26	-1.50			2.25	0.60	0.20	0.36	
				1272					- 7		1.00	0.24	0.50	0.50
			3.50	0.60	-1.50	0.30 V.40	-1.50 -1.50		0	7.75	1.20	0.90	0.90	0.7
		- 6	8.00	1.00	-1.60	0.80	-1.50	1.	М	4.10	1.50	4.30	1.70	3.00
		н	4.50	1,:0	1.30	1.50	-1.50	4	1	1.50	1.20	5.10	2.30	1,00
		1	1.90	1.00	5.70	2.20	-1.50	5000	3	0.10	1.10	0.70	2.56	2.50
		31	0.75	0.90	3.20	2.64	-1.00		K		0.90	-0.60	1.90	33.00
		K	0.25	0.74	0.80	2.10	31.75	1	T.		0.74	-0.60	1.50	7.00
		£	••	0.60	0.50	1.70	11.00	- 1	Mi.		0.60	-0.60	1.20	0.75
		¥		0.50	0.20	1.30	1.25	1	M. Committee		0.90	-0.60	0.70	
				0.40	0.1C	0.80	0.50		2W	8.7	0.40	-0.60	0.40	
		21		0.30	-	0.40	**	•	Aug .		0.40	-0.50	0.20	**
		440		0.20		0.20	**	.0	CM	4.5	C. 36	0.60	••	**
	1	6M	~			.16	**		84	***	0.36	≈1.60 ≈1.60	**	••
		100	••			0.10	**	170	10V 12V		0.24	40.50	***	••
		204				-			-					
								- 1	1 hav	**	0.26	-0.50		
								1	184		0.20	+ 1,50 +6,50		
								•	201		0.10	-0.50		
								0	274	••	0.20	-0 10		
								1/2"8	2111		0.16	-0. %		
								-,	264		0.24	-0.5		

	O	Tard. Av	S med -	.20 mph				Re	verse Av	Special a	2.16 mm		
Positi-u	A . AOB	D	D ⁵	D ₃	D	05	Position	Location	v_1	-18	D ₃	Di	D,
Hone	12E	-0.06k		0.001	-0.002	0.003	0	1.2E		0.001		0.901	-
	106	-0.064	0.001	0.001	-0.002	0.003	1	100	0.004	0.001	,	0.901	
	2	-0.063	0.001	0.001	-0.002	0.005		80	0.005	0.002	**	2.007	
08.4	6E	-0.063	0.001	0.002	-0.002	0.003		68	0.007	0.202	••	0.001	
	4E	-0.063	0.001	0.003	-0.001	0.003		42	0.008	0.001	••	0.302	
	21	0.063	0.001	0.003	-0.001	0.004		20	0.000	0.000	0.001	0.202	
	C.B.						17		0.01	0.003	0.001	0.003	0.
4	1000	-0.061	0.003	0.003	••	0.004	4.7	- A	0.024	0.005		0.003	0.
		-C.056	0.004	0.002		0.005		В			0.002		
	C	-0.038	0.007	0.003		0.006		C	0.043	0.007	0.003	0.003	0.
	0	0.016	0.008	0.005		0.006	1.0	D	0.087	0.008	B.JOF	0.003	0.
			0.008	0.006		0.005	1	2	0.106	0.008	0.006	0.003	0.
	7	0.051	0.006	0.010	0.301	0.005	- 1		0.005	0.006	0.010	0.004	0.
	0	0.02	0.004	0.013	0.002	0.005	- 1	0	-0.007	0.004	0.011	0.005	0.
- 1	H	0.00	0, 102	0.009	0.002	0.007			-0.012	0.002	0.008	0.006	0.
	1	0.004	0.001	0.005	0.003	0.009	- 1	1	-0.015	0.001	0.005	0.006	0.
78 7 1	1	0.00		0.003	0.003	0.013		3	-0.015	0.001	0.002	0.905	0.
		0.002		0.001	3,000	0.014			-0.015			0.004	0.
0.4	L	0.001		0.001	0.400	0.012	- 1	L	-0.015		••	U. 004	0.
		0.001	-	0.001	0.001	0.000	- 1		-0.015			0.003	0.
				••	••	3.006			-0.015			0.003	C.
7 3 0 0	2W		••	••	••	0.00%	1	24	-0.015			0.002	0.
	- 14				••	0.002		140	-0.015			0.000	0.
10 V V	611		••	••		0.901	0	68	-0.015	••		0.002	0.
	2			••		0.001	1	84	-0.015			0.002	
1	10V			••	••	••	•	100	-0.015	••		0.00	
1. 25,0							178	129	-0.015			0.002	
							1	14	-0.015			0.002	
							1	100	-0.015	••	••	0.002	
								184	-0.015	**		0.37	
							•	200	.0 705	**	••	0,002	
							0	221	-0.215			0.002	
							1/2"8	214	-0.015	**	••	0.002	
							4/4 0	264	-0.015			0.002	

* Trace of D. fairs and reading could not be made

(2 of 6 shoots)

Table A16(Continued)

		-	rward, Avy			tical Pre	ssure, pa	at indica		Au	Speed -	2.4 mph		
				1000		-	B		NA.				*	6
KOA	Position	Location	6		8	<u></u>	P ₁₀	Position	Location	P ₆		P ₈	19	10
10	1"8	122	0.90		2.90		1.50	0	6E	0.15	0.10	••		
		108	0.96	••	2.90	0.10	1.50		6E	0.30	0.12			••
	1/2"8	82	1.0	0.08	2.90	0.16	1.50	1/2"5	4E	0.48	0.17	0.10	0.16	
		6E	1.18	0.00	2.90	0.18	1.50	•	21:	0.37	0.20	0.16	0.20	
	o	A.E	1.43	0.15	2.90	0.20	1.50	l"s	A	0.22	0.22	0.56	0.32	
		28	1.38	0.17	2.92	0.22	1.50		B	0.20	0.28	0.20	0.36	••
	1	A	1.25	0.18	3.20	0.32	1.50		C	0.40	0.42		0.40	3.10
		3	1.20	0.25	3.16	0.36	1.50	1	D	0.70	0.50		0.40	0.70
		C	1.39	0.37	2.90	0.40	5.70	T	E	1.20	0.60		0.40	-0.50
		D	1.57	0.40	2.90	0.40	5.20	1/2"8	r	3.00	0.79		0.50	-0.60
		E	2.05	0.50	2.80	0.46	1.50		0	4.10	0.90	0.16	0.90	-0.50
		7	3.50	0.70	2.74	0.60	1.50		H	2.83	1.00	1.40	1.50	-0.50
		0	4.47	0.85	2.60	0.80	1.50		1	1.30	0.91	2.50	2.10	-0.50
	4	H	2.45	0.95	2.80	1.32	1.40		J	0.75	0.76	1.50	2.20	-0.50
		I	1.25	0.95	3.60	1.90	1.20		K	0.45	0.55	0.95	1.70	-0.60
		3	0.35	0.80	1.90	2.20			L	0.38	0.46	0.80	1.40	-0.50
		K	0.10	0.60	0.60	1.60	-0.40		M	0.30	0.35	0.70	1.10	-0.40
		L		0.50	0.40	1.40	-0.30		N	0.25	0.28	0.70	0.70	
	1	×		0.40	0.20	1.00	0.20	1	2W	0.25	0.20	0.70	0.38	••
	- 1	×	-0.05	0.25	0.10	0.64			4W	0.25	0.10	0.64	0.22	
		2M	-0.05	0.20	••	0.40	••	o	6W	0.25	0.08	0.64	0.14	
		No.	-0.05	0.10		0.20	••		8w	0.25		0.64		
		6W	-0.05	0.07	**	0.10		- 1	10M	0.25	••	0.04	••	
	1	8M	-0.05		••			1	12W	0.25		0.64	••	••
		10M	-0.05					7	14W	0.25		0.64		
	₹	12W	-0.05			••		1/2"8	16W	0.25		0.64		
	1/2"W	14W	-0.05						18W	0.25		0.64		
		16W	-0.05					1"8	20W	C.25	••	0.64		
	1 'W	1.6M	-0.05					- 1	22W	0.25		0.64		
		20V	-0.05						548	0.25	••	0.64		
		22W	-0.05					•	26W	0.25		0.64		••
	7	244				••		•						

	POT	ward, Av	about -	3.1				7.61	CEES.	-ed =	EA make		
Position	Location	E	39	9,	P.	D ₅	Position	Location	D1	5	Dg	DL	D
1"8	122	0.027	-0.002	-0.004	-0.002	0.006	Q	100	0.001	0.001	0.001		
	108	0.027	-0.001	-0.004	-0.002	0.006		800	0.004	0.001	0.002		-
1/2"8	6	0.030	••	-0.003	-0.002	0.006		6E	0.001	0.001	0.002		•
	6E	0.025		-0.002	-0.002	0.006	1/2"8	#E		0.002	0.004		•
Ŷ	48	0.025		-0.001	-0.002	0.006		21		0.002	0.003		
	27	0.025	0.001	-0.001	-0.001	0.006	1,"8	A	0.003	0.004	0.003		0.
	1	0.026	0.002	-0.002	-0.001	0.006		В	0.009	0.008	0.004	0.00	0.
	•	0.030	0.005	-0.002	-0.001	0.008		C	0.018	0.012	0.006	0.001	0.
	C	0.033	0.010		-0.001	0.010	1	D	0.021	0.013	0.008	0.001	0.
	D	0.034	0.013	0.002		o.ao	V	E	0.025	0.013	0.012	0.000	-0.
	1 7	0.032	0.014	0.005		0.009	1/2"8	7	0.018	0.008	0.025	·· 002	-0.
	7	0.021	0.011	0.016		0.009	T T	0	0.012	0.004	0.031	0.004	-0.
	G	0.012	0.007	0.031	0.002	0.009	1	H	0.007	0.00	0.015	0.006	0.
	×	0.005	0.004	0.023	0.004	0.011	- 1	I	0.005	••	0.004	0.006	0.
-	I	0.003	0.002	0.01	0.005	0.C15	- 1	J	0.004	-0.001	0.000	0.005	0.
	3	0.002	0.001	0.005	0.004	0.023		ĸ	0.004	-0.002	-0.001	0.003	0.
	x	0.001	0.004	0.003	0.003	7.029	- 1	L	0.004	-0.002	-0.001	0.002	0.
	L	••	•-	0.002	0.003	J. 026		M	0.004	-0.002	-0.002	C. 001	0.
1	M	-		0.001	0.002	0.019		H	0.004	-0.002	-0.002	0.001	0.
	#					0.011	i	2W	0.004	-0.002	-0.002	••	0.
	24			••		0.006	•	Appl .	0.004	-0.002	-0.002		-0.
	6W			••		0.003	0	6W	0.004	-0.002	-0.002		-0.
1	6W					0.002	1	8W	0.004	-0.002	-0.002		-0.
	84					0.001		10M	0.004	-0.002	-0.002		-0.
	10/					••		124	0.004	-0.002	-0.002		-0.
							V	160	0.004	-0.002	-0.002	••	-0.
							1/2"8	16W	0.004	-0.002	-0.002		-0.
								18W	0.004	-0.002	-0.002		-0.
							1"5	20M	0.004	-0.002	-0.002	••	-0.
							1	22W	J.004	-0.002	-0.002		-0.
								24W	0.004	-0.002	-0.002		-0.
							•	26M	0.004	-0.002	-0.002		-0.

(3 of 6 sheets)

Table A16(Continued)

					Yer	tical Fre	seure, Ps	at Indica	ted Cell					
	_	Pot	record, Av	E Speed =			_		No.	verge, Av	g pood :		10000	-
Row	Position	Location	6		8	9	10	Position	Location	6		8	_9_	10
11	0	126	0.50	••	0.50	0.24	0.75	1"8	122		0.05		••	
	1	100	0.50	0.12	0.50	0.24	0.75	1/2"K	10E	0.10	0.10			•••
		816	0.55	0.13	0.50	0.24	0.75		812	0.12	0.15			
	1/2"8	6E	0.70	0.11	0.48	0.30	0.75	ç	6 z	0.23	0.18			
		420	0.80	0.20	0.50	0.32	0.75		4-3C	0.30	0.25		0.10	
	7	28	0.76	0.15	0.50	0.34	0.75	•	21	0.22	0.25	0.10	0.16	
	1"8	A	0.70	0.30	0.62	0.40	0.75	1/2"8	A	0.10	0.32	0.20	0.20	
		3	0.74	0.28	0.60	0.44	0.75		3		0.35	0.10	0.24	
		c	0.80	0.35	0.50	0.50	0.60	1,"8	C	0.20	0.50		0.20	
		D	C.90	0.50	0.48	0.56	0.60	1	D	0.25	0.60	-0.10	0.22	••
		R.	1.05	0.58	0.40	0.60	0.50			0.50	0.65	-0.16	0.30	
		P	1.43	0.68	0.40	0.60	0.50		ř	1.05	0.85	-0.16	0.42	
		ō	1.45	0.76	0.46	0.80	0.50	i	ŏ	1.37	0.95		0.70	
		H	1.05	0.90	0.56	1.08	0.50	1	H	1.05	0.90	0.20	1.00	
	•	I	0.58	0.88	0.62	1.30	0.50	7	1	0.65	0.95	0.56	1.15	
	1/2"8	3	0.24	0.70	0.42	1.32	0.25	1/2"8	3	0.35	0.80	0.52	1.18	
	-,	K	0.10	0.50	0.20	1.10		-	X	0.21	0.55	0.30	1.10	••
	0	L	0.08	0.50	0.16	0.95		0	L	0.18	0.50	0.24	0.90	
		н	0.05	0.45	0.10	0.80		- 1	×	0.15	0.45	0.20	0.80	••
	1/2"%	N		0.30		0.60			×	0.10	0.35	0.10	0.60	
	1"x	24		0.20		0.30		1	2W	0.05	0.25	0.10	0.30	
	1	48		0.15		0.20		7	41		0.15	0.10	0.24	••
		6 W		0.10		0.10		1/2"8	6w		0.10	0.10	0.20	
	1	8w		0.10				1	8w		0.10	0.10	0.14	
	7	10M							10W		0.08	0.10	0.10	
									12W		0.05	0.10	0.10	
								Ö	14W		0.05	0.10	0.10	
									16W			0.10	0.10	••
								1/2"#	18W			0.10	0.10	••
									20M			0.10	0.10	
								1"¥	22V		••	0.10	0.10	
								1	24W			0.10	0.10	
								7	26W			0.10	0.10	

	_	and In	g Speed =	3 3	rcer herb	etion, in	at India		reree. Av	- Basel a	67-3	_	_
		WELL NO	_	0.	D _a	-	-		D.			- 1	-
Position	Location				-3		Position.	Location			3	-3	_
0	122	0.005	-0.003	-0.010	-0.002	-0.043	1/2"8	106	0.001	••		••	-
i	102	0.005	-0.003	-0.010	-0.002	-0.043		84:	0.002	••	-		-
T	88	0.006	-0.202	-0.010	-0.002	-0.042	. 0	6E	0.001			_	-
1/2"8	62	0.006	-0.002	-0.009	-0.002	-0.042	1	4E	-	0.002		_	
1 -	4 x	0.006	-0.001	-0.008	-0.002	-0.042	Ţ	25	0.001	0.002	0.002	_	
	2E	0.006	••	-0.008	-0.002	-0.0k1	1/2"8	A	0.002	0.006	0.002	••	0.0
1"8	A	0.007	0.001	-0.008	-0.002	-0.040		3	0.004	0.010	0.005	••	0.0
1	3	0.008	0.005	-0.008	-0.001	-0.039	1"5	C	0.007	0.015	0.007		0.0
	C	0.010	0.011	-0.006		-0.039		D	0.009	0.015	0.010		0.0
	D	0.011	0.016	-0.005		-0.038		2	0.010	0.014	0.017		0.0
	x	0.011	0.018	-0.002		-0.040		7	0.008	0.009	0.034	0.002	0.0
	7	0.008	0.014	0.016	0.001	-0.039		6	0.005	0.004	0.042	0.004	0.0
_ 1	0	0.005	0.008	0.043	0.002	-0.038		H	0.003		0.015	0.006	0.0
_	H	0.003	0.004	0.034	0.004	-0.036		1	0.002	••	0.002	0.006	0.0
7	I	0.002	0.002	0.014	0.005	-0.030	1/2"8	J	0.001	-0.002	-0.003	0.005	0.0
1/2"3	J	0.001	••	0.007	0.004	-0.010		x		-0.002	-0.00h	0.003	0.0
	x			0.004	0.003	0.071	o	L		-0.003	-0.005	0.002	0.0
0	L			0.003	0.002	0.051	1	x		-0.003	-0.006	0.001	
	H			0.002	0.001	0.031		×		-0.003	-0.006	••	-0.00
1/2"#	*					0.014	1	24	••	-0.003	-0-006		-0.a
1,1	2W					0.007	1.	40		-0.003	-0.007		-0.Q
	411					0.003	1/2,8	6W		-0.003	-0.007		-0. a
7	6W				/ 			8w		-0.003	-0.007	•••	-0.0
								10V		-0.003	-0.007		-o. a
								12W		-0.003	-0.007	••	-0.a
							0	144		-0.003	-0.007	••	-0.a
								16W		-0.003	-0.007		-o.a
							1/2"1	184		-0.003	-0.007	••	-o.a
							1"X	20W		-0.003	-0.007		-c.a
							1,2	-			-0.007	••	-0. Œ
								SAM		-0.003	-0.007	••	-0. a
							7	26W			-0.007	-	-0.a

(h of 6 shoots)

Table A16(Continued)

		For	mard. Av	Speed =	2.20 mph			at ine ca		erse. Av	Speed -	1.77 mm		
low	Position	Location	P ₆	P.,	18	Pg	P ₁₀	Position	ocation	P6	P7_	P ₈	Pg	P ₁₀
13	1"8	8E 6E	0.02	0.03	:	=		1"8	10E SE	0.05	0.08	••	:	
	1/2,JI	4E 2E	0.12	0.08	:	0.05		1/2°3	6E	0.10	0.08	=	0.05	
	0	A	0.14	0.16		0.15		1 8	2E	0.13	0.12		0.09	
	1/2"N 1"N	D E	0.15 0.20 0.22 0.30	0.25 0.28 0.40 0.46	=	0.20 0.20 0.20			A B C D	0.05 0.05 0.10 0.12	0.28 0.35 0.40	:	0.10 0.15 0.15 0.15	
		a	0.38	0.58	0.04	0.45		-9	7	0.20	0.63	-	0.20	
		i i	0.30 0.15 0.05	0.65 0.60 0.52	0.10 0.18 0.12	0.61		1/2"8	н	0.40	0.68	0.10	0.35 0.59 0.70	
	1 10	K	0.01	0.37	0.04	0.51		420	Ĵ	0.20	0.65	0.20	0.77	
	1	L M H 2W LW	0.01	0.30 0.20 0.13 0.10	0.02	0.40 0.35 0.20 0.05		Î	K L M M	0.10 0.08 0.04	0.55 0.45 0.35 0.27 0.15	0.10 0.04 0.04	0.69 0.60 0.50 0.35	
	•	6W	Ī		=	-			8.4 64 8.4	-	0.12	=	0.15 0.08 0.09	
								1/2"8	10h		-		0.02	

PROBLEM COS	Porward	AVE Spec	d = 2.20				Reverse		ed = 1.77	aph	
Position	Location	D ₆	_D7_	D ₈	<u> </u>	Position	Location	16	D ₇		_ D ₀
1"8	242	-0.002	-0.001		0.009	1,"8	16E	0.001			
	221	-0.002	-0.001		0.009		14E	0.001			••
100	20E	-0.002	-0.001		0.009		12E	0.001	••	••	0.001
MENT	186	-0.002	-0.001		0.009		10E	0.002	••	••	0.00
100	16E	-0.002	-0.001	**	0.009	WORLD SEAL	8E	0.002		••	0.00
	148	-0.002	-0.001	••	0.009	1-1/2"8	6E	0.002	0.000	••	0.00
	125	-0.001	-0.001	••	0.009		4E	0.002	0.001		0.00
	100	-0.001	-0.001		0.009	1"8	2	0.003	0.001		0.00
	8E	-0.001	-0.001	••	0.909	7-1	A	0.005	0.002	€.000	0.003
	6E	-0.000	-0.001		0.009	20,000		0.009	0.003	0.001	0.00
1/2"	4g	••	-0.001	**	0.009		C	0.014	0.006	(.(01	0.00
	25	••			0.009	30.00	D	0.015	0.002	0.01	0.013
0	A	0.002	-0.001	••	0.009			0.015	••	0.001	0.01
1	3	0.005	-0.000		0.010		7	0.010	-0.001	3.00?	0.031
1/2"N	C	0.011	0.001	0.000	0.014		G	0.005	0.001	0.004	0.035
1"N	D	0.014	0.003	0.001	0.013		H	0.002	0.003	0.005	0.019
		0.015	0.006	0.001	0.012	1/2"8	1.	0.001	0.009	0.005	0.00
	7	0.011	0.019	0.001	0.011		J	0.000	0.018	0.004	0.004
1 3000	0	0.007	0.031	0.003	0.C11	0	X.		0.021	0.002	0.003
	н	0.003	0.021	0.005	0.014		L		0.017	0.002	0.003
- 15 m	1	0.001	0.010	0.005	0.019		H		0.013	0.001	••
	J	0.001	0.005	0.004	0.028				0.007	0.000	
Add to	K	0.000	0.003	0.003	0.027	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	SM .		0.003		••
4	L	••	0.002	0.002	0.022		PA.		0.001	**	••
	M. N.	••	0.001	0.005	0.017		6W	••	7	•	
			0.001	0.001	0.009						
0.00	2W		0.001	0.000	0.004						
	W	••	0.001	••	0.003						
68000	6W			••	0.002						
	84	••	••	••	0.001						- 10
1000	10W		••	••	0.001						
	12W	••	••		0.000						
DOMESTIC LAND	144		••	-	••						

. Not working

(5 of 6 shoots)

Table Alf(Concluded)

		Pos	mard. Ave	Speed -	C-35 mp		TOTAL TO	i, at indica		Breek Er	peed -	7		_
low	Position	Location	16	7	8	- 9	10	Position	Location	6	P ₇	. 8	9	10
15	0	ða.		0.02		••	•	0	123		0.07	••		•
-	1	6E	0.01	0.06		••			10E		0.05	**	••	
		lei	0.01	0.06					8E		0.08			
	1/27	24	0.02	0.10		0.05			6E	0.05	0.08	••		
	1"#	A	0.03	0.10		0.09		1/2	4E	0.08	0.11		0.05	
	1		0.04	0.15	••	0.10		171	22	0.08	0.15		0.06	
		C	0.07	0.20		0.12		1	A	0.05	0.15		0.10	
	1/2"	D	0.08	0.22		0.15				0.03	0.15		0.10	
	1	2	0.10	0.40	••	0.20			C	0.04	0.20	••	0.10	
		r	0.10	0.31	••	0.20			D	0.05	0.21		0.75	
	0	0	0.12	0.38		0.27		•	1	0.05	0.27		0.12	
	- 1	H	0.11	0.41	0.10	C. 35		1/27	r	0.10	0.31		0.15	
		I	0.12	0.40	0.10	0.45		Q	0	0.12	0.38		0.22	
		J	0.08	0.35	0.10	0.40			H	0.12	0.38		0.32	
		ĸ	0.06	0.28	0.10	0.40			I	0.10	0.45	0.04	0.40	
		L	0.06	0.22	0.08	0.35		•	J	0.05	0.37	0.04	0.46	
		H	0.0	0.20	0.04	0.27		1/2"8	K	0.02	0.30	0.02	0.40	
		H	0.02	0.10	* mm	0.20			L	0.01	0.30	0.01	0.38	
		24		0.10		0.10		1	H		0.22		0.32	
	_	FM		••		0.05			N	**	0.17		0.27	
	- 4	6W		••		0.03		7	2W		0.15		0.18	
		8N						Q	Lw		0.10		0.10	
									6w		0.08		2.05	
								1	8w		0.05			
								7	10W					

	TOPMETO.	AVE Spe-	ed = 2.35	ap h			Keveree	AVE Spee	a = 1.71	mph	
Position	Location	26	D.7	D ₈	Do	Position	Location	_b ₆ _	D7_	D ₈	D ₉
1'8	242	••	-0.002	••	-0.030	9	10		0.001		••
	22%	••	-0.002	-	-0.030	1	82		0.002		
	202	••	-0.002	••	-0.030	▼	68	0.001	0.002	••	
	188	••	-0.002		-0.030	1/27	4E	0.002	0.003		••
	163	••	-0.002	••	-0.030	1"1	25	0.002	0.004		
	1AE	••	-0.002	••	-0.030		A	0.002	0.005		0.00
1/2"3	128		-0.002		-0.030		3	0.005	0.006	**	0.00
0	102	0.001	-0.002		-0.030		C	0.010	0.008	0.001	0.00
	8E	0.001	-0.002		-0.030		D	0.016	0.013	0.002	0.00
	6E	0.001	-0.001		-0.030		E	0.018	0.018	0.002	0.00
, I	No.	0.001	-0.000	**	-0.030	1/2"11	r	0.017	0.038	0.002	0.00
1/2"#	21	0.002	-0.000		-0.030	Ŷ	0	0.017	0.046	0.004	0.00
1"1	A	0.003	-0.001		-0.030		H	0.004	0.025	0.006	0.00
	3	0.007	-0.001		-0.028		7	0.002	0.008	0.006	0.01
V	C	0.014		••	-0.026		J	••	0.003	0.005	0.02
1/5,1	۵	0.017	0.002	0.001	-0.025	1/2"8	K			0.003	0.06
	X	0.020	0.004	0.002	-0.026		L	**		0.002	0.04
	. 7	0.016	0.020	0.002	-0.027		×			0.001	0.01
0	0	0.010	0.046	0.003	-0.026		N			0.001	-0.00
	H	0.004	0.034	0.005	-0.024	V	24			0.000	-0.00
	I	0.002	0.016	0.006	-0.020	٥	P.M.	**	••		-0.01
	3	0.002	0.006	0.005	-0.002		6W				-0.01
	K	0.001	0.004	0.004	0.065		OM			••	-0.01
	L		0.003	0.003	0.054		10W				-0.01
	N	••	0.005	0.008	0.033	1	12W			••	-0.a
	T T			0.000	0.015		144				-0.01
	20	••		0.000	0.007	i	16V		••	••	-0.01
	W	••			0.003		18W				-0.a
	6W BW				0.002		20H			••	-0.01
40	ew.	••	••				55A		••	**	-0.01
							244			••	-0.01
							204				••

9 Set working

(6 of 6 sheets)

Table 4-17

Multiple-Wheel Heavy Gear Load Fluxible Favorent Test, Dynamic Instrumentation Loading Date

Item 4; Load Contition: 30 kips, Single Wheel, 100 psi

				. 61			SAGUE, P.	at Indic	ated Cells		e Could	3.34 mg/h		
		10	reard, Av		5.50 apn				Ve	ASLES VA				
lov	Position	Location	_1_	P ₂		F.,		Position	Location	-1		P3	PL	-5
5	0	128		-0.30	-3.20	-0.19	-1.80	1"8	122	••	0.10			
-		10E		-0.26	-3.26	-0.15	-1.80	1	1OE	••	0.17	••		
		8z		-0.20	-3.16	-0.10	-1.80		82		0.20		0.04	
		6E	••	-0.11	-3.08	-0.05	-1.74		6E		0.30	0.20	0.10	••
		48		-0.05	-3.70	••	-1.66		₹4E		0.37	0.40	0.11	
		28		••	-3.00	0.05	-1.47		22		0.39	0.36	0.17	0.15
		A		0.18	-3.08	0.15	-1.41		A		0.56	0.20	0.22	0.30
		3	••	0.49	-3.08	0.25	-1.50	1	B		0.99	0.32	0.32	0.30
		С		1.07	-3.00	0.38	-1.53		C		1.50	0.40	0.47	0.24
		D	17.00	1.55	-2.88	0.50	-1.56	1	D		1.99	0.64	0.56	0.21
		E	28.10	2.00	-2.40	0.62	-1.50		Ľ	38.75	2.35	1.24	0.69	0.24
	1	P		2.58	4.32	0.93	-1.14	1	r		2.81	7.20	1.02	0.63
		G		2.25	19.24	1.25	-0.21		G		2.30	20.40	1.34	1.83
		H	-	1.40	8.80	1.40	3.57		H		1.41	8.00	1.42	4.66
		1		0.79	2.00	1.38	7.56		I		0.85	0.48	1.32	7.9%
		J	••	0.31	0.80	1.02	5.22		J	••	0.41	-0.40	1.00	4.47
		K		0.20	0.40	0.79	2.10	1	K		0.24	-0.80	0.69	1.23
		L		0.08	0.28	0.59	1.05		L	••	0.20	-0.80	0.59	0.72
		M		0.05	0.28	0.49	0.60		м	••	0.10	-0.88	0.42	0.12
		M		0.02	0.20	0.28	0.15	•	N	••	••	-1.00	0.22	-0.24
		24		••	0.20	0.15		0	2W	••		-1.00	0.04	-0.45
		48			0.20	0.10		1	4W	••	••	-1.00	-0.02	-0.54
		6W			0.20	0.05	••	1	6W			-1.00	-0.07	-0.54
	1	8w			0.20				8w		••	-1.00	-0.09	-0.54
	1	10W			0.20	••	••	- 1	10W		••	-1.00	-0.10	-0.54
	1	12W		••	0.20		••	1	12W		••	-1.00	-0.10	-0.54
	7	146	••			••	_	V	114			••		••

(1 of 6 sheets)

	Section 1	Jo.	mard, Av	Book -	3.06 mph		20125.332	il et faile		verse, Av	g Speed	2,44 mph		STEP IN
	heities	lecetion	76		78	<u> '•</u>	P ₁₀	Position	Location	16	-7	P8	Pg	P ₁₀
9	Ī	908 168 168 148 128	=	-0.58 -0.58 -0.56 -0.56 -0.52	-1.95 -1.95 -1.95 -2.00 -1.95	-0.07 -0.06 -0.06 -0.06	-0.62 -0.62 -0.62 -0.62	1/2	20E 18E 16E 14E 12E	=	0.04 0.04 0.06 0.10	=======================================	0.06	0.09 0.14 0.15 0.13 0.10
		10E 6E 6E 4E 2E	===	-0.39 -0.26 -0.22 -0.20 -3.10	-1.95 -1.90 -1.85 -1.85 -1.90	0.05 0.10 0.13	-0.59 -0.58 -0.55 -0.50 -0.47	7\5_A	102 82 62 42 23	=	0.12 0.28 0.34 0.40 0.50	=	0.09 0.11 0.16 0.20 0.28	0.09 0.11 0.13 0.16 0.21
		A B C D	32.40 107.60	0.40 1.04 1.70 2.42	-1.90 -1.65 -1.85 -1.85 0.10	0.17 0.24 0.37 0.49 0.57	-0.39 -0.35 -0.40 -0.43 -0.43		A B C D	3.40 78.50 74.20	0.72 1.26 2.44 2.80 3.36	0.10 0.20 0.75 1.60	0.31 0.43 0.56 0.67 0.83	0.35 0.37 0.35 0.36 0.45
		y u H I	0.80 0.70 0.60 0.50 0.40	3.16 2.78 1.72 0.78 0.38	5.25 3.10 0.70	0.87 1.16 1.30 1.29 1.08	-0.35 1.62 5.45 4.51		P O H I J	=	3.26 2.20 1.40 0.68 0.22	4.50 4.60 0.45 -0.60	1.12 1.35 1.40 1.26 0.91	0.77 1.73 4.29 5.71 2.97
		E E	0.30 0.10 0.00	=======================================	-0.20	0.75 0.60 0.48 0.26 0.17	2.08 0.97 0.55 0.20 0.13	1/2"# 1"#	E L M H	=	-0.10 -0.20 -0.20	-0.55 -0.55 -0.55 -0.55	0.69 0.53 0.40 0.20 0.12	0.57 0.33 0.11 -0.07
		6W 6W 10W 12W	Ē	0.10 0.10 0.10 0.12 0.08	-0.න -0.න -0.න -0.න -0.න	0.08	0.10 0.10 0.08 0.07 0.10	1/2 " #	44 64 84 104 124	=	-0.20 -0.20 -0.20 -0.20	-0.55 -0.55 -0.55 -0.55	0.07	-0.07 -0.07 -0.07 -0.07
		160 160	=	0.06	-0.25		0.06	0	14W 16W		-0.20	-0.55	••	-0.07

Santa States	76	mard. Av	Speed =	3.06 mb	COL PAST	CULOR, II	at Indic		verse, Av	- beed	2.44 mb		
Position	Location	D ₁	D ₂	D ₃	Dia	D ₅	Position	Location	D	D ⁵	D ₃	Dla	D ₅
1	FAE 162 162 142 122	-0.085 -0.085 -0.085 -0.085	0.005 0.906 0.006 0.006 0.006	Ē	0.002 0.005 0.005 0.005	=	1/2"H	202 182 162 142 122	Ē	0.001	-0.002 -0.002 -0.002	Ē	-0.00 -0.00 -0.00 -0.00
	108 68 68 148	-0.055 -0.055 -0.055 -0.055	0.007 0.009 0.008 0.00L 0.005	=	0.002	Ē	1/2"H	108 82 62 62 42 22	0.020	0.002 0.002 0.002	-0.001	0.001 0.001 0.003	-0.70 -0.00 -0.00
	A B C D	-0.085 -0.084 -0.082 -0.083 -0.085	0.010	0.001 0.001	0.00k 0.00k 0.00k 0.00k	0.002 0.002 0.002		A B C D	0.002 0.003 0.005 0.005 0.006	0.005 0.011 0.017 0.018 0.019	-0.001 -0.001 -0.001	0.003 0.002 0.002 0.003	-0.00
	7 6 8 1	-0.063 -0.063 -0.060 -0.073 -0.058	0.016 0.010 0.005 0.003 0.001	-0.001	0.007 0.010 0.016 0.021 0.029	0.001 0.002 0.005 0.005		0	0.008 9.011 9.018 0.034 0.068	0.00k 0.00k 0.002 0.001	-0.001 -0.001	0.006 0.012 0.018 0.021 0.015	-0.00 0.00 0.01
		0.089 0.099 0.057 0.025 0.012	0.001	-0.001 -0.001 -0.001 -0.001	0.003 ,0.006 0.003 C.002	0.002	1/2 "	E L H H	0.110 0.035 0.001 -0.011 -0.019	0.001 0.001 0.001 0.001	Ē	0.009 0.006 0.00k 0.002	0.00
	low Gu Bu 100 120	0.005 0.002 0.00L 0.00L	=	-0.001 -0.001 -0.001	0.001	-0.001 -0.001 -0.001	7/2 M	GV GV BV 10V 12W	-0.021 -0.022 -0.021 -0.021 -0.020	0.002	=	=	0.00
	160 160	:	:	:	:	-0.001	•	160 160	-0.021	0.002	-	-	

(2 of 6 sheets

Tuble AT WCoutinued)

		/0	rward, Av	K Speed -	3.25 mph			100000	He	verse, Av	g Speed -	Carlo Mark		
ov	Position	Location	P6	P-7	Pa	P9	P ₁₀	Position	Location	16	P ₂	P ₈	19	10
10	1"8	20E	1.00	••	5.10	-	2.61	0	202	0.20	••	~0.35	••	
		18E	1.00	0.18	5.00		2.60	1	100	0.20		0.30		••
	1/2"8	1GE	1.00	0.30	5.00		2.58	j	LEE	0.20		0.35	0.0	
		146	1.00	9.40	5.00		2.56	1	14E	0.20	0.16	0.35	0.00	0.0
	0	126	1.00	0.62	5.00	••	2.52	i	122	0.20	0.25	0.40	0.07	••
		106	1.00	0.84	5.00	••	2.54		102	0.20	0.72	0.40	0.12	
	10.00	SIE.	85.40	1.20	5.20	0.09	2.60	ľ	8E	70.60	0.94	0.70	0.18	0.04
	1/2"8	6E	2.35	1.46	5.30	0.12	2.62	1	(E	-1.00	1.10	0.90	0.26	0.00
	-	4E	2.60	1.62	6.00	0.24	2.76	1	48	-1.00	1.38	1.70	0.38	0.28
	1 8	2292	2.80	1.78	5.65	0.32	3.10	1	26	-1.00	1.60	0.40	7.45	0.62
		A	2.80	2.46	5.60	0.45	3.52		A	-1.00	2.64	0.35	1.62	1.12
	1	B	1.00	4.02	5.50	0.66	3.56	100	В	-1.00	4.50	0.40	0.77	1.00
		C	-1.90	6.22	6.00	0.86	3.22		С	-1.00	7.72	1.30	1.11	0.60
	1	D	-1.50	7.80	6.20	1.05	3.24		D	-1.00	9.04	2.10	1.26	0.60
		E	-1.50	9.45	6.70	1.20	3.30	1/2"N	E	-1.00	10.40	3.40	1.50	0.64
		r	-0.90	11.08	8.00	1.66	3.83	1"11	2	-1.00	10.54	7.35	2.03	1.60
		0	0.60	9.20	7.50	2.15	5.22	1	G	-1.00	8.02	6.90	2.42	3.80
		Н	1.00	6.02	3.70	2.50	9.08	1	Н	-1.00	5.20	2.9	2.53	9.14
	- 1	I	1.90	3.14	1.00	2.37	13.82	1	1	-1.00	2.9	2.40	2.2	12.54
	1	J	1.00	1.60	0.40	1.99	10.32	i	J	-1.00	1.60	2.40	1.77	8.94
	1	K	1.00	0.76		1.37	4.60	- 1	K	-1.00	0.72	2.40	1.26	4.66
		L	0.50	0.46		1.16	2.38	1	L	-1.00	0.54	2.40	1.03	4.36
	ı	M	0.50	0.22		0.95	1.70	7	H	OC	0.38	2.40	0.82	2.49
		N	0.50	••		9.53	0.46	0	91	-1.00		2.40	0.51	1.40
		2W	0.50	••	••	0.32	0.12	1"8	5A	-1.00		2.4	0.30	0.97
		4W	••			0.18		1	48	-1.00	••	2.40	0.14	0.80
	1	6W				0.08	••	J.,	GM	-1.00		2.40	0.09	0.80
	7	8w	••	••	••	••		1/2"8	8w	-1.00		2.40	••	0.80
									10M	-1.00		2.40		0.80
								Ŷ	12W	-1.00		2.40		0.80
								1	144	-1.00	••	2.40		0.80
								7	16W				••	

	For	ward, Ave	Speed "	3.25		tion, in.			verse, At	frend -	2.51 mpn		
Position	Location	D ₁	D ₂	D ₃	DL	D ₅	Position	Location	<u>_</u>		D ₃	$D_{\hat{k}_{\mathbf{k}}}$	D
1"s	208	0.025	0.007	-0.002	-0.009	-0.007	0	20E	-0.001	2.001	••	••	
	18E	0.025	0.008	-0.002	-0.009	-0.007	1	18E		0.001		*.	••
1/2"8	16E	0.025	0.008	-0.002	-0.009	-0.007		16E		0.002			••
	14E	0.025	0.008	-0.002	-0.009	-9.007		14E		0.003			
0	1.2E	0.025	0.009	-0.002	-0.009	-0.007	4	122		0.003			
	102	0.025	0.010	-0.002	-0.009	-0.007		10E		0.004	••		••
	8E	0.025	0.013	-0.002	-0.009	-0.007		8E		0.007		0.001	•
1/2"8	CE	0.025	0.011	-0.002	-0.009	-0.007		6E		0.003		0.002	••
	FE	0.025	0.01	-0.002	-0.008	-0.07		4世		0.003	-	0.003	•
1"L	25	0.025	0.01	-0.002	-0.007	-0.007	i	21	0.000	0.006		0.004	••
1	A	0.026	0.014	-0.002	-0.006	0.006		A	0.004	0.012	••	0,006	-
	D	0.026	0.022	-0.002	-0.006	-0.005	- 1	В	0.005	0.023		0.005	-
	C	0.027	0.028	-0.001	-0.006	-0.005		С	0.011	0.039	-0.001	0.005	-
	D	0.027	0.042	-0.001	-0.006	-0.005		D	C.OLI	0.045	-0.001	0.005	-0.0
	E	0.025	0.046	-0.001	-0.005	-0.005	1/5,M	E	0.008	0.044	-0.0CI	0.007	-0.0
	r	0.024	0.031	-0.001	-0.003	-0.005	1 "31		0.006	0.023	-0.001	0.012	
	G	0.025	0.017	-0.001	0.004	-0.005	- 1	G	0.010	0.012	-0.001	0.024	0.0
	n	0.026	0.009	-0.001	0.024	-0.003		H	0.019	0.005	-0.001	0.045	0.0
	1	0.030	0.004	-0.001	0.048	0.003		I-	0.037	0.002	-0.001	0.050	0.0
	J	0.035	0.002	••	0.039	0.016		J	0.066	0.001	-0.001	0.025	0.0
	K	0.037	0.001		0.021	0.029	1	K	0.083	••	-0.001	0.009	0.0
	L	0.032			0.015	0.026	1	L	0.073	••	-0.001	0.004	0.0
	Ħ	0.026			0.011	0.028	¥	H	0.059		-0.CO1	0.001	0.0
	×	0.014	••		0.005	0.013	0		0.027		-0.001	-0.003	0.0
	24	0.000	••	••	0.006	0.006	1 8	24	0.023	••	-0.001	0.004	0.0
	lets.	0.002			0.001	0.003	1	lett	0.016		-0.001	+0.005	-0.0
1	6M	0.001			0.001	0.001		(dat	O.014		-0.001	-0.005	-0.1
7	8w		••				1/2"8	BM	0.024		-0.001	-0.005	-0.0
								104	0.00	••	-0.001	-0.005	-0.0
							0	124	0.024		-0.001	-0.005	-0.0
							1	144	0.014		-0.000	-0.005	-0.0
							T	16M					•

() of 6 shares

Tails Al Toostimed)

100					Vel	tical Pro	saure, P	al, at Indic				3 00		
940			merd, Av	_		-	-				g Speed -		-	P
Nov	Position	Location	6	P7	Pa	<u> </u>	P ₁₀	Position	Location	P6	P ₇	-8	_2_	P ₁₀
u	1	20E 16E 14E 14E	0.19 0.19 0.18 0.17 0.20	0.32 0.32 0.34 0.35 0.38	0.26 0.26 0.28 0.29 0.29	0.10 0.12 0.12 0.12 0.13	0.33 0.33 0.32 0.33 0.32	1/2"8	162 142 122 107	-0.09	0.03 0.05 0.09 0.12 0.20	=	0.02	0.03
		10E 8E 6E 4E 2E	0.15 0.14 0.09 0.14 0.14	0.45 0.51 0.57 0.64 0.67	0.29 0.32 0.40 0.40 0.42	0.15 0.17 0.21 0.22 0.27	0.33 0.33 0.34 0.36 0.41		B SE YE	-0.03 0.04 0.05 0.08	0.22 0.25 0.32 0.50 0.81	0.16	0.07 0.11 0.16 0.21 0.29	0.04 0.07 0.13 0.18 0.13
		A B C D	0.14	0.80 1.02 1.28 1.47 1.64	0.40 0.45 0.50 0.60 0.60	0.33 0.36 0.47 0.53 0.62	0.47 0.48 0.48 0.48		C D E F	0.08	1.17 1.38 1.55 1.62 1.37	0.16 0.20 0.30 0.45 0.33	0.38 0.56 0.73 0.86	0.09 0.08 0.11 0.23 0.49
	1/2,0	P O H I	0.06	1.71 1.46 1.03 0.57 0.31	0.55 0.40 0.20 0.10	0.76 0.88 0.93 0.91	0.59 0.75 1.72 1.20 0.99		M I J K	0.10 0.10 0.09 0.10 0.10	0.95 0.57 0.35 0.23 0.18	0.10	0.88 0.82 0.68 0.47 0.42	0.90 1.14 0.98 0.60 0.48
		E L N H	=======================================	0.16 0.01 0.01 0.00	=======================================	0.58 0.18 0.37 0.23 0.12	0.59 0.38 0.27 0.09 0.02	1/2"8	N N 2W 4W 6W	0.10 0.09 0.09 0.08 0.08	0.13 0.08 0.07 0.06 0.05	=======================================	0.33 0.21 0.13 0.09	0.35 0.19 0.11 0.08 0.08
		en en	Ξ	Ξ	Ξ	0.06	Ξ		10W 12W 14W 16W	0.10 0.11 0.10 0.11 0.10	0.05 0.05 0.08 0.06 0.05	=	0.03	0.08 0.03 0.06 0.06
								4	18v 20v 22v	0.11	0.05	=	::	0.06

	Por	ward, Av	g Speed -		tical per	LACTION, 1	n., at Indi		rerse. Av	g Speed =	3.00 mob		-
Position	Location	_D,	D ⁵	D,	Di	D ₅	Position	Location	D	05	Dg	DL	105
1	20E 18E 16E 14E 12E	0.006 0.006 0.007 0.007 0.006	-0.055 -0.055 -0.055 -0.055 -0.054	-0.002 -0.002 -0.002	-0.019 -0.019 -0.019 -0.019	-0.011 -0.011 -0.011 -0.011	1/2"8	20E 16E 14E 15E	=	=	0.001	0.001	=
	10E 6E 6E 4E 2E	0.007 0.007 0.007 0.006 0.006	-0.054 -0.053 -0.052 -0.052 -0.051	-0.002 -0.002 -0.002	-0.019 -0.019 -0.018 -0.018	-0.011 -0.011 -0.011 -0.011		100 80 60 40 40	0.001	0.002 0.003 0.005 0.006 0.006	0.002 0.002 0.002 0.002	0.002 0.002 0.003 0.003	0.0
	A B C D	0.007 0.007 0.008 0.008 0.009	-0.500 -0.410 -0.012 0.039 0.085	-0.002 -0.002 -0.002	-0.016 -0.017 -0.016 -0.016	-0.010 -0.009 -0.008 -0.008		A B C D	0.001 0.002 0.002 0.002	0.019 0.035 0.079 0.095	0.002	0.006 0.007 0.007 0.006 0.009	0.0
100	9 8 1 3	0.009 0.009 0.010 0.013 0.016	0.044 0.022 0.010 0.00k	0.001	-0.013 -0.003 0.020 0.061 0.050	-0.003 -0.008 -0.005 0.004 0.020		P O H I	0.009 0.009 0.001 0.001	0.070 0.007 -0.008 -0.014 -0.018	0.001	0.017 0.033 0.063 0.060 0.060	0.0
	K L N N	0.018 0.017 0.014 0.010 0.005	=	0.001 0.005 0.005 0.005	0.022 0.016 0.00 0.00	0.037 0.037 0.031 0.018 0.009	i	K L M B	0.015 0.014 0.012 0.008 0.004	-0.019 -0.019 -0.019 -0.020	=	0.007 0.003 -0.003 -0.005	0.0
1	en en	0.003	Ξ	0.001	Ξ	0.003	1/2"8	4W 6W 84 10W 12W	0.002	-0.019 -0.019 -0.019 -0.019	=	-0.005 -0.005 -0.005 -0.005 -0.005	=
								16# 16# 18# 20# 22#	0.002	-0.019 -0.019 -0.019	=	-0.005 -0.005 -0.005 -0.005	

(4 of 6 sheets

Table AllContinued

			mard, Av	. Preside	Vert	ical Pres	sure, psi	at Indicat	ed Colls	verue, Av	a Strange	1.97		
Nov	Position	Location	6	17	P ₈	Fg	10	Position	Location	6	P _{eq}	1/8	79	P ₁₀
13	13	268 242 222 208 188		0.23 0.23 0.25 0.24 0.23	0.12 0.11 0.11 0.11 0.12	0.14 0.14 0.14 0.14	0.07 0.07 0.07 0.08	1"8	262 242 205 182		0.02 6.02 0.03 0.03	:	=	:
		16E 14E 128 10E 8E		0.24 0.26 0.28 0.32 0.36	0.10 0.12 0.12 0.13	0.14 0.14 0.16 0.17 0.18	0.07 0.08 0.08 0.08		168 148 128 108 88		0.06 0.07 0.09 0.11	0.05 0.08 0.09	0.02	0.01
	1/2"	62 48 22 A D		0.40 0.42 0.49 0.55 0.66	0.14 0.13 0.12 0.13 0.14	0.20 0.23 0.26 0.29 0.34	0.09 0.10 0.13 0.16 0.18	1-1/2"8	GE LE 2E A B		0.18 0.20 0.25 0.35 0.52	0.08 0.09 0.09 0.07	0.06 0.08 0.12 0.16 0.22	0.02 0.04 0.07 0.08 0.08
	1/2"m 1"m	C D E F		0.83 0.92 0.97 1.00 0.89	0.17 0.19 0.20 0.20 0.17	0.40 0.46 0. 0.3	0.18 0.18 0.19 0.26 0.35		E F		0.73 0.83 0.90 0.97 0.80	0.16 0.19 0.19 0.23 0.14	0.30 0.35 0.41 0.52 0.58	0.06 0.07 0.08 0.15 0.27
		H J K L		0.68 0.43 0.27 0.17 0.12	0.05 -0.02 -0.02	0.65 0.62 0.53 0.41 0.35	0.45 0.53 0.46 0.31 0.22	1/2"5	H I J K L		0.62 0.40 0.27 0.16 0.12	-0.05 -0.05 -0.05 -0.05	0.63 0.58 0.50 0.38 0.31	0.44 0.52 0.47 0.30 0.24
		22		0.10 6.77 0.04 0.03 0.02	=	0.29 0.19 0.12 0.08 0.05	0.16 0.07 0.04 0.01		M SM PM EM EM		0.10 0.05 0.05 0.03 0.02	-0.05 -0.05 -0.05 -0.05	0.26 0.17 0.12 0.07 0.05	0.18 0.08 0.04 0.01
		8w 10w 12w 14w 16w		0.02	=======================================	0.02 0.02 0.02	0.01	1/2"8	10W 12W 14W 16W		0.02	• 0.05 • 0.05 • 0.05 • 0.05 • 0.05	0.03 0.02 0.02 0.01	::
		18v 20v		0.02		0.01	=		18V 20V		0.01	-0.05	0.01	••

	Pormero	AVE Spe					Kevers	AVE Sp			
Position	Location	D ₆	Dy	D _B **	Dg	Position	Location	D ₆	Dy	08	B9
179	26E 24E 22E 20E 18E	0.031 0.031 0.031 0.031 0.031	0.008 0.008 0.008 0.008		-0.012 -0.012 -0.012 -0.012	1*8	26E 24E 22E 20E 18E	0.002 0.002 0.003 0.004	=		:
	16E 14E 12E 10E	0.032 0.033 0.037 0.042 0.054	0.008 0.008 0.008 0.008 0.009		-0.012 -0.012 -0.012 -0.012		16E 14E 12E 10E 8E	0.00% 0.008 2.012 0.017 0.037	:		0.002
0	6E Mg 22: A D	0.0k3 0.0k3 0.0k8 0.062 0.088	0.009 0.009 0.010 0.011 0.013		-0.012 -0.011 -0.020 -0.009 -0.008	1-1/2"s	GE LE 2/E A B	0.010	0.001 0.002 0.003 0.004		0.001 0.007 0.009 0.009
1/27	C D E F	0.138 0.180 0.193 0.142 0.081	0.017 0.016 6.017 0.029 0.038		-0.006 -0.006 -0.005 -0.005		C D E P	0.148 0.165 0.150 0.078 0.033	0.008 0.011 0.020 0.037 0.035		0.008
	H 1 J K	0.043 0.022 0.010 0.006	0.033		0.00L 0.021 0.067 0.068 0.067	1/2"8	H 1 J K	0.008 -0.006 -0.018 -0.013	0.024 0.012 0.005 0.003 0.003		0.028 0.050 0.070 0.054 0.051
	en SA H	0.003 0.003 0.002 0.002	=		0.057 0.033 0.028 0.009 0.004		# EN	-0.015 -0.015 -0.014 -0.014	0.00k 0.00k 0.003 0.003 0.00k		0.037 0.016 0.005 -0.001 -0.004
1	10v 12v 14v	Ξ	=		0.002	1/2"8	100 120 140 160 180	0.01 0.01 0.01 0.01 0.01	0.00k 0.00k 0.00k 0.00k 0.00k		-0.005 -0.005 -0.005 -0.005 -0.005

[.] He prossure recorded

table 417(Concluded

	-	Fo	rward. Av	Speed -	2.26 mph	TICK PE	sasma, bi	i at Indic	Res Cells	verse. Av	Speed a	1.61 mb		
Row	Position	Location	P6.	-7	P ₈	19	P ₁₀	Position	Location	P6*	P7	18	Pg	P ₁₀
19	1"8	26E 24E 22E 20E 18E		0.07	=	0.06 0.07 0.07 0.07	Ē	Î	182 162 142 128 108		0.02 0.03 0.04	=	0.02	0.02
		168 14E 12E 10E 8E		0.08 0.08 0.10 0.12 0.14	0.02	0.07 0.08 0.09 0.10 0.11	0.02	1/2"	SE LE 2E A		0.08 0.11 0.13 0.15 0.21	0.03 0.05 0.05 0.06 0.07	0.05 0.06 0.08 0.10 0.13	0.03 0.02 0.04 0.06
	1-1/2"s	2E A B		0.22 0.25 0.30 0.40	0.06 0.08 0.09	0.12 0.13 0.16 0.20 0.23	0.02 0.03 0.06 0.06	1/27	B C D E		0.30 0.41 0.46 0.50 0.51	0.08 0.08 0.10 0.11 0.10	0.16 0.22 0.26 0.30 0.37	0.07 0.07 0.07 0.07
	2"8	C D E F		0.50 0.53 0.56 0.59 0.52	0.12 0.13 0.10 0.08 0.05	0.27 0.31 0.34 0.40	0.07 0.08 0.10 0.13 0.19	1/2"8	g H I J K		0.43 0.33 0.20 0.13 0.06	0.10	0.41 0.44 0.41 0.36 0.28	0.17 0.24 0.26 0.24 0.17
	1-1/2"s	H J K L		0.39 0.27 0.17 0.10 0.07	Ē	0.46 0.43 0.37 0.27 0.23	0.24 0.27 0.24 0.16 0.13		L M M 2W Lu		0.02	=	0.24 0.22 0.15 0.11 0.06	0.11 0.11 0.06 0.05 0.02
	1'8	M N 2W LW 6W		0.03	Ξ	0.13 0.12 0.07 0.05 0.03	0.10 0.03 0.02 0.01		64 84 104 124 144	e	=		0.06 0.04 0.03 0.03	::
		8w 10w 12w		Ξ	Ξ	0.02	Ξ		16W 18W 20W		=	=	0.05	=

	POPPER	d. Avg Spe	ed - 2.3		ARCHE PLAN		Reverse	Avg Spe	d = 1.51		04077
Position	Location	16	07	Dg	Dg	Position	location	D _E	D7	Dg	29
1"8	268	-0.035			-0.004	0	SYE		••		0.00
100	24E	-0.035			-0.004	1	221		••		0.00
Wall Place	228	-0.035			-0.003		20E				0.00
107 Mag 27	206	-0.035			-0.003	1	18E				0.00
	18E	-0.035			-0.003		16E	0.001			9.00
	16E	-0.035	••		-0.003		14E	0.002			0.00
White States	145	-0.034			-0.00	- 1	1.22	0.002			0.00
PERMIT	122	-0.034			-0.003	- 1	100	0.003			0.00
	100	-0.330			-0.00%	- 1	38	0.005			0.00
NO Division	3E	-0.032	-		-0.00%		6E	0.006			0.00
1.40	36	-0.032	-		-0.004	1/2 1	NE.	0.007	••		0.00
PROPERTY.	NE.	-0.032			-0.004	1"N	22	0.011			0.00
THE PERSON	22	-0.031	••		-0.003	1	A	0.019	0.001		0.00
	A	-0.027	-		-0.003		B	0.036	0.002		0.00
1-1/2"8		-0.018	0.001		-0.002		С	0.075	0.003		0.00
Sec.	C	0.004	0.002		-0.002	1	D	0.095	0.004		0.0
The Wanter	D	0.056	0.002		-0.001		E	0.066	0.006		0.00
A 18 MILES		0.094	0.003		-0.001	1/27	7	0.011	0.009		0.00
2"8		0.050	0.006		-0.001	0	0	••	0.009		0.0
	G	0.025	0.006		••	- 1	H	-0.007	0.006		9.0
	H	0.012	0.008		0.004	4	1	-0.010	0.003		0.0
The state of the s	1	0.005	0.005		0.011		3	-0.012	0.001		0.0
		0.003	0.001		0.026	1/2"8	K	-0.012			0.0
1-1/2"8		0.002	••		0.038	100	L	-0.012			0.0
700	L	0.001	-		0.037	44. 11.4		-0.013	**		0.00
1.8		0.001	••		0.031			-0.013	••		0.0
76.0					0.010	1 12	2	-0.013	-		0.00
75 (1947)	54	=	**		0.005		64	-0.013	•••		0.00
7.0	64				0.003		~ ~	-0.013			
363 16. 254					0.003		100	-0.023	•		
	100				0.001		124	-0.013			
310	120	-			0.001	1 1 1	114	-0.013			
1/2"8	146				0.001	1	164	-0.013	••		-
0	16M	••					104	-0.036	••		
9079 0015 -0	STATE OF THE PARTY					The state of the s	90M				

* A pressure recorded.

(6 of 6 shoots

Table :-18

Multiple-Wheel Heavy Gear Load Flexible Payment Test, Dynamic Instrumentation Loading Date

1tem 3: Load Condition: 30 kips per Wheel, Twin Tandem 747, 100 pai

		lon-	ward, Ave	Speed -	2.40 mph	A DITTE			Rev	erse, Av	a press -	2.52 mpt		- Call
Row	Position	Location	P ₁	12	P ₃	PL	P5.	Position	Location	P1.	12	-1,	34	3
5	1"8	20E 18E 16E 14E 12E		0.09 0.23 0.34	0.14 0.15 0.17 0.23	-0.18 -0.17 -0.14 -0.08		17	200 160 160 140 127		0.11 0.19 0.29 0.43 0.57	0.00	0.01 0.03 0.06 0.14	
		10E 8e 6e 4e 2e		0.46 0.51 0.51 0.46 0.39	0.34 0.47 0.50 0.23 0.04	0.10 0.29 0.46 0.54 0.43			102 8E 6E LE 2E		0.70 0.73 0.69 0.61 0.60	0.20 0.42 0.52 0.34 0.23	0.30 0.53 0.75 0.77 0.63	
	0	A B C D		0.42 0.56 0.83 1.03 1.26	-0.01 -0.03 -0.02 0.02 0.10	0.24 0.11 0.09 0.10 0.15		°	A B C D E		0.66 0.88 1.27 1.50 1.78	0.17 0.13 0.16 0.18 0.27	0.47 0.37 0.38 0.45 0.54	
		P G H I J		1.81 2.37 5.50 2.84 2.60	0.45 1.62 2.64 10.35 3.43	0.40 0.93 1.74 2.58 6.50			y G H I		2.30 2.71 5.80 2.73 2.39	0.71 2.02 2.78 11.25 3.60	0.89 1.57 2.48 3.15 6.90	
	170	K L H H		2.07 1.79 1.47 0.98 0.58	2.38 1.40 0.70 0.19 0.06	3.40 3.20 2.78 1.80 1.01			K L M M		1.82 1.54 1.24 0.75 0.42	2.53 1.55 0.92 0.40 0.22	3.29 3.02 2.57 1.52 0.85	
		6W 8W 10W 12W		0.32 0.17 0.06 0.01	0.02	0.54 0.27 0.10			EM EM 10M 12W		0.21 0.07 -0.04 -0.04	0.18 0.16 0.16 0.16 0.15	0.42 0.21 0.10 0.03 0.02	
								- 1	14W 16W 1/9W		-0.05 -0.05 -0.06	0.16 0.16 0.15	=	

(continue)

Table 11 (Continued)

	0.0	10	rward, Av	Speed	2.59 apple	major Street		si, at ladic	Ne	verse, Av	g Speed a	2.95 mph		
•	Position	Location	-5	1,2	P3	Pi	P.,	Position	Location	1,	P ₂	P	Fk	-
	176	26E	-0.72		-1.22			0	248	-	0.05	-		
		242	-0.12		-1.20			1	2/28	0.31	0.10	-		
		221	-0.70	0.06	-1.20		-	1	5-W	0.06	0.18	-		-
	0	50E	-0.65	0.12	-1.20	-	-		3.6E	0.26	0.32			-
	1	1/hr	-0.49	0.22	-1.20			- 1	162	0.75	0.53		0.03	•
		16E		0.43	-1.20	0.02		1	142	1.90	0.75	0.08	5.31	-
		16E	1.00	0.67	-1.16	0.10		1	1.28	3.61	1.05	0.36	0.25	-
	1/2"	128	2.25	0.90	-0.92	0.25		- 1	100	3.31	1.32	1.38	13.56	-
	1	102	3.12	1.11	-0.22	0.51		- 1	(SE	1.56	1.40	5.18	₄98	-
	1	82	1.47	1.22	3.40	0.86	••	- 1	GE.	0.74	1.33	5.90	51	~
		6E	0.30	1.24	6.38	1.30		- 1	ME	0.40	1.1k	1.26	1.46	0.1
	2"3	4E	-0.19	1.06	1.86	1.42	0.25	- 1	22	0.39	1.09	0.60	1.07	0.2
	1	22	-0.26	0.97	0.16	1.20	0.10		A	0.62	1.20	0.36	0.77	-
		A	-	1.02	-0.32	0.68			3	1.44	1.60	0.20	0.57	-
			0.70	1.29	-0.ko	0.51		1	C	3.46	2.26	0.20	0.56	-
	100	C	2.33	1.78	-0.40	0.49			D	5.18	2.67	0.26	0.65	-
		D	3.90	2.10	-0.38	0.51	-	- 1	E	7.50	3.17	Outsi	0.83	-
	200		6.15	2.53	-0.22	0.62	••		F	9-37	4.15	1.86	1.39	-
			6.87	3.48	0.56	1.07		- 1	Ga .	9.84	4.90	8.42	2.49	***
		0	9.70	4.50	6.32	1.91		i	M	10.52	5.22	12.90	4.00	••
	- 1	H	11.20	5.07	12.74	3.20		- 1	1	6.43	5.20	9.84	5.34	0.1
		T	7.43	5.28	8.98	4.56	0.65	- 4	3	2.60	4.38	17.UB	5.72	19.5
		3	2.75	4.77	16.50	5.47	12.30	1	K	1.00	3-37	9.26	5.50	-
	4		0.94	3-77	10.82	5.86	4.20		L	0.59	2.67	4.54	5.00	2.0
		L	0.55	3.26	5.58	5.50	4.10	- 1	H	0.33	2.42	2.25	4.29	36.2
		×	0.33	2.75	2.60	4.82	13.20				1.61	0.72	2.79	0.1
			0.12	1.82	0.66	3.17		- 1	2W	-0.10	0.94	0.22	1.60	-
		24	0.01	1.14	0.24	1.80		- 1	48	-0.17	0.53	0.06	0.93	
		64		0.46	0.06	0.95			64	-0.17	0.32		0.44	-
	100			0.34		0.43		- 1	8w	-0.17	0.16	-	0.16	-
		84		0.17		0.14		- 1	106	-0.15	77.05	••	0.06	
		10V		0.01			=		126	-0.1	6.01			-
	-	124						- 1	16	-0.12				
									18w	-0.10	-	***		
								- 1	-					
								- 1	20H	-0.10	•••			-
								1	5/M		••		-	
									264	-0.10				
									200	0.20				•

(2 of 7 sheets)

Table & M(Continued)

		10	rward, Av	Speed -	2.7 mph	The State of the S		at Indica		verse. Av	Speed .	2.6 mph	IS MITTER	
Roy	Position	Location	P ₆	7	· Pg	Pg	P ₁₀	Position	Location	P6	P.7	PB	Pg	10
9	2*8 1-1/2*8	12E 10c 8E 6E 4E	1.90 2.10 1.00	0.50 0.60 0.84 0.80 0.60	1.10 1.30 1.90 1.90	0.18 0.42 0.76 1.00	1.10 1.10 1.00 1.00 1.00	k°s	172 108 68 68 48	2.50 3.00 2.24 1.50 1.10	1.00 1.16 1.16 1.16 1.00	0.80 1.60 1.80 1.40	0.44 0.90 1.40 1.90	::
		A B C D	-0.70 -0.50 0.42 2.80 4.40	0.60 0.58 0.70 1.50 1.60	0.70 0.50 0.30 0.24 24.00	0.80 0.50 0.32 0.36 0.42	0.75 0.80 0.90 0.90 0.95		A B C	1.00 1.10 1.90 3.90 6.20	1.10 1.10 1.50 1.90 2.40	1.00 1.00 1.00 1.00	1.60 1.00 0.90 1.10 1.16	:
	La grand	P O H	6.60 10.60 12.24 14.16 10.00	1.90 2.70 3.40 3.80 4.10	0.30 0.80 3.70 5.40 5.10	0.56 1.16 2.16 3.36 4.60	0.95 0.95 1.00 0.95	3 "s	E 0 H	8.90 11.60 12.64 14.10 9.70	2.90 3.60 4.~	1.20 2.30 5.50 6.00 5.60	1.50 2.50 3.90 6.10 7.50	:
		J K L M	1.38 0.90 0.44 0.10	3.70 3.00 2.50 2.10 1.30	7.00 5.50 3.50 1.90 0.80	5.30 5.30 5.00 4.20 2.70	Ē		J K L M	4.70 2.20 1.70 1.30 0.70	3.60 3.00 2.50 2.00 1.30	5.10 3.90 2.10 1.20 0.80	7.90 7.20 6.40 5.40 3.40	=
		2W 6W 8W 10W	=	0.82 0.32 0.16	0.50	0.80 0.40 0.18	:	7-	2W 4W 6W 8W 10W	0.52 0.50 0.48 0.48	1.00 0.60 0.40 0.36 0.30	0.70 0.70 0.70 0.70 0.70	2.00 1.00 0.50 0.30	0.50 0.50 0.50 0.50 0.50
									12W 14W 16W 18W 20W	0.48 0.48 0.48 0.48	0.20	0.70 0.70 0.70 0.70 0.70	:	0.50 0.50 0.50 0.50 0.50
									56M 57M 55M	0.48 0.48	=	0.70 0.70 0.70	:	0.50 0.50 0.50

	Pot	ward, Ave	Speed =	2.7 mph				Res	erse, Av	Speed =	2.6 mph		
Position	Location	D ₁	D2	D3*	D _k	D ₅	Position	Location	D,	p ⁵	D3.	Di	D ₅
2"3	12E	0.020	0.007		••	-0.001	4"S	12E	0.415	0.006		0.002	0.0
1-1/2"5	10E	0.016	0.004		0.002			10E	0.00.0	0.003		0.003	0.0
	8E	0.013	0.002		0.003	0.002		8E	0.008	0.002		0.004	0.0
	6E	0.010	0.002		0.704	0.006		6E	0.010	0.002		0.004	0.0
1"8	hE .	0.013	0.003		0.003	0.027	100	4E	0.015	0.004		0.003	0.0
100	2E	0.017	0.006		0.002	0.048		2E	0.025	0.008		0.002	0.0
	A	0.029	0.011		0.002	0.032		A	0.045	0.016		0.001	0.0
8-6	3	0.054	0.021		0.001	0.024		В	0.080	0.026		0.001	-0.0
FL 22	C	0.083	0.030		0.202	0.020		C	0.103	0.032		0.003	-0.0
	D	0.089	0.033		0.002	0.020		D	0.103	0.033		0.004	-0.00
4 3		0.092	0.036		0.003	0.019	100	E	0.105	0.034		0.005	-0.00
	2	0.111	0.038		0.006	0.019	3"8		0.106	0.030		0.009	-0.00
	0	0.085	0.030		0.011	0.023	1	0	0.075	0.021		0.014	0.0
	H	0.050	0.050		0.015	0.031		H	0.035	0.010		0.017	0.0
1	I	0.025	0.000		0.019	0.046	- 1	1	0.017	0.004		0.018	0.03
	J	0.012	0.005		0.020	0.060		J	0.010			0.016	0.0
	K	0.005	0.002		0.017	0.070	- 1	K	0.005	-0.002		0.011	0.0
	L	0.004	0.002		0.015	0.075		L	0.004	-0.003		0.009	0.0
- 1	H	••			0.012	0.075	ı	H	0.004	-0.004		0.007	0.0
	N	••			0.007	0.059	1		0.003	-0.00k		0.003	0.00
1	7A 5A	••	0.500		0.004	0.038		511	0.003	-0.00k		0.002	0.0
	6W	••			0.001	0.022		W.	0.002	-0.004			0.00
- 1	8w	••			••	0.012		en en	0.002	-0.00k		••	-0.00
	10W		••		••	0.003	- 1		0.002	-0.00k		••	-0.00
					••		- 1	104	0.002	-0.004		••	-0.0
100	12W	••	**		••	0.002	1	12W	••	-0.00k		••	-0.01
E	16W	••	••		••	0.001	- 1	144		+0.00k			-0.0
	16W	-	••		••	0.001		16W	••	-0.104		••	-0.00
1-1/2"8	TOM		••		••	••	- 1	184	••	-0.00		••	-0.03
1-42.0								50M		-0.0 M		••	-0.01
10 V								5/M 55M	••	-0.001		••	-0.01
2"8								264	::	-0.00k			-0.0

s Not working.

(3 of 7 sheets)

Table At #(Continued)

	The same of	, oi	THE AV	Speed -	2.0 mb		Walter of	at Indica	Re	verse, Av	Speed -	2.7 mm		Land of
	Position	lecation	16	1	Pa	-	10	Position	Location	P6	7,	P8	-9	10
16	178	LE	2.00	0.50	-2.80	0.40	-1.50	0	122	3.90	0.62		0.50	••
		108	3.00	0.64	-2.30	0.80	-1.50		108	4.00	0.90	4.70	0.90	•
			1.40	0.70	-0.30	1.20	-1.50		86	2.00	1.04	8.00	1.42	••
		68	-0.40	0.90	1.00	1.64	-1.50		GE AE	0.60	0.80	5.10	1.96	1.0
	Part of the last		-0.50	0.70	-0.60	1.76	-1.00		1000	-		0.70	1 10000000	1.0
	SECTION AND ADDRESS.	21	-0.70	0.54	-1.40	1.40	••	471 S	22	0.50	0.80	0.50	1.50	3.7
		A	-0.60	0.50	-1.40	0.90	-1.50		A mil	0.60	0.90	0.50	1.10	0.7
				0.70	-1.70	0.70	-1.50			1.10	1.20	0.40	0.90	1.2
		C	1.60	1.10	-1.80	0.80	-1.50		C	3.00	1.60	0.40	0.96	1.25
		D	3.20	1.50	-1.80	0.84	-1.50		D	4.80	1.44	0.30	1.00	1.25
	2017		5.30	1.70	-1.80	1.00	-1.50		E	7.00	2.30	0.60	1.30	1.2
			8.42	2.40	-1.80	1.72	-1.25		7	9.10	2.90	1.50	2.10	1.2
		G	9.77	2.90	1.10	2.90	-1.25		0	10.10	3.40	4.90	3.44	1.2
	0	H	11.80	3.50	4.50	4.50	-1.25	S. 10 TO	н	11.70	3.80	5.90	5.10	1.2
		1	8.40	3.50	3.20	6.00	2.75		1	7.70	3.60	4.90	6.60	6.25
	CONTRACTOR	3	3.60	3.40	7.10	6.90	13.20	and the second	3	3.30	3.20	7.22	7.00	17.50
		X	1.30	2.60	5.10	7.00		July 19	K	1.30	2.40	2.40	6.50	0.7
	1"8	L	0.90	2.30	3.00	6.40	7.00		L	0.70	1.90	0.50	5.50	10.7
		H	0.52	1.80	1.75	5.40	25.00		M	0.50	1.70	-0.30	5.00	27.7
			0.30	1.40	0.60	3.40	1.50		×	••	1.20	-0.50	3.20	1.7
	001018-41	2W	••	0.90	0.30	1.90	2.50	100	2W	-0.30	0.90	-0.50	2.00	0.75
	O CONTRACTOR	M		0.50	••	1.00	0.50		44	-0.30	0.50	-0.60	1.20	1.00
		6W	••	0.36		0.50	0.25		6W	-0.30	7.40	-0.60	0.50	1.0
	100	84	••	0.20	••	0.20	0.25	100	8w	-0.30	0.10	-0.60	0.30	1.00
		10V	••	••	-	••			10M	-0.30		-0.60	0.22	1.00
								1,8	1.2W	-0.30		-0.60		1.00
									144	-0.30		-0.60	••	1.00
									1GW	-0.30	**	-0.60	••	1.0
								A STATE OF	18w	-0.30	-	-0.60	••	1.00
									20M	-0.30		-0.50	••	1.0
								4 (4)	22W	-0.24	••	-0.50	••	1.00
									24W	-0.24		-0.50		1.00
									26W	-0.20		-0.50		1.00

MILE U.S.	Por	mard, Av	Speed =		- 1 - 1			Re	verse, Av.	Speed .	2.7 mph		
Position	Location	D1	D ⁵	D3.	Di	D ₅	Position	Location	<u></u>	D ₂	D3*	Di	D ₅
1,8	125	-0.dig	0.001		-0.003	-0.049	0	125	0.020	0.011		0.005	
TEMPORE	10	-0.055	-0.001		-0.002	-0.048		10E	0.018	0.009		0.007	
1 1 1 20	a	-0.060	-0.003		••	-0.045		8E	0.016	0.008		0.009	0.0
The second	6E	-0.060	-0.003			-0.041		6E	0.018	0.010		0.007	0.0
	LE .	-0.057	-0.001		-	-0.031		4E	0.020	0.013		0.006	0.0
	2	-0.053	0.001		-0.002	-0.028		2	0.032	0.019		0.006	0.0
	A	-0.040	0.00		-0.003	-0.036		A	0.055	0.036		0.005	0.0
THE REAL PROPERTY.		-0.019	0.025		-0.003	-0.042	100	3	0.091	0.049		0.005	0.0
STATE OF THE PARTY	C	0.105	0.073		-0.003	-0.046		C	0.148	0.058		0.007	0.0
	D	0.080	0.056		••	-0.046	1 3 3	D	0.100	0.061		0.009	0.0
		0.070	0.052		*	-0.048	100		0.105	0.062		0.011	0.0
A COMPANY		0.139	0.056		0.004	-0.046			0.155	0.057		0.017	0.0
100	0	0.105	0.002		0.012	-0.041	100	G	0.050	0.037		0.024	0.0
0		0.055	0.029		0.018	-0.029	100	H	0.015	0.019		0.029	0.0
		0.026	0.015		0.023	0.017		1	. **	0.009		0.029	0.1
5024	J	0.011	0.007		0.025	0.087		J	-0.012	0.004		0.026	0.1
		0.005	0.004		0.021	0.087		к.	-0.014	-		0.019	0.1
178	L	0.004	0.001		0.019	0.108	40	L	-0.015	••		0.015	0.1
1000		••	0.001		0.005	0.143	- 1		-0.015			0.011	0.1
	30.00		••		0.008	0.104	- 1		-0.017	••		0.006	0.0
E. 18	24		••		0.003	0.059	4	24	-0.017	••		0.003	0.0
S. W. CO.	6W	••	••		-	0.030		PA.	-0.018	••		••	-0.0
	OW .	=	=			0.005	10	6N	-0.018			••	-0.0
	10W	-	7.75		-	0.003	1.7	10W	-0.019			••	-0.0
	12V		-			••			-0.019	-		•	-0.0
					7.0		1"8	12W	-0.019	••			-0.0
								144	-0.020	••		••	-0.0
							1	16W	-0.020				-0.0
							2.5	18W	-0.020			••	-0.0
									- 10000				-0.0
								22W	-0.020	**			-0.0
							2.24	264	-0.020				-0.0
								56M	-0.020	••			-0.0

. But working.

(% of 7 sheets)

Tuble Alg(Continued)

			rward, Av			tical Pre	saure, ba	at Indica	red Calls	verse, Av	· Cread ·	97-4		
	100	THE PERSON NAMED IN COLUMN TWO			-	-	-						-	
ROW	Position	Location	-6		-8	<u>P9</u>	10	Position	Location	16	-7	-8	<u> </u>	F ₁₀
11	0	128	4.20	3.00	3.30	1.10	1.25	0	128	3.50	3.00	0.20	0.50	
		100	4.90	3.10	3.42	1.30	1.25		126	3.10	3.00	0.80	0.90	-0.25
	Marin Carlo	82	3.40	3.40	5.00	1.70	1.25		88	1.30	3.20	2.60	1.40	-0.25
		6E	2.22	3.20	6.00	2.10	1.10	HAT THE PERSON	6 <u>z</u>	0.20	3.10	2.20	1.70	-0.25
		4E	1.80	3.10	4.20	2.10	1.00		4E	-0.30	3.00	-0.60	1.70	0.10
	TEST BUT IN	25	1.60	3.20	3.62	1.90	2.25		28	-0.42	2.80	-1.30	1.10	2.10
		A	1.80	3.24	3.40	1.40	0.75			-0.38	3.00	-1.40	0.80	-0.90
			2.00	3.44	3.22	1.30	0.75	10.11			3.30	-1.40	0.50	-0.90
		C	2.80	3.70	3.20	1.30	0.80		C	1.00	3.40	-1.40	0.60	-0.90
		D	3.50	4.00	3.10	1.40	0.80	J. BR.S	D	1.90	3.70	-1.44	0.70	-0.90
		E	4.30	4.30	3.10	1.50	0.90	1"S	E	2.90	4.10	-1.46	0.80	-0.95
		7	5.70	4.70	3.00	2.00	0.90	THE RESERVE	F	4.00	4.80	-1.02	1.44	-0.95
	4 15 15 19	0	6.20	5.40	3.40	2.90	1.00	10.00	G	4.90	5.00	0.24	2.40	-0.95
	37 1 27 17 100	H	6.40	5.50	3.84	3.90	0.75	The second second	н	5.30	5.20	1.10	3.60	-0.90
	VASA DISE		4.40	5.70	3.60	4.90				4.00	5.40	1.06	4.60	-1.00
		J	2.20	5.40	4.20	5.40	-0.25		J	2.10	5.20	1.80	4.90	-1.05
		K	0.90	4.90	3.24	5.22	-0.25		K	1.00	3.10	1.10	4.60	-0.95
		L	0.60	4.70	2.20	4.40	-0.25		L	0.60	2.30	0.50	4.10	-1.00
		N.	0.30	4.30	1.50	4.00	-0.30	The second	H	0.42	1.80	0.18	3.60	-1.10
				3.50	0.80	2.76	••			•	1.30	-0.50	2.14	-0.90
	5.9 66 04	2W	••	3.20	0.50	1.60	0.25		2W	••	0.90	-0.64	1.50	-0.75
		No.	-	2.90	0.20	0.90	0.30		WW .	••	0.70	-0.76	0.80	-0.75
	The State of	6W		2.70	0.20	0.50	0.30		6W	••	0.40	-0.80	0.40	-0.75
	NAME OF THE OWNER, OF	Bu	-	2.50	0.20	0.22	0.25	1 2 2	8w		0.20	-0.92	0.20	-0.75
		10W	••	2.30	0.10	••	0.25		10W		••	-0.92	••	-0.75
	1"H	124	••	2.10	••		••		12W	••		-0.80	••	-0.75
700	100	144	••	2.00	••	••			144	••	••	-0.80		-0.75
	SET TO RULL	16W	••	2.00		**	••	100	16W		••	-0.80	••	-0.75
	10 M	18W	-	1.50	-	**	••		18w		••	-0.80	•	-0.75
	100	50M		1.40	•	**	••		50M		••	-0.80	••	-0.75
		22M	••	1.00	••	-	••		22W	••	••	-0.80	••	-0.75
		SIM	••	••		•	**		54M		••	-0.80	••	-0.75
								10000	26W			-0.80	••	

Service Contract	Por	Ward, Av	Speed =				n., at Indi		verse, Ave	Speed =	2.7 mph		S TO U
Position	Location	<u>D</u> 1	D2	D3.		D ₅	Position	Location	_ <u>D</u> _	D ⁵	D3.	Di	D ₅
0	122	0.035			-0.003	0.010	0	128	-0.008	0.011			
Late Died in	100	0.028	-0.004		-0.002	0.011	100	10E	-0.015	0.008		0.005	0.00
	82	0.025	-0.005		••	0.014	11.0	8E	-0.016	0.007		0.007	0.01
	6E	0.025	-0.006			0.019		6E	-0.017	0.009		0.005	0.0
44	48	0.024	-0.004		••	0.025		4E	-0.013	0.013		0.004	0.00
	28	0.028			-0.001	0.025		28	-0.009	0.021		0.004	0.02
	A	0.035	0.010		-0.002	0.020	1,447	A	0.001	0.034		0.004	0.00
		0.040	0.027		-0.002	0.015			0.016	0.054		0.004	0.0
	C	0.050	0.043		-0.001	0.011		C	0.030	0.064		0.006	0.00
	D	0.055	0.052		••	0.010	100	D	0.035	0.065		0.007	0.3
- 7		0.060	0.056		••	0.009	1"8		0.035	0.065		0.000	0.0
TO STATE	7	0.060	0.060		0.005	0.010	Section 1		0.035	0.061		0.016	0.0
	0	0.050	0.050		0.013	0.017	due of the same	3	0.022	0.038		0.024	0.0
	H	0.030	0.030		0.020	0.029		H	0.006	0.020		0.026	0.0
	1	0.015	0.014		0.027	0.063		1	-0.005	0.009		0.029	0.10
0.1	3	0.007	0.006		0.030	0.095	The State of	3	-0.010	0.004		0.026	0.11
Jan Park	K		0.001		0.026	0.111		K	-0.OL3	••		0.018	0.12
175	L	••			0.022	0.127		L	-0.014			0.013	0.12
	H	••	••		0.018	0.136	- 1	H	-0.014	••		0.008	0.11
10.5		•	-0.003		0.012	0.101			-0.014	••		0.003	0.06
	24		-0.003		0.006	0.058	10.7	2W	-0.015	••		••	0.03
	LW .	••	-0.003		0.002	0.030	and the second	lete	-0.014			-0.003	0.02
30 1 15 15	6W	••	-0.003		••	0.016		6W	-0.014			-0.003	0.00
	8W	••	-0.003		-	0.008		8w	-0.024	**		-0.003	0.00
178	10W 12W	**			:	0.003	707	10W	-0.014			-0.003	0.00
		10000				. 70.5		12W	-0.024	••		-0.003	0.00
								144	-0.013	-		-0.003	0.00
								16W	-0.013	••		-0.003	0.00
								18v	-0.013	••		-0.003	0.00
								50N	-0.013	••		-0.003	0.00
								22H	-o.a3	••		-0.003	0.00
								24W	-0.013	••		-0.003	0.00
								26W	-0.013			-0.003	0.00

8 But smoking

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Table AM(Continued)

F2	Seature and	10	mard. Av	Speed -	2.65			in at leaster	Re	verse, Av	Speed -	2.50 mph		47000
-	Position	Location	16	1	78	3	P ₁₀	Position	Location	P6_		P ₈	<u>'</u> 9	P10
13	170	263 243 252 263 163	0.42 0.42 0.42 0.48	0.29 0.32 0.32 0.43	0.42 0.40 0.42 0.39 0.40	0.46 0.48 0.48 0.48	0.33 0.34 0.35 0.35	i	26E 24E 20E 10E	0.03 0.06 0.08 0.16	0.07 0.17 0.13 0.30	0.07 0.05 0.08 0.07 0.07	0.06 0.08 0.10 0.12 0.17	=
		168 148 153 108 68	0.65 1.02 1.53 1.64 1.20	0.54 0.60 0.91 0.97 0.98	0.40 0.42 0.46 0.51 0.84	0.53 0.63 0.80 1.01 1.30	0.35 0.35 0.35 0.35 0.35	1"8	16E 1ME 12E 10E 6E	0.39 0.95 1.66 1.69 0.97	0.41 0.63 0.57 0.76 0.96	0.06 0.05 0.05 0.27 0.88	0.20 0.33 0.49 0.80 1.20	0.0
		8 4	0.71 0.47 0.43 0.49 0.72	1.03 0.92 0.97 0.92 1.02	1.05 0.73 0.50 0.34 0.29	1.53 1.51 1.38 1.11 0.98	0.35 0.28 0.21 0.22 0.22		41 22	0.21 -0.06 -0.03 0.10	0.60 0.70 0.71 0.79 0.90	0.89 0.46 0.11 -0.05 -0.13	1.36 1.31 0.97 0.66 0.51	-0.00 -0.11 -0.11 -0.00
		C D E	1.19 1.5k 1.92 2.03 3.42	1.43 1.65 1.73 2.29 2.70	0.22 0.25 0.18 0.47 0.72	0.97 1.03 1.15 1.54 2.14	0.23 0.23 0.23 0.22 0.21		C D E F	0.63 0.98 1.40 2.37 2.97	1.35 1.50 1.81 2.10 2.59	-0.11 -0.13 -0.09	0.54 0.58 0.75 1.20 1.89	-0.0
			3.11 1.98 1.16 0.53 0.37	2.80 3.02 2.62 2.21 2.04	1.23 1.80 1.49 1.05 0.83	2.81 3.41 3.71 3.50 3.18	0.21 0.20 0.12 0.08		H I J K L	2.82 2.00 1.20 0.52 0.30	2.86 2.71 2.59 2.01 1.75	1.33 1.70 1.46 1.18 0.95	2.70 3.34 3.55 3.24 3.02	-0.1 0.0 0.1
		# 2 2 4 6 6	0.23	1.12 0.85 0.51 0.34 0.11	0.57 0.24 0.08	2.80 1.91 1.23 0.71 0.36	E		M H 2W 4W 6W	0.18 -0.10 -0.19 -0.28 -0.27	1.57 1.19 0.74 0.45 0.39	0.78 0.44 0.26 0.24 0.21	2.61 1.82 1.11 0.60 0.30	0.1 0.1 0.1
		86 106 186 186	-0.04 -0.03 -0.02	0.05	-0.04 -0.03 -0.02	0.11	:		84 104 124 144 164	-0.25 -0.25 -0.25 -0.25	0.28 0.13 0.20 0.15 0.11	0.20 0.15 0.18 0.18 0.19	0.10	0.1 0.1 0.0 0.0
									1.6w 25W 25W 26W 26W	-0.24 -0.25 -0.25 -0.25	0.13 0.16 0.14 0.10 0.23	0.18 0.19 0.18 0.20 0.20	=	0.0

		- Joseph	d. Avg Speed = 2.				Revers		d = 2.50 mph	
	Position	Location	<u>p</u> 6 <u>p</u> 4.	<u>D</u> 8	_ <u>Po</u>	Position	Location	D ₆		Dg
3	ĵ	262 242 262 202 182	0.003 -0.003 -0.002	-0.005 -0.005 -0.005 -0.005	-7.022 -0.022 -0.022 -0.022	i	262 242 222 202 186	0.001 0.002 0.003 0.006 0.010	0.000	0.001
		162 1142 122 103 88	0.005 0.005 0.005	0.001	-0.026 -0.021 -0.022	1"8	162 142 122 102 82	0.005 0.005 0.005	0.002 0.005 0.006	0.002 0.003 0.004 0.006 0.011
		4	0.001 0.005 0.014 0.030	0.001 0.002 0.003	-0.003 -0.003 -0.000 -0.000		62 42 22 A B	0.006 0.009 0.017 0.031 0.047	0.005 0.005 0.004 0.004	0.020 0.031 0.034 0.025 0.022
		C D H	0.066 0.051 0.055 0.059 0.069	0.001 0.002 0.003 0.007 0.014	-0.021 -0.022 -0.023 -0.022 -0.017		C D E P	0.056 0.058 0.059 0.052 0.034	0.007 0.006 0.00 0.017 0.023	0.021 0.020 0.022 0.028 0.040
			0.031 0.017 0.009 0.00k 0.003	0.020 0.025 0.027 0.024 0.020	-0.00k 0.032 0.10k 0.097 0.112		N I J K L	0.017 0.006 0.002 -0.002	0.026 0.027 0.024 0.017 0.014	0.065 0.114 0.136 0.119 0.137
		***************************************	0.00T 0.00T 0.00S	0.017 0.010 0.006 0.003 0.007	0.116 0.114 0.067 0.095 0.092		en Sh Pa B B	-0.002 -0.003 -0.003 -0.003	0.000 0.006 0.003 0.001	0.143 0.056 0.022 0.005 -0.005
		00 100 190 3/40	Ē	Ξ	0.002 0.005 0.003		0v 10v 12v 14v 16v	-0.003 -0.003 -0.003 -0.003	=	-0.009 -0.011 -0.011
	•	160 180			0.001		18w 20w 22w 24w 26w	-0.003 -0.003 -0.003 -0.003		-0.01 -0.01 -0.01

· Dit wetter.

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Table AMConcluded

				A	Ye A	rucal m	essure, p	si, at Indica	red Cells		- C 3	2.66 mg/n		
			LANG VA	Deed -	15.0 mpl		•				P ₇			P
OV	Position	Location	P ₆	P7	- 28	P ₉	P ₁₀	Position	Location	P ₆			Pg	P ₁₀
15	1"8	26E	-0.06	0.57	-0.30	0.28	-0.50	0	20E	••	0.08	0.04		0.05
		241	-0.08	C.57	-0.30	0.26	-0.12	1"8	SIT		0.06			0.0
		55E	-0.05	0.57	-0.30	0.27	-0.57	1	22E		0.06			0.03
		20E	-0.05	0.67	-0.35	0.27	-0.54		50E		0.19			0.02
		18E	-0.02	0.55	-0.38	0.28	-0.55		18E	0.06	0.27		0.04	
		16E	0.04	0.65	-0.42	0.30	-0.56	1	16E	0.16	0.27	-0.03	0.0%	
		146	0.21	0.78	-0.38	0.36	-0.56	1	14E	0.37	0.55		0.11	••
	1	12E	0.32	0.93	-0.35	0.45	-0.56		12E	0.60	0.50		0.24	
		10E	0.37	1.06	-0.30	0.56	-0.56		102	0.66	0.62	0.12	0.40	0.03
		BE	0.25	1.06	-0.20	0.73	-0.56		8E	0.52	0.72	0.31	0.60	0.04
		6 z	0.15	1.03	-0.16	0.84	-0.56		6E	0.34	0.80	0.42	0.72	0.00
		LE.	0.04	0.97	-0.16	0.86	-0.58		4E	0.24	0.59	0.33	0.69	0.08
		21		1 02	-0.27	0.75	-0.56		2E	0.20	0.70	0.25	0.50	0.04
		A	0.05	0.98	-0.35	0.66	-0.56		A	0.19	0.61	0.10	0.38	0.04
		B	0.20	1.12	-0.43	0.60	-0.58		В	0.28	0.83	0.13	0.28	0.04
		C D E	0.46	1.44	-0.41	0.60	-0.60		C	C.47	0.95	0.05	0.28	0.04
		D	0.65	1.32	-0.45	0.67	-0.60		D	0.65	1.36	0.09	0.32	0.0
		E	0.95	1.50	-0.45	0.74	-0.63	1	E	0.92	1.32	0.0	0.40	0.04
	1		1.68	1.77	-0.36	1.00	-0.67		r	1.58	1.76	0.17	0.69	0.06
		0	2.26	2.15	-0.25	1.38	-0.70	1	G	2.13	1.85	0.34	1.09	0.18
		н	1.97	2.31	0.31	1.84	-0.68	ľ	н	1.79	1.98	0.92	1.55	0.24
		1	1.12	2.28	1.73	2.21	-0.66		I	1.17	2.12	1.61	1.94	0.36
		J	0.65	2.06	1.12	2.48	-0.64	1	J	0.76	1.96	0.71	2.13	0.60
		K	0.35	1.74	0.66	2.21	10.83		K	0.47	1.67	0.50	1.94	10.26
		L	0.26	1.49	0.56	2.02	1 60	ľ	L	0.29	1.50	0.42	1.70	0.80
		н	0.17	1.30	0.42	1.80	0.36		н	0.21	1.42	0.36	1.49	-0.08
		H	0.06	1.07	0.30	1.25	0.34	1	N	0.05	1.00	0.19	1.03	-0.06
	1	2W		0.74	0.20	0.76	0.30	- 1	2W	••	0.68	0.08	0.56	-0.10
		44	0.0	^.52	0.12	0.40	0.24	-	4W		0.63	0.04	C.24	-0.10
		6W	J.06	0.20	0.08	0.18	0.14	1	634	••	0.37			-0.16
		8w	0.0	0.13	0.06		0.14	1	8w		0.36		-0.18	-0.16
		10W	0.04	0.21	0.09	-0.07	0.07		10W 12W		0.22		-0.19 -0.20	-0.14
		12W		0.06	0.06	-0.10	0.05				0.30			
		16W		0.09	0.05	-0.13 -0.12	0.03		16W 16W	•.•	0.10	0.04	-0.20	-0.10
		18w		-	0.06	-2.10			18W		0.21		-0.20	-0.08
						-0.08			20M		0.30		0.20	-0.06
		50M			0.05				22W		0.26		-0.20	-0.08
	i,	24W				-0.05 -0.03			244		0.36		-0.20	-0.08
								•						-0.08
	7	26W				-0.03		T	26W	••	0.25		-0.20	-(

	former	d. Avg Spee				at Indicated		a, Avg Spee	ed = 1.66 mph	
Position	Location	D ₆	D7*	D8	ಶ್	Position	Location	D ₆	D-7 D-8	D ₉
1"8	26E	-0.004		-0.002	0.004	0	26€	0.002		0.002
	24E	-0.004		-0.002	0.004	1*8	24E	0.003		0.002
	222	-0.003		-0.002	0.004		22E	0.005		0.002
	20E	-0.001		-0.002	0.004		20E	0.008		0.002
	18E	0.002		-0.002	0.004		18E	0.011	0.002	0.003
	16E	0.005		-0.001	0.004		16E	0.014	0.002	0.003
	14E	0.006		-	0.004		14E	0.014	0.004	0.004
	12E	0.004		0.001	0.005		12E	0.011	0.004	0.005
	105			0.002	0.005		10E	0.008	0,006	0.007
	8E	-0.002		0.003	0.009		80	0.008	0.007	0.013
	6E	-0.002		0.003	0.013		6E	0.009	0.007	0.019
	4E	-0.001		0.003	0.020		4E	0.013	0.005	6.02
	2E	0.004		0.001	0.023		2E	0.023	J. 004	0.027
	A	0.014		0.001	0.018		A	0.038	0.004	0.023
	В	0.032		0.001	0.013		В	0.056	0.005	0.019
	C	0.049		0.002	0.009		C D	0.066	0.007	0.017
- 1	D	0.056		0.002	0.008		D	0.068	0.009	0.016
	E	0.061		0.003	0.008		E	0.068	0.077	0.017
1	7	0.066		0.008	0.009		r	0.061	0.018	0.024
	G	0.056		0.015	0.014	1	0	0.041	0.025	0.037
	н	0.036		0.023	0.009		н	0.022	0.329	0.063
	1	0.020		0.029	0.060		1	0.009	0.029	0.105
1	J	0.010		0.031	0.098		J	0.003	0.025	0.127
	K	0.006		0.027	0.117		K	••	0.017	0.129
	L	0.004		0.023	0.126	1	L		0.014	0.131
	м	0.003		0.020	0.137		H	-0.000	0.010	0.128
- 1		0.002		0.012	0.113		N	-0.001	0.005	0.077
- t	2W	0.001		0.007	0.068	i	21	-0.001	0.002	0.040
1	4W			0.004	0.038	i i	r.m	-0.001		0.020
	6W			0.002	0.021		6W	-0.001	-0.001	c.010
_1	8W			0.001	0.011	1	BM	-0.001	-0.002	0.007
	10W				0.005		10W	-0.001	-0.002	0.005
	12W				0.002		12W	-0.001	-0.002	0.005
	14W	••			0.001		14W	-0.001	-0.002	0.005
	16W				0.001		16W	-0.001	-0.002	0.005
7	18k						18w	-0.00L	-0.002	0.005
							50M	-0.001	-0.002	0.005
							221	-0.000	-0.002	0.6-
						1	264	-0.001	-0.002	0.00
							26W	-0.001	-0.002	0.005

• Not working

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Table 4-19

Multiple-Wheel Heavy Gear Load Flexible Payerset Test, Dynamic Instrumentation Loading Data

Item %; Load Condition: 30 hips per Wheel, Twin Tanden, 100 pei

H	_		met.	We figured	7.52 pm	rtical	Personal Property in	at Indio	ated Cell	-	- Bearing	2.50 mg		
ow.	Position	Location		7,	-	7	15	Position	Location			7.	-	7
,	1"8	262	••	-0.52	2.08	-0.25	••	2"11	ave	••	0.10		0.08	
		24E		-0.44	1.08	-0.25		• •	:25		0.24		0.16	-
		22X	••	-0.30	1.12	-0.19		- 1	200		0.64	0.12	0.32	_
		200	••	-0.08	1.12	-0.10			182	••	1.08	0.36	0.48	
		188		0.20	1.20	0.10			162		1.64	0.76	0.72	0.
		16E		0.70	1.60	0.25			142		1.84	1.60	1.00	0.
		14E	••	1.14	2.00	0.50	0.18	3 "X	1.21		1.68	2.88	1.28	0.
		125	••	1.20	3.00	0.80	0.50	1	102		1.26	2.56	1.40	1.
		10E		0.82	2.86	1.00	1.09		a.		0.84	1.60	1.40	2.
		388		0.26	1.40	1.10	1.81		62		0.76	1.20	1.20	2.
		6E	••	••	0.40	1.08	1.90		4E	••	0.84	1.08	1.08	1.
		4E			••	0.92	0.93		20	••	1.24	1.00	0.96	1.
		21	••	0.30		0.80	0.10		A		2.16	1.20	1.20	9.
		A		1.00	0.20	0.83	-0.37		В	••	3.82	1.80	1.68	0.
		3		2.38	0.72	1.15	-0.47	1	c		5.90	3.92	2.52	1.
		C		4.40	2.40	1.70	-0.22	٧ .	D		6.B4	7.24	3.20	1.
		D		5.42	4.80	2.15	0.10	2"M	E		7.46	12.60	3.80	1.
	1"5	Z	••	6.40	9.24	2.80	0.55	1	7		7.90	15.76	4.88	4.
	1.5	7	••	7.52	13.92	4.03	2.39	v	G		7.22	13.52	5.80	9.
		0	**	7.56	12.20	5.15	7.00	1."#	M		5.50	19.64	6.00	11.
		H	••	5.82	19.20	5.92	10.28	1	1		3.42	10.80	5.52	12.
		1		3.46	10.84	5.95	11.66		J		2.W	3.20	4.48	13.
		3		1.84	2.84	5.21	13.28		K	••	1.10	1.40	3.20	8.
		I	••	0.60	0.80	3.93	8.34		L		0.76	0.88	2.60	5.
		L	••	0.50	0.48	3.15	5.42		K	••	0.60	0.80	2.04	3.6
		×	••	0.30	0.40	2.53	3.43		16		0.30	0.60	1.26	1.6
		X	••	0.10		1.58	1.11		2V	**	0.10	0.60	0.64	0.9
		2W	••		**	0.89	0.31		44	••		0.60	0.32	0.
	- 1/1	W			-	0.50	0.04		6W			0.60	0.12	
		6W	**			0.28	••		8M	••	••	0.60		0.
		8w		**		0.12	••	_ 1	10M		••	0.60	**	0.
		10M			••	0.10			12W			0.60		0.
		12W				0.08			14W			0.60	**	0.3
		144				0.08		1	16W		**	0.60		0.
		16W		••	••	0.07	••	į	1.8M		••	0.60	**	0.
		184	••	••		0.07			20M			0.60		0.3
		20M		••	**	0.07			55A	••		0.60		0.
		22N	••			0.07		1	24H			0.60		0.3
	9	SPA				0.07		T	264			0.60	••	0.3
	1.00	26H			••	0.07								

(1 of 7 shoots)

Table 419(Continued

	_		1				rtice. Pr	et fure. D	si, et ladic	ated Cell				_	_
7 1"S 26E0.560.76 1"B 26E - 0.84 - 0.060.66 22E - 0.84 - 0.060.66 22E - 0.54 - 0.080.66 22E - 0.54 - 0.080.66 22E - 0.54 - 0.080.66 22E - 0.54 - 0.500.65 22E - 0.55 22E - 0.55 210 0.08 0.020.66 22E - 2.10 0.08 0.0.080.66 22E - 2.10 0.08 0.080.66 22E - 2.10 0.08 0.090.200.20 18E - 2.10 0.08 0.00 0.920.25 18E - 2.10 0.08 0.00 0.920.25 18E - 2.10 0.08 0.00 0.920.25 18E - 2.10 0.08 0.00 0.920.25 18E - 2.10 0.08 0.00 0.920.25 18E - 2.10 0.08 0.00 0.920.25 18E - 2.10 0.08 0.00 0.920.25 18E - 2.10 0.08 0.00 0.920.25 18E - 2.10 0.08 0.00 0.920.25 18E - 2.10 0.08 0.00 0.920.25 18E - 2.10 0.08 0.00 0.25 18E - 2.10 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.08 0.00 0.25 18E - 2.00 0.00 0.00 0.00 0.00 0.00 0.00 0.				reard, At		-	1.	-	Do atatan	-	_		-	- 5	
	ROW	Position	Location		-2					2000					
20x	7	1"5				-0.56			1.4						
2007															
188		i													
16g 0.50 4.20 0.52 -0.45 14g 0.30 4.92 1.20 0.80 0.06 14g 6.40 0.44 1.60 -0.36 14g 5.40 4.52 1.04 0.45 1.27 1.27 4.53 0.92 5.88 0.15 12g 1.50 10.04 1.28 1.11 0 10g 4.36 1.20 4.84 0.99 10g 2.04 0.68 1.26 1.26 1.26 1.26 1.27 1.20 0.60 1.26 1.27 1.27 1.20 0.60 1.26 1.27 1.27 1.20 0.60 1.26 1.27 1.20 0.60 1.26 1.27 1.20 0.60 1.26 1.27 1.20 0.60 1.26 1.27 1.20 0.60 0.88 1.20 3.00 12g 1.55 0.44 0.80 0.21 22g 2.91 1.00 0.88 1.20 3.00 1.20 22g 2.91 1.20 0.68 1.20 0.33 0 8 9.00 0.60 1.60 0.45 1.20 0.48 1.20 0.48 1.20 0.40 1.20 1.20 0.40 1.20 0.40 1.20 1.20 0.40 1.20 1.20 0.40 1.20 1.20 0.40 1														0.46	
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12Z											_				
0 108		ė							- 1						
6E - 1.32 1.12 1.20 2.67 6Z - 1.65 0.28 1.20 3.00 4E - 1.20 0.60 0.88 1.26 2Z - 1.95 0.44 0.80 0.21 A - 3.84 0.60 0.88 0.30 B - 7.05 0.84 1.20 -0.33 0 B - 9.00 0.60 1.60 0.45 C 1.05 11.55 1.20 1.72 -0.06 E - 16.14 8.40 3.04 0.36 E - 16.14 8.40 3.04 0.36 F 5.50 18.60 16.60 3.72 1.99 F 5.50 18.60 16.60 3.72 1.99 F 5.50 18.96 13.20 5.52 11.04 H - 15.00 21.72 5.52 9.93 H - 15.00 21.72 5.52 9.93 H - 14.10 21.64 5.60 16.60 3.72 1.99 E - 16.14 8.40 3.00 0.36 E - 17.76 11.40 3.40 3.40 3.50 F 5.50 18.96 13.20 5.52 11.04 I - 9.60 13.20 5.52 11.04 I - 9.60 13.20 5.52 11.04 I - 2.55 0.64 3.52 9.24 I - 1.65 0.40 2.99 5.65 I - 1.65 0.40 2.99 5.65 I - 1.65 0.40 2.99 5.65 I - 1.65 0.40 3.52 9.24 I - 1.05 0.40 0.96 5.86 II - 0.30 - 1.52 1.23 II - 0.30 - 0.40 3.50 - 0.60 III - 0.30 - 0.20 2.44 3.61 II - 0.30 - 0.30 - 0.20 2.44 3.61 III - 0.30 - 0.30 - 0.20 2.44 3.61 III - 0.30 - 0.30 - 0.20 2.44 3.61 III - 0.30 - 0.30 - 0.20 2.44 3.61 III - 0.30 - 0.30 - 0.20 2.44 3.61 III - 0.30 - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96 III - 0.30 - 0.20 - 0.80 0.96		ĭ								82		2.04			3.66
Let 1.20 0.60 0.88 1.26 Let 1.80 1.00 1.50 0.84 0.80 0.21 A 3.84 0.60 0.88 0.30 A 5.16 0.20 1.20 0.88 A 7.05 0.84 1.20 -0.33 0 B 9.00 0.60 1.60 0.48 A 5.16 0.20 1.20 0.48 A 5.16 0.20 1.20 0.48 A 5.16 0.20 1.20 0.48 A 5.16 0.20 1.20 0.48 A 5.16 0.20 1.20 0.48 A 5.16 0.20 1.20 0.48 A 5.16 0.20 1.20 0.48 A 0.30 0.36 D 1.50 2.20 0.66 D 1.60 0.40 0.66 D 1.60 0.40 0.66 D 1.60 0.40 0.66 D 1.60 0.40 0.66 D 1.60 0.40 0.66 D 1.60 0.40 0.40 D 1.60 0.40 0.40 D 1.60 D 1.60 D 1.60 D D D D D D D D D			65.		1.32	1.12	1.20	2.67	1	6x		1.65	0.28	1.20	
22															1.50
S						0.44		0.21		21					
C 1.05 11.55 1.20 1.72 -0.06			A												
D = 13,60 3,20 2.08 0.06 E = 16,14 8,40 3.04 0.36 E = 17.76 11,40 3,40 1.50 F 5,50 18,66 16,60 3.72 1.95 F 5,50 18,96 11,60 4.84 6.30 H = 15,00 21.72 5.52 9.93 H = 14,10 21.64 5.60 10.80 I = 9,60 13,20 5.52 11.04 I = 9,60 13,20 5.52 11.04 I = 1.05 0.40 2.92 5.50 M = 1.05 0.40 2.92 5.96 M = 1.05 0.20 2.44 3.81 M = 0.30 - 1.52 1.23 M = 0.30 - 1.52 1.23 M = 0.30 - 0.30 - 0.80 M = 0.30 - 0.80 0.36 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.20 M = 0.30 - 0.30 - 0.30 M = 0.30 - 0.30 M = 0.30 - 0.30 M = 0.30 - 0.30 M = 0.30 - 0.30 M = 0.30 - 0.30 M = 0.30 - 0.30 M = 0.30 - 0.30 M = 0.30 - 0.30 M = 0.30 - 0.30 M = 0.30 - 0.30			3		7.05	0.84	1.20	-0.33	0	3		9.00	0.60	1.60	0.45
			C	1.05	11.55	1.20			4		1.10				
Total Section Sectio				-											
18.96 11.60 1.84 6.30 0 18.00 12.00 5.28 6.37										Z					2.50
H - 15.00 21.72 5.52 9.93 I - 9.60 13.20 5.52 11.04 I - 9.09 10.40 5.16 11.61 I - 9.09 10.40 5.16 I - 9.09 10.40 5.16 I - 9.00 10.40 5.16 I - 9.00 10.40 5.16 I - 9.00 10.40 5.16 I - 9.00 10.40 5.16 I - 9.00 10.40 5.16 I - 9.00 10.40 5.16 I - 9.00 10.40 5.16 I - 9.00 10.40 5.16		178							1						3.60
1"S 1 9.60 13.20 5.52 11.04 1 9.09 10.40 5.16 11.61 11.61 1 9.09 10.40 5.16 11.61 11.61 1 9.09 10.40 5.16 11.61 11.61 1 9.09 10.40 5.16 11.61 11.61 1 9.09 10.40 5.16 11.61 11.61 1 9.09 10.40 5.16 11.61 11.61 1 9.09 10.40 5.16 11.61 11.61 1 9.09 10.40 5.16 11.61 11.61 1 9.09 10.40 5.16 11.61 13.11 1 9.09 10.40 5.16 11.61 13.11 1 9.09 10.40 5.16 11.61 13.11 1 9.09 10.40 5.16 13.11 1 9.09 10.40 5.10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		7.91	0		18.96	11.60	4.84	_	1		••	-			
J - 5.10 2.80 4.76 12.93 X - 2.55 0.64 3.52 9.24 L - 1.65 0.40 2.92 5.85 M - 1.05 0.20 2.44 3.81 M - 0.30 - 1.52 1.23 M - 0.60 0.96 M - 0.30 - 1.52 1.23 M - 0.60 - 0.86 0.58 M - 0.30 - 0.60 0.96 M - 0.30 - 0.80 M - 0.80 M - 0.80 M - 0.80 M - 0.80 M - 0.80 M - 0.80 M - 0.80 M - 0.80 M - 0.80 M									- 4						
R		1"5							1						
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M 1.05 0.20 2.44 3.81 M 1.80 2.04 3.06 N 0.30 1.52 1.23 N 0.96 0.30 1.32 1.35 N 0.96 0.80 0.58 N 0.96 0.96 0.80 N 0.96 0.80 0.58 N 0.96 0.80 0.58 N 0.96 0.96 N 0.96 0.96 0.58 N 0.96 0.96 N 0.96 0.80 0.58 N 0.96 0.96 N 0.96 0.96 N 0.96 0.96 N 0.96 0.96 N 0.96 0.96 N 0.96 0.96 N 0.96 0.96 N 0.96 0.96 N 0.90 0.90 N 0.9		i													
			_												
2N 0.80 0.36															
					_				1					1.32	
6u 0.20 6u 0.30 0.20 6u 0.30 0.08 12u 0.30 12u 12u 0.30 12u 12u 0.30 12u			1.4					0.36	4						
8W 0.30 0.08 12W 0.30			64												
10H 0.30 12M 0.30 15W 0.30 20M 0.30 22M 0.30 22M 0.30 22M 0.30 22M 0.30 22M 0.30 22M 0.30 22M 0.30 22M 0.30		7	8w							Part .		0.30		0.08	-
12W 0.30 14W 7.30 16W 0.30 20W 0.30 22W 0.30 22W 0.30 22W 0.30 22W 0.30									1						
20h - 0.30									3						
1.8w 0.30 20w 0.30 22w 0.30 2kw 0.30									1	244		2.30			
20H 0.30 22H 0.30 2kH 0.30									1	16W		0.30	••		
22W 0.30 2W 0.30															-
1 2kW 0.30															
										264		0.30			

(2 of 7 sheets)

Table Al Continued

		To	reard, Av	Speed -	2.60 20	111111			le	PETOD AV	Speed .	2.65		
	Position	Location	-6	1	18	7,	10	Position	Location	16		Fa	- 5	10
9	178	24E 22E	:	0.24	1.00	-0.08	-0.08	5"8	24g 22g	=	0.13	-	0.08	-0.05
	2"8	50E		0.63	1.10	0.09	-0.05		50E	••	0.58	-	0.20	-0.06
	2-1/2"8	162	=	1.15	1.10	3.50	0.10		16E	=	1.70	0.10	0.32	-0.07 -0.93
		14E 12E	Ξ	1.75	1.50	0.70	0.29		11st	-	2.30	0.60	0.85	0.39
	0.20	102		0.90	1.45	1.03	1.06		100		2.30	1.10	1.33	0.62
		*		0.43	0.90	1.07	1.64		8		1.29	1.00	1.37	1.74
	3"8	62		0.20	0.80	0.97	1.60		62		1.08	0.80	1.26	2.19
		4		0.25	0.75	0.84	0.88		22		1.20	0.85	1.10	1.63
		- T		1.45	0.75	0.76	-0.13		A		3.07	0.95	1.22	0.76
		c		3.16	1.00	1.03	-0.30	478	c		7.52	2.80	2.50	0.65
		D		6.75	2.05	1.92	-		D	-	8.45	1.10	2.96	1.01
		•	=	7.86	3.50	3.49	0.33		•		9.10	5.50	3.57	1.39
		0	-	9.10	4.85	4.63	4.85		0		8.76	6.00	5.48	6.40
		H	•	7.11	6.55	5.44	7.91		H	-	6.39	6.90	5.69	9.15
		j	-	4.50 2.50	5.65	5.68	9.06	5*8		••	2.38	3.90	5.33	9.7.
				1.25	0.85	4.09	8.53	, ,	1	=	1.11	0.90	3.19	8.21
		L		0.83	0.40	3.38	5.79	the state of	L	••	0.98	0.80	2.58	5.74
		H		0.58	0.30	2.84	3.87		H	•	0.72	0.80	2.12	2.54
		24		0.26	0.20	1.80	0.44		24		0.40	0.75	0.80	2.01
		W	••	0.07	••	0.60	0.10		les .	••	0.14	0.60	0.44	0.75
	2-1/2"8	64 8u		0.05		0.35	-0.06	4"8	6M BM		0.10	0.50	0.24	0.59
		10		0.05		0.10	0.05		J.OM		0.10	0.55	0.20	0.54
	2 8	12W	-	0.05		0.06	-0.04		124		0.10	0.55	-0.04	0.54
	1-1/2"8	164		0.05		0.05	-0.02	des distriction	148		0.10	0.55	-0.05	0.55
	1	184		0.05	=	0.04			16M	=	0.10	0.55	-0.05	0.57
	1	20M		0.05	••	0.04	**		20M		0.10	0.55	-0.05	0.57
	178	24V	=	0.05	-	0.05			22W	=	0.10	0.55	-0.05	0.59
		26W		0.05		0.05			26M		0.10	0.55	-0.05	0.59

	Por	mard, Av	Speed -		THE P	1100.01	in., at Ind			g Speed -	2.65 mb		
Position	Location	_D ₁	p ⁵	D ₃	Di	D ₅	Position	Location	D ₁	D ⁵	D3	Di	D ₅
1"8 2"8 2-1/2"8	242 222 202 182 162	0.021 0.021 0.021 0.021 0.021	-0.002 0.002 0.036 0.061	-0.003 -0.003 -0.003 -0.003	-0.010 -0.010 -0.009 -0.009 -0.007	-0.007 -0.007 -0.007 -0.007 -0.007	578	24E 22E 20E 18E 16E	0.001	0.005 0.008 0.015 0.023 0.039	0.003 0.004 0.004 0.004	0.001	-0.002 -0.003 -0.003
1	1 kg 122 102 62	0.022 0.023 0.025 0.029 0.036	0.041 0.031 0.025 0.022 0.021	-0.002 -0.002 -0.001 -0.001	-0.00A 0.001 0.011 0.028 0.031	-0.007 -0.005 -0.003		141 122 102 82 62	0.003 0.005 0.009 0.015 0.024	-0.009 -0.013 -0.011	0.004 0.005 0.003 0.003	0.007 0.013 0.023 0.037 0.031	-0.003 -0.003 0.004
	A B C	0.040 0.041 0.035 0.027 0.021	0.024 0.030 0.042 0.063	-0.001 -0.001 0.001	0.021 0.012 1.006 0.00h 0.005	0.015 0.019 0.015 0.007 0.003		A A B	0.034 0.036 0.029 0.024 0.022	-0.005 0.008 0.029 0.052 0.067	0.003 0.003 0.004 0.003	0.011 0.001 -0.003 -0.003 0.002	0.006 0.006 -0.003 -0.017
		0.019 0.029 0.020 0.027 0.045	0.090 0.098 0.102 0.080 0.051	0.001 0.002 0.003	0.007 0.011 0.023 0.048 0.008	0.001 -0.001 -0.003 0.006		D I P O N	0.021 0.023 0.031 0.069 0.082	0.069 0.070 0.062 0.037 0.011	0.002	0.007 0.014 0.034 0.063 0.079	-0.016 -0.007 0.008 0.032
	I. J E L	0.075 0.120 0.139 0.151 0.167	0.029 0.025 0.007 0.004 0.003	0.00k 0.005 0.006 0.006	0.090 0.104 0.091 0.071	0.025 0.046 0.054 0.070	5 8	I J K L	0.126 0.160 0.158 c.162 0.162	-0.00% -0.013 -0.017 -0.018 -0.019	-0.001 -0.003 -0.004 -0.004	0.01 0.078 0.047 0.029 0.017	0.058 0.069 0.070 0.067 0.061
2-1/2"0		0.140 0.005 0.050 0.027 0.015	0.002 0.001 0.001	0.006 0.006 0.005 0.005	0.030 0.015 0.008 0.004	0.061 0.037 0.018 0.007 0.001	1	II 24 M Gr Gr	0.105 0.057 0.034 0.022 0.016	-0.019 -0.019 -0.019 -0.019	-0.00k -0.00k -0.00k -0.00k	0.001 -0.009 -0.013 -0.014 0.015	0.036 0.013 0.002 -0.006
200 201/200	10# 12# 16# 16# 18#	0.008 0.005 0.003 0.002 0.002	0.001 0.001 0.001 0.001	0.00k 0.003 0.003 0.003	0.002 0.001 0.001	-0.002 -0.002 -0.002		194 124 144 164 164	0.013 0.013 0.013 0.013	-0.018 -0.018 -0.018 -0.018	-0.00k -0.00k -0.00k -0.00k	-0.015 -0.015 -0.015 -0.015	-0.011 -0.011 -0.011 -0.011
10	SOF SOF SOF	0.001	:	0.002	0.001	-0.001 -0.001		204 224 244 264	0.013 0.013 0.014	-0.018 -0.018 -0.018	-0.00h -0.00h -0.005	-0.015 -0.015 -0.015	-0.011 -0.011

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Table AM(Continued

		To	merd. Av	Speed -	2.16 mg	111111111111111111111111111111111111111	annua' la	in the sale	10.004	estili. In	Etend -	2.90	_	-
Row	Position	Location	6	1	8	9	10	Position	Location	6	7	8	9	10
10	1"#	262	••	-0.20	-2.00	-0.14	-0.70	0	262	••				-0.01
	1	241	••	-0.07	-2.00	-0.08	-0.70	1	24 E	••	0.16	••	0.08	-0.02
		22E		••	-2.00	-0.06	-0.68		225	••	0.30		0.14	-0.01
		20E		0.30	-2.00	••	-0.70	1	200	••	0.63	••	0.20	-0.01
		186		0.79	-2.00	0.11	-0.69		18E		1.13		0.35	-0.01
		162	2.20	1.30	-1.90	0.25	-0.63		16Z	1.60	1.60	0.50	0.55	0.01
		14E	4.30	1.98	-1.80	0.49	-0.50		14E	3.10	2.31	0.80	0.80	0.12
		124		2.19		0.70	-0.32		122		2.20	2.50	1.10	0.47
		10	••	1.68	2.10	0.90	0.10		10E	••	1.60	2.20	1.26	1.09
		SE	••	1.10	0.75	1.0	1.25		8E	••	1.07	0.60	1.29	2.57
		6E		0.60	-0.20	0.95	2.40		(E		0.85		1.16	2.90
		4E		0.58	-0.25	0.86	1.41		4E		0.89		1.00	1.47
		21		0.80	-0.30	0.75	0.35	1	22		1.50	0.30	0.9	0.75
		A	••	1.72	-0.20	0.77	-0.17	- 1	A	••	2.64	0.30	1.10	0.40
		•	.40	3.09	-0.15	0.96	-0.32	1	В	2.30	3.60	0.70	1.47	0.31
		C	12.10	5.24	-0.10	1.41	-0.27		C	21.10	5.70	2.10	2.25	0.48
		D		6.35	0.70	1.80	-0.08		L		7.30	3.90	2.72	0.73
		E F		7.20	2.50	2.22	0.16		E		7.82	5.80	3.25	1.10
		7	56.80	8.35	5.10	3.26	1.15		r	59.20	8.30	6.40	4.24	2.04
		G	0.70	8.40	4.20	4.30	4.20		0	0.70	7.58	5.70	4.94	6.13
		Ħ	••	6.51	7.00	4.98	7.32		H	••	5.63	7.00	5.07	8.51
		1		4.22	5.10	5.17	€.26		1	••	3.68	2.60	4.81	9.05
		3		2.31	1.80	4.62	10.08		J		2.15	-0.50	3.92	10.58
		K		1.19	0.50	3.70	8.03		K		1.17	-0.50	2.68	7.18
		L		0.82	0.30	3.	5.49	1	L	••	0.82	-0.60	2.40	4.93
		M	••	0.57	0.20	2.54	3.65		K	••	0.55	-0.60	1.90	3 4
				0.25		1.64	1.40		×		0.26	-0.60	1.24	1.45
	0	2₩		0.1€		0.93	0.46		SA		0.10	-0.50	0.74	0.59
	1	A.M				0.52	0.10		44		••	-0.50	0.43	0.29
		(SM	••	••		0.27	••		GW	••	••	-0.40	0.22	0.10
		8w		••		0.13	-0.07		8w		••	-0.40	0.09	0.04
		104	••			0.05	-0.08		10W	••	••	-0.40	0.02	0.04
	1"8	12W	••	••			••		124		••	-0.40	••	0.0
									148	••	••	-0.40	••	0.06
								1	160	••	••	-0.40		0.07
									1.8w	••	••	-0.40	••	0.08
									50%	••	••	-0.40	••	0.09
									224	••	••	-0.40		0.10
								1	Sirk		••	-0.40	••	0.10
								₹	26H	••		-0.40		0.10

	Po	mend, Av	Speed =	2.78 mph				ke	verse, Av	g Speed =	2.90 mph		
Position	Location	D ₁	D ⁵	23		D ₅	Position	Location	D ₁	p.5	Dg	D _{1,}	De
1"W	26E	-0.076	-0.073	-0.001	-0.026	-0.017	0	200	••	0.004	0.005	0.001	
	SPE	-0.076	-0.072	-0.001	-0.027	-0.017	- 1	2LE		0.006	0.006	0.002	
	222	-0.076	-0.070	-0.001	-0.027	-0.017	1	220	0.001	0.011	0.006	0.002	
	20E	-0.076	-0.066	-0.001	-0.027	-0.017	1	50E	0.001	0.017	0.007	0.003	•
	18E	-0.076	-0.058	-0.001	-0.027	-0.017		180	0.001	0.027	0.008	0.004	-
-90.	16E	-0.076	-0.050	••	-0.027	-0.017		168	0.002	0.040	0.008	9.007	•
	142	-0.076	-0.045		-0.025	-0.017		14E	0.003	0.042	0.009	0.01	-
	121	-0.075	-0.056		-0.022	-0.015		121	0.004	0.035	0.009	0.017	0.1
	102	-0.074	-0.065		-0.015	-0.014		10E	0.008	0.029	0.009	0.028	0.0
	8E	-0.071	-0.070	0.001	-0.005	-0.010	1	38	0.013	0.026	0.009	0.043	0.1
	62	-0.065	-0.072	0.001	0.002	-0.005	- 1	6z	0.022	0.021	0.00	0.041	C.
- 1	4E	-0.054	-0.070	0.001	-0.004	0.003	1	LE.	0.034	0.044	6.011	0.026	0.0
	28	-0.035	-0.062	0.002	-0. CL	0.006	1	21	0.037	0.066	0.023	0.020	0.0
	A	-0.049	-0.040	0.002	-0.021	0.001		A	0.035	C.107	0.023	0.017	0.1
		-0.050	0.019	0.002	-0.023	-0.005	i i	В	0.033	0.169	0.002	c.019	0.
- 1	C	-0.064	0.125	0.002	-0.023	-0.010		c	0.030	0.189	0.003	0.026	0.
- 1	D	-0.066	0.1.22	0.003	-0.cg	-0.012		D	0.031	0.170	0.000	0.037	0.0
	E	-0.067	0.207	0.004	-0.015	-0.013		E.	0.034	0.173	0.00	0.049	0.0
	7	-0.066	0.200	0.005	0.005	-0.C1		r	0.040	0.190	0.007	0.086	0.0
	0	-0.060	0.152	0.008	0.057	-0.01		G	0.059	765	0.004	0.149	0.0
	M	-0.046	0.0%	0.00	0.115	0.006		И	0.090	0.020	0.001	0.169	0.0
	I	-0.010	0.0-6	0.012	0.179	0.040		1	0.141	-0.002	-0.002	0.166	0.1
	J	0.119	0.00	0.015	0.177	0.077		J	0.189	-0. CL	-0.004	0.166	0.3
	K	0.186	0.012	o.a€	0.161	0.128	1	K	0.180	-0.018	-0.005	0.097	0.3
	L	0.117	0.005	0.016	0.125	0.119		L	0.170	-0.020	-0.005	0.061	0.1
	H	0.170	0.006	0.016	0.093	0.126		ĸ	0.194	-0.021	-0.005	0.034	0.2
•		0.150	0.003	0.015	0.052	0.108		- 16	0.083	-0.0F2	-0.005	0.006	0.0
0	24	0.086	0.003	0.015	0.027	0.067	1	24	0.031	-0.021	-0.005	-0.003	0.1
	lew .	0.047	0.002	C.OLL	0.014	0.037		NA.	0.010	-0.021	-0.005	-0.008	0.0
	6W	0.025	0.002	0.01	0.008	0.020	1	GM		-0.020	-0.005	-0.ao	-
	84	0.01	0.000	0.013	0.005	0.00	1	84	-0.007	-0.020	-0.005	-0.000	-0.0
	10W	0.008	n.000	0.012	0.003	0.005		104	-0.010	-0.020	-0.005	-0.010	-0.
1"8	12W	0.005	0.000	0.011	0.003	0.004		124	-0.010	-0.020	-0.006	-0.010	-0.
	144	0.003	0.001	0.011	0.008	0.003		144	-0.010	-0.020	-0.006	-0.00	-0.
	16M	0.002	0.000	0.010	0.002	0.003		164	-0.010	-0.020	-0.006	-0.010	-0.
	18W	0.002		0.010	0.002	0.003		18w	-0.010	-0.020	-0.006	-0.010	-0.
	20W	0.001		0.009	0.002	0.003	1	20W	-0.010	-0.020	-0.006	-0.010	-0.
	22V	0.001		0.008	0.001	0.002		224	-0.009	-0.020	-0.006	-0.00	-0.0
	26V	-	-	0.007	0.001	0.002	1	264	-0.009	-0.020	-0.006	-0.010	-0.
	26u			0.006	0.001	0.002	V	26M	-0.009	-0.020	-0.006	-0.009	-0.0
						(Continue						(4 of 7	

Toble AT (Continue)

TIT-OF-ED-TWO

		100		Speed -	100	riles. Pr	PROMPS, D	d, et ladio	स्त स्त्राह		g Speed -	2.74		
LE	heliles	lessies	The state of the s	1,	-	7,	710	Position	Location	76	4	₹.	7,	P ₁₀
11	19	201 201 201 101	0.26 0.27 0.30 0.30 0.19	0.60 0.67 0.81 1.06 1.42	2.40 2.45 2.50 2.50 2.50	0.17 0.20 0.22 0.30 0.39	0.82 0.82 0.82 0.82 0.83	ï	262 242 222 202 102	=	0.07 0.15 0.32 0.60 1.03	0.10 0.20	0.07	0.74
		162 132 133 102 8	0.72 0.57 0.15 0.22 0.28	1.93 2.51 2.58 2.19 1.68	2.70 2.65 4.10 4.65 3.35	0.53 0.71 0.92 1.07 1.17	0.87 0.99 1.19 1.57 2.76		162 142 123 102 82	0.10 2.8) -0.30 -0.18 -0.15	1.70 2.11 1.92 1.22 0.70	3.40 1.25 3.30 2.2,	0.43 0.63 0.87 0.99 1.02	0.08 0.20 0.49 1.15 2.60
		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.27 0.23 0.21 -0.06 -0.35	1.30 1.27 1.53 2.17 3.18	2.70 2.50 2.50 2.50 2.75	1.12 1.11 0.93 0.95 1.10	3.60 2.65 1.66 1.17 1.03		62 142 22 A	-0.17 -0.05 	0.47 0.62 (.86 1.80 3.09	-1.65 -1.75 -1.60 -1.65 -0.90	0.65 0.73 0.66 0.76 1.11	2.57 0.98 0.03 -0.30 -0.36
		C D E F	-0.41 -0.43 -0.43 0.40 -0.15	5.30 5.86 6.51 6.32	2.90 3.20 3.25 3.05 3.25	1.50 1.79 2.12 2.86 3.63	1.10 1.25 1.44 2.13 3.50		C D E F	-0.28 -0.30 -0.45 -0.30	5.56 5.22 5.64 5.98 5.50	0.65 1.35 1.60 1.45	2.68 2.65 2.46 3.22 3.77	-0.25 -0.10 0.13 1.04 2.70
			0.07 0.10 0.10 0.07	1.80 0.87 0.61	3.30 2.10 1.00 0.45 0.30	4.18 3.70 2.90 2.48	5.51 5.87 5.31 3.20		H J K L	=	4.26 2.88 1.65 0.89 0.60	1.60 1.50 -0.90 -1.05	3.95 3.76 3.07 2.32 1.92	4.05 4.56 4.91 3.64 2.67
		# # # # # # # # # # # # # # # # # # #	0.03	0.10	0.20	2.04 1.26 0.73 0.36 0.18	2.12 0.87 0.24 -0.08		10 21 21 14 64	=	0.41 0.12 -0.14 -0.18	-1.05 -1.10 -1.10 -1.10 -1.05	1.58 1.03 0.57 0.28 0.12	1.85 0.73 0.27 -0.09 -0.20
		00 100 120 110 160	=	=	Ē	0.07	-0.10 -0.09 -0.06 -0.06 -0.05		36 100 120 140 160	=	-0.17 -0.17 -0.16 -0.16 -0.16	-1.00 -1.00 -1.00 -1.00	0.01 -0.03 -0.09 -1.10 -0.10	-0.24 -0.24 -0.24 -0.24
	1	184 204 224	Ξ	Ξ	Ξ	Ξ	-0.05 -0.04		184 204 224 244 264	=	-0.15 -0.15 -0.15 -0.15	-1.00 -1.00 -1.00 -1.00 -1.00	-0.11 -0.11 -0.11 -0.11 -0.10	-0.22 -0.23 -0.22 -0.22 -0.22

	PRINCIPLE OF THE PRINCI		regret, Ave	Speed -	2.90		Day Very Mary	L - NA	cated Gage	verse, Av	Speed =	2.74		
	Position	Location	3	25	_ B,	- Pa	D ₅	Position	Location		D ⁵	D3	10	105
11	Î	26E 26E 28E 26E 16E	0.030 0.030 0.030 0.030 0.031	0.009 0.010 0.012 0.017	-0.008 -0.008 -0.008 -0.008	-0.018 -0.019 -0.019 -0.019	-0.017 -0.017 -0.018 -0.018	Ï	26E 24E 22E 20E 16E	=	0.903 0.006 0.010 0.017 0.026	0.007 0.008 0.008 0.010	0.001	0.00
	Ĭ.	168 1148 128 108 68	0.031 0.031 0.032 0.034 0.237	0.030 0.031 0.022 0.015 0.008	-0.008 -0.007 -0.007 -0.007	-0.017 -0.015 -0.011 -0.005 0.003	-0.018 -0.017 -0.016 -0.015 -0.010		162 142 123 102 62	0.001 0.003 0.005 0.011	0.035 0.035 0.026 0.021 0.019	0.012 0.012 0.013	0.00k 0.008 0.015 0.025 0.035	0.00
		& W	0.042 0.053 0.076 0.057 0.047	0.006 0.008 0.318 0.040 0.005	-0.006 -0.005 -0.005 -0.005	0.008 0.001 -0.006 -0.015 -0.017	-0.005 0.002 0.004 -0.001	i	62 12 22 4	0.021 0.039 0.035 -0.008 -0.08	0.022 0.035 0.057 0.097 0.151	0.015 0.015 0.016 0.017	0.036 0.028 0.020 0.021	0.02 0.03 0.03 0.02
		C D E 7	0.0k1 0.0k0 0.0k0 0.0k0	0.135 0.147 0.160 0.195 0.145	-0.005 -0.00k -0.003 -0.002	-0.015 -0.013 -0.006 0.015 0.070	-0.013 -0.015 -0.017 -0.018 -0.012		C D E P	-0.02 -0.020 -0.021 -0.036	0.182 0.180 0.182 0.176 0.098	0.017 0.016 0.015 0.011	0.030 0.039 0.053 0.091 0.152	0.015 0.025 0.030 0.030
		1	0.051 0.065 0.061 0.093 0.098	0.083 0.065 0.080 0.080	0.006 0.010 0.013 0.013	0.125 0.154 0.191 0.167 0.134	0.008 0.050 0.092 0.121 0.133		1	0.035 0.035 0.054 0.059 0.058	0.048 0.024 0.010 0.005 0.006	-0.002 -0.003 -0.004	0.180 0.184 0.179 0.110 0.073	0.00 0.12 0.14 0.14
			0.098 0.053 0.053 0.090 0.025	0.005 0.002 0.002 0.008	0.013 0.012 0.011 0.010	0.100 0.052 0.026 0.013 0.007	0.140 0.119 0.072 0.038 0.718		H H SH SH GH	0.056 0.037 0.013 -0.003 -0.010	0.003	-0.00h -0.00h -0.00h -0.00h	0.046 0.026 0.002 -0.003	0.130 0.080 0.030 0.000
		100 150 150 150	0.009	=======================================	0.008 0.707 0.006 0.006	0.00k 0.00g 0.00g 0.00g	0.008 0.004 0.003		10v 12v 12v 14v 16v	-0.015 -0.018 -0.018 -0.018	0.003 0.003 0.003 0.003	-0.005 -0.005 -0.005 -0.005	-0.006 -0.006 -0.006 -0.005	-0.00 -0.00 -0.00
		\$00 500 500 500 500	Ē	=	0.005 0.006 0.005 0.003	0.001 0.001 0.001	Ē		184 201 224 244 264	-0.029 -0.039 -0.039 -7.088 -0.08	0.003 0.003 0.003 0.003	-0.005 -0.005 -0.005 -0.005	-0.005 -0.005 -0.005 -0.005	-0.000 -0.000 -0.000 -0.000

Tuble Al MContinued

		To a	and Au	Steed -	2.72 213	TACAL PR	sama' M	i, at lidic	in the second	erse. Ave	Street	2.61 min		
Row	Position	Location	16	F ₇	8	Fg	10	rogition	Location	-6	17	B	19	F ₁₀
13	2"8	24E 24E 22E 20E 18E	0.25 0.25 0.25 0.25 0.25	0.46 0.47 0.60 0.80 1.10	0.45 0.45 0.45 0.40	0.31 0.31 0.39 0.48	0.33 0.35 0.35 0.33 0.38	0	24E 22E 20E 16E 16E		0.10 0.25 0.49 0.79 1.22	0.20	0.06 0.09 0.12 0.22 0.39	0.02
		16E 14E 12E 10E 6E	0.15 0.20 0.20	1.45 1.75 1.88 1.56 1.23	0.60 0.80 1.00 0.70 0.40	0.59 0.73 0.91 1.03	0.41 0.47 0.60 0.87 1.22		14E 12E 10E 8E 6E		1.40 1.31 0.90 0.39 0.21	0.60 1.00 0.60 0.05 -0.10	0.53 0.72 0.82 0.71 0.72	0.12 0.03 0.03 1.12 1.22
		GE LE 2E A B	0.35 0.20 0.20 0.25 0.18	0.95 1.00 1.18 1.76 2.35	0.40 0.50 0.50 0.50 0.60	1.04 0.95 0.90 0.92 1.05	1.41 1.03 0.69 0.44 0.38	1"8	AE 2E A B		0.22 0.52 1.13 1.95 3.00	-0.15 -0.10 0.20 0.60	0.57 0.52 0.60 0.62 1.22	0.60 0.12 -0.04 -0.99
		E P	0.10	3.35 3.80 4.10 4.50 4.21	1.00 1.05 1.05 1.25 1.75	1.61 1.61 1.81 2.32 2.86	0.48 0.53 0.69 1.09 1.71		D E F G		3.50 3.75 4.00 3.69 2.62	1.00 1.10 1.40 1.65 1.00	1.52 1.80 2.32 2.75 2.92	0.0. 0.19 0.61 1.33 2.06
		H J K L	0.10 0.10 0.10 0.10 0.10	3.25 2.30 1.30 0.65 0.45	1.10 0.50 0.15	3.12 3.12 2.73 2.15 1.83	2-39 3-02 2-79 1-98 1-48		I K L M		1.97 1.10 0.53 0.35 0.20	0.15	2.78 2.31 1.79 1.52 1.20	2.60 2.40 1.79 1.41 1.05
	1"11	M M EW W GW	0.10	0.30		1.55 0.97 0.51 0.25 0.13	1.12 0.45 0.10		Bi Ziri Giri Giri Biri		-0.10 -0.18 -0.20 -0.20		0.60 0.42 0.20 0.66	0.42 0.10 -0.03 -0.05
	-	8W 10W 12W	=======================================	Ξ	 	0.08			10W 12W 14W 16W 16W		-0.20 -0.20 -0.20 -0.20			-0.07 -0.07 -0.07 -0.07
									5/M 55M 56M		-0.20 -0.20 -0.20			-0.07 -0.07

	Forvar	1. Avg Spe	ed = 2./3	mich		heverse	Avg Spe	ed = 2.61 m	ot.
Position	Location	DE	17	₽ ₈ • ₽ ₉	Position	Location	16	1:7	Le Lo
1°S	262	-c.026	0.007	-0,000	0	26E	0.00		••
	24E	-0.026	0.007	-0.096		24E	0.009		
	225	-0.028	0.008	-0.00%		22E	0.035		••
	20E	-0.022	0.007	-0.006	1	20E	0.022		
	18E	-0.015	0.000	-0.000		18E	0.031		
	16E	-0.005	0.006	-0.00F		16E	0.045		
	14E	-0.00k	0.005	-0.00%		14E	0.045		0.00
- 1	1.2E	-0.016	0.005	-6.005		122	0.098		0.00
1	10E	-0.027	0.002	-0.004		10E	0.033	-0.001	0.00
	812	-0.034	0.001	••		38	0.030	-0.002	0.03
	6E	-0.035	0.001	0.004		EE.	0.035	-0.002	0.02
1	4E	-0.033	0.001	0.011		4E	0.046	-0.001	0.02
	2E	-0.025	0.002	0.025		2E	0.072		0.02
	A	-0.002	C.003	0.009	1"S	A	0.113	0.001	0.01
	P	0.054	0.00	0.003	1	B	0.180	0.007	0.01
	c	0.143	0.006	-0.003		C	0.19	0.013	0.00
1	D	0.136	0.010	-0.004	1	D	0.180	0.021	0.00
		0.209	0.014	-0.005	i	E	0.180	0.028	0.11
1	P	0.202	0.025	-0.002		7	0.198	0.030	0.020
•	G	0.150	0.035	0.006		G	0.077	0.028	0.04
0	H	0.085	0.035	.024		H	0.036	0.030	0.070
1	I	0.045	0.030	0.058	-	1	0.025	0.017	0.10
	3	0.020	0.011	0.094		J	0.025	0.00	0.11
1	K	0.010	0.003	0.127		K			0.07
V	L	0.008	0.002	0.125		L	-0.001		0.116
179	M	0.005	0.001	0.127		M	-0.002		0.10
1	×	0.003		0.106		N	-0.001	0.002	0.0
	24	0.003		0.059	i	24	-0.002	0.005	0.02
1	P.M.	0.000		0.030		LW	-0.002	O. OOK	0.07
	6 W	0.001		0.015		6H		0.00%	-0.002
	8M			0.008		(M	-	0-005	-0.00
1	10W			0.004		10W		0.005	-0.00
	12W		••	0.003		124		0.00	-0.00
	144			0.002		14W		0.005	-0.00
	16W			0.002		16e		0.00	~0.00
	18v	**		0.002		180		0.006	-0.005
	20W			0.002		50		0. 907	-0.00%
	224			0.002		55		0.007	-0.005
1	244			0.002		244		o. aas	~0.00°
7	26H			0.002		5(4)	••		-

[.] Not working.

Table #9(Concluded)

		Po	mard, Av	g Speed -	2.46 mph	CACCAL TI	THE PERSON NAMED IN	i. at Indica		verse, Av	E Speed	2.73 mb		
<u>Low</u>	Position	Location	16	17	18	10	10	Position	Location	P6	F ₇	T _B	19	10
15	1	248 228 208 148 166	0.10 0.10 0.10 0.10 0.10	0.35 0.49 0.60 0.72 0.90	=	0.30 0.31 0.34 0.40	0.08 0.09 0.09 0.09	Î	24E 22E 20E 18E 16E	=	0.10 0.30 0.45 0.65 0.88	0.05	0.06 0.10 0.17 0.23 0.32	0.01
		14E 12E 10E 6E 6E	0.10 0.10 0.10 0.10 0.10	1.05 1.09 0.96 0.79 0.68	=	0.97 0.69 0.75 0.80 0.80	0.13 5.19 0.29 0.40 0.42		142 102 102 82 62	0.09	0.90 0.72 0.45 0.32	0.25	0.45 0.55 0.62 0.59 0.52	0.10 0.15 0.32 0.46 0.45
		22 A B	0.10	0.69 0.87 1.22 1.74 2.25	0.25	0.79 0.74 0.75 0.89 1.09	0.33 C.22 0.15 0.11 0.20		A B C	0.10 0.11 0.15 0.10	0.35 0.52 0.96 1.49 2.11	0.05	0.47 0.30 0.45 0.62 0.69	0.35 0.15 0.06 0.05 0.05
		D E F O N	5.85 11.70	2.50 2.83 2.95 2.77 2.19	0.25 0.35 0.60 1.65 0.90	1.23 1.41 1.75 2.01 2.22	0.25 0.31 0.54 0.88 1.37		D E P O M	2.39	2.35 2.60 2.72 2.55 2.05	0.50 9.60 1.10 1.40 0.30	1.09 1.23 1.60 1.84 1.99	0.11 0.20 0.41 0.78 1.25
		1 5 6 1	-	1.51 0.92 0.50 0.39 0.29	0.30	2.15 1.92 1.51 1.32 1.12	1.83 1.64 1.02 0.79 0.55		J K L	=	0.90 0.55 0.40 0.32	-0.15 -0.25 -0.25 -0.25	1.90 1.63 1.29 1.10 0.96	1.73 1.43 1.00 0.75 0.58
		20 LM 61 80	=	0.19	=	0.71 0.45 0.22 0.10 0.05	0.21	178	Si 2M UN GN BN	=	0.19 0.03 0.05 0.05	-9.15 -0.05	0.76 0.38 0.20 0.10 0.05	0-39 -11 9-12
		10W 12W	, F	:	=	0.02	=		108 128 168 168 188	=	0.05	=	0.01	-
									20M 22M 24M 26M	=	0.0 0.0	:	=	=

	Pormerd.	Ave Sne	ed - 2.46 s	rtical Deflection, in.		Heverse.	Ave Ste	- 2.73	arch	
Position	Location	D ₆	D ₇	pg. pa	Position	location	D ₆	127	r8	Dg
1	242 223 202 163 164	0.005 0.011 0.020	0.001 0.001 0.001	-0.026 -0.026 -0.026 -0.026		24E 22E 20E 18E 16E	0.00k 0.008 0.015 0.025 0.033	=		0.002
	1 AE 1 2E 1 OE 8E 6E	0.024 0.015 0.006 0.001	-0.001 -0.004 -0.005 -0.005 -0.004	-0.026 -0.025 -0.023 -0.020 -0.005		14g 12g 10g 8g 6g	0.032 0.024 0.017 0.017	-0.001 -0.005 -0.004 -0.003		0.003 0.005 0.009 0.005 0.023
	A B	0.001 0.012 0.033 0.061 0.130	-0.003 -0.003	0.002 0.004 -0.007 -0.011		A B C	0.033 0.056 0.095 0.150 0.176	-0.003 -0.002 -0.008 0.008		0.029 0.020 0.020 0.016
	D E 7 0	0.145 0.161 0.196 0.150 0.086	0.005 0.020 0.029 0.034	-0.012 -0.002 -0.009		E F O	0.176 0.176 0.119 0.092 0.045	0.026 0.023 0.035 0.036 0.029		0.016 0.018 0.027 0.048 0.081
	I J H L	0.050 0.024 0.011 0.008 0.006	-0.002 -0.001	0.057 0.096 0.120 0.130 0.132		J R L	0.002	0.002 -0.005 -0.005		0.118 0.135 0.136 0.130 0.118
	# G	0.001 0.002 0.005	-0.003 -0.003 -0.003 -0.003	0.109 0.062 0.031 0.003 0.005	178	38	=======================================	0.003		0.075 0.033 0.011 0.002
	100 120 110 160 160	=======================================	-0.001 -0.001 -0.001 -0.001	0.001 0.001		104 124 114 164 184	=	0.005 0.005 0.005 0.005		=======================================
- 6	201	•		•		200 220 240 250	=	0.005		=

The working.

(7 of 7 sheets)

Table A-20

Multiple-Wheel Heavy Gear Land Flexible Payement Test, Dynamic Instrumentation Leading Data

Item 3; Load Condition: 30 kips per Wheel, 12 Wheels, 100 psi

		Po	romed Av	e Spend	- 1.91 mph	resent Pro	same. D	ei, at Indic				1 64 - 1		
			D D				D		Ke	AGLES VA	E Speed	1.94 mph		
Row	Position	Location	-1	P ₂	P3	P ₁₄	P ₅	Position	Location	P ₁	Pg	P3	Pla	P5
5	0	122	0.90		2.40	••		None	12E	0.15	0.41		0.15	
		106	0.90	0.10	2.40		••	- 1	10E	0.15	0.50	••	0.15	
		8E	1.65	0.10	2.43	••		i	8E	30	0.57	-	0.15	
		6E	1.20	0.25	2.43	0.10	••		Gr.	0.35	0.70	••	0.15	••
	- 1	4E	1.50	0.41	2.43	0.10		1	4E	0.57	1.05		0.20	
		212	2.55	0.85	2.55	0.19		7	20	0.93	1.51	••	0.25	••
		A	4.20	1.55	2.55	0.32	••	l"N	A	2.76	2.45	••	0.45	
	1	В	5.10	2.40	2.85	0.65	••	1	В	6.45	3.42	0.24	0.72	
		C	13.80	3.55	3.45	1.25			C	10.50	4.85	0.96	1.40	
		D	15.00	4.25	4.05	1.49			D	10.50	5.40	2.04	1.81	••
		E	15.00	4.90	5.40	1.95			E	10.20	6.00	3.90	2.55	
			15.90	6.08	10.80	3.30	••	1	F	10.65	6.80	9.45	4.20	
		0	16.80	7.90	10.20	5.00		7	G	10.65	7.30	7.9%	5.95	
	- 1	H	10.20	7.21	9.00	6.45	••	0	н	6.30	7.15	7.80	7.00	
		I	4.20	6.80	12.15	7.50			I	2.70	6.40	10.65	7.50	
		J	2.40	5.85	4.75	7.55		ı	J	1.95	5.52	5.10	7.15	
		K	3.00	5.10	1.80	6.20	••]	K	3.00	5.05	1.65	5.51	
	1	L	4.20	4.85	1.20	5.25		ŀ	L	4.20	4.95	1.05	4.73	••
	1	Н	6.60	4.70	0.75	4 - 35			H	6.00	5.05	0.75	3.90	••
		N	12.90	3.00	0.90	3.05	••	•	24	10.05	5.58	0.90	3.00	
		SM.	15.00	5.75	3.00	2.75	••	None	2W	10.20	6.33	3.45	3.25	••
		46	15.00	0.70	9.30	3.60			414	10.20	6.95	9.45	4.45	
		6W	16.20	7.25	9.90	5.20	••		6W	10.20	7.10	3.55	6.15	
		8w	11.10	7.30	5.10	6.60			8w	6.60	6.75	7.50	6.95	
	1	10W	4.50	6.70	10.80	7.40			10W	3.00	5.75	10.50	7.30	
		12W	1.50	5.40	7.50	7.70	••		12W	1.20	4.45	6.15	7.10	••
		146	0.60	3.90	1.95	6.40			14W	0.30	3.00	2.25	5.39	
		16W		2.60	0.45	4.30	••		166	-0.30	2.05	1.20	3.80	
		18W		1.70	0.15	2.50			181	-0.30	1.15	0.60	2.25	••
		50M		0.85		1.20	'		50M	-0.30	0.55	0.45	1.25	••
		55M		0.50		0.65			22V	-0.30	0.20	0.45	0.70	
		24W		0.25	••	0.30			SIM	-0.30	0.02	0.30	0.35	•
		26W		0.10	••				26W	-0.30	••	0.30	0.10	

(1 of 7 sheets)

Table A20(Custimed)

4		-			1.60 mph	tical Pr	essure. P	i, at Indic	ated Celle	radio e sa				
Roy	Position	Legiton	P,	P ₂	P3	P _k	P.	Position	Location	P ₁	Pg	3	Pi	P ₅
7	1"S	24E 22E 20E 18E 16E	=	0.10 0.12 0.20 0.26 C.27	i	0.02	E	2"8	26E 24E 22E 20E 18E	=	0.07 0.10 0.18 0.21 0.30	=	0.05	!
	2"8	14E 12E 10E 8E 6E	Ē	0.27 0.27 0.27 0.29 0.38	=	0.08 0.10 0.03 0.07 0.04	Ē	1"8	16E 11/E 12E 10E 8E	0.15 0.15	0.32 0.37 0.38 0.42 0.51	=	0.05 0.08 0.08 0.09 0.10	=
		A B C	0.30 0.75 2.07 4.65 9.30	0.62 1.05 1.62 2.49 3.75	0.27	0.05 0.10 0.25 0.52 1.06	=	28	62 42 27 A B	0.36 0.54 1.14 2.55 6.30	0.69 1.00 1.50 2.27 3.30	0.09 0.15 0.15 0.15 0.15	0.11 0.12 0.19 0.30 0.53	=
		D E F O H	9.90 9.93 11.70 13.14 0.16	4.28 5.04 6.19 6.85 7.17	1.50 3.90 14.43 12.96 10.38	1.37 1.89 3.09 4.49 5.85	69.00		C D E F	10.50 10.80 10.20 12.00 11.85	9.55 5.27 5.98 6.88 7.25	0.90 2.25 6.00 16.80 10.86	1.01	Ē
		I J K L	3.00 1.50 1.56 2.25 3.96	6.63 5.79 4.90 4.72 4.65	19.35 9.48 1.65 0.60 0.30	7.08 7.45 5.89 5.00 4.22	77.10 3.60		H I J K L	6.45 2.70 1.95 2.70 3.90	7.10 6.38 5.59 4.99	12.00 18.60 6.93 1.50 0.90	5.70 6.27 6.09 4.65 3.90	78.00 66.00 6.00
	1"8	II 2M LM 6W 8W	8.70 10.50 11.10 13.20 9.75	4.90 5.60 6.53 7.10 7.26	6.30 1.56 12.06 15.06 9.81	3.00 2.57 3.27 4.69 6.10	38.40		N N 2W LW GW	5.85 10.50 10.50 11.25 12.24	4.99 5.52 6.33 7.00 7.18	0.30 0.90 4.20 15.75 12.66	3.18 2.45 4.60 3.51 4.85	=
	Ò	10W 12W 11W 16W 18W	3.33 1.20 0.45 0.15 0.15	6.60 5.31 3.98 2.59 1.62	18.60 13.38 3.00 0.45 0.15	7.12 7.59 6.50 4.21 2.61	73.80		8v 10v 12v 11v 16v	7.26 3.00 1.35 0.54 0.15	6.88 5.92 4.60 3.21 2.13	11.10 19.50 8.25 2.10 0.90	5.65 6.18 6.01 4.60 3.08	73.80
		20v 22v 24v 26v	Ē	0.97 0.55 0.27 0.15	Ē	1.42 0.75 0.31 0.10	Ē		18v 20v 22v 24v 26v	=	1.37 0.72 0.39 0.12 0.09	0.30	1.90 1.09 0.62 0.30 0.10	E

(2 of 7 shoots

Table MCContinued

15 ELDE	No.					ical Pre	Sure. De	, at Indica	ted Colls	100		A to produce		-
			roard. Av						Re	ABLES VA				
Roy	Position	Location	P ₆	-7	P8	<u> </u>	10	Position	Location	<u>P6</u>		-8		
9	178	12E 10E 6E 6E	0.90 0.90 1.00 1.00	0.23 0.23 0.30 3.50 0.60	2.60 2.60 2.60 2.60 2.60	0.20 0.30 0.30 0.30 0.30	0.70 0.86 0.80 0.80 0.80	3-1/2"8 3"8	125 106 82 62 42	=	0.35 0.40 0.40 0.45 0.75	=	0.30 0.30 0.30 0.30	i i
		A B C D	1.60 2.80 5.80 10.30 11.30	8.50 1.35 2.05 2.90 3.45	2.40 2.40 2.30 2.40 2.80	0.50 0.70 1.00 1.80 2.40	0.80 0.80 0.80 0.80 0.80		A B C D	0.75 2.00 5.50 10.00 10.30	1.15 1.75 2.55 3.65 4.15	0.10 0.70 1.50	0.40 0.90 1.00 1.80 2.50	=
		B P O H	11.50 12.00 13.40 8.50 3.70	5.60 5.60 5.75 5.45	3.80 7.00 6.80 7.00 8.80	3.0° 4.70 6.60 8.20 9.10	0.80 0.80 0.50 0.20	2-1/2"S 2"S	F 0 H I	10.00 10.50 11.00 5.75 3.00	4.70 5.50 5.80 5.75 5.25	3.50 6.20 4.90 5.00 5.20	3.30 5.40 7.50 8.60 9.20	0.10
		J K L M	2.00 2.00 3.00 5.00 10.00	4.75 4.25 4.05 3.95 4.15	5.60 2.00 1.30 0.80 0.70	9.10 7.10 6.10 5.10 3.60	Ē	1"5	J K L H	1.75 4.25 3.25 5.00 9.50	4.55 4.15 4.05 4.15 4.35	2.50 0.50 0.30 0.36 0.90	8.50 6.50 5.50 4.50 3.70	=
		2W 4W 6W 8W 10W	12.00 11.60 13.00 9.20 3.80	4.80 5.30 5.85 5.90 5.35	2.40 5.80 6.80 6.00 7.50	3.70 4.80 6.60 8.20 9.20	=		2W LW 6W 8W 10W	10.00 9.50 11.00 7.50 3.50	4.90 5.50 5.65 5.55 4.95	2.70 5.00 5.30 4.60 6.20	4.00 5.40 7.20 8.40 8.80	0.10
		12W 11W 16W 18W 20W	1.60 0.80 0.60 0.40	4.35 3.30 2.25 1.50 0.80	6.00 1.80 0.80 0.50 0.30	9.00 7.30 4.90 3.00 1.70	Ξ		12M 14W 16W 18W 20W	1.25 0.50 -0.50 -0.75 -0.75	3.95 2.95 2.05 1.25 0.70	3.40 0.80 0.40 0.20	8.46 6.90 4.70 3.00 1.70	0.20 0.30 0.30
		56A 54A 55A	Ē	0.50 0.30 1.50	0.20	0.80 0.40 0.20	Ξ		25M 26M 26M	-0.75 -0.75 -0.75	0.35 0.15 0.10	Ξ	0.86	0.30 0.30 0.30

	Tor	need. Av	E Speed -		cical hari	ection, 1	n., at Indi		verse, Av	Speed a	1.6		
Position	Location	D	D2	D3	Dla	D ₅	Position	Location	D ₁	p ⁵	D ₃	D _k	D,
1	12E 10E 8E 6E 4E	0.030 0.030 0.032 0.038 0.048	-0.007 -0.006 -0.005 -0.002 0.008	-0.010 -0.009 -0.009 -0.009 -0.007	-0.007 -0.007 -0.007 -0.007 -0.007	0.02% 0.023 0.023 0.073 0.023	3-1/2"8 3"8	125 106 85 62 43	0.005 0.010 0.013 0.020 0.038	0.002 0.007 0.007 0.013 0.021	0.003 0.006 0.006 0.008	0.002	0.0
	A B C D	0.070 0.090 0.105 0.115 0.123	0.015 0.030 0.042 0.054 0.058	-0.00k 0.00k 0.016 0.0k8 0.060	-0.006 -0.005 -0.003 0.001 0.003	0.023 0.023 0.024 0.025		A B C D	0.065 0.010 0.105 0.108 0.110	0.035 0.068 0.055 0.060 0.060	0.019 0.032 0.050 0.081 0.086	0.012 0.003 0.007 0.012 0.016	0.0
	P O H I	0.125 0.100 0.065 0.043 0.036	0.059 0.048 0.032 0.022 0.020	0.065 0.081 0.112 0.092 0.050	0.06 0.012 0.020 0.027 0.028	0.023 0.038 0.055 0.075 0.090	2-1/2"8 2"8	r o n	0.105 0.700 0.043 0.033 0.040	0.055 0.096 0.084 0.084	0.090 0.105 0.093 0.052 0.030	0.019 0.006 0.090 0.086	0.0
	J K L M	0.000 0.000 0.096 0.103 0.110	0.027 0.038 0.044 0.048 0.057	0.030 0.025 0.026 0.032 0.057	0.025 0.018 0.016 0.014 0.010	0.110 0.143 0.126 0.100 0.062	1"8	J K L	0.063 0.098 0.105 0.104 0.100	0.090 0.0k2 0.0k6 0.0k9	0.023 0.028 0.035 0.046 0.050	0.020	0.1 0.0 0.0
	2W 4W 6W 8W 10W	0.123 0.100 0.065 0.035 0.020	0.064	0.077 0.086 0.114 0.105 0.058	0.019 0.029 0.029 0.030	0.040 0.035 0.043 0.065 0.080		EW 6W 6W 10W	0.100 0.093 0.098 0.015 0.005	0.053 0.034 0.036 0.003 -0.004	0.080 0.088 0.090 0.061 0.009	0.016 0.021 0.034 0.038	0.0
	12W 14W 16W 18W 20W	0.010	0.006 0.003 0.002 0.001	0.031 0.018 0.010 0.006 0.004	0.026 0.020 0.013 0.007 0.003	0.098 0.138 0.108 0.065 0.038		12M 1MW 16W 16W 20M	-0.005 -0.008 -0.008 -0.008	-0.007 -0.009 -0.009 -0.009	0.002 -0.006 -0.010 -0.002 -0.013	0.017 0.009 0.003 -0.002 -0.005	0.1 0.0 -0.0 0.0
	56A 56A 55A	Ξ	=	0.003	0.002	0.020		22W 2NW 2GW	-0.008 -0.008 -0.009	-0.009 -0.009 -0.009	-0.02k -0.02k	-0.006 -0.006 -0.006	-0.0

(3 of 7 mosts)

Table A20(Continued)

	_					rucel Pr	essure, p	i, at Indica	sted Cell		don'T	1,42 mm	_	_
	_		roard, Av	_		_		_		_	_		_	- 5
OV.	Position	Location	6	_7_	8	_9_	10	Position	Location	6	_7_	8	9	P)
10	1"N	122	0.40	0.03	0.10	0.60	1.25	3-1/2"	128		0.30	••	0.30	
		100	0.40	0.03		0.56	1,00	1	102	0.10	0.32	0.10	0.30	
		82	0.40	0.03		0.56	1.00		6E	0.16	0.32	0.10	0.30	••
		6E	0.40	0.04		0.50	1.00	3"1	EE.	0.20	0.47	0.10	0.30	••
		4E	0.80	0.60		0.50	1.00		4E	0.36	0.65	0.10	0.30	
		2E	1.00	0.88	••	0.60	1.00	1	22	0.80	1.00	0.10	0.12	••
	1	A	2.20	1.42	-0.05	0.76	1.00		A	2.00	1.55		0.60	-
	1-1/2"	3	5.00	2.05	-0.10	1.24	1.00		3	5.40	2.38	0.10	1.00	••
		C	9.20	2.90	-0.05	2.00	1.00		C	10.00	3.35	0.50	1.80	
		D	9.50	3.42		3.50	1.00		D	10.50	3.85	1.40	1.34	
		7	9.70	3.95	1.00	3.24	1.00		E	10.20	4.29	3.30	3.03	
		7	12.00	4.75	5.40	4.50	0.75		7	11.90	5.05	6.90	4.96	0.2
		0	14.50	5.40	5.30	6.16	0.75		0	13.00	5.37	4.30	6.90	0.7
		н	8.90	5.55	5.30	7.70	26.00	1	н	5.80	5.45	5.70	8.75	34.5
	7	I	4.00	5.25	8.20	8.70	4.75		I	3.00	5.00	6.50	8.90	1.7
	5,M	J	1.80	4.75	5.00	8.70	2.25		J	1.80	4.37	1.00	8.30	2.5
		K	1.70	4.20	0.90	7.00	34.50		ĸ	2.30	3.97	-0.5C	6.50	33.2
		L	2.40	4.05	0.20	6.00	15.50		L	3.30	3.95	-0.30	5.40	10.2
		×	4.00	4.02	-0.30	5.04	1.75		H	5.00	3.97	-0.20	4.60	
	1	×	5.90	4.20	-0.70	3.90	0.75		H	9.80	4.25	0.30	3.80	
		24	11.30	4.13		3.60	0.75		2M	10.20	4.70	2.50	4.10	***
		44	11.90	5.27	5.00	4.40	0.50		PR.	11.00	5.25	4.80	5.40	0.2
		6W	12.60	5.65	6.70	6.24		1	6и	13.10	5.55	4.40	7.10	0.7
		84	11.50	5.73	5.20	7.30	20.75		8w	8.20	5.28	5.30	8.20	32.5
		10W	4.70	5.21	8.20	8.80	12.25		10W	3.50	4.55	4.70	9.70	3.5
		12W	1.90	4.45	6.70	8.90	0.75		12W	1.30	3.59	1.10	8.10	2.5
	11	168	0.80	3.28	1.50	7.10	33.00		144	0.30	2.60	-0.70	6.30	37.5
		16W	0.40	2.31	0.60	4.90	4.00		16W	-3.00	1.78	-0.70	4.30	1.7
	1 1 /offer	18W	0.20	1.52	0.30	2.90	0.50		18v	-0.50	1.05	-0.70	2.70	0.2
	1-1/2 %	20W		0.95	0.10	1.70	0.25	ł	20N	-0.60	0.60	-0.70	1.60	0.2
		22M		0.57	0.10	0.90		1	25A	-0.70	0.35	-0.70	0.90	0.2
	1	SFA		0.35		0.40		1	248	-0.70	0.10	-0.70	0.40	0.2
	7	26W		0.20	**	0.24		7	26H	-0.70		-0.70	0.20	0.2

	70	rward. Ave	Speed -	1.85 mph			in. at Indi			Sheed .	1.42 mph		
Position	Location	D	D	D ₃	LL	D ₅	Position	Location	D	D	D ₃	D	D ₅
1"N	125	-0.035	-0.007	-0.014	-0.004	-0.027	3-1/2"₩	122	0.003	0.003	0.003	0.001	
1	102	-0.035	-0.005	-0.013	-0.004	-0.027	1	100	0.006	0.005	0.003	0.001	0.00
	8E	-0.033	-0.00h	-0.013	-0.004	-0.027		8E	0.010	0.009	0.004	0.001	0.00
	6E	-0.027	0.003	-0.011	-0.004	-0.027	3"11	6E	C-050	0.016	0.007	0.001	0.00
	4E	-0.023	0.009	-0.011	-0.004	-0.027	1	4E	0.036	0.029	0.012	0.002	0.00
1	21	-0.003	0.012	-0.006	-0.003	-0.027		21	0.075	0.046	0.021	0.003	0.00
V	A .	0.090	0.037	0.003	-0.002	-0.027		A	0.165	0.059	0.039	0.006	0.00
1-1/2"H	3	0.097	0.052	0.023	0.001	-0.025		3	0.103	0.065	0.073	0.010	0.01
	C	0.083	0.061	0.060	0.004	-0.027		C	0.113	0.066	0.106	0.016	0.01
	D	0.105	0.064	0.076	0.007	-0.020		Ð	0.141	0.064	0.109	0.021	0.02
	E	0.143	0.064	0.081	0.011	-0.018		2	0.600	0.059	0.104	0.025	0.02
	7	0.100	0.053	9.088	0.019	-0.008		7	0.052	0.042	0.109	0.032	0.05
	0	0.053	0.636	0.109	0.026	0.015		0	0.026	0.029	0.110	0.035	0.08
	X	0.025	0.025	0.092	0.032	0.083		Ħ	0.023	0.024	0.064	0.036	0.12
- 1	1	0.019	0.024	0.050	0.034	0.085		I	0.031	0.029	0.032	0.032	0.10
2"H	J	0.025	0.027	0.026	0.030	0.094		J	0.056	0.041	0.018	0.025	0.12
1	X.	0.093	0.047	0.014	0.023	0.141		X	0.130	0.054	0.035	0.019	0.12
1	L	0.145	0.054	0.026	0.020	0.120		L	0.155	0.057	0.045	0.016	0.07
	H	0.135	0.059	0.036	0.018	0.095		×	0.101	0.058	0.059	0.016	0.05
	3	0.105	0.066	0.072	0.016	0.050		3	0.090	0.058	0.093	0.018	0.03
	24	0.170	0.069	0.102	0.018	0.026		2W	0.150	0.052	0.093	0.023	0.02
	4W .	0.105	0.059	0.101	0.025	0.020		PR.	0.037	0.033	0.092	0.026	0.03
	6W	0.075	0.040	0.115	0.025	0.030		6W		0.016	0.094	0.032	0.06
	8N	0.00	0.024	0.107	0.035	0.093		8W	-0.022	0.003	0.047	0.031	0.12
	10W	0.020	0.014	0.060	0.037	0.118		10W	-0.031	-0.005	0.077	0.027	0.08
	12W	0.010	0.007	0.033	0.038	0.110		12V	-0.037	-0.008	-0.007	0.019	0.09
	IN	0.005	0.004	0.017	0.025	0.160		1#A	-0.039	-0.010	-0.013	0.010	0.10
	16W	0.003	0.002	0.009	0.016	0.113		16W	-0.041	-0.010	-0.017	0.003	0.02
Aire	18M	0.000	0.001	0.005	0.010	0.067		184	-0.041	-0.010	-0.019	-0.002	-0.00
1-1/2	20M	••	0.001	0.003	0.005	0.040		50M	-0.042	-0.010	-0.019	-0.004	-0.02
	22W	**	**	0.002	0.003	0.023		22M	-0.0k2	-0.010	-0.019	-0.005	-0.03
	261	-		**	0.002	0.023	1	SPA	-0.0k2	-0.010	-0.23	-0.006	-0.03
7	26W				0.000	0.006	7	26W	-0.042	-0.010	-0.019	-0.006	-0.0kg

(4 of 7 sheets

Tubls A2QContinued

			rverd, Av		Ver	rtical Pre	ssure, p	il at Indic	ated Cells	verse, Av	- Coard -	V 765 mink		
		10					b		Fe.				-	
ROW	Position	Location	P ₆	P7	P8	P ₉	P ₁₀	Position	location	P ₆	P7_	P ₈	19	P ₁₀
11	0	12E	0.30	0.63	2.60	0.80	••	2*8	12E	0.10	0.40	••	0.70	
	- 1	102	0.30	0.63	2.50	0.80		1	10E	0.10	0.35	**	0.70	••
	1	8z	3.00	0.63	2.50	0.60	••	1	38	0.10	0.35	••	0.60	••
	- 1	6E	0.30	0.50	2.50	0.50	~	V	SE.	0.20	0.45	••	0.60	••
		4E	0.40	0.65	2.40	0.40		3"8	4E	0.30	0.10	••	0.60	••
		22	0.80	0.84	2.30	0.50		- 1	2E	0.60	0.95		0.72	
	1	A	1.50	1.45	2.30	0.7C	••		A	1.40	1.65		0.90	••
		В	2.70	1.90	2.20	1.00			B	3.30	2.05	••	1.26	••
		C	4.40	2.57	2.20	1.50			C	4.60	2.80	0.48	1.86	••
		D	5.26	3.05	2.20	1.90	••		D	6.60	3.25	0.80	2.40	
		E	5.30	3.47	2.10	2.40			E	7.70	3.70	1.40	2.90	••
		7	9.70	4.22	2.60	3.50		1	P	11.60	4.35	3.90	4.40	••
		0	13.50	4.75	2.50	4.80			G	13.50	4.80	4.40	6.00	••
		н	9.70	4.95	4.60	6.30		1	н	8.40	4.80	7.40	7.30	
		1	3.60	4.75	9.20	7.50		ł	1	3.30	4.45	8.50	8.48	••
		J	1.70	4.25	3.30	7.70		ŀ	J	1.80	4.00	3.00	8.36	••
		K	1.30	3.85	2.20	6.40	••	1	K	1.70	3.60	0.50	6.50	••
		L	1.70	3.75	1.50	3.30	**		L	2.10	3.55	0.30	5.60	••
		H	2.50	3.60	1.20	4.50	••	1	M	3.10	3.50	0.40	4.60	••
		N	4.50	3.70	0.90	3.40	••	i	N	5.04	3.75	0.60	3.80	••
		24	6.30	4.15	0.70	3.20		- 1	5M	7.10	4.11	1.40	3.96	••
		₩.	9.00	4.63	1.61	3.70	••	1	414	11.70	4.64	3.90	5.00	••
		6W	13.00	5.03	2.00	5.00			CH	12.80	4.78	4.80	6.60	
		8w	9.00	5.03	3.00	6.40		- 1	8W	6.46	4.50	8.90	7.90	••
		10W	4.46	4.65	8.00	7.50	••	100	10W	2.70	3.70	6.40	8.40	
		12W	1.70	3.95	6.80	7.80		1	12W	1.20	2.75	1.30	7.30	••
		14W	0.70	3.00	1.90	6.50		100	14W	0.50	1.95	1.00	5.10	
		16W	0.38	2.15	0.90	4.40		- 1	166	0.10	1.30	0.90	3.60	••
		18w	0.10	1.45	0.50	3.50	••		18W	••	0.75	0.80	2.30	••
		20W	••	0.90	0.40	1.40			20W		0.45	0.70	1.80	
		22N		0.50	0.30	0.80			55A	••	0.15	0.70	1.30	••
	(1)	SPA		0.30	0.20	0.36	••		SAM		••	0.70	0.90	
		26W		0.18		0.20		▼	26W		••	0.70	0.80	

	Por	ward, Av	E Speed =	1.60 mph				ker	rerse, Av	g Speed -	1.75		
Position	Location	_ p ³	D ⁵	D ₃	$D_{\mathbf{l}_{\mathbf{i}}}$	D ₅	Position	Location	D ₁	p ²	D3	Di	D ₅
0	122	0.054	-0.007	-0.007	-0.004	0.035	2"8	12E	0.003	0.003	0.003	0.001	••
	10E	0.055	-0.007	-0.007	-0.004	0.035		10E	0.006	0.006	0.004	0.001	••
	8E	0.055	-0.005	-0.007	-0.004	0.035	1	8E	0.010	0.010	0.006	0.001	••
	6E	0.056	-0.001	-0.004	-0.004	0.035		6 E	0.015	0.019	0.009	0.002	
	4E	0.063	0.007	-0.003	-0.004	0.038	3"8	4E	0.030	0.032	0.01	0.003	0.0
- 1	25	0.073	0.021	0.001	-0.003	0.038		2E	0.048	0.050	0.023	0.00	0.0
- 1	A	0.079	0.041	0.012	-0.002	0.038		A	0.070	0.064	0.040	0.007	0.0
	B	c.083	0.054	0.032		0.039		B	0.089	0.069	0.073	0.012	0.0
	C	0.105	0.063	0.068	0.004	C.0/5	i	С	0.111	0.069	0.10	0.018	0.0
	D	0.130	0.066	0.087	0.008	0.043		D	0.125	0.067	0.108	0.023	0.0
	E	0.153	0.066	0.069	0.011	0.047		Ē	0.128	0.061	0.104	0.027	0.0
	7	0.113	0.054	0.097	0.021	0.060		F	0.070	0.045	0.108	0.035	0.0
- 1	0	0.074	0.037	0.115	0.027	0.075		0	0.040	0.031	0.105	0.038	0.0
- 1	H	0.050	0.026	0.094	0.035	0.102		H	0.030	0.027	0.066	0.038	0.1
_	1	0.043	0.024	0.053	0.037	0.113	- 1	1	0.034	0.031	0.037	0.035	0.2
	J	0.045	0.032	0.033	0.033	0.128		đ	0.041	0.044	0.031	0.027	0.1
	K	0.060	0.048	0.028	0.025	0.136		5	0.068	0.058	0.040	0.021	0.1
1	L	0.069	0.056	0.033	0.021	0.120		L	0.084	0.061	3.048	0.019	0.0
	H	0.074	0.061	0.043	0.019	0.100		ĸ	0.085	0.062	0.066	0.018	0.0
	N	0.085	0.068	0.077	0.017	0.073		×	0.104	0.061	0.095	0.020	0.0
	2W	0.125	0.071	C.103	0.020	0.048		24	0.128	0.053	0.094	0.026	0.0
	PA.	0.120	0.060	0.105	0.026	0.039		N. P.	0.091	0.031	0.094	0.032	0.0
	6W	0.065	0.041	0.117	0.033	0.058		6M	0.035	0.013	0.082	0.035	0.0
1	8 u	0.036	0.024	0.107	0.038	0.090		EM	0.019	**	0.033	0-033	0.1
	10M	0.019	0.013	0.060	0.040	0.110		10W	0.031	-0.005	0.009	0.025	0.3
	12W	0.010	0.006	0.032	0.036	0.120		12V	0.008	-0.007	-0.004	0.014	0.1
	144	0.005	0.003	0.016	0.027	0.130		14W	c.006	-0.008	-0.009	0.006	0.0
	16W	0.003	0.001	0.010	2.018	0.100		16M	0.005	-0.008	-0.017	0.001	0.0
	18w	0.001	-	0.007	0.016	0.070		1.8M	0.005	-0.008	-0.013	-0.003	0.0
	50M	,	••	0.005	0.006	0.036		50M	0.005	-0.008	-0.013	-0.005	0.0
	254		••	0.001	0.003	0.020		22V	0.005	-0.008	-0.013	-0.006	•
	SPA		••	••	0.001	0.010	- 1	SFA	0.005	-0.008	-0.013	-0.006	-0.0
	56A			**	••	0.005		26M	0.005	-0.006	-0.013	-0.006	-0.0

(5 of 7 sheets)

Table	440	COME	

		To	mard, Av	beed -	1.91	resear II	APPERAT M	I at Indie		verse. Av	Epeed .	1.96 mph		
	Position	Location	P ₆	17	78	<u> </u>	P ₁₀	Position	Location	P ₆	P7	P8	- Pg	P10
13	Ï	268 242 222 202 102	0.40 0.44 0.60 0.60 0.56	0.30 0.36 0.42 0.44 0.50	2.00 2.00 2.00 2.00	0.30 0.30 0.33 0.36 0.45	0.25 0.25 0.25 0.25 0.25	5"8	26E 24E 22E 20E 18E	0.08 0.36 0.40	0.18 0.20 0.32 0.42 0.44	=	-0.15 -0.15 -0.15	=======================================
		162 142 122 102 8	0.40	0.62 0.60 0.56 0.44 0.42	2.00 1.95 1.75 1.55 1.50	0.60 0.63 0.66 0.75 0.45	0.5 0.5 0.5 0.5 0.5		162 142 125 102 82	0.40 0.40 0.20 0.20	0.50 0.50 0.46 0.44	0.10 0.10 0.10 0.10	0.03 0.30 0.33 0.30 0.15	=======================================
		62 32 A	0.0k 0.20 0.6k 1.2k	0.42 0.50 0.70 1.02 1.33	1.55 1.50 1.50 1.45 1.45	0.33 0.30 0.30 0.30 0.54	0.25 0.25 0.25 0.25	13	GE LE 2E A B	0.12 0.32 0.40 0.96 1.52	0.42 0.58 0.80 1.16 1.60	0.10 0.10 0.10 0.15 0.25	0.06 0.03 0.03 0.15 0.30	::
		C D E P	2.04 2.60 3.00 5.72 8.56	2.00 2.21 2.62 3.14 3.60	1.50 1.50 1.55 1.90 2.00	0.87 1.20 1.65 2.40 3.39	0.25 0.25 0.25 0.25 0.25		C D E	2.52 3.00 4.36 7.88 9.80	2.22 2.60 2.90 3.58 4.00	0.50 0.60 0.95 1.90 2.65	0.87 1.20 1.50 2.52 3./3	::
		I J K	5.24 2.48 1.40 0.80 1.12	3.90 3.76 3.40 3.00 2.96	3.35 7.00 5.00 2.10 1.50	4.35 5.31 5.70 4.90 4.05	0.25 0.15 0.15 0.35	3 8	H I J K L	6.08 2.60 1.48 1.16 1.32	3.40 3.40 3.00 2.98	5.15 7.10 2.65 0.95 0.70	4.80 5.70 5.70 4.20 4.76	0.90
		N N 2N LW	1.26 2.04 3.26 5.80 8.84	2.90 2.96 3.26 3.72 4.00	1.40 1.05 1.00 1.25 1.45	3.45 2.64 2.10 3.00 3.84	Ē	1	H 2W UU 6W	1.60 2.48 4.00 7.24 9.40	2.98 3.22 3.60 3.90	0.55 0.50 0.85 1.75 2.40	3.00 2.84 2.34 2.85 3.60	=======================================
	Y .	8v 10v 12v 14v 16v	5.40 2.08 0.84 0.40 0.12	4.00 3.50 2.76 2.00 1.50	3.15 6.75 3.25 1.25 0.75	4.80 5.70 5.55 3.93 2.40	0.20		8W 10W 12W 14W 16W	5.68 3.16 1.60 0.60 0.20	2.02 3.64 3.00 2.38 1.76	4.00 7.15 3.90 1.25 0.75	4.80 5.55 5.64 4.53 3.15	0.45
		184 204 224 244 264	Ē	0.76 0.40 0.20 0.10	0.50 0.60 0.25 0.20 0.20	1.35 0.60 0.30 0.15	=	2 S	18W 20W 22W 2W 26W	=	1.10 0.78 0.58 0.30 0.20	0.50 0.40 0.40 0.40	1.80 1.05 0.36	=

		forward	AVE Spe	d - 1.91			n., at Indicated		AVE Spe	ed = 1.96	mph	
	Position	Location	D6	<u>D7</u>	D ₈	<u> </u>	Position	Location	D6	D7_	D ₈	D ₉
13	"	262 242 225 208 108	-0.005 -0.005 -0.005 -0.005	-0.008 -0.008 -0.008 -0.008	-0.00k -0.00k -0.00k -0.00k	-0.056 -0.056 -0.056 -0.055	5"B	26E 24E 22E 20E 18E	0.001 0.001 0.001 0.001	0.002 0.005 0.005 0.005	0.001	0.000 0.000 0.000 0.000
		162 132 122 102 62	-0.005 -0.005 -0.005 -0.006 -0.003	-0.008 -0.008 -0.008 -0.008	-0.00k -0.00k -0.00k -0.00k	-0.055 -0.055 -0.055 -0.055 -0.055		162 142 122 102 82	0.002 0.002 0.003 0.005 0.009	0.002 0.003 0.004 0.006	0.001	0.00 0.00 0.00 0.00
		68 18 28 A	0.001 0.009 0.021 -0.039 0.051	-0.006 -0.005 -0.008 0.006 0.022	-0.00k -0.002 -0.002	-0.055 -0.055 -0.055 -0.055 -0.054		6E 2E A	0.016 0.028 0.043 0.057 0.062	-0.007 0.012 0.020 0.036 0.066	-0.002 0.003 0.006 0.006	-0.00 -0.00 0.00 0.00
		C D E F	9.060 0.063 0.063 0.052 0.037	0.060 0.076 0.080 0.088 0.104	0.003 0.005 0.009 0.017 0.023	-0.052 -0.050 -0.068 -0.038 -0.022		C D B	0.064 0.063 0.058 0.04 0.08	0.095 0.100 0.096 0.104 0.100	0.025 0.020 0.023 0.030 0.033	0.01 0.02 0.02 0.04
		# I	0.026 0.024 0.031 0.066 0.054	0.086 0.050 0.030 0.085 0.088	0.028 0.030 0.026 0.021 0.017	0.057 0.079 0.079 0.137 0.121	Ť	H I J R	0.023 0.027 0.031 0.052 0.056	0.062 0.035 0.026 0.032 0.042	-0. /33 0.030 0.023 0.018 0.017	0.14 0.10 0.11 0.13
		H H SH GH	0.058 0.064 0.067 0.055 0.036	0.036 0.070 0.094 0.094	0.016 0.015 0.017 0.023 0.028	0.088 0.068 0.023 0.026 0.028		64 54 64	0.057 0.057 0.050 -0.033 0.016	0.058 0.088 0.086 0.085 0.086	0.017 0.018 0.022 0.027 0.030	0.05 0.03 0.02 0.03
		100 150 150 100 160	0.020 0.110 0.055 0.003 0.002	0.0% 0.0% 0.02% 0.013 0.007	0.033 0.033 0.065 0.017 0.011	0.115 0.107 0.118 0.146 0.005		100 120 120 110 160	0.005 -0.002 -0.005 -0.006 -0.007	0.052 0.018 0.002 -0.005 -0.010	0.029 0.026 0.020 0.012 0.006	0.11 0.99 0.06 0.11 0.04
		1.0r 20r 22r 25r 25r 25r	0.00L 0.00L 0.00L 0.00L	0.00£ 0.00£ 0.00£ 0.00£	0.005 0.002 0.001 0.001	0.068 0.086 0.024 0.075 0.035	174	10v 20v 20v 26v	-0.007 -0.007 -0.007 -0.007	-0.015 -0.015 -0.015	0.003 -0.002 -0.002 -0.002	0.000 0.000 0.000 0.000

(6 of 7 sheet

Table A2Q Concluded)

		Fo	rward, Av	g Speed =		tical Pro	seure, p	i at Indic		verse, Av	Speed -			
low	Position	Location	P ₆	P ₇	P ₈	Pg	P ₁₀	Position	Location	P ₆	r_{γ}	Pa	Pg	?10
15		26E 24E 22E 20E 18E	0.54 0.66 0.98 1.34 1.46	0.30 0.39 0.52 0.65 0.75	1.50 1.50 1.56 1.64 1.76	0.40 0.14 0.52 0.64 0.80	out	None	26E 24E 22E 20E 18E	0.04 0.16 0.36 0.72 0.98	0.10 0.15 0.30 0.41 0.53	0.06	0.06 0.24 0.33	out
		16E 14E 12E 10E	1.08 0.56 0.20 0.08	0.91 0.89 0.79 0.65 0.63	1.94 1.90 1.56 1.26 1.16	1.00 1.24 1.40 1.32 1.04			16r 14e 12e 10e 8e	0.94 0.56 0.40 0.32 0.32	0.59 0.51, 0.45 0.40 0.28	0.50 0.52 0.36 0.24 0.06	0.60 0.75 0.75 0.75 0.45	
		6E LE 2E A B	0.08 0.20 0.42 0.70	0.01 0.71 0.88 1.19	1.10 1.02 1.02 1.02 1.00	0.80 0.64 0.56 0.56 0.72			€E -E 2E A B	0.30 0.38 0.44 0.72 1.10	0.28 0.28 0.48 0.80 1.15	=	0.45 0.30 0.24 0.27 0.45	
		C D E F	1.22 1.62 2.06 3.00 3.66	1.59 1.80 2.01 2.47 2.81	1.04 1.06 1.16 1.22 1.58	0.96 1.20 1.36 1.72 2.56			C D E P	1.68 2.00 2.60 4.12 5.02	1.62 1.85 2.10 2.58 2.90	0.12 0.22 0.44 0.82	1 26 2.86 2.46	
		H I J K L	2.82 1.64 0.84 0.74 0.80	2.95 2.96 2.65 2.44 2.35	.10 2.62 2.00 1.10 0.86	3.24 3.84 4.00 3.48 3.04			H J K L	3.84 2.30 1.42 1.10 1.16	3.02 2.89 2.58 2.36 2.31	1.84 2.62 1.90 0.96 0.70	3.60 4.26 4.26 3.39 3.00	
		M N 2W LW 6W	0.90 1.40 2.00 2.98 3.90	2.39 2.40 2.65 2.94 3.15	0.61 0.14 0.50 0.75 0.90	2.68 2.16 2.00 2.24 2.80			X 2W UV 6W	1.20 1.60 2.46 3.70 4.70	2.23 2.37 2.60 2.85 3.10	0.56 0.40 0.44 0.72 1.04	2.46 2.26 2.26 2.56 2.70	
		8w 10w 12w 14w 16w	3.34 1.80 0.80 0.10 0.20	3.19 2.94 2.51 1.98 1.41	1.44 2.38 2.12 1.16 0.62	3.40 4.00 4.20 3.60 2.60			8w 10w 12w 14w 16w	4.20 2.58 1.50 1.02 0.64	3.08 2.80 2.32 1.85 1.29	1.64 2.64 2.42 1.50 0.96	3.45 4.05 4.23 3.66 2.55	
		18W 20W 22W 24W 26W	0.10 -0.10 -0.10 -0.10	0.97 0.56 0.35 0.21 0.10	0.30 0.20 0.10 0.08 0.04	1.60 1.00 0.50 0.24 0.12			18w 20w 22w 24w 26w	0.50 0.30 0.30 0.30 0.30	0.91 0.52 0.25 0.10	0.72 0.44 0.42 0.38 0.38	1.80 1.14 0.60 0.30 0.06	

14 P. I. E. S.	Forward	Avg Spe	ed = 1.94	mph			Reverse	AVE SP	eed =	mph	
Position	Location	D ₆	D7	D8	Dg	Position	Location	D ₆	D ₇	D8	Do
Î	26E 24E 22E	-0.006 -0.005 -0.005	-0.002	-0.004 -0.004 -0.004	0.030 0.030 0.030	None	26E 24E 22E	0.005	0.001	=	0.001 0.001 0.001
	18E	-0.005 -0.006	-0.005	-0.004	0.030		18E	0.002	0.001	=	0.002
	16e 14e 12e 10e 8e	-0.006 -0.005 -0.005 -0.00k -0.003	-0.002 -0.003 -0.003 -0.003	-0.00k -0.00k -0.00k -0.00k	0.030 0.030 0.030 0.030 0.030		16E 14E 12E 10E 8E	0.003 0.003 0.005 0.007 0.012	0.002 0.003 0.006	0.002 0.002 0.002 0.007	0.002 0.003 0.003 0.004
	6E 4E 2E A	0.001 0.009 0.024 0.044 0.057	-0.003 -0.001 0.004 0.012 0.032	-0.004 -0.003 -0.003 -0.002	0.030 0.030 0.030 0.030 0.031		6E 4E 2E A B	0.020 0.035 0.051 0.067 0.071	0.008 0.014 0.023 0.041 0.071	0.002 0.003 0.00k 0.008	0.00k 0.005 0.007 0.009 0.003
	D E P	0.066 0.069 0.069 0.058 0.041	0.048 0.081 0.086 0.094 0.108	0.004 0.006 0.019 0.018 0.027	0.033 0.034 0.038 0.047 0.065		C D E F	0.071 0.068 0.063 0.047 0.033	0.101 0.102 0.101 0.100	0.019 0.023 0.027 0.033 0.037	0.019 0.023 0.031 0.051 0.065
	H I J K L	0.028 0.026 0.035 0.050 0.058	0.091 0.056 0.037 0.031 0.034	0.033 0.035 0.030 0.024 0.020	0.115 0.129 0.142 0.134		H I J R L	0.028 0.034 0.047 0.061 0.064	0.066 0.037 0.030 0.037 0.047	0.037 0.033 0.026 0.020 0.020	0.123 0.122 0.125 0.119 0.099
	H H W W W	0.063 0.071 0.074 0.063 0.044	0.042 0.077 0.097 0.099 0.111	0.018 0.019 0.025 0.031	0.115 0.078 0.053 0.046 0.057		# # # # 6v	0.065 0.064 0.058 0.041 0.022	0.061 0.090 0.093 0.088 0.090	0.028 0.020 0.025 0.030 0.03k	0.079 0.052 0.043 0.051 0.075
	86 100 120 100 160	0.027 0.015 0.009 0.005 0.003	0.101 0.069 0.042 0.022 0.014	0.035 0.038 0.033 0.025 0.017	0.089 0.115 0.124 0.137 0.117		8v 10v 12v 14v 16v	0.009 -0.003 -0.005 -0.006	0.065 0.026 0.008 -0.002 -0.006	0.034 0.031 0.024 0.016 0.008	0.133 0.116 0.118 0.090
	1.8W 20W 22W 2WW 26W	0.001	0.009 0.006 0.00k 0.003	0.010 0.006 0.003 0.001	0.077 0.046 0.027 0.016 0.010		18v 20v 22v 24v 26v	-0.006 -0.006 -0.006 -0.006	-0.010 -0.011 -0.011	-0,001 0.002 0.003	0.055 0.030 0.017 0.007

Table A-21

Mu'tiple-Wheel Heavy Sear Load Flexible Pavement Test, Dynamic Instrumentation Loading Date

[test 4; Load Condition: 30 haps per Wheel, 12 Wheels, 100 psi

		Pol	roard, Avg Speed			APPERT A P	al, at Indic	Re	verse, Av	g Speed -	1.61 mpt		
	Delties	location	1, 1,	,	Ph	7,	Position	Location	P ₁ *	Pg	P,	P _k	15
5	Î	202 202 202 102 162	0.24 0.25 0.25 0.24 0.28	3.60 3.60 3.60 3.55 3.55	-0.09 -0.07 0.03 0.03	1.30 1.28 1.26 1.26	Bone	24E 20E 18E 17E		0.06 0.08 0.08 0.08	=	0.14 0.19 0.26 0.30 0.32	::
		148 122 108 68	0.23 0.35 0.35 0.55	3.55 3.55 3.60 3.65 3.70	0.03 0.02 0.02 0.07 0.20	1.33 1.36 1.34 1.27 1.30		14E 12E 10E 8E		0.07 0.09 0.16 0.30 0.69	0.05	0.34 0.36 0.40 0.48 0.64	:
		22	1.55 2.63 4.26 6.22 7.63	3.85 4.25 5.00 7.70 15.20	0.42 0.90 1.54 2.59 3.85	1.52 1.43 1.75 2.42 3.61	17	4E 2E A B		2.83 4.87 6.74 7.76	0.15 0.50 1.55 6.20 14.50	0.98 1.56 2.49 3.78 5.21	0.32
		D E F O	8.18 8.50 8.35 6.46 4.34	15.95 13.55 12.10 16.75 9.05	4.60 5.34 6.66 7.50 7.53	4.76 6.48 10.96 12.32 12.68		D E P O H		8.05 8.22 7.51 5.68 3.85	13.20 10.15 10.25 14.05 6.65	5.94 6.64 7.61 7.90 7.43	6.56 11.35 11.06 11.64
		I J E L	3.00 2.97 4.14 5.24 6.16	2.80 1.20 1.30 2.40 4.30	6.73 5.65 4.82 4.63 4.62	13.77 8.64 3.92 2.61 2.00		I J K L		3.04 3.50 5.09 6.00 6.85	2.00 0.95 1.50 2.90 5.25	6.43 5.45 4.97 4.96 5.19	11.81 7.02 3.16 2.20 2.00
		20 44 60	7.60 8.55 8.32 6.43 4.01	12.50 13.60 10.20 14.65 9.10	5.09 6.18 7.15 7.80 7.66	2.18 5.26 10.26 12.20 12.08		2W WW 6W 8W		7.75 8.10 7.50 5.96 3.89	14.70 11.40 9.50 14.50 7.95	5.95 6.89 7.56 7.83 7.10	2.78 6.06 11.05 11.46 11.20
		100 120 150 160 160	2.16 1.07 0.52 0.20 0.06	2.55 0.60 0.15	6.67 5.08 3.58 2.26 1.37	13.20 8.96 4.05 1.44 0.46		10W 12W 16W 16W 18W		2.30 1.30 0.70 0.32 0.14	2.75 1.15 0.60 0.40 0.35	5.88 4.38 2.96 1.89 1.05	11.92 7.80 3.64 1.66 0.55
		204 224 244 264	I	:	0.78 0.42 0.22 0.12	0.10		204 224 244 264 284		0.02	0.30 0.35 0.35 0.35	0.54 0.20 0.01 -0.09	0.06 -0.14 -0.16 -0.16

D procure recorded.

(1 of 8 shorts)

Table A21 (Continued

		Jo.	rangel. Av	Street v	1.65 mgb	riled Pr	essure, D	si, at in c		verse. Iv	a Append a	1.79 mph	·)	
Row	Position	Location	1	12		7,	F ₅	Position	Location	1	12	1,	Pa	P ₅
7	1"8	24E 22E 20E 18E 16E	::	0.28 0.30 0.26 0.27 0.19	0.50 0.50 0.50 0.45 0.35	0.03 0.07 0.14 0.18 0.19	0.13 0.12 0.10 0.10 0.10	1°3	242 228 208 188 168	=	0.06 0.06 0.10 0.12 0.12	=	0.16 0.21 0.27 0.35 0.40	=======================================
	2"8	14E 12E 10E 8E 6E	=======================================	0.18 0.17 0.26 0.44 0.81	0.35 0.35 0.30 0.30 0.35	0.19 0.15 0.14 0.18 0.27	0.06 0.06 0.04 0.02		142 122 102 82 63	=	0.12 0.14 0.22 0.36 0.72	0.10	0.40 0.40 0.42 0.48 0.63	=
		2Z A B C C	39.80	1.45 2.48 4.03 5.90 7.36	0.55 0.85 1.75 5.00 19.10	0.48 0.91 1.57 2.56 3.82	0.06 0.40 0.98 2.22	378	A B C	48.80 0.30 0.15	2.74 4.65 6.52 7.79	0.15 0.45 1.50 7.35 23.40	0.95 1.48 2.33 3.56 5.02	0.10 0.34 0.96 2.50
		E F G	20.45	7.88 8.30 8.34 6.48	21.00 15.30 13.05 26.05 11.70	4.48 5.18 6.48 7.30 7.32	3.32 5.10 10.16 11.40 12.60		D E F	37.85	8.18 8.43 7.78 5.86 3.93	20.50 12.75 14.70 23.90 7.20	5.73 6.41 7.30 7.66 7.19	4.10 6.70 12.04 11.42 12.96
		I J K L	25.15 39.40 0.80	2.88 2.74 3.82 4.70 5.70	1.75 0.10 0.10 0.50 2.25	6.59 5.39 4.58 4.34 4.35	15.32 9.12 3.68 2.15 1.46		I B L	39.00 36.10 0.55	3.40 4.84 5.77 6.67	0.85 0.30 1.00 2.35 5.45	6.23 5.20 4.71 4.70 4.93	13.58 5.18 2.94 2.02 1.82
	1"8	N 2W Law GH BW	43.90	7 22 6.31 6.44 3.98	16.80 18.75 11.90 25.25 13.70	5.90 6.84 7.54 7.42	1.54 4.34 9.86 12.20 12.43	2"8	30 60 60 80	47.00	7.69 8.45 7.98 6.27 4.20	21.80 15.80 12.10 24.55 10.45	5.65 6.69 7.36 7.60 7.13	2.58 5.90 11.64 11.60 12.34
	0	10W 12W 14W 16W 16W	=	2.14 1.04 0.50 0.20 0.05	2.55	6.50 4.93 3.45 2.16 1.28	15.16 10.22 4.10 1.14 0.30	i	10v 12v 16v 16v 18v	Ē	2.53 1.51 0.86 0.51 0.30	0.53 0.55 0.60	5.91 4.40 2.96 1.89 1.10	14.18 8.55 3.64 1.46 0.36
		20M 22M 25M 26M 26M	:	=	=	0.73 0.37 0.18 0.08 0.03	=		204 224 244 264 264 284	=	0.19 0.13 0.12 0.13	0.60 0.60 0.55 0.55	0.60 0.28 0.12 0.02	-0.08 -0.27 -0.26 -0.29 -0.26

(2 of 8 shoets)

Table A21(Continued

				g Speed -		rtical Pr	eseme b	si, at Indic	ated Cells		Speed -	1 11		
Row	Position	Location	76	7	P ₈	Pg	P ₁₀	Position	Location	16	F7	- 8	79	P ₁₀
9	14.	125 106 85 62 45	0.40 0.35 0.40 0.45 0.40	0.20 0.40 0.90 1.68	0.20 0.20 0.18 0.21 0.21	0.15 0.20 0.45	0.90 0.92 0.86 0.86	7*8 6*s	12E 10E 8E 6E	-0.10 -0.10	0.11 0.33 0.77 1.92	0.03	0.62 0.63 0.70 0.89 1.20	=
		A B C D	0.15	3.20 5.38 7.72 9.44 10.16	0.21 0.28 0.37 0.65 0.73	0.86 1.48 2.40 3.58 4.26	0.80 0.98 1.30 2.02 2.80	5*8	A B C	-0.12 -0.20 -0.22 -0.18 -0.24	3.49 5.91 8.21 9.55	0.08 0.16 0.40 0.64 0.61	1.71 2.51 3.69 4.96 5.67	0.10 0.18 0.54 1.40 2.38
		E P O H	0.10	10.60 10.20 7.80 5.32 3.60	0.68 0.59 0.77 0.55 0.19	4.91 6.20 6.58 7.24 6.60	4.00 7.78 9.22 9.52 10.80		F G H	-0.20 -0.20 -0.10	9.88 8.81 6.46 4.29 3.26	0.54 0.54 0.59 0.30 0.09	6.22 7.10 7.47 7.02 6.15	3.96 8.01 8.40 8.56 9.56
		X L H	0.30	3.60 5.24 6.60 7.68 9.50	0.05 0.05 0.10 0.20 0.5h	5.60 4.59 4.48 4.40	7.40 3.50 2.26 1.58 1.40	L°s	J K L N	-0.20 -0.21 -0.18 -0.27 -0.30	1.03 5.80 7.04 7.96 8.97	0.13 0.24 0.37 0.65	5.35 4.87 4.87 5.00 5.61	6.34 3.00 2.06 1.52 1.71
		2W 6W 6W 10W	=======================================	10.40 10.22 7.80 5.00 2.68	0.64 0.53 0.65 0.52 0.15	5.70 6.60 7.29 7.31 6.40	3.24 7.30 9.32 9.20 10.30	3-1/2"8	24 44 64 84 104	-0.32 -0.20	9.30 8.56 6.43 4.08 2.09	0.58 0.51 0.58 0.32 0.10	6.57 7.20 7.44 6.95 5.87	3.64 7.70 9.58 8.02 9.26
		12W 16W 16W 12W 20W	=	1.34 0.92 0.32 0.16	Ē	5.12 3.71 2.35 1.40 0.81	7.46 3.70 1.40 0.50 0.20	3,78	12W 16W 16W 18W 20W	E	0.82 0.03 -0.48 -0.69 -0.90	0.03	4.57 3.04 2.01 1.32 0.80	7.11 3.48 1.80 0.83 0.33
		56A 57A 55A	Ξ	Ξ	Ē	0.46 0.25 0.20	0.16		22W 26W 26W 26W 30W	=	-0.92 -0.93 -0.94 -0.95 -0.96	=	0.52 0.33 0.21 0.11 0.12	0.08

	Por	ward, Av	Speed -		reiest be	recrion.	in., at Ind			g Speed .	1.77 pek		
Position	Location	D	p ⁵	D ₃	Di	D ₅	Position	Location	L _d	D ⁵	D,	D ₁	<u> 1</u> 5
3/17	12E 10E	0.059	0.017	-0.003	-0.024	-0.020	7"8	12E	=	0.007	0.01	0.008	0.00
	82	2.059	0.019	-0.003	-0.026	-0.020		82		0.008	0.006	0.009	0.00
	6E	0.060	0.028	-0.003	-0.026	-0.021		62	-	0.032	0.00.5	0.009	0.00
	148	0.060	0.040	-0.303	-0.027	-0.021	6"8	NE.	-	0.054	0.022	0.012	0.00
	2	0.059	0.062	-0.003	-0.026	-0.021		25	0.003	0.083	0.025	c.al	0.00
		0.060	0.097	-0.002	-0.024	-0.022		A	0.003	0.115	0.027	0.020	0.00
		0.059	0.115	-0.001	-0.018	-0.023		3	0.006	0.137	0.029	0.032	0.01
	C	0.062	0.138	0.001	0.006	-0.022	5"8	C	0.021	0.163	0.029	0.054	0.02
		0.068	0.184	0,003	0.018	-0.017	1						
		0.063	0.129	0.003	0.066	-0.006		E	0.029	0.163	0.027	0.007	0. 330
	ó	0.10	0.078	0.011	0.094	0.017	1	ó	0.099	0.047	0.020	0.144	0.00
	H	0.137	0.050	0.015	C.123	0.051		n	0.148	0.037	0.018	0.170	0.107
	1	0.159	0.041	0.017	0.166	0.079	- 1	1	0.153	0.047	0.037	0.169	0.131
		0.175	0.052	0.018	0.137	0.101		3	0.154	0.073	0.019	0.102	0.137
ALC: The second	K	0.191	0.085	0.017	0.078	0.122	- 1	K	0.148	0.113	0.020	0.052	0.12
16 5 5 5	L	0.178	0.192	0.017	0.056	0.116		L	0.12	0.116	0.020	0.042	0.999
		0.154	0.111	0.017	0.042	0.100	4 °s	- 1	0.095	0.125	0.020	0.039	0.075
		A COLUMN TO SERVICE		A LANGE	1000	7.4	1		0.046			11111	
	2N	0.065	0.182	0.021	0.041	0.031	- 1	W IN	0.058	0.156	0.015	0.074	0.037
(B) (A) (G)	64	0.073	0.002	0.024	0.113	0.042		64	0.092	0.041	0.005	0.130	0.069
1 V BE2/100	8W	0.119	0.045	0.027	0.137	0.070	3-1/2"8	8W	0.136	0.008	0.000	0.149	0.094
44 Bill	100	0.155	0.023	0.028	0.181	0.099		100	0.150	0.005	-0.002	0.155	0.110
	124	0.165	0.013	0.027	0.154	0.117		12W	0.145	-	-0.003	0.101	0.121
	144	0.173	0.000	0.024	0.095	0.133	3"8	140	0.140	-0.003	-0.005	0.041	0.110
100	160	0.149	0.005	0.021	0.051	0.113		16v 18v	0.099	-0.003	-0.005	0.016	0.073
18 18 18 18	18V 20V	0.088	0.003	0.015	0.026	0.071		50M	0.054	-0.003	-0.006	-0.003	0.034
					-		- 1	•		311.5	110000	Contract of	- In Maria
100,67	22V	0.028	0.002	0.013	0.008	0.020		244	0.009	-0.002	-0.005	-0.005	-0.003
AND THE REAL PROPERTY.	26W	0.009	0.002	0.009	0.004	0.006		26V		-0.001	-0.005	-0.006	-0.006
The state	201	0.004	0.002	0.007	0.003	0.003		20v	-	-0.001	-0.00	-0.005	-0.005
	300	0.002	0.000	0.006	0.002	0.002		30V	-		-0.003	-0.00k	-0.005

(continue)

(2 of 8 days

Tuble A28(Continued

			mand Av	g Speed -	1.59 mph	rticel Pr	seems b	t at adio	ated Celle	weree, Au	. Bread .	1.47		
Row	Position	Location	-6	7,	-8	P9	P ₁₀	Position	Location	16	3	-8	.5	10
10	Ï	164 142 125 100 85	1.00 0.80 1.50 1.30 0.90	-0.18 -0.20 -0.20 -0.10 0.16	=	0.25 0.25 0.20 0.19 0.21	-0.20 -0.20 -0.20 -0.24 -0.25	1	160 140 127 100 60	Ē	0.22 0.23 0.23 0.30 0.57	0.45 0.50 0.40 0.45 0.60	0.40 0.40 0.40 0.40	=
		62 42 22 A	1.40 1.60 1.50 99.60 2.00	0.58 1.40 2.68 4.56 6.98	1.40	0.30 0.51 0.6; 1.40 2.33	0.26 -0.22 -0.20 -0.06 0.30		2 A	124.80 0.90	1.0k 2.03 3.82 6.00 8.19	0.65 0.65 1.25 2.10 4.75	0.60 0.86 1.44 2.21 2.43	0.80
		C D E P	2.60 63.00 118.60 1.50 1.70	8.52 9.18 9.61 9.76 7.5h	5.20 6.10 4.65 4.55 7.85	3.46 3.99 4.60 5.86 7.66	1.04 1.84 3.04 7.40 8.72		C D E P	1.60 74.80 118.60	9.50 9.97 10.32 9.11 7.09	7.80 7.10 5.80 6.05 7.05	4.56 5.14 5.78 6.72 7.01	1.80 2.95 4.77 9.46 9.31
		I I I	1.90 1.00 1.40 75.30 99.70	5.21 3.48 3.36 4.70 5.84	5.20	7.90 6.33 5.40 4.57 4.38	9.80 11.96 8.38 3.80 2.18		H I J K	84.40 104.60	5.01 3.82 4.44 6.04 7.19	2.50 0.30 0.50 1.35 2.40	6.79 5.97 5-13 4.52 4.56	10.45 11.86 7.46 3.16 2.0
		N N N N N N N N N N N N N N N N N N N	7.00 1.60 130.20 2.60 1.80	7.06 8.82 9.02 9.08 8.06	0.85 5.60 6.30 4.85 8.20	4.63 5.47 6.34 7.05	1.50 1.02 2.70 7.02 9.44		10 20 20 40 60	130.40 1.20	8.20 9.34 10.07 9.62 7.58	4.10 7.60 6.30 5.70 7.35	4.71 5.20 6.02 6.82 7.26	1.76 2.05 4.32 9.00 9.00
		16H 15H 14H 16H	1.70 1.60 1.40	5.07 2.74 1.31 0.68 0.24	6.60 2.75 c.40	7.05 6.25 5.02 3.64 2.33	9.72 12.10 9.26 4.34 1.46	3-1/27	8v 10v 12v 14v 16v	Ē	5.01 2.86 1.56 C.84 0.39	3.30	6.68 5.43 4.19 2.90 1.83	9.84 11.82 8.20 3.82 1.51
		184 204 244 244 264	Ē	0.10	Ē	1.40 0.80 0.45 0.23 0.11	0.44	3"	1.6W 20W 22W 25W 26W	=	0.14	=	1.12 0.60 0.85 0.09 -0.02	-0.69 0.11 -0.17
									26v 30v	=	=	=	-0.11	-0.16

2011/201	70	ward, Av	Speed -	1.89 mb	PROPER DE	144C DECIL	in., at Ind	Re	verse, Av	Bool -	1.47	Section 1	7.
Position	Location	_ p ³ _	p ⁵	D3	D	D ₅	Position	Lostion	4	De	<u>b</u>	4	3
ï	162 112 122 102 82	-0.0k0 -0.0k0 -0.0k0 -0.0k0	-0.010 -0.010 -0.010 -0.007	=	-0.008 -0.008 -0.008 -0.008	-0.006 -0.006 -0.006 -0.006	ĵ	168 188 138 138	0.001 0.002 0.003 0.003	0.008 0.006 0.013 0.009 0.007	0.007 0.009 0.013 0.025 0.029	0.008 0.009 0.003 0.003	0.00
	62 142 22 A	-0.0k0 -0.0k0 -0.0k0 -0.0k0	-0.001 0.01k 0.0k1 0.130 0.140	0.001	-0.010 -0.000 620.0-	-0.007 -0.007 -0.008 -0.008 -0.007		15 25 A	0.005 0.005 0.006 0.010 0.015	0.045 0.075 0.130 0.245 0.157	0.023 0.033 0.033 0.036 0.036	0.005 0.007 0.011 0.001 0.037	0.00
	C D E F	-0.035 -0.033 -0.003 -0.020 0.004	0.176 0.203 0.134 0.078	0.007 (1.009 0.012 0.017 0.022	0.013 0.025 0.065 0.103 0.137	-0.005 -0.002 0.002 0.017 0.055		C D B T	0.023 0.030 0.039 0.070 0.119	0.176 0.200 0.180 0.074 0.065	0.037 0.037 0.035 0.032 0.032	0.066 0.089 0.120 0.171 0.169	0.0
	H J K L	0.099 3.140 0.129 0.219 0.209	0.047 0.038 0.051 0.131 0.180	0.026 0.027 0.027 0.026 0.025	0.154 0.187 0.156 0.097 0.071	0.075 0.112 0.130 0.142 0.135			0.212 0.164 0.173 0.210 0.133	0.00 0.096 0.098 0.176 0.172	0.025 0.025 0.027 0.029 0.029	0.181 0.173 0.107 0.076 0.076	0.1
	EN EN	0.153 0.086 0.066 0.09h 0.039	0.174 0.164 0.216 0.165 0.101	0.026 0.026 0.032 0.035	0.056 0.065 0.068 0.120 0.159	0.117 0.077 0.050 0.044 0.061			0.086 0.052 0.063 0.063	0.137 0.144 0.166 0.058 0.017	0.005 0.007 0.003 0.006 0.000	0.065 0.061 0.100 0.154 0.155	0.0
	low 12w 14w 16w	0.100 0.185 0.162 0.231 0.192	0.060 0.033 0.020 0.011	0.038 0.039 0.036 0.032 0.028	0.170 0.198 0.173 0.111 0.062	0.098 0.128 0.142 0.150 0.150	3-1/276	100 150 150 150 160	0.156 0.153 0.207 0.000	-0.020 -0.029 -0.032 -0.032	-0.602 -0.603 -0.603	0.198 0.152 0.091 0.037 0.086	0.11 0.11 0.11
	1.0x 20x 22x 24x 26x	0.118 0.110 0.038 0.023 0.026	0.008 0.008 0.006 0.007 0.006	0.025 0.021 0.017 0.015 0.013	0.096 0.021 0.014 0.010 0.008	0.050 0.050 0.08 0.027 0.020	Ť	18v 20v 20v 20v 26v	-0.005 -0.005 -0.005	-0.031 -0.031 -0.030 -0.039 -0.039	-0.05 -0.05 -0.05 -0.05	-0.00 -0.03 -0.027 -0.027	0.0 0.0 -0.0 -0.0
1-1/27	2 De .	0.003	0.006	0.001	0.007	0.008		NOV.	-0.006	-0.029	-0.00h	-0.06	-0.G

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Table 424(Continued

			mord. A	og Spane	. 35	rtical n	essure, N	at India		variet, In	Bed :	1.5.00		
how	Position	Location	6	1	8	9	10	Position	Location	6	7	- 8	9	10
12	0	200		0.20	2.40	0.48	0.25	3"8	20E		0.42	-	0.53	-
	1	182		0.16	2.40	0.40	4.6		. BE		0.44		0.58	
	- 1	142			2.40	9.56	0.25		160		0.42		0.63	
	1	14E			2.40	0.52	0.25		142		0.35		0.60	
		122			2.40	0.49	0.25		1.290		0.36		0.61	
		10E			2.40	0.42	0.25		100		0.38		0.59	-
	i	8E		0.16	2.40	0.14	0.25		6z		0.58		0.62	
	- 1	62		0.54	2.40	0.47	0.25		6E		0.9		0.72	
		14E		1.21	2.40	0.63	0.25		LE.		1.60	-	0.9.	
		25	••	2.12	2.40	0.92	0.25		21		2.98	0.40	1.37	
		A		3.56	2.70	1.42	0.25	1	A		4.72	1.05	2.06	0.14
		3		5.17	3.00	2.05	0.56		b	-	6.52	2.60	2.87	0.40
		C		6.96	3.95	2.97	0.55	1	C		8.16	4.35	3.94	1.28
		D	19.80	7.72	5.50	3.48	0.55	1	D	8.10	8.90	4.50	4.46	2.12
		E	40.60	8.38	7.35	3.99	0.57		E	19.8	9.30	4.50	4.95	3.11
				8.64	13.40	5.08	1.21		F		8.80	7.05	5.84	5.70
		0	-	€.9€	17.75	5.80	2.67	- 1	G		6.60	8.10	6.27	7.32
	- 1	11		4.54	26.20	6.0	1.86	1	H		4.52	3.00	5.96	9.92
	i	1		,.12	37 - 35	6.56	0.49		I		3.40		5.34	12.30
		J		2.76	27.45	4.62	0.25		3		3.60		4.59	7.60
	1	K		3.68	13.00	4.09	0.25	1	8 .		4.74	1.00	4.10	2.98
		L		4.70	8.30	3.87	0.25		L		5.70	1.45	4.07	1.96
		W		5.44	5.75	5.81	0.25		Ħ		6.26	2.40	4.27	1.40
		H		7.08	4.25	4.06	0.25		34		7.76	4.25	4.58	1.42
	- 1	2W	21.90	8.29	6.30	4.5	0.37	i	24	26.30	9.02	4.50	5 - 37	2.76
	- 1 -	4M		8.78	13.35	5.43	0.03	1	44	-	8.72	5.90	5.88	5.12
		6W		7.20	18.90	6.07	2.31	1	64		6.98	7.60	6.23	6.76
		8w		4.61	24.70	6.16	1.91		BM		4.64	4.10	5.95	8.80
	1	10M		2.40	35 - 75	5.52	0.45	2"8	104		2.84	0.45	4.08	12.30
		12W		1.18	30.35	4.42	0.49		126	••	4.52		3.89	8.68
		166		0.42	24.45	3.24	-0.15	1	146		0 70		2.29	3.62
	1	16W		0.14	5.45	2.4	-0.13	- 1	26W		0.28		1.61	1.66
		18M			2.40	20	-0.14		28W				1.17	0.62
	1	20M		-	1.30	U.66	-0.13	į	201		•		0.69	0.20
		224	•••	-0.18	0.00	0.35	-0.15	"B	22		••		0.37	••
		244		-0.18	0.35	0.20	-0.16	1	214		••		0.18	
		26W		0.12	0.20	0.10	-0.14	1	16M				0.09	
		20M			0.10	0.06	-0.11	1	28W		••	••	-c.03	
		30W			L 10	0.04	-0.10	•	30W				-0.03	

	701		2 Speed =					Nev	PENP. AV	Bre and -			
Position	Location	P3	D ³	D,	1/2	D ₅	Position	location	4	T _a	D	Tr.	125
0	202	0.080	0.065	-0.002	-0.008	-0.006	3"8	200		.003	0.009	0.003	0.00
1	188	0.080	0.065	-0.002	-0.008	-0.006	1	130	0.000	1.03	0.01	0 004	0.00
	168	0.080	0.065	-0.002	-0.00A	-0.006		16E	0.000	3.004	0.003	0.005	0.00
	1 NE	0.380	0.065	-0.002	-0.008	-0.0%		14E	0.004	0.006	0.006	0.005	0.00
	128	0.080	0.065	-0.002	-0.008	-0.006	- 1	1.290	0.004	0.009	0.017	0.006	0.0
	102	0.080	0.065	-0.002	-0.008	-0.006		1 CE	0.005	6.003	0.021	0.007	0.0
	• (8)	0.080	0.067	-C.008	-0.009	-0.006	1	8EC	0.005	0.023	0.025	0.008	0.0
	68	0.080	0.075	-0.002	-0.006	-0.0C.5	1	€ €	0.005	0.042	0.029	0.009	0.0
1	NE.	0.080	0.091	-0.002	-0.07	-0.006		LE.	0.005	0.073	0.034	0.010	0.0
	28	0.780	0.114	-0.002	-0.006	-0.006		23	0.006	0.122	0.038	0.015	0.0
	A	0.077	0.161	-	-0.004	-0.006	1	A	0.009	0.169	0.041	0.025	0.0
	3	0.078	0.171	0.003	0.003	-0.005		•	0.011	0.171	0.0-2	0.043	ο. α
	c	0.079	0.190	0.007	0.017	-0.002	1	C	0.015	0.174	0.042	0.074	0.0
	D	0.080	0.203	0.000	0.031	0.002		D	0.023	0.175	0.041	0.099	0.0
	E	0.081	0.206	0.013	0.11	0.005	- 1	K	0.028	0.162	0.039	0.127	0.0
		0.090	0.153	0.020	0.113	0.022	- 1	7	0.082	0.102	0.035	0.178	0.0
	0	0.102	0.095	0.026	0.146	0.049		0	0.082	0.066	0.031	0.181	C.Z
		0.115	0.066	0.031	0.169	0.09	- 1	7	0.119	0.057	0.029	0.185	0.1
	I	0.130	0.070	0.033	0.176	0.123	1	I	0.141	0.073	0.029	0.172	0.1
	J	0.156	0.076	0.033	0.169	0.144	1	J	0.172	0.113	0.030	0.114	0.1
	K	0.217	0.120	0.331	0.09	0.154		ĸ	0.181	0.164	0.031	0.065	0.2
	L.	0.211	0.161	0.030	0.074	0.143		L	0.146	0.172	0.031	0.056	0.1
100	-	0.169	0.161	0.030	0.058	0.174	- 1	*	0.105	0 159	0.031	0.053	0.0
		0.110	0.176	0.030	0.047	0.080		31	0.061	0.160	0.026	0.066	0.0
	20	0.075	0.174	0.033	0.067	0.054	- 1	24	0.055	0.157	0.024	0.114	0.0
	let .	0.096	0.154	0.037	0.12	0.017		ber .	0.058	0.100	0.005	0.165	0.0
	eu .	0.068	0.097	0.041	6.165	0.067		GM	0.080	0.057	0.02	0.167	C. 0
	CM .	0.071	0.053	0.041	0.179	0.107		(%)	0.113	0.030	0.006	0.165	0.1
	10	0.115	0.027	0.063	C.FOR	0.138	8.8	104	0.141	0.014	0.002	0.161	0.1
	12V	0.136	0.023	0.041	0.175	0.154		120	0.166	. o. or ,		0.106	0.1
	Ales	0.187	0.000	0.037	0.113	0.163		114	0.7 1	0.007		0.047	0.1
- 1	160	0.165	0.002	0.031	0.00	0.135		16	6.1.	0.006		0.016	0.0
	18W	0.097		0.02	0.032	0.053		1.00	0.43	0.0		3.002	0.0
	800	0.056	-	O. CER	0.018	0.053		200	0.041	0.0 3		-0.005	0.0
	254	0.032	-0.03	0.018	0.40	0.030	3,8	254	0.030	0.006		-0.006	-0.0
	glat	0.018	-0.001	0.45	0.005	0.017		26-01	0.055	0.008	••	-0.008	-1.0
	200	0.012	-0.002	0.015	0.009	0.01		160	0. QP 0	0.009		-0.008	-0 q
	200	0.008	-0.002	0.00	0.000	0.007	4	200r	C JEO	0.009		-0.007	-0.0
V	30W	0.005	-0.002	0.000	-	0.005	▼	300	()20	0.009		-0.007	-0.6

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Table#21(Continued)

		Por	nerd. Av	g Sneed -	1.91 mph	tical Pr	essure, b	al, at Indic	ated Cells	verse, Av	Eneed a	1.80 mesh		
Row	Position	Location	P ₆	P ₇	P ₈	Po	P ₁₀	Position	Location	P6	P7_	18	Pg	P10
13	178	24E 22E 20E 18E 16E	0.40 0.40 0.40 0.40	0.50 0.61 0.61 0.49 0.35	1.60 1.60 1.55 1.55 1.50	0.37 0.46 0.59 0.68 0.73	0.03 0.10 0.14 0.18	6"8	24E 22E 20E 18E 16E	0.30 0.20 0.20 0.20 0.20	0.47 0.55 0.64 0.60 0.53	0.10 0.15 0.15 0.20 0.25	0.25 0.30 0.40 0.52 6.56	0.03 0.05 0.07 0.10 0.21
		148 128 108 68 68	0.40 0.40 0.40 0.40	0.16	1.50 1.40 1.40 1.35 1.35	0.72 0.64 0.53 0.45	0.15 0.06 -0.05 -0.24 -0.27		14E 12E 10E 8E 6E	0.10 0.10 0.20 0.30	0.43 0.37 0.40 0.55 0.88	0.30 0.30 0.35 0.40	0.54 0.47 0.41 0.39 0.40	0.29 0.32 0.36 0.30 0.27
		A B C	0.40 0.40 0.40 0.40	0.92 1.65 2.68 3.89 5.21	1.50 1.70 1.95 2.30 2.65	0.54 0.74 1.09 1.60 2.08	-0.30 -0.27 -0.18 0.04 0.45		A B C	0.40 0.50 0.50 0.60 0.90	1.46 2.43 3.74 5.10 6.48	0.60 1.10 1.90 3.00 3.80	0.56 0.86 1.40 2.05 2.89	0.26 0.26 0.38 0.60 1.16
		E P G H	1.60	5.84 6.80 6.68 5.47 3.96	2.60 2.90 4.75 6.80 4.60	2.66 3.02 3.83 4.30 4.61	0.75 1.11 1.96 2.91 5.15	5"s	D E P G H	5.90 11.55 6.80 1.50 1.40	7.09 7.63 7.48 5.74 4.06	4.20 4.70 7.60 8.05 2.90	3.31 3.73 4.49 4.88 4.78	1.57 2.09 3.41 5.06 7.85
		I J E L	=	2.72 2.45 2.96 3.57 4.17	1.90 1.05 0.95 1.00 1.30	4.18 3.74 3.20 3.10 3.02	7.56 6.04 2.24 1.87 1.29		I J K L	1.70 1.60 1.50 1.40 1.40	3.12 3.19 3.95 4.54 5.20	0.75 0.70 1.30 1.95 2.50	3.64 3.22 3.20 3.30	9.76 6.05 2.80 1.95 1.00
		18 24 44 64 84	1.80	5.38 6.52 6.93 5.85 3.90	1.75 2.00 3.30 6.40 5.00	3.13 3.60 4.16 4.62 4.77	0.85 1.23 2.02 3.01 4.75		N LW 6W 8W	1.40 9.60 1.00 1.50	6.32 7.78 7.42 6.03 4.11	3.45 4.25 6.55 8.40 3.70	3.65 4.23 4.69 5.0k 4.82	1.39 2.02 3.10 4.50 6.98
		10W 12W 16W 16W 18W	=	2.24 1.25 0.65 0.33 0.16	1.95 0.75 0.25	4.27 3.48 2.52 1.67 1.02	7.73 6.80 3.26 1.36 0.50		10W 12W 16F 16F	1.90 1.50 1.50 1.65 1.60	2.51 1.49 0.84 0.49 0.32	0.90 0.50 0.50 0.50 0.50	4.14 3.20 2.30 1.50 0.98	9.79 6.70 3.40 1.71 0.87
		58A 54A 55A 50A	=	0.07	=	0.58 0.31 0.16 0.08	0.15		204 224 244 264 264	1.60 1.60 2.10 2.00 2.00	0.22 0.19 0.15 0.18 0.17	0.60 0.60 0.60 0.60	0.57 0.35 0.18 0.10 0.05	0.56 0.40 0.36 0.33 0.37

	Porverd	AVE Spec	ed = 1.91 m	ph	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	RC /erse	AVE Spee	d = 1.891	ph
Position	Location	D ₆	<u>b7</u> .	p ⁸ p ³	Position	Location	D ₆	D7	p8. p3
1"11	242	-0.048	0.002	-0.013	6"8	242	0.003	••	0.001
	221	-0.048	0.002	-0.012		22E	0.0	••	0.00
	508	-0.048	0.002	-0.a2		SOE	0.003		0.001
	186	-0.0k8	0.002	-0.012	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	18E	0.004	••	0.000
	16E	-0.049	0.002	-0.012		16E	0.004		0.002
	142	-0.049	0.002	-0.012	46	148	0.005	••	0.000
115	121	-0.049	0.002	-0.075	1000	122	0.008	••	0.003
	102	-0.048	0.002	-0.012		100	0.011		0.003
A COLUMN	82	-0.0kk	0.002	-0.012		8E	0.020		0.00
	6E	-0.037	0.001	-0.012		6E	0.036	••	0.004
74	NE .	-0.022	-0.003	-0.012		LE	0.065	0.003	0.00
		0.006	0.006	-0.013		200	0.113	0.005	0.005
	A	0.100	0.009	-0.012		A	0.186	0.010	0.007
		0.120	0.010	-0.012		3	0.141	0.018	0.01
	C	0.127	0.016	-0.008	- 1	C	0.162	0.028	0.019
	D	0.155	0.020	-0.005	1	D	0.183	0.031	0.025
100		0.179	0.003	-0.001			0.161	1.037	0.034
	7	0.115	0.029	0.013		7	0.059	0.032	0.058
1	G	0.064	0.030	0.039	5"8	0	0.032	0.028	0.091
		0.033	0.025	0.073	1	н -	0.028	0.017	0.115
	1	0.025	0.013	0.099		1	0.04	0.011	0.123
	J	0.038	0.008	0.116	-1	3	0.084	0.012	0.12
- 1		0.119	0.000	0.123		I	0.158	0.011	0.109
	L	0.176	0.012	0.115		L	0.149	0.013	0.090
	×	0.163	0.013	0.100		H	0.103	0.016	0.073
		0.155	0.018	0.063			0.122	0.023	0.06
	2W	0.202	0.024	0.042		24	0.134	0.023	0.041
	44	0.155	0.030	0.039		lett	0.030	0.027	0.052
	6W	0.094	0.034	0.055	49 (4.0)	6W	-0.009	0.024	0.078
	84	0.053	0.026	0.088		BN .	-0.034	0.015	0.104
	10V	0.029	0.04	0.112		10V	-0.049	0.005	0.111
- 1	12W		0.008	0.126		164	-0.054	0.004	0.118
		0.010	0.006	0.133			-0.056	0.003	0.098
	16W	0.006	0.004	0.112		16W	-0.057	0.001	0.063
	18V	0.005	0.002	0.076		18W	-0.057	-	0.009
10	20%	0.004	0.002	0.046	100	20V	-0.056	••	0.008
	22V	0.003	0.00%	0.026		22W	-0.056	•	-0.003
-	SPA	0.003	70	0.034	0.00	SPA	-0.056	••	-0.008
STORE STATE	26W	0.003	-	0.008		264	-0.056		-0.01
	20M	0.008		0.005 (Cont.)		28M	-0.055		-0.012

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		To.	nest, Av	pool -	Hollin	Pulled by	2007	el at folio	lin	PETER AV	g Speed -	nd m		
	Position	icestian	_6_	7			10	Position	Location	6	-1	8	_2_	10
15	i	308 908 908 908 908	0.08 0.08 0.06 0.06	0.45 0.55 0.79 0.99 1.37	1.46 1.44 1.46 1.46 1.38	0.89 0.35 0.42 0.48 0.63		Bose	325 302 202 262 242	=======================================	0.11 0.24 0.30 0.63 1.10	0.06 0.08 0.10 0.10 0.17	0.10 0.16 0.17 0.27 0.42	
		202 162 162 142 122	0.02	1.53 1.38 1.00 0.68 0.50	1.12 1.00 0.82 0.63 0.41	0.80 0.97 1.09 1.09			22E 20E 18E 16E 14E	0.05	1.57 1.67 1.29 0.76 0.38	0.15 0.17 0.56 0.48 0.60	0.61 0.83 1.00 1.03 0.91	
		108 62 62 42 23	0.00 0.00 0.00 0.29	0.36 0.37 0.52 0.88 1.38	0.34 0.34 0.36 0.40 0.54	0.85 0.72 0.64 0.66 0.78			122 102 62 62	0.04 0.04 0.05 0.05	0.13 0.04 0.06 0.28 0.52	0.84 0.94 0.94 0.96 1.06	0.69 0.48 0.31 0.33 0.35	
		A B C D	0.16 0.15 0.01	2.09 2.87 3.73 4.07 4.39	0.74 1.01 1.37 1.56 1.78	1.04 1.40 1.88 2.12 2.41			A B C D	0.16 0.19 0.25 0.20 0.19	0.93 1.47 2.19 3.00 3.29	1.20 1.40 1.68 1.96 2.12	0.48 0.70 1.07 1.57 1.79	
	1	7 6 8 1 J	0.06 0.10 0.07 0.08 0.09	1.49 3.82 2.93 2.12 1.96	2.26 2.24 1.52 0.74 0.41	2.92 3.18 3.42 3.22 2.88			E P O H I	0.14 0.08 0.10 0.15 0.15	3.50 3.64 3.14 2.42 1.78	2.26 2.79 2.60 1.96 1.34	2.04 2.55 2.88 2.88 2.71	
		K L H H	0.10	2.33 2.68 3.04 3.94	0.45 0.50 0.64 1.03 1.40	2.55 2.46 2.42 2.56 2.91			J K L H	0.16 0.22 0.26 0.29 0.30	1.72 2.11 2.43 2.74 3.56	1.08 1.14 1.20 1.40 1.72	2.44 2.20 2.15 2.17 2.37	
		64 64 84 104 124	0.10 0.08 0.05 0.03	4.73 4.10 2.92 1.75 0.98	1.94 2.34 1.72 0.86 0.39	3.30 3.63 3.66 3.30 2.73		Н	2W 4W 6W 8W 10W	0.27 0.24 0.22 0.25 0.24	4.00 4.11 3.59 2.76 1.76	2.02 2.46 2.60 2.00 1.32	2.69 3.06 3.30 3.32 2.96	
		16W 16W 18W 20W	0.02 0.02 0.02 0.02 0.02	0.51 0.25 0.12 0.07 0.03	0.12	1.99 1.32 0.84 0.49 0.26			12W 14W 16W 18W 20W	0.20 0.18 0.18 0.18 0.18	1.08 0.58 0.31 0.15 0.07	1.03 0.96 0.96 1.00 0.98	2.42 1.73 1.21 0.77 0.50	
	1	26W 26W 26W 30W 32W	0.02	0.01	=======================================	0.15 0.08 0.04 0.02 0.01			224 244 264 284 304 324	0.17 0.18 0.18 0.17 0.16	0.05 0.03 0.03 0.04 0.04	1.00 1.02 1.04 1.06 1.06	0.30 0.19 0.12 0.08 0.06	

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Tuble 121(Concluded)

	Vertical Deflection, in., at Indicated Gages Porward, Avg Speed - 1.05 mph Reverse, Avg Speed - 1.05 mph											
~	Position	Location	D ₆	Dy	D ₈	Do	Position	Location	D ₆	3	p8.	1,
5	0	30E	0.019	0.004		-0.012	lione	325	0.001	-0.001		
98	16101-600536	30E	0.019	0.004		-0.012	STATE OF THE PARTY OF THE PARTY.	308	0.002	-0.001		10.376 -176
		268	0.019	0.004		-0.012		268	0.002	-0.00		
		24E	0.019	0.004		-0.012		26€	0.003	-0.001		
		225	0.019	0.004		-0.012		248	0.004	-0.00		
		202	0.019	0.004		-0.012		221	0.004	••		
		18E	0.019	0.004		-0.012		18E	0.005	••		0.001
		168	0.018	0.004		-0.012	Mark Mark Season	182	0.006	-		0.001
		14E	0.018	0.004		-0.012		162	0.007			0,002
		124	0.018	0.003		-0.012		142	0.008	••		0.002
		100	0.019	0.002		-0.012		125	0.012			0.003
	Eddin Villa	8E	0.022	0.002		-0.012		100	0.018	••		0.003
		8E 6E	0.031	0.003		-0.012		8E	0.030	••		0.003
		45	0.068	0.005		-0.013		6E	0.050	0.001		0.003
		21	0.077	0.008		-0.013		4E	0.083	0.004		0.004
		٨	0.130	0.009		-0.013		21	0.132	0.010		0.006
		3	0.153	0.010		-0.011		A	0.181	0.019		0.006
		C	0.162	0.020		-0.008		3	0.164	0.029		0.0.8
	CONTRACTOR OF THE PARTY.	C	0.182	0.025		-0.005	ALC: NO DESCRIPTION OF THE PERSON OF THE PER	C	0.168	0.042		0.021
			0.186	0.029		-0.001		D	0.169	0.045		0.028
	ATTACK TO	7	0.138	0.038		0.015		E	0.151	6.046		0.038
	A CAR SECTION	0	0.088	0.040		0.024		7	0.084	0.044		0.067
		H	0.058	0.033		0.082		0	0.051	0.036		0.105
	49.	The state of	0.052	0.019		0.108	O 10 T	H	0.043	0.025		0.117
		O H I J	0.073	0.010		0.126		1	0.062	0.015		0.129
		K	0.125	0.009		0.132		J	0.104	0.014		0.131
		L	0.148	0.011		0.122		K	0.164	0.016		0.113
		H	0.157	0.014		0.106		L	0.167	0.019		0.095
	1	N	0.171	0.024		0.067	Curto News	H	0.152	0.004		0.076
		2N	0.187	0.034		0.045		N	0.150	0.033		0.048
		4W	0.150	0.044		0.042		2W	0.146	0.038		0.042
	TOTAL STREET	6W	0.096	0.046		0.061	Short Indiana	4W	0.071	0.036		0.056
	100	8W	0.055	0.039		0.095	A CONTRACTOR OF THE PARTY OF TH	6W	0.024	0.032		0.084
		10W	0.029	0.022		0.121		8w	-0.002	0.021		0.112
		12W	0.016	0.012		0.136	Thomas district	10W	-0.019	0.007		0.120
		14W	0.009	0.008		0.142	A THE COLD	12W	-0.026	0.004		0.117
		16W	0.005	0.005		0.120	ALC: N. P. S. British	144	-0.028	0.003		0.101
		18W	0.004	0.003		0.080	1.00	16W	-0.029	0.002		0.064
	The Control of the Control	20W	0.003	0.002		0.048		18W	-0.029	0.001		0.026
		22W	0.002	0.001		0.027		20V	-0.028	••		0.003
		24W	0.002	0.001		0.015		22W	-0.027			-0.010
		26W	0.002	0.001		0.009		SIM	-0.027	••		-0.016
	Service Co.	284	0.001	0.001		0.006		26W	-0.026			-0.018
		30W	0.001	0.001		0.004		26W	-0.026			-0.019
		32W	0.001	0.001		0.003		30W	-0.026			-0.019
		THE WAY	59.7172					32W	-0.026			-0.019

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The three columns give the static row number, the assembly load point on that row, and the location of the static load for the indicated cell or gage reading. Figure Al shows the locations of the loading points for each wheel assembly; figures A2 and A3 show the locations of the static loads for items 3 and 4, respectively.

For example, the heading of table A-14 indicates that this table contains static load test data for the 12-wheel assembly at 30,000 lb per wheel on item 3; therefore, figures Al and A2 are to be used in conjunction with the table. Look down the right side under column heading row until rows 1 and 3, load points 1 and 2, and location G are located. This identification means that with the 12-wheel assembly over location G, assembly load point 1 is on static row 1 and assembly load point 2 is on static row 3. Figure A2 shows that soil pressure cell Pl (4.5-ft depth) is located on static row 1 at location G. Thus the values of total and rebound pressure for cell Pl represent the maximum static load pressure values at a depth of 4.5 ft for assembly load point 1 under a load of 30,000 lb per wheel or a total load of 360,000 lb. The other pressure cell values across the table on this line represent pressure measurements offset from assembly load point 1. Figure A2 shows no pressure cell at the location of assembly load point 2 on static row 3; therefore, all of the values across the table on this line represent offset pressure values for load point 2. These offset pressure values are the same for both assembly load points 1 and 2; however, the offset distances for the pressure values differ for the two load points. The above discussion also applies to the static load deflections at the bottom of the table. At location G, figure A2 shows that no deflection gages exist at assembly load points 1 and 2 on static rows 1 and 3, respectively; therefore, all deflection values across the table on this line represent offset deflection values for the load points. These offset deflections, as for the pressures, are the same values for both assembly load points, but the offset distances from the load points are different. All offset distances from the assembly load points can be calculated or else measured directly from figure Al and figure A2 or A3.

The dynamic loading test data are given in tables A-16 through A-21. These tables are slightly different from the static test data tables. No total or rebound values could be given for the dynamic load data, and only one response value was obtained; this value and how it was determined will be discussed

later. Each table gives data for only one item; vertical pressures and vertical deflections, respectively, are given in the top and bottom half of the table. A table for a specific item under specific load conditions will not always include both pressures and deflections for a dynamic row. For the outside instrumented pressure and deflection rows (dynamic rows 5 and 15) and depending on the wheel assembly, for dynamic rows 7 and 13, both measurements of pressure and deflection on these rows were not always determined from the oscillograph recordings. In reducing the oscillograph records, the main information extracted, due to time limitations, was the maximum instrumentation responses, which is why only the main instrumented rows were analyzed. These tables give the induced instrumentation responses for both forward and reverse runs and the average speed in miles per hour for each.

Additional information to be used in conjunction with figures Al and Al and the appropriate figure A2 or A3 is listed to the left of each block of data for forward and reverse runs. This additional information consists of the dynamic row number on the left side of the figure for both runs (the dynamic row numbers are identified in figure Al). Only one row number is given, which is different from the tables for static tests because as explained in the main report, assembly load point 1 was always the guiding point. For both forward and reverse runs, position and location columns are given. The position column gives the position north or south that load point 1 was offset from the row at each location. As an example, an indication of 1"N means load point 1 was 1 in. off on the north side of the row; therefore, the assembly load point was 1 in. north from the center of a cell or gage if the location was within the instrumentation grid (A through N). An indication, under position, of 0 indicates assembly load point 1 was centered on the row.

The location column is the same as the locations for the static load tests; except for the dynamic load tests, data were extracted from the recordings for several feet along the row being run before and after the load cart traversed the instrumentation grid (A through N) in each item. For example, a designation of lOE in the location column would identify data recorded 10 ft east of the first grid system location (A) on the row indicated in the first column of the table; lOW would identify a similar location 10 ft west of the last grid location (N).

The positions listed in the tables apply specifically to load point 1,

but for load point 2 of all the assemblies, these positions are also true, as discussed under major testing program. As an example, if the table lists at a location a position of 2"S for dynamic row 7, then assembly load point 1 is 2 in. south of the center of row 7, and assembly load point 2 is 2 in. south of the center of dynamic row 5. For the locations, the location applies specifically to assembly load point 1; and for all assemblies except the singlewheel and the twin-tandem assemblies, these locations also apply to load point 2. There was no second load point for single-wheel tests. Load point 2 of the twin-tandem assembly is offset 29 in. behind load point 1. For this reason, when using the dynamic test data tables of the twin-tandem tests, this offset (29 in. behind) must be considered. As an example, for the twin-tandem assembly, if for dynamic row 7 the location is listed as F, then the maximum response for load point 2 would be at location E on a forward run; however, it would be at location G on a reverse run. As an example for the other assemblies, if the location of dynamic row 7 was F, this would be the location for load point 1 on row 7 and the location of load point 2 on either dynamic row 5 or 9 (refer to figures Al and A4).

Use of the dynamic load data tables is the same as that previously described for the static load tables. The dynamic load data presented in this appendix are the best of two or more runs on a row if more than one run under an assembly was necessary, as discussed in the main report.

For both static and dynamic load tables presented, minus values will be noticed throughout the tabulated data responses. These minus values indicate that the instrument responses under both static and dynamic load tests were above the reference (which was discussed in the main report) used for the particular gage or cell, but negative values do not mean that the gage or cell actually responded in a negative direction. Positive values always indicate increases in vertical pressure or downward vertical deflection. As will be noticed in the tabulated data, the minus values occur at large offset distances from a gage or cell; therefore, they may be assumed to represent a shift in the zero reference for the gage or cell. This is not an electrical zero shift in the gage or cell but is actually a shift in the soil behavior. The reference for each gage and cell was discussed in detail in the main report. If the data presented are to be used to develop stress or deflection basins at various depths under loads, all of the data, including minus values,

should be plotted to the fullest offsets given and then the zero reference should be shifted to the top of the curves. This procedure would eliminate the minus values and give a truer basin curve representing the basin generated beneath a loaded assembly.

In addition to tests conducted with the loaded assemblies, both static and dynamic load tests were conducted with the empty assembly movers. These data are not presented in this appendix, but an analysis is presented in the main text of this volume. The 12-wheel prime mover, even though it had a large deadweight, did not have an effect on the gages or cells for the static load tests because of the wide wheel spacing. Neither did it have an effect on the dynamic tests; however, it did affect the dynamic load data recorded for the outside dynamic rows (see figure A4). The twin-tandem prime mover affected both the static and dynamic load data because the spacing of the outrigger wheels was much closer than that on the 12-wheel mover. Table A-22 gives the effects and, consequently, the corrections to be applied to the

Table A-22

Corrections Due To Prime Mover To Be Applied to

All Twin-Tandem Maximum Deflections for

MWHGL Flexible Pavement Tests

Item No.	Depth _ft	Correction Point 1, in.	Correction Point 2, in.
3	0.00	0.002	0.003
	0.75	0.002	0.003
	2.75	0.002	0.002
	4.50	0.001	0.002
	7.50	0.001	0.001
	12.00	0.000	0.000
4	0.00	0.006	0.007
	0.75	0.006	0.007
	2.75	0.005	0.006
	4.50	0.004	0.004
	7.50	0.001	0.002
	12.00	0.001	0.001

static test data of all twin-tandem loads. No effects on the soil pressure cells were discernible (this was discussed in the main report). This table lists only the deflection corrections for each depth immediately under each load point and not offset corrections (only zero offset for each point). Corrections of the dead-load effect of the twin-tandem mover for dynamic load tests were not tabulated or presented. The single-wheel mover was very light and had no effects on either static or dynamic load data. The above corrections must be applied when utilizing any static load test data, since the data presented were not corrected for these effects.

Another very important correction that must be applied to all of the static load deflection data is the 12-ft-depth reference plane induced movements under load. Figure A5 gives these corrections for each load and assembly for both the maximum values and offset values. The development of these 12-ft-depth movement curves was fully discussed in the main report. These corrections must be added to every deflection gage movement at all depths under static loading conditions. The static load data presented in the data tables were not corrected for this movement.

3. DEFLECTIONS

a. Static Load Tests

The initial reduction of the static load deflection data is presented in the data tables. Induced movements for each load and assembly were calculated by taking the difference between the load and no-load readings before and after the load tests. This yielded the total and rebound values. The total deflection values are the differences between load and initial no-load readings; therefore, they represent the total movement that occurred under load. This total movement consists of two parts: one part is permanent deformation, which is not recoverable, and the other part is elastic deflection or the recoverable part. The rebound values are the differences between the load and the final no-load readings; therefore, these values are a representation of all or a portion of elastic or recoverable deflection. Permanent deformation is represented by the difference between the total and the rebound values. The rebound value and its difference from the total value represent the elastic and permanent deflections, respectively, if and only if no residual deflections or strains occurred under the loadings. The analysis and establishment of a zero reference for each gage were discussed in the main

text. The data as determined from this analysis were used and not the data from the initial reduction presented in the tables. However, the rebound values in the tables are close to the values determined from the analysis.

b. Dynamic Load Tests

Only one value is given in the data tables for the responses of each gage on the forward and reverse runs of the dynamic load tests. This value corresponds closely to the maximum elastic values determined for the static load tests, using the procedures discussed in the main report. Basically, the reduction of the dynamic load response data was the same and had the same associated problems as the static load data.

The first step in the reduction of data was to establish the zero or no-load reference from which each deflection gage was responding. behavior of the soil during dynamic loading was discussed in the main report. Based on the behavior exhibited during the dynamic and static load tests and to be consistent with the analysis of the static load data, a reference was chosen that would be comparable to the static load test data reference. The delayed rebound reference level was chosen for the static load tests, and, consequently, the reference level was chosen for the dynamic load tests after the gages had been passed over in a dynamic run. This reference level represents the immediate elastic rebound value; however, the delayed rebound did not appear to be as large, if it existed at all, as that for the static tests.

On an oscillograph record for a gage, a trace was made by the gage which represented the no-load condition. As the gage was approached by a moving loaded assembly, this line began to register deflection and reached a maximum deflection as the load passed over the gage location. The line rose as the loaded assembly moved away from the gage and came back to a position that was usually below the starting no-load condition. This trace then represented the unloaded condition.

In order to determine the offset values parallel to the direction of travel and the maximum response, the instrumentation grid pattern was first drawn onto the oscillograph record using the photocell blips as discussed in Volume III-A. Next, a horizontal reference was drawn tangent to the unloaded trace at a distance back from the grid pattern where the line stopped rising. The scale of each deflection gage was determined from calibration steps put

on the records, as discussed in Volume III-A under major testing program. The scale at which the particular deflection gage was operated was set on a variable-scale ruler and the responses of the gage at each offset, including zero offset, from the reference line were read directly in inches of deflection. This procedure was followed for each deflection gage, and the responses measured represent elastic deflection very close to the maximum elastic deflection as determined for the static test data. These are the values presented in the data tables. An example of an oscillograph record with the superimposed grid pattern and reference line is shown in figure 28 of Volume III-A.

4. STRESSES

a. Static Load Tests

The initial reduction of vertical stress measurements is presented in the data tables. Induced stresses for each load and assembly were calculated by taking the difference between the load and the no-load readings before and after the load tests. This resulted in total and rebound values. The total values are the differences between load and initial no-load readings. Rebound values are the differences between the load and the final no-load readings; therefore, these values represent a portion or all of the elastic recoverable stress. The difference between the values of total stress and rebound represents the residual stress locked in the soil. The tabulated initial reduction of stress data was not the data used in the main report results. The data used came from the analysis and establishment of zero references for each pressure cell as discussed in the main report.

b. Dynamic Load Tests

Only one value is given in the data tables for the response of each pressure cell on the forward and reverse runs of the dynamic load tests. These values correspond closely to the maximum elastic stresses determined for the static load tests from the analysis in the main text. The analysis of the dynamic load tests was basically the same as the analysis of the static load tests with respect to initial no-load reference and corrections.

To be consistent with the analyses of the static load stress data and the dynamic load deflection measurements, the reference datum for each pressure cell was taken as a horizontal line tangent to the cell's unloaded trace at the point where the cell trace stopped rising after a load passed over it. This was the same procedure followed for determining the dynamic load deflection responses. The horizontal reference for each cell was drawn along with the deflection reference after the instrumentation grid was superimposed on the record of a run. This cell reference represented the elastic stress reference datum for the cell.

Once the reference for a cell was established, the scale of the pressure cell was set on a variable-scale ruler. The pressure cell scale was determined from the calibration steps on the record, as previously discussed in the main text. The cell responses were read from the reference line directly in psi of pressure at each offset as determined by the grid. These measured values of vertical elastic stress are very close to those determined for the static load tests and are the values presented in the dynamic load tables.

SECTION II

EVALUATION OF MEASURING INSTRUMENTS

Due to the great volume of static and dynamic load data used for the MAGL analysis and the data to be used for future analysis, with respect to actual soil behavior, some of the factors affecting accuracy of the test results will be discussed in this appendix of the report on instrumentation. Accuracy, as used in this report, applies to the ability of the soil instrumentation to properly reflect the existing conditions in and behavior of the soil within which the measuring instrument is buried (or conditions and behavior which would exist with the device absent). Also, an attempt will be made to convey an idea of the consistency and reproducibility of the instrument readings. No special tests were performed to evaluate the instrumentation responses; therefore, the evaluation will be made utilizing actual data taken during load tests as well as previous work done for this purpose with some of the instruments. Lastly, in this part of the appendix the loss of instrumentation and the probable causes will be presented.

1. ACCURACY

Accuracy is the degree to which the results from instruments as installed compare to what the results would have been if the instruments had not been in the soil. Therefore, accuracy is a measure of the disturbance of the conditions and behavior caused by the presence of an instrument in the system. Accuracy, as stated above, is difficult to evaluate because the only known value is of the system responding with the instrument present; how the system would behave without the instrument is unknown. If the actual behavior or response were a known fact, then there would be no need to instrument the system to measure the responses. Thus, the fact is evident that accuracy cannot be evaluated; only an indication of accuracy can be evaluated based on theoretical and other concepts.

a. Soil Pressure Cells

A pressure cell constructed of metal or some similar rigid material, and necessarily constructed to obey Hooke's law in its compressibility, can be expected to alter the stress distribution in soil, resulting in a concentration of stress in the vicinity of the cell in the same manner that a large stone will concentrate stresses in a sand or plastic soil mass. Theoretically, a very thin, compressible (but not flexible) plate will distort the stress pattern in the soil very slightly. This suggests a cylindrical cell that is thin in proportion to its diameter. The probable existence of anomalous local stress variations, due to lack of complete homogeneity in the soil, indicates the need for a large pressure response area in a pressure cell. The concentration of stress by a pressure cell would be expected to depend greatly on its compressibility; therefore, if its compressibility were less than that of the soil, indicated pressures would probably be higher than true pressures. In reverse, if the cell compressibility were higher than that of the soil, arching action (at least in granular soils) might be expected to withhold an appreciable portion of the normal stress from the cell; as a result, indicated pressures would probably be lower than true pressures.

A few factors affecting the accuracy of all soil pressure cells under field conditions are error parameters of effects, such as eccentric loading, unmatching compressibility, and the technique of cell installation. The modulus of the soil in which the cell is embedded may be either larger or smaller than the modulus of the cell, therefore causing a distortion of the stress pattern in the immediate vicinity of the pressure cell and possibly causing a source of error. Another limitation of soil pressure cells is the stability with time, which is determined by cell design and craftsmanship. Such possible changes are resistance changes in the gage wires, imperfect temperature compensation, and variations of the elastic constants of the cell material. A discussion of error factors can be found in reference 5.

As reported in reference 5, laboratory tests performed under controlled conditions have repeatedly demonstrated the ability of the WES pressure cell to yield results of an overall accuracy of ±0.5 percent of full-load pressure. The SR-4 strain gage itself has an accuracy of approximately 0.1 percent, and the balance of the inaccuracy is accounted for by gage bonding, imperfect diaphragm performance, mechanics of the flexural ring, and fluid transfer cavity behavior. This degree of accuracy is reduced when the cell is installed under actual field conditions and when the factors discussed previously are in action on the cell.

In a study of stress distribution using WES pressure cells in a mas; of homogeneous sand (reference 6), the data were rigorously examined for

determinations of cell performance. This study analyzed the variability of individual readings, which will be discussed later, and made comparisons of actual soil conditions with theoretical soil conditions by the consideration of stresses on mutually perpendicular planes and free-body force summations. The general conclusion in this study based upon the variability of readings and the theoretical comparisons was that the WES pressure cells were accurate to within 10 percent or better.

For the accuracy of the commercial SA-E soil pressure cell, only the manufacturer's specifications could be used. No laboratory tests other than calibration tests and no prior field experience with the cells were available for determining the accuracy. Manufacturer's specifications were as follows:

Linearity at full scale (measured in air) 0.5%

Hysteresis at full scale (measured in air) 0.5%

Temperature effect on sensitivity, per deg 0.8%

For a measure of stability, the manufacturer reported that no drift was noted after six weeks of testing in moist soil. The accuracy of the SA-E cells would appear to be about 0.5 percent, but as will be discussed later, this degree of accuracy was greatly reduced (more than in the WES cells) when the cells were installed in the field with all of the previously discussed factors acting on the fells.

b. Pore Pressure Cells

The Wind pore pressure cell is distinguished from the earth pressure cells principally by the fact that the liquid pressures act directly on the measuring diaphragm. Critical diameter-thickness considerations governing the design of earth pressure cells are not important for pore pressure cells. Thickness of the cell is based on space requirements of the transducer assembly, and the diameter is governed by conditions of use.

The cells are embedded in a pocket of sand, particularly in clayey soils, which is placed in the drill hole just prior to installation of the cell. Particular care with preparatory measures and installation procedures is necessary to avoid trapping air between the porous stone and the diaphragm of the cell. Entrapped air would cause erroneous indications with loss of low-pressure response.

Pore pressure readings accurate within 0.5 percent are readily obtainable by observing the precautions and practices applicable to installation and use of all pressure cells. The preciseness of calibration, both for load and temperature sensitivity, and steps taken to correct observed readings for temperature variations are limiting factors in the overall accuracy attained.

c. <u>Deflection Gages</u>

Most of the discussion of theory and error parameters that were previously discussed in regard to the soil pressure cells is also applicable to the WES deflection gages and their effect on soil behavior by being present. A major consideration is whether the gage movements are actually representative of the soil body at the point of measurement. The gage movements are considered to be representative of the soil mass if careful installation methods are used. Linear variable differential transformers (LVDT) were mounted within WES deflection gage housings. This particular type of deflection gage has not been used before; therefore, laboratory tests of soil-body movements with the gage installed and prior field performance were not available to determine an indication of accuracy. An indication of accuracy must be based on the LVDT specifications and laboratory calibration tests. Also, the field performance and factors in the field affecting the gage must be considered. The field performance will be discussed under consistency and reproducibility.

Due to the material of the gage housing and reference plate being of different modulus than the soil, stress concentrations and/or arching action probably occur in the vicinity of the gage. This concentration of stress around the gage should not have an appreciable effect on the load-induced soil-body movements, and the gage should register a fairly accurate indication of the body movements. Distortions in the soil body caused by the gage should be limited to a small area around the gage and should not affect movement a few feet or more below the gage, which is the movement that the gage is actually measuring (between the gage plate and the reference flange at a deep depth). As mentioned in the main text, lateral earth pressures acting on the gage housing with eccentric loads on the plate from small offsets are believed to affect the gage response, causing the measurement to be larger than the actual movement; therefore, loading position in the field was important. When the load was actually centered over the gage, the true response was believed

to be measured. This effect was noted mainly on the shallow-depth gages and decreased with depth of the gages. Thus from the above discussion, two factors in the field affecting the shallow-depth deflection gages appear to be lateral earth pressure coupled with large eccentric loads, both resulting from loads close to the gage position but not centered over the gage position. Loadings at 1-ft offsets or greater did not produce this effect. Other factors that could cause errors in the field are improper installation of the gage and assembly and changes of stability with time. Resistance changes in the gage wire with time, temperature effects, or variation of the clastic contents of the gage and assembly materials with time could result in error parameters.

Laboratory tests and calibrations of the LVDT element used in the deflection gage have yielded a resolution of 0.0002 in. with a digital voltmeter as the displacement monitor, a repeatability of ±0.001 in., and an accuracy of ±0.002 in. or better, considering the possible error parameters that could exist in the laboratory calibration tests including the associated equipment.

The optically monitored reference rod movements must also be considered under deflection gages. Accuracy of the optical system, utilizing a vernier-scaled height-measuring instrument and a self-leveling surveying level, theoretically is the accuracy of the vernier scale, which gave readings directly to 0.001 in. and estimated to 0.0001 in. This accuracy would occur only under perfect conditions, such as never moving the level once it was established and never moving the height instrument, only moving the vernier scale.

These perfect conditions did not exist in the field. The main factor greatly affecting the accuracy of the optical measuring system in the field was the inability to leave the surveying level and the height instrument in place. The effect of this error factor will be discussed under consistency and reproducibility.

d. Strain Gages

Microdot, Inc., embedment-type strain gages were used. Time limitations aid not permit laboratory testing and calibration of these gages; therefore, the manufacturer's specifications must be used as an indication of their accuracy. These specifications are as follows:

Filament resistance 120 + 3.5 ohms

Tolerance of reported value +3%

Range of microstrain (linear within 1%)

+6000

Temperature range

0-500 F

Maximum elongation without failure

2%

Accuracy would be about 1 to 2 percent.

Factors greatly affecting accuracy of these strain gages in the field are fragility, which will be discussed later, bending of the gages to the material being tested, degree of disturbance in the material behavior caused by the presence of the gage, matching of the gage modulus to the modulus of the material being tested, and temperature effects. To accurately indicate the strain in a material, the gage must be firmly bonded to or in the material, should have the same modulus as the test material, should be stable with temperature changes, should not disturb the natural behavior of the material, and should be fairly rugged. These factors apply specifically to mechanically operated strain gages.

e. Associated Equipment

Performance parameters or sources of error associated with the recording devices or other indicating means for the gages and cells should also be considered in their effect on accuracy. These associated equipment effects influence both the degree of accuracy and the consistency and reproducibility of instrument indications.

Small errors exist in the direct reading equipment (SR-4 strain indicators) and digital voltmeters from variations in the equipment and also from human ability in precisely reading the indicators. In the recording equipment, small errors enter from variation in the recorders and the associated signal amplifiers, which have the function of increasing the magnitude of the signal from an instrument circuit without distorting or warping the signal. For static measurements or very slowly changing indications, a direct meter reading indicator is usually used; but for fast-changing responses, meters are unsuitable due to their slow response. Therefore, some type of recording system with suitable response characteristics is necessary.

The primary performance parameters to be considered in all types of indicator and recording equipment are frequently response, relative phase shift of input components of different frequency, sensitivity, and stability. Such factors as variable sensitivity, shifting reference levels, temperature drift, and sensitivity to vibration or noise (disturbances which are carried along with the desired information) may cause problems. The degree of sensitivity, especially with respect to vibration or noise, decrease with increase of amplification required for the instrument response signal; therefore, the accuracy and consistency decrease with increase of amplification and consequently noise level.

2. CONSISTENCY

Consistency is difficult to separate from accuracy. Several factors that affect the accuracy of an instrument are also factors that determine the consistency of measurements from the instrument. No specific tests were conducted in order to determine the consistency of the instrumentation registrations; therefore, the indications of consistency to be discussed are taken from the actual test data. The results to be presented in the following paragraphs are the combinations of all the factors determining accuracy and governing field performance that add together to dictate the consistency of the behavior of the instruments under actual field use. Also (but probably not the least of these factors) added to the above are the error sources of the complete system of power supply, gage, amplifier, and indicator or recorder.

a. Soil Pressure Cells

In previous work with WES soil pressure cells (reference 6), which included a rigorous analysis of the data for cell performance, one of the findings showed that variability of individual readings expressed as a percentage of measured reading was as follows: 1.5 percent for 50 percent of all data and 5.6 percent for 99 percent of all data. An analysis of readings taken on different cells under identical loading conditions showed that the variability of the readings was as follows: 3.1 percent for 50 percent of all data and 11.9 percent for 99 percent of all data. Further analysis with theoretical comparisons led to the general conclusions that pressure cells used in that study were accurate to within 10 percent and that residual stress

measurements made regularly throughout a 9-month life of the test section were accurate to within 0.5 psi.

The results of the above previous rigorous analysis of the WES soil pressure cells corresponded to the cell behavior observed during the MWHGL tests. For all of the static loads, a study of cell indications at each depth from two and usually more loadings with each load point of each test configuration and load showed that the consistency of readings from the cells was within approximately 10 percent or less. This means that in the ranges of measured pressures, the variation of readings for identical test conditions was approximately +1 psi or less. Figure A6, which shows data for the 6-wheel 30,000-lb-per-wheel load tests in item 3, is a typical example of the behavior of the WES cells for all of the 30,000-lb-per-wheel load tests for both items 3 and 4. As can be seen, the average of the two groups of readings at each instrumented depth would be within +1 psi of either group. Figure A7 is typical of the single-wheel response; this curve is for the 30,000-lb single-wheel tests of item 3 and is typical of both items, where the duplicate determinations were within 0.5 psi of each other. Both figures A6 and A7 give responses of duplicate cells in addition to two or more readings from one cell for the 6-wheel tests; therefore, the ranges of the individual cell responses given above also apply to readings from duplicate cells, which means that the responses of the duplicate cells at each depth were within 1 psi or less. The cell histories in figures 63 and 64 in the main text of this volume show that the stability of the majority of the WES cells, over a long period of time (1-1/2 years), for the periods without testing was approximately +0.5 psi; about half of this variation is the accuracy possible in reading the SR-4 strain indicator.

As can be observed in figures A6 and Å7, the consistency of the cells decreased with the number of wheels of the load assembly; in other words, the consistency of the single-wheel determinations was better than the 6-wheel data. However, the 6-wheel determinations were representative of the 12-wheel tests. Another conclusion, not illustrated, from the static load tests was that the consistency decreased with magnitude of load; the consistency of the 15,000-lb-per-wheel load tests was better than that of the 30,000-lb-per-wheel load tests.

For the SA-E soil pressure cells, the histories in figures 63 and 64

of the main text of this volume show that the output signals of the SA-E cells were very erratic, even at the time of installation. This indicated that the cells output responses could not be expected to be very stable or dependable. The data from these cells under load tests were also erratic. Based on the SA-E cell output signal histories and their behavior under load, the decision was made that the data from these cells should not be used.

The degree of consistency for the dynamic load tests was the same as that given for the static tests. For the dynamic load tests, there were more cell readings to compare because there were results from both forward and reverse runs. These test results showed the cells behaved in the same manner as during the static load tests; that is, the consistency decreased with increase of load and number of wheels. Signal responses of the SA-E cells could not even be recorded for the dynamic load tests because the instability and noise level exceeded the actual pressure indication from the cells.

Position effects of load points during the dynamic loading tests did not appear to have an appreciable effect on the soil pressure cells and were not considered to be a source of inconsistency. If any effects were present, they were within the 10 percent range established for the static load tests. Another source of error that appeared to be negligible, but was thought to have been a source of some error, was the degree of accuracy to which the records for the dynamic load tests of the pressure cells could be read or measured. This also seemed to be within the 10 percent range of consistency previously discussed.

b. Pore Pressure Cells

The pore pressure cells are believed to have the accuracy stated previously of ± 0.5 percent. Careful installation of the cells was observed, and field conditions did not readily affect the cells.

c. Deflection Cages

The analysis of the consistency of readings from the WES soil deflection gages must be based wholly on the results of the MVHGL tests since no record of previous work with the gages exists and no tests were conducted for this purpose. As mentioned previously, these results portray the integrated effects of all factors that could affect the gages both in the gage system and under field conditions. For the deflection gage behavior, a distinction

must be made between items 3 and 4, whereas, the soil pressure cell results applied to both items. This distinction is made because the outside row of deflection gages in item 4 behaved differently from the inside row of deflection gages. In each item the inside and outside deflection gage lows were connected to separate power supplies. Due to each gage in item 4 on either the outside row or the inside row showing the same inconsistency, the conclusion must be drawn that something was wrong in that gage circuit or electrical arrangement. The cause of the trouble could not be determined. In addition, which gage row was in error could not be determined. This discrepancy was not noticed until the analysis of the data because the inconsistency did not manifest itself under the load tests of the single-wheel assembly, which was used to perform the preliminary tests. The discrepancy manifested itself and increased with increase in load and number of wheels. The discrepancy was a constant difference in readings between the gage rows at all gage depths.

A typical example of the deflection gage behavior as to consistency is shown in figure A8 for the single-wheel 30,000-lb load static tests in item 3. These curves are typical of the behavior under all test loads and wheel assemblies of both items; even item 4 showed the same relation, but data from the inside row differed by a constant amount from data from the outside row.

For item 3 the curves in figure A8 show that for the single-wheel 30,000-1b load, the consistency of readings from duplicate gages at each depth was within ±0.001 in. of deflection. The consistency of readings for the 12-wheel 30,000-1b-per-wheel load tests was ±0.001 in. for the same gage and ±0.002 in. for duplicate gages. In item 3 consistency decreased slightly with increase of load and number of wheels, resulting in an overall degree of consistency of ±0.001 in. or less for the same gage and ±0.002 in. or less for duplicate gages. These values are within the range of values given previously for the accuracy of the deflection gages.

For item 4 the single-wheel 30,000-lb load tests showed no difference between the gage rows and yielded consistency of +0.001 in. for duplicate gages. The 12-wheel 30,000-lb-per-wheel load tests showed a consistency of +0.002 in. for each gage on both rows, but these static tests showed a difference of 0.025 in. of deflection between readings from the outside row and those from the inside row. This difference was a constant amount for all

duplicate gages at every depth; in other words, the inside row of gages yielded a curve that was shifted to the right and values at every depth were larger by 0.025 in. of deflection than the values from the outsid gage row. In item 4 the consistency decreased with the increase of load and number of wheels, and the discrepancy between the gage rows increased with load and number of wheels. Due to the fact that items 3 and 4 have different stress and strain distributions in the soil because of the weak 2-CBR layer in item 4, it was impossible to determine which gage row in item 4 responded correctly.

For the dynamic load tests, the discrepancy again manifested itself in item 4 results of deflection by the same amount for the static load tests of the 6- and 12-wheel assemblies but was less than the static load test for the twin-tandem assembly. Due to both forward and reverse dynamic load runs being made, more data were collected for comparisons. These data showed that the degree of consistency decreased slightly under the dynamic load testing. This slight reduction is believed to be due to position effects, which were more critical for the deflection gages than for the soil pressure cells, and to the degree of closeness to which the movements could be measured on the oscillograph recordings.

In item 3 the degree of consistency varied from ±0.001 in. for the same gage and duplicate gages under the single-wheel 30,000-1b tests to ±0.002 in. for the same and duplicate gages under the 12-wheel 30,000-1b-per-wheel tests. As for the static load tests, this degree decreased slightly with increase of load and number of wheels.

For item 4 the degree of consistency was ±0.002 in. for the same and duplicate gages under both the single-wheel and 12-wheel 30,000-lb-per-wheel tests, with the exception of the 0.025-in. deflection difference under the 12-wheel tests. The consistency decreased with the increase of load but not with the number of wheels.

At times the data from the reverse runs were slightly different from that of the forward runs of the dynamic load tests. This was not true for the soil pressure cell results and is believed to be due to the effect of load position being more critical for the deflection gages. The slight difference varied from zero to ± 0.005 in., depending on the position of the load points. This effect of position decreased with decrease of load and increase

of depth. With respect to position effects, the best run, whether forward or reverse, was the one used to obtain the data under a given loaded assembly, and the degrees of consistency discussed perviously apply to the results of the best run.

The long-time stability of the majority of the deflection gages can be seen in figures 67 and 68 in the main text of this volume. These are no-load or zero readings taken for 1-1/2 years. The stability of most gages was good before and after the testing periods; these periods were discussed under analysis of data in the main text.

d. Reference Rods

The degree of consistency of reference rod measurements of movements of the 12-ft-depth reference plane was low. This analysis had to be based wholly on the data from the MWHGL tests because no special tests for this purpose were conducted. Offset versus deflection curves were drawn for each load and assembly to be used as corrections for the deflection gages, as previously discussed. The development of and basis for these curves were discussed under analysis of data in the main text because the data from the reference rods did not dictate these curves even though the data fell around the curves.

For the single-wheel 30,000-lb load, the variability of the data from the curve used at the maximum deflections was 56 percent. The 6-wheel 30,000-lb-per-wheel load tests gave the best data; they had a variability from the curve used at the maximum deflections of 33 percent. For the 12-wheel 30,000-lb-per-wheel load tests, the variability at the maximum deflections was 53 percent. The twin-tandem 30,000-lb-per-wheel load tests yielded a variability at the maximum deflections of 37 percent. The above variations from the correction curves used represent the maximum variation of the data from the curves and are a measurement of the consistency of the reference rod movements.

Theoretically, the optically measured movements should have been as good as the accuracy of the vernier scale on the height-measuring rod, which was to the nearest 0.001 in. This accuracy and the degree of consistency were reduced greatly by the method that had to be used in making the measurements. The surveying level had to be turned from one item to the other upon the movement of the load cart from one item to the other for the static tests; however,

this would cause only a slight error, if any, because the surveying level and line-of-sight stayed fixed for the load tests in an item. Large errors and large inconsistencies in the measured data resulted from the fact that the height-measuring rod had to be moved each time a wheel or a low-hanging part of the load cart passed over or near the reference rod location. As an example, if a wheel of one of the assemblies was moving along static row 1, when the wheel came to the reference rod position, the height-measuring rod would be pulled and the wheel allowed to pass; then the rod would be put back. This procedure resulted in the large errors inherent in the optically measured reference rod movements. As can be deduced from the above procedure, these errors were mainly present at the maximum deflection points, which were the most important. Offset data did not have such large variability, and the offsets fell relatively close to the curves used. The curves used are belisved to be within +0.005 in. of the actual deflections under load of the reference plane at the 12-ft depth. Figure A9 shows a reference rod measurement position.

e. Strain Gages

consistency of the strain gages in the asphaltic concrete was not evaluated due to the high rate of gage loss (which will be discussed in the next section) and the instability of the working gages. As previously mentioned, due to the lack of time, no laboratory tests were conducted with the strain gages and no evaluation of the gages could be made from the field test data because of the high instability of the gages in working only part of the time. The gages that were not lost seemed to have reached their limits after the first static tests and, consequently, would break connection at times, then would register at other times.

3. LOSS OF INSTRUMENTATION

The loss of instrumentation during the static and dynamic load tests was negligible except for the pavement strain gages. During the instrumentation tests, the instruments that were lost completely or that has doubtful responses were as follows:

a. One WES soil pressure cell (Pl, 0.75-ft depth) in item 4 gave unreliable results throughout the testing period.

- b. The output signals of all three SA-E soil pressure cells were considered unreliable even though they registered response of a sort throughout the testing period; these cells were P8 (2.75-ft depth) in item 4, P8 (2.75-ft depth) in item 3, and P10 (0.75-ft depth) in item 3.
- c. One WES soil deflection gage (D3, 2.75-ft depth) in item 3 stopped working about halfway through the tests; gage D7 (2.75-ft depth) in item 3 was operating near its limits for about the last half of the tests (when a gage is operating near its limits, it loses some of its linearity and the readings may be in error by a slight amount); and gage D8 (2.75-ft depth) in item 4 began to show erratic behavior before tests started and was not considered reliable.
- <u>d</u>. Only two of the eight pavement strain gages operated throughout the test period, and they were of questionable behavior.
- e. One of the bottom temperature probes stopped working at the start of the tests.

Two WES soil pressure cells in item 4, P6 (0.75-ft depth) and P2 (7.5-ft depth), stopped working after all tests including traffic were completed. Cell Pl in item 4 gave unreliable responses but never stopped working. Cell P6 stopped working four days after the finish of the twin-tandem 240,000-lb static load tests, which were conducted after the completion of traffic tests in traffic lane 1. Cell P2 stopped working three months after cell P6 stopped. The causes of the unreliable behavior of cell P1 and the complete loss of cells P2 and P6 could not be determined. Cell P6, which was a shallow-depth cell (0.75-ft depth), may have been damaged during the 240,000-lb twin-tandem static load tests.

Two of the SA-E soil pressure cells, P8 (2.75-ft depth) in item 4 and P10 (0.75-ft depth) in item 3, stopped working completely during the traffic tests. The reasons could not be determined; however, the failure may have been a function of the large output signal instability exhibited by the SA-E cells, as shown in figures 63 and 64 in the main text. These histories of output signal instability of the cells were the basis for doubting the reliability of the SA-E cells during the instrumentation tests.

During the traffic tests, the surface deflection gage in each item

stopped working because the gages had reached their limits of movement. The surface gage in item 3 was replaced and was still working one year later, but the surface gage in item 4 could not be replaced due to the core rod being broken off at the top of the reference rod.

Deflection gage D8 in item 4, which began erratic behavior before the static and dynamic load tests were started, was at the 2.75-ft depth on top of the subgrade and is believed to have been damaged by water on top of the subgrade entering the gage housing. Gage D3 in item 3, also at the top of the subgrade, went out in the middle of the static and dynamic load tests and is believed to have possibly been damaged by water entering the gage housing. Gage D7 in item 3 was operating out of its linear range one year after the completion of testing, but it could be calibrated in the lower part of the nonlinear range before the calibration curve became asymptotic to the abscissa's axis.

As can be seen in figures 67 and 68 in the main text, the deflection gages in both items at the top of the subgrade experienced drastic movements during the construction of the test section. This large deflection occurred after the subbase became saturated, which resulted in free water standing on the subgrade, and was discussed in Volume III. A. The top of the subgrade is believed to have been softened by the water, consequently allowing the deflection gages to seat themselves in the subgrade; this is the reason for the gages to have operated near their limits of movement and possibly to have been lost. The seemingly erratic behavior of these gages during the testing period was discussed under analysis of data in the main text.

Originally 8 pavement strain gages were to be installed; however, a total of 10 gages were installed because two strain gages were replaced immediately after the first lift of asphaltic concrete was rolled, which occurred immediately after the first gages were installed. The gages were too fragile and the asphalt pavement roller mutilated them. This immediately made the condition of the eight working gages questionable. Three of the eight were lost during the paving and rolling of the top pavement lift. The remaining five gages had very erratic behavior under the first static load tests (12-wheel 180,000-1b load). Some of them would work, then stop, and start again later.

During the dynamic load tests with the 12-wheel 180,000-lb load, one of the five stopped working permanently. One more stopped during the 12-wheel 360,000-lb static load tests, and another one stopped during the dynamic load tests. This left two working very erratically for the remaining tests. One of the two stopped immediately after the finish of the static and dynamic load testing and before traffic started. One gage was still working occasionally one year after the completion of testing. The strain gages installed in the MWHGL test section pavement failed for two reasons: they were not sufficiently rugged to withstand the construction processes and did not have a large enough range for the strains induced by the large loads.

One bottom temperature probe failed before tests started on the test section, and the other bottom probe failed during traffic. Both bottom probes were replaced at the same time as the surface deflection gage in item 3. The temperature probes failed for undetermined reasons.

A summary of the instrumentation channel losses, which were considered satisfactory overall, is listed in table A-23.

Table A-23
Instrumentation Losses

Type of Instrumentation	Total Installed	No. Lost
WES soil pressure cells	17	2
SA-E soil pressure cells	3	2
Deflection gages	18	3
Pore pressure cells	2	0
Temperature probes	4	0*
Pavement strain gages	8**	8

^{*} Two failed and were replaced so no data were lost.

A high percentage of soil instrumentation, cells and gages, is considered to have been performing accurately during the instrumentation testing program and a high percentage was still active one year after the completion of testing; however, some instruments are questionable as to their reliability due to possible damage under traffic tests.

^{**} One registered intermittently.

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. S'MMARY

Future similar installations could profitably use the WES soil pressure cells, pore pressure cells, and deflection gages. The type temperature probe used was satisfactory. A method(s) better than the optical technique used in this work is needed to determine surface and reference plane deflections.

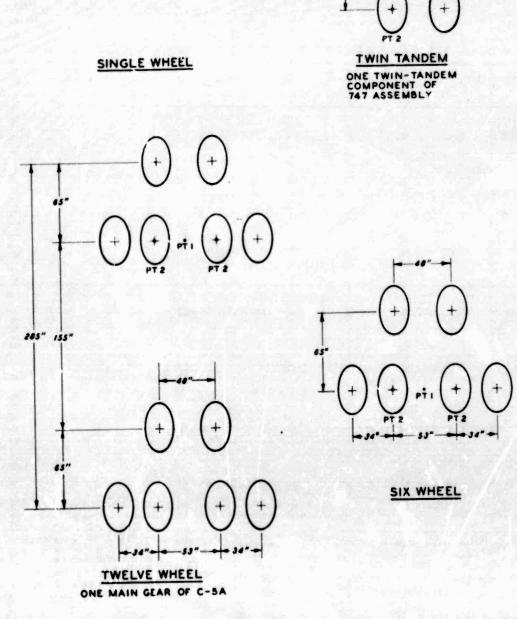
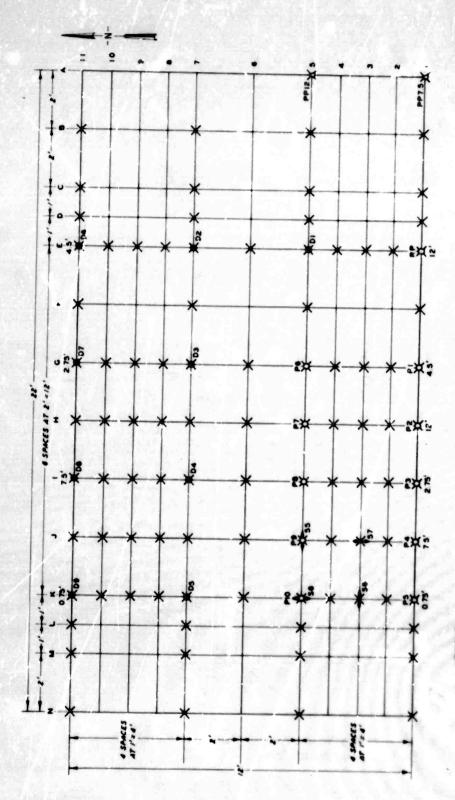


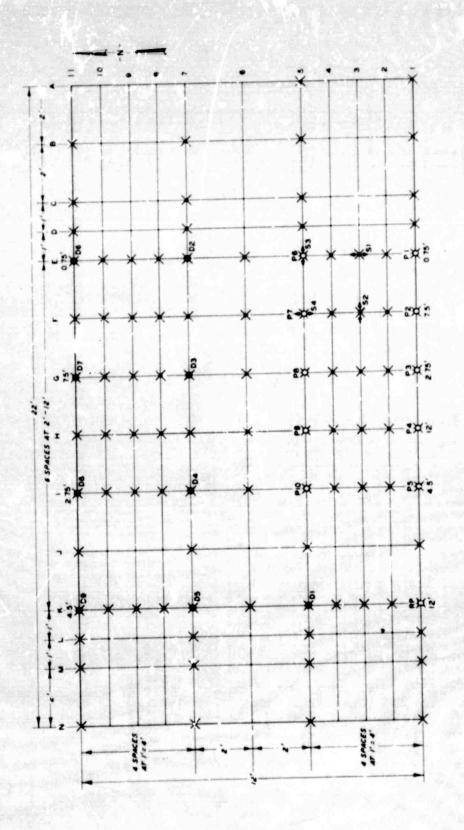
Figure Al. Locations of Assembly Loading Points of Wheel Assembly Used in Flexible Pavement Tests



O PRESSURE CACE
O DET.LECTION CACE
A PORE PRESSURE CACE
O REFERENCE PLATE
X LOADING POINT

STRAIN CACES

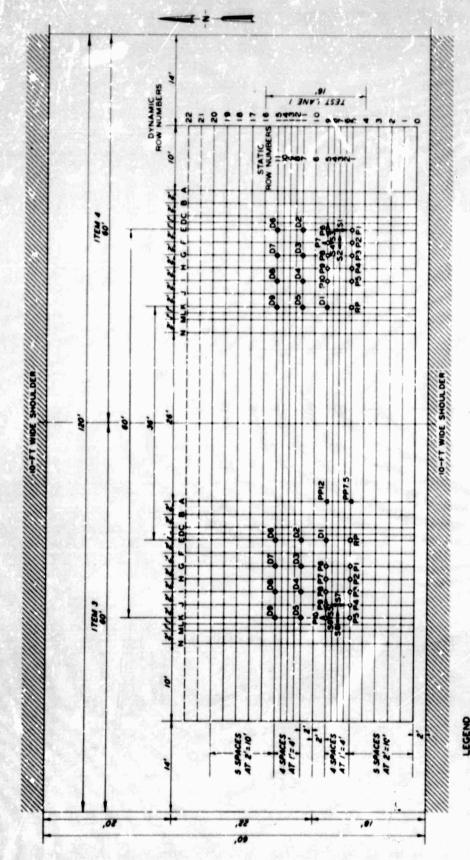
Static Loading Grid System, Item 3, Flexible Favement Test Section Figure A2.



Static Loading Grid System, Item 4, Flexible Pavement Test Section STRAIN GAGES

Figure A3.

LEGEND PRESSURE GAGE DEFLECTION GAGE REFERENCE PLATE LOADING POINT



STRAIN GAGES

C PRESSUR GAGE

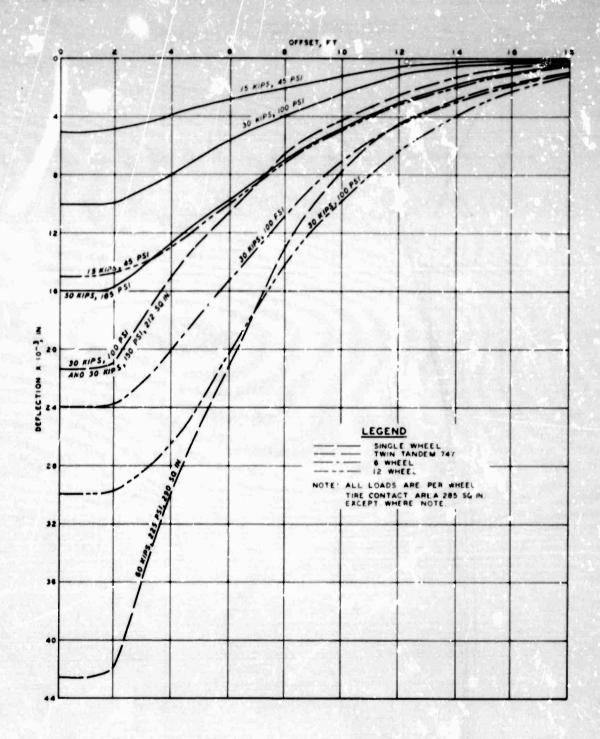
DEFLECTION GAGE

PROFE PRESSUR GAGE

REFERENCE PLATE

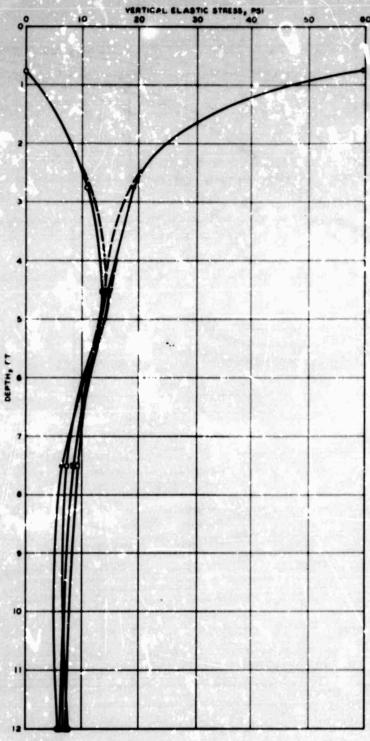
STRAW GAGES

Figure A4. Static and Dynamic Loading Grid System, Flexible Pavement Tests



OFFSET VS DEFLECTION AT 12-FT DEPTH ALL LOADS ARE PER WHEEL FLEXIBLE PAVEMENT TESTS

Figure A5. Correction to be Applied for Induced Movements Under Load



LEGEND

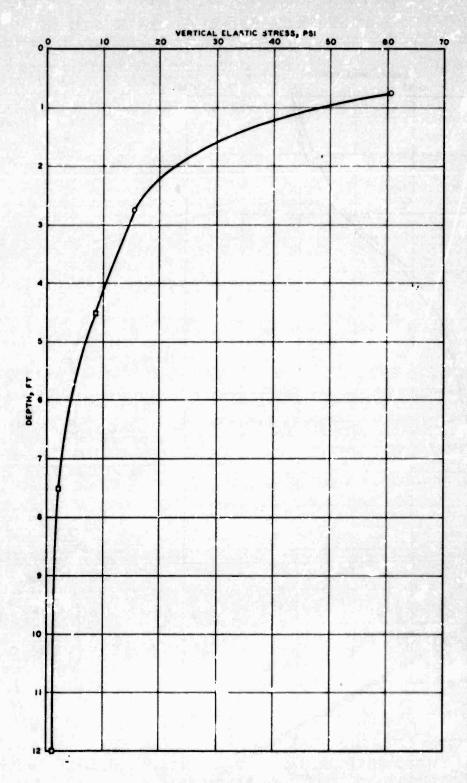
LOAD POINT

- 0 ROW 1, PI THRU PS

LOAD POINT 2

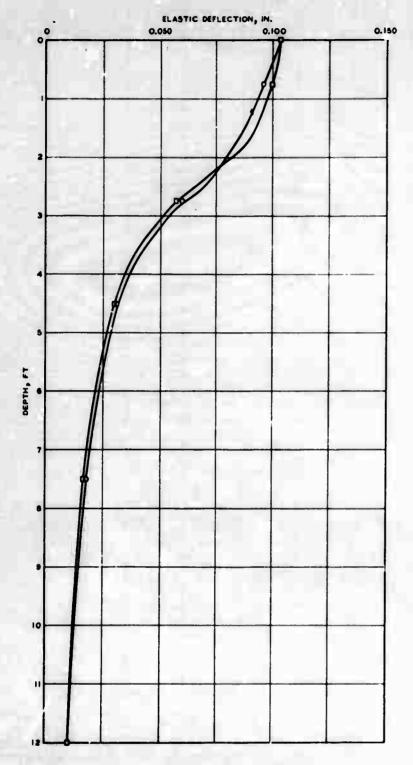
- e ROW 1, PI THEU PS A ROW 5, PS THRU PIO (PY I AT ROW 3) T ROW 5, PS THRU PIO (PT I AT ROW 6)

Figure A6. Depth Versus Vertical Elastic Stress, Six-Wheel, 180-kip Static Loading, Item 3, Flexible Pavement (Initial Data)



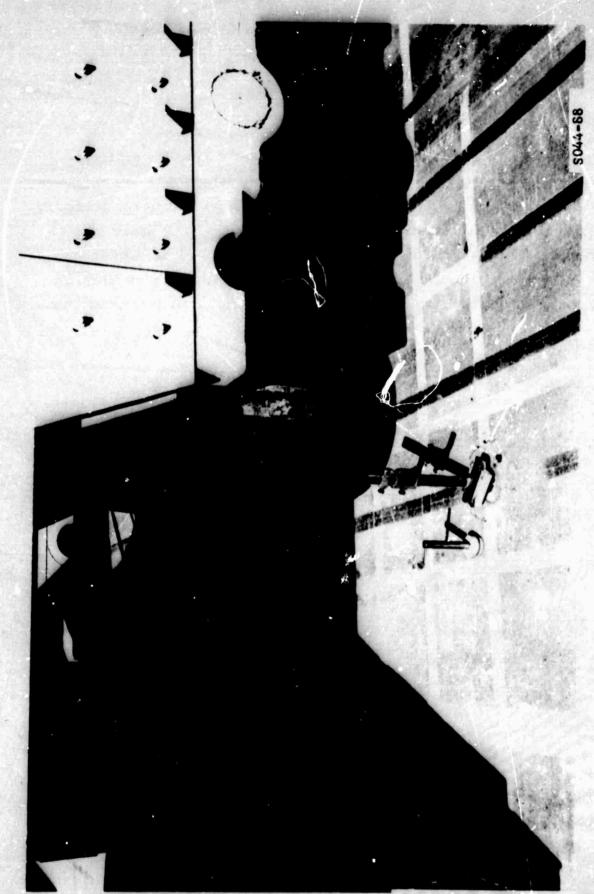
LEGEND
O ROW 1, PI THRU PS
D ROW 5, PG THRU PIO

Figure A7. Depth Versus Vertical Elastic Stress, Single-Wheel, 30-kip Static Loading, Item 3, Flexible Pavement Tests (Initial Data)



DEGEND OF THE DESTRUCTION OF THE

Figure A8. Depth Versus Vertical Stress,
Single-Wheel, 30-kip Static Load,
Item 3, Flexible Pavement Tests
(Initial Data)



NOT REPRODUCIBLE

Figure A9. Load Cart in Position for Reference Rod Measurement

WART-IK-10-TT2

APPENDIX B: RIGID PAVEMENT INSTRUMENTATION MEASUREMENTS

SECTION I

INTRODUCTION

This appendix is a listing of the data collected during the multiplewheel heavy gear load (MWHGL) rigid pavement tests. These data are complementary to the information presented in the basic report. Data are presented for load tests for single, twin-tandem, 12-wheel, and 6-wheel assembly loadings, from 15,000 to 41,500 lb per wheel. Loadings were either static or dynamic (slowly moving) loads. Data consist of measurements of deflection, strain, pressure, crack width, and deflection response to vibratory loading.

SECTION II

DATA REDUCTION AND PRESENTATION

Data were recorded on 14-channel magnetic tape, and an arrangement was provided for a paralled recording on an oscillograph recorder. The data were reduced from the oscillograph traces manually. All calibration factors were predetermined for the transducers by the manufacturers and checked by Government personnel during the acceptance tests. All gain settings, calibrations, and sensitivity factors were incorporated manually in the data-reduction process. Data were tabulated to the nearest 0.001 in. for deflection readings, to the nearest microinch per inch for strain, and to the nearest 0.1 psi for pressure readings. Data were rounded to these accuracies based on manufacturer's specified accuracies and on past experience with similar instrumentation readings. An explanation of the gage identification system is shown in table Bl.

1. STATIC AND DYNAMIC LOAD TESTS

a. Single-Wheel Assembly

Static loading tests were conducted at various positions along the test section. A total of 16 different positions were loaded with a single-wheel load of 15,000 lb. The test positions are shown in figure Bl. The same load positions were tested under a single-wheel load of 22,500 lb except for positions 15 and 16. The 22,500-lb wheel load was not placed on item 4 to avoid any possibility of premature cracking.

Data collected during static testing with the single-wheel load are summarized in table B2. The data represent the change in either deflection, strain, or pressure from the unloaded to the loaded condition. The loads applied were relatively small and are considered to be in the elastic range of the structure. Two columns of figures present the data obtained under single-wheel loads of 15,000 and 22,500 lb with the exception of test positions 15 and 16. In instances where a dash line is shown, the noise level was too high to determine a reasonable reading. An arbitrary criterion was established for noise levels. When the signal-to-noise ratio was less than 10:1, the reading was discarded. Where a blank is shown, either the transducer did not register or the indicated load was not tested at that point.

Dynamic single-wheel loadings were applied to the test section after completion of the static tests. The wheel positions in the various traffic lanes are shown in figure R2. These tests were conducted with the load cart traveling at about 3 mph. Data collected from the single-wheel dynamic load tests are shown in table B3 for the 15,000-lb load and in table B4 for the 22,500-lb load. The load was applied down a particular lane in the west direction and then the load cart was backed down the same lane in the east direction. Data for test item 4 are presented in table B3 only, as the 22,500-lb load was not applied to test item 4. The values tabulated are the peak values obtained as the load was traversing the traffic lane.

b. Twin-Tandem Assembly

Static loading tests were conducted with a twin-tandem assembly loaded to 15,000 and 22,500 lb per wheel. Test positions were determined from the position number and location. The position number indicates the wheel position relative to a gage. The location refers to a particular gage and indicates the general vicinity of the load. Sometimes the same relative wheel position holds for several different types of gages; thus, the need to include a location designation is apparent. The various test positions are shown in figures B3-B5. The data are presented in table B5. The 22,500-lb load was not applied to test item 4 as there was some chance of cracking the pavement.

Twin-tandem dynamic loadings were applied to the test pavements with loads of 15,000 and 22,500 lb per wheel. The traffic lines where the dynamic loads were applied are shown in figure B6. These tests were conducted with the load cart moving at about 3 mph. Data collected from the slowly moving twin-tandem assembly tests are shown in table B6 for the 15,000-lb-per-wheel load and in table B7 for the 22,500-lb-per-wheel load. The load was applied along a particular traffic line in the west direction with the load cart facing west, and then the cart was backed down the same traffic line in the east direction with the load cart still facing west. Data for test item 4 are presented in table B6 only, as the 22,500-lb-per-wheel load was not applied to test item 4. The values in tables B6 and B7 represent the peak values obtained as the load cart was traversing the traffic lane.

c. 12-Wheel Assembly

Static loading tests were conducted with the 12-wheel assembly loaded to 15,000 and 22,500 lb per wheel. As with the twin-tandem static load tests, the load location was determined from a position number and a location. The position number defines the position of the wheels relative to a gage and the location designates the general vicinity of the load and the gage of primary interest. The wheel positions for the various position numbers are presented in figures B7-BlO. The data are presented in table B8. As before, the load of 22,500 lb per wheel was not applied to test item 4 to avoid cracking the pavement.

Twelve-wheel-assembly dynamic loadings were applied to the test pavement along the traffic lines shown in figure Bll. Data collected from the 12-wheel-assembly dynamic load tests are shown in table B9 for the 15,000-lb-per-wheel load and in table BlO for the 22,500-lb-per-wheel load. The load was applied along a particular traffic line in the west direction with the load cart facing west. Data for test item 4 are shown only in table B9 as the 22,500-lb-per-wheel load was not applied to test item 4. The tabulated values are the peak values obtained as the load cart was traversing the traffic line. The locations of these lines were discussed and presented in Volume III-A.

d. 6-Wheel Assembly

A limited amount of static load testing was conducted using one 6-wheel bogie of the 12-wheel assembly. The test vehicle was constructed such that each 6-wheel bogie of the 12-wheel assembly was an independent load cart and could be moved separately. Static load testing was conducted with a 22,500-lb-per-wheel load at various positions on test items 1, 2, and 3. The test positions used were identical to those used for the 12-wheel assembly where possible. The fact that no trailing 6-wheel bogie was present made it impossible to use some of the 12-wheel-assembly test positions. The test positions correspond to those presented in Volume III-A for the 12-wheel assembly. Data collected are presented in table B11.

Dynamic load tests were conducted with the 6-wheel assembly loaded to 22,500-lb-per-wheel and are summarized in table Bl2. The loads were applied in the same manner as previously discussed, i.e., along one traffic line in the west direction and then along the same line in the east direction

with the load cart always facing west. The values tabulated represent peak values only.

2. SUPFLEMENTAL TESTS

After reviewing the results of the static and dynamic load tests, supplemental tests appeared desirable to further define the shape of the deflected slab under various gear assemblies. These tests consisted of strain measurements and optical deflection measurements on test item 2.

a. Strain Measurements

An array of 10 strain gages was mounted on the top surface on item 2. This array consisted of two arms of five strain gages each at right angles to each other. The arms were oriented in the north and east directions and spaced 30 in. apart except for the last strain gage on the east arm, which was 37 in. from the nearest gage. The intersection of the arms was in the center of the southwest panel of test item 2. A sketch of the gage layout is shown in figure B12.

Two separate tests were conducted using the supplemental strain gages. The first consisted of moving the 30,000-lb single-wheel load cart along the east arm of the strain gage layout. The load cart was started on the east edge of the pavement and moved toward the center of the slab in 25-in. increments. The strain gages were read at each 25-in. increment until the load reached the center of the slab. The results of this test are presented in table B13. The second test was conducted with the twin-tandem load cart and was intended to provide information on the short-term stability of strain measurements. The twin-tandem assembly was loaded to 15,000 lb per wheel and positioned such that the tandem dimension was in the eastern direction and the twin dimension was in the northern direction. The center of gravity of the twin-tandem assembly was positioned over the center of the southwest panel and strain readings were taken immediately after the load was positioned. Strain readings were taken again after the load had been in position for 15 minutes. The results of this test are shown in table B14.

b. Optical Deflection Measurements

Optical measurements of slab deflections were attempted on a grid system established on test item 2. Small reference plugs were attached to

the slab surface using an epoxy resin adhesive. The rod consisted of a steel rule with a target sight and vernier attachment that allowed readings to be made by the rodman to the nearest 0.001 of an inch. Two level stations were established on either side of the test track by casting small concrete pedestals to hold the level at a convenient elevation. The results of the optical tests were somewhat inconclusive due to the inability to measure the small deformations that occurred over the relatively large distances. The instrument man followed a policy of sighting the target along the edge of the cross hair, but the deformations a short distance away from the load were so small that it was not possible to achieve reliable repeatability of readings. Averaging several sets of level readings and estimating the radius of curvature by passing a circular arc through three points indicated that a crack may have formed in the southwest slab of item 2, but the validity of the conclusion is questionable due to the unreliable nature of the data.

3. TRAFFIC TESTS

a. 12-Wheel Assembly

After completion of instrumentation testing, 12-wheel-assembly traffic was applied to the test section. This assembly represents one main gear of a C-5A aircraft. The traffic patterns for application of this accelerated traffic are shown in figure Bl3. Traffic was applied in a sequence that would produce a favorable transverse distribution of traffic on the pavement - lines 1, 2, 3, 4, 5, 5, 4, 3, 3, 2, and 1. Traffic was applied with the load cart traveling forward on each traffic line, then traveling backward along the same line with the load cart always facing west. Thus, one traffic pattern consisted of 22 passes of the 12-wheel load cart.

A large number of transducers had failed before the start of 12-wheel traffic, and additional strain gages were mounted on the top slab surface to replace some of the gages that had failed. A layout of the instrumentation that was used during the 12-wheel traffic testing is shown in figure B14. Transducer output was recorded on magnetic tape on a continuous basis, and copies on chart paper were produced during the tests at specific intervals for monitoring purposes. Peak values manually selected from the charts are presented in table B15. The peak deflection values presented in the table are all recoverable deflections. Permanent deformations were also calculated

from the residual voltage output of the differential transformers. The permanent deformations are shown graphically in figures B15-B22. These readings were taken periodically during the 12-wheel-assembly traffic testing period.

In addition to the electrical instrumentation readings, crack width was monitored using a Whittemore gage. Crack width was measured at several locations as shown in figure B23. The results of the measurements are shown graphically in figures B24-B28.

Dynaflect measurements were made on each test item at the end of each working day. The Dynaflect is a nondestructive testing device that is mounted in a trailer. The Dynaflect induces a sinusoidal load of 1000 lb peak-10-peak to the pavement with two opposing eccentric fly wheels. The load is applied to the pavement at a frequency of 8 Hz through two steel wheels. Pavement deflection is sensed by an arm of five geophones extended perpendicular to the axle between the steel loading wheels. One geophone is positioned directly below the axle between the steel loading wheels and the other geophones are spaced at 12-in. intervals along the arm. Representative data for three test positions in all items and both lanes are presented in tabular form in table B16. The representative test positions are shown in figure B29.

b. Twin-Tandem Assembly

The 12-wheel-assembly traffic testing was conducted on the south lane of the test section and, therefore, did very little damage to the north lane. Following completion of the 12-wheel-assembly traffic testing, traffic was applied to the north lane using a twin-tandem gear with the same geometry as one assembly of the Boeing 747 aircraft. This assembly was loaded to 41,500 lb per wheel, and traffic was applied to the center portion of the north lane. The dimensions of the twin-tandem assembly were such that the maximum concrete stresses generated with the wheels tangent or perpendicular to a joint is nearly the same for the range of radii or relative stiffness of the four test items. The location of the traffic pattern was, therefore, not critical. Trafficking only the center of the lane avoided any areas of edge effects that might have been introduced by the 12-wheel traffic applied to the south lane along the longitudinal joint.

The north lane was instrumented with top surface strain gages on

items 2 and 3 as shown in figure B30. Traffic was applied on five traffic lines similar to the 12-wheel traffic. The traffic patterns are shown in figure B31. Traffic was applied with the load cart traveling forward on each traffic line and then traveling backward along the same line with the load cart always facing west. The trafficking sequence by line number was as follows: 1, 2, 3, 4, 5, 4, 3, 2, 2, 3, 4, 4, 3, 3, 2. The full sequence is referred to as a traffic pattern and consists of 30 passes of the twintandem load cart.

A total of 68 traffic patterns were applied to the north lane with the twin-tandem gear. Periodically charts of the transducer outputs were produced on the site and peak values were manually reduced from these charts. The peak values thus obtained are listed in table B17.

SECTION III

EVALUATION OF MEASURING INSTRUMENTS

1. CONSISTENCY OF MEASUREMENTS

The ability of a transducer to produce consistent, repeatable readings is a function of many factors including (a) environment, (b) type of measurement (static, dynamic, etc.), and (c) inherent transducers accuracy - to name only a few. Other sources of error are introduced as the complexity of a system increases. All conditioning, recording, and playback equipment are subject to fluctuations in voltage, amperage, etc. Human error is also reflected in test data and is often difficult to detect when the absolute values of the data are small. The manual reduction of data involved arithmetic operations on vast quantities of numbers and is a likely point for human error. The discussions in the following paragraphs are all subjective in nature as they were drawn from test data that were not specifically collected to determine consistency of data.

a. Soil Pressure Cells

Soil pressure cells used in the rigid pavement test section (see locations in figure B32) were a type of commercially manufactured transducers that had not been previously used by CERL for measurements in a pavement structure. A preliminary test was performed prior to installation that indicated the cell tested was over-registering about 1/2 psi over the entire range. This test was preliminary and some boundary condition effects were undoubtedly introduced, but the test seemed to indicate reasonable results could be expected for measuring pressure in clay soils. The cells were embedded in the pavement structure for several months prior to loading. The cells were erratic from the start of static testing through the completion of the traffic testing.

The erratic behavior made it impossible to conclude how consistent the readings were, and no statement can be formulated in regard to the effects of changes of gear assembly or wheel loads. The poor results obtained during the static and dynamic load tests with all gear configurations and during the initial portion of the 12-wheel-assembly traffic tests led the field crew to the conclusion that all pressure cells had failed and they were not monitored during the bulk of the 12-wheel-assembly traffic tests.

b. Deflection Gages

The basic principle behind the measurement of deflection by linear variable differential transformers (LVDT) has been successfully employed for some 20-25 years. The original LVDT gages required external electronics to supply the carrier. The advent of integrated circuits has made it possible to encapsulate the electronic equipment for the carrier signal in the transformer housing, thus reducing the noise on long cable runs. Integrated-circuit type LVDT's were used in the rigid pavement ter's section.

The laboratory accuracy of an LVDT gage is about 0.001 in., but the problems associated with field testing (temperature changes, slab warping, etc.) reduce the consistency of readings to about +0.001 in.

c. Strain Gages

Strain gages were the transducers most sensitive to environmental effects and load positioning of all those that were used on the test section. Contraction and expansion of the concrete slabs due to temperature changes were reflected in the strain data. No meaningful consistent measurements could be extracted from the strain data other than that collected during the trafficking period with the 12-wheel and twin-tandem assemblies. The consistency of strain readings for these tests was judged to be between ± 1 and $\pm 5~\mu in./in$. The manner in which the data were recorded and reduced eliminated the environmental effects and reflected only load strains.

A problem arises in the measurement of strain on a rigid pavement when cracking occurs. The strains will tend to gradually grow larger under repeated applications of load until a crack occurs, at which time, the strain is generally relieved and drops to some lesser reading and gradually grows larger again. This process continues until the cracking either destroys the gage or the pavement is cracked into pieces so small that each segment of pavement acts as an individual block and is too small to act as a flexural member. When cracking occurs, reproducibility of strain measurements is impossible to achieve.

d. Optical Deflection Measurements

The optical measurements of pavement deflection made during the

supplemental tests on test item 2 showed poor reproducibility. During these tests, attempts were made to measure transient deflections, which are very small in rigid pavements. Even though level monuments were constructed as close as possible to the test section to minimize the length of shots, the ratio of sight distance to measured deflection was very large and contributed greatly to the inability to repeat readings. These data were not presented due to the poor reproducibility that made the value of the readings questionable.

The optical measurements of permanent pavement deflection made during the traffic testing phase of the study appeared to be quite consistent. The permanent deflections were rather large, compared to transient deflections, and were reproducible to about 0.Cl ft. The difference in the reproducibility of the level readings for transient and permanent deflections was due to the differences in the amount of movement associated with each type of deflection.

2. LOSS OF INSTRUMENTATION

An abnormally high number of gage failures were experienced during the life of the rigid test pavement. These failures can be classed in three different categories as follows: (a) failure of electronic components, (b) failure due to improper installation and/or environmental effects, and (c) failure due to mechanical damage. Each type of gage failed at some time during the test program. A description of the type of failure encountered with each type of gage is presented in the subsequent paragraphs.

a. Deflection Gages

Apparently the deflection gages failed primarily through two causes: failure in the integrated circuits wi him the transformer housing and failure due to pavement cracks forming in the immediate vicinity of the gages, which affected the bond between the concrete and the gage or parted the lead wires. Failure due to cracks in the pavement could hardly be classed as an instrumentation failure; however, this is pointed out as a guide for future installation. It is a consideration that should not be ignored.

b. Embedded Strain Gages

Posttraffic examination or the condition of the embedment strain gages revealed an as-yet unexplained phenomenon. Details of the gage installation

techniques were described in the main body of this report. The gages were positioned at the extreme lower slab surface such that the lower face of the foil envelope protecting the strain gage often was exposed to the subgrade soil. Posttraffic examination of these gages showed many to be corroded completely away or corroded to such a point that the gage was inoperable. Chemical analysis provided no evidence of chemical decomposition. Two possible causes were postulated: some material in the soil reacted with either the foil envelope or the water to form a corrosive environment that escaped the chemical analysis; or, a more likely possibility, an electrolytic cell was created by the combination of water, oxygen, and currents produced by the dissimilar metals of the gages. None of the gages showed an appreciable loss of bond even though some had been partially corroded away. Use of an installation technique such as bonding to embedded concrete beams might have avoided some of the strain gage failures.

b. Top Surface Strain Gages

Failures in the top surface strain gages were mainly due to infiltration of moisture through the waterproofing compound and to mechanical damage such as accidentally hitting one of the gages with a load wheel. Failure of these gages presented no real problems, however, as they were readily accessible for repair.

c. Pressure Cells

Only one pressure cell was recovered during the posttraffic tests. Examination of this cell revealed that the strain gage sensing elements had lost bond with the active diaphragm, rendering the cell useless. Examination of one cell cannot be considered conclusive; however, all pressure cells produced signals similar to that generated by the one cell that was retrieved in the posttraffic tests.

3. SUMMARY

Based on observations and experience during the tests of the rigid portion of the MWHGL test section, the following comments are made for guidance in future design and installation of instrumentation to determine the reaction of rigid pavements to static and slowly moving loads and to traffic.

a. Redundancy

When the transducers are not accessible for repair and replacement in the event of mechanical malfunction, redundancy on the order of 100 percent is desirable if a test is to last for an extended period of time. Accessibility to the transducer and supporting electronic equipment should be maintained insofar as possible. In general, transducers are located at critical points in the pavement structures. Failures are most likely to occur at these critical points and the loss of transducers at these points should be anticipated.

b. Deflection Measurements

The most accurate means of measuring rigid pavement deflections is by electronic devices such as the LVDT's. The recoverable deformations in rigid pavements are very small and are extremely difficult to detect by means other than electronic devices. Accessibility to the transducer and supporting electronic equipment is essential. In providing accessibility, however, care must be taken not to induce stress concentrations that might adversely affect pavement performance.

c. Strain Measurements

Gage installation techniques should be of primary concern for embedded strain gages. A promising technique seems to be casting the strain gages in a concrete beam under laboratory conditions and then casting the beam in the pavement during the construction phase. This technique would allow testing the beam in flexure prior to installation in the pavement, and the amount of concrete cover over the gage could be closely controlled. Extreme care should be exercised to ensure that the concrete beam would have the same properties as the test pavement. Shape and texture of the beam should also be carefully selected to ensure adequate bond with the pavement concrete. Surface strain gages appear to offer no particular problems. Care should be taken to provide moisture protection during installation. Mechanical damage at times is unavoidable and some amount of damage should be anticipated.

d. Pressure Measurements

Pressures in soil are difficult to measure due to a variety of reasons. Soil arching, mismatched moduli of soil and gage, and presence of moisture are only a few of the complications that affect soil pressure measurements. Apparently more data are required to successfully instrument a

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rigid pavement structure to measure soil pressures. These pressures are relatively small and the soil environment is somewhat hostile for electrical transducers. A test program is recommended to advance the state-of-the-art in pressure measurements under rigid pavements. Until pressure measurement techniques for soil under rigid pavement are improved, it is recommended that pressure measurements either not be attempted or else held to a very nominal amount.

TABLE B1

IDENTIFICATION OF RIGID PAVEMENT INSTRUMENTATION

a. DEFLECTION GAGES

Characters in the following sequence:

Item number (1, 2, 3, or 4)

D for deflection gage

Compass direction or center of slab (N, S, E, W, or C)

J for joint Not used for gages Orientation of joint (T for transverse or L for longitudinal) in center of slab.

EXAMPLE: 1DWJT would identify a deflection gage in item 1 west of the transverse joint.

b. STRAIN GAGES

Characters in the following sequence:

Item number (1, 2, 3, or 4)

S for strain gage

Compass direction or center of slab (N, S, E, W, or C)

J for joint. Not used for gages in the center of a slab.

Orientation of joint or gage (T for transverse or L for longitudinal)*

EXAMPLE: 2SNJL would identify a strain gage in item 2 north of the longitudinal joint.

c. PRESSURE CELLS

Characters in the following sequence:

Item number (1, 2, 3, or 4)
Depth of embedment below surface, ft (3 or 7). If no number appears, cell was at slab/subgrade interface.

P for pressure cell

Longitudinal coordinate**

Transverse coordinate**

EXAMPLE: 27P23 would identify a pressure cell in item 2 that was 7 ft below the surface at longitudinal coordinate 2, transverse coordinate 3.

d. PARTIAL DEFLECTION GAGES

Characters in the following sequence:

Item number (1, 2, 3, or 4)
Length of reference rod measured from bottom of slab, ft (3, 5, or 9)

PD for partial deflection gage

EXAMPLE: 23PD would identify a partial deflection gage that was installed to measure deformation at the 3-ft depth in item 2.

All center strain gages were mounted on the top slab surface and were oriented in the longitudinal or transverse direction. All gages in the vicinity of a joint were mounted near the bottom slab/subgrade interface and were oriented parallel to the particular joint.

Grid system shown in figure B32.

TABLE B2

SINGLE-WHEEL-ASSEMBLY STATIC TESTS

CAGE*	15,000-1b	22,500-16	UNITS
	WHEEL LAD	WHEEL LOAD	
	TEST POSIT	ION 1	
1DC	.013	200	in.
1DWJT	.002	.006	in.
1DEJT	.001	001	in.
1SCT	-	29	µin/i
1SCL	1	1	µin/i
1SSJL	2	1	µin/i
1SNJL	0	1	µin/i
1SWJT	1	2	µin/i
	TEST POSIT	ION 2	
1DC	.004	.015	in.
1DWJT	.002	.004	in.
1DEJT	.004	.005	in.
1DSJL	.009		in.
1DNJL ·	.011		in.
1SCT		7	uin/i
1SCL	1	3	µin/i
	TEST POSIT	ION 3	
1DC	.001	.008	in.
1DEJT	.013	•	in.
LDNJL	.002	.002	in.
ISCT	3	11	uin/i
ISCL	2	3	uin/i
1SEJT	12	22	µin/i
	TEST POSIT	ION 4	
2DC	.010	.013	in.
2DWJT	.010	.007	in.
2DEJT		.001	in.
2DSJL	.002	.003	in.
	.002	.002	in.
2DNJL	16	25	uin/i
2SCT			uin/ii
2SCL	7	8	uin/ii
2S\$JL	0	4 2	uin/ii
2SNJL	0		uin/i
2SEST 2SWJT	i	0 1	uin/1
25451			() - Li
2DC	TEST POSIT	.004	in.
2DWJT		.003	in.
2DSJL	.009	.012	in.
	.008	.009	in.
2DNJL		••••	
2SCT	2	2	µin/i
2SCL			uin/i
2SSJL	16	25	űin/i
2SNJL	2	10	µin/ir

^{*}See table B1 for gage identification system.

TABLE B2 (Continued)

AGE	15,000-16	22,500-16	ONITS
	WHEEL LOAD	WHEEL LOAD	
	TEST POS		CHILDREN, N. 1998
2DC	.001	.002	in. in.
ZDWJT	.004		in.
DEJT	.016		in.
2D6JL	.002	.003	in.
DNJL	.002		pin/in
SCT		3	Pin/in
2SCL		3	μin/in
2SSJL	1 2	1 2	μin/in
2SNJL		Approximate and tree.	P111/111
	TEST POS		
23PD		.006	in.
25PD		.010	in.
29PD		.018	in.
2P13		.6	psi
27P13		.7	psi
	TEST POS	SITION 8	
2P11		1.5	psi
2P41		1.3	psi
2P51		4	psi
2P42		.1	psi
2P34		- 11	psi
2P44		1	psi
2P54		9	psi
23P23		.2	psi
	TEST POS	SITION 9	
23PD	.007		in.
25PD	.007		in.
29PD	.010		in.
2P13	-1.7		psi
27223	.4		psi
	TEST POS	SITION 10	
2911		4.8	psi
2P41		-5.6	psi
2P51		.4	psi
2P34		-1.5	
23P23		1 July 1 1 1 1 1 5	psi
	TEST POS	SITION 11	
3DC	.007	.009	in.
3DWJT	.002	.003	in.
3DEJT	.001	.001	in.
3DSJL	.002	.003	in.
Charles and the control of the contr	5	8	µin/i
38CT	11	12	µin/i
3SCL 3SSJL	- - 0	2	µin/i
3SNJL		2	µin/ii
30110 E			Sheet 2 of 3

TABLE B2 (Concluded)

GAGE	15,000 - 1b WHEEL LOAD	22,500 -1b WHEEL LOAD	UNITS
	TEST POSIT		
3DC	.001	.002	in.
3DWJT	.001	.002	in.
3DEJT	.001	.001	in.
3DSJL	.009	.011	in.
3SCT			µin/i
3SCL	2	Min. 12 14 11 11 15 15 15 17 18 14	µin/i
3SNJL		10	pin/i
	TEST POSIT		
3DC	.002	.002	in.
3DWJT	.008	.009	in.
3DEJT	.008	.010	in.
3DSJL	.003	.005	in.
3SCT		2	µin/i
3SCI.	2		µin/i
3SEJT	•	11	µin/i
	TEST POSIT		
33PD		.005	in.
35PD		.009	in.
	TEST POSIT	TION 15	
4DC	.043		in.
4DNJL	.002		in.
4DSJL	.006		in.
	TEST POSIT	TION 16	
4DC	.038		in.
4DNJL	.040		in.
4DSJL	.051		in.

TABLE B3

PEAK VALUES OF SLOWLY MOVING 15,000-LB SINGLE-WHEEL-ASSEMBLY INSTRUMENTATION TESTS

EAST	.012 .013 .004 .008	.008 .013 .005 .010	.010 .010 .010 .010	3 EAST 1TEM . 019 .015 .010 .004 .008 .010	.010 .017 .008 .003	.011 .017 .009 .003 .007	MEST	.011 .019 .006 .002 .006 .007	.00! .00! .00!	6 .005 .005 .007 .005 .001	in. in. in. in. in. in. in. in. in.	
:	.012 .012 .013 .004 .008	.008 .013 .005 .010	.010 .010 .010 .010	.019 .015 .010 .004 .008	.010 .017 .008 .003 .007	.011 .017 .009 .003 .007	34	.011 .019 .006 .002 .006 .007	.00! .00! .00!	5 .005 -009 -009 -005 -001	in. in. in. in. in. in. in.	
:	.012 .004 .008 .011	.013	.011 .010 .013 .011	.019 .015 .010 .004 .008	.017 .017 .018 .003 .007	.017 .009 .003 .007 .010	34	.019 .006 .007 .006 .007	.000 .000 .001	.005 .001	in. in. in. in. in. in.	
	.012 .004 .008 .011	.013	.014 .010 .708 .011	.015 .010 .004 .008 .010	.008 .003 .007	.009 .003 .007 .010		.019 .006 .007 .006 .007	.002 .001	.005	in. in. in. in. in.	
	.013 .004 .008	.005	.010	.010	.008 .003 .007	.009 .003 .007 .010		.006 .007 .006 .007	.002 .001	.005	in. in. in. in.	
	.011 .011	.011	.011	.010 .010	.007	.017		.006 .007	.no	.005	in. in. win/in	
	.011 .011	.011	.011	.010	.007	.017		.077	.m	1.001	in.	
	•011	•011	•011	•010	.278	.010		.077	.m	1.001	win/in	
	•006					1744				1 11		
	.006											1
•	.006			ITIM								
		.006		.006	ורח	205	.004	.001.			in.	
100									.002			
	•012						•1000		• 302	.007		
		•009		•		•001		•100	1.	•0.1		
									- 4		MAII/ LII	
.00h			•075	.006							in.	
.007	.008	.008	•029						•006			
.007							.010	.011			in.	
.006	.008	.006							.020	.016	in.	
.073	.105								•		in.	
· noli			.006		•203	.0011	.003	.003			in.	
4	36	11		15			2	5			win/in	
26	1,4	49		45							win/in	
											sin/in	
									5		Ain/in	
				ITEM I								
	-010					-016	-010	.015	.018	.018	in.	
-01,0		.030									in.	
	.007 .006 .003 .001 .010	.0014 .0014 .007 .008 .007 .008 .006 .008 .003 .005 .0014 .006 .005 .006 .006 .006 .006	.007 .008 .008 .007 .006 .008 .006 .003 .005 .005 .004 .006 .005 4 36 11 26 49	.001 .006 .009 .009 .007 .007 .007 .006 .008 .006 .006 .003 .005 .005 .006 .006 .005 .005 .006 .006 .006 .006 .006 .006 .006	.001 .002 .006 .006 .009 .008 .001 .001 .009 .008 .001 .001 .005 .005 .005 .006 .006 .008 .006 .006 .006 .003 .005 .005 .001 .001 .001 .006 .005 .006 .006 .003 .005 .005 .001 .001 .001 .006 .005 .006 .006 .003 .005 .005 .001 .001 .001 .006 .005 .006 .006 .003 .005 .005 .006 .006 .006 .006 .006 .006 .007 .007 .007 .010 .030 .030 .022 .022	.001 .002 .006 .006 .009 .008 .0014 .0014 .005 .005 .006 .006 .007 .008 .008 .009 .009 .009 .006 .008 .006 .006 .006 .006 .003 .005 .005 .0014 .0014 .003 .0014 .006 .005 .006 .0014 .003 .0014 .006 .005 .006 .0014 .003 .0015 .005 .006 .0014 .003 .0016 .006 .005 .006 .0014 .003 .0017 .007 .007 .0010 .0010 .0010 .002 .0010 .0010 .0010 .002	.001 .002 .002 .002 .005 .006 .005 .009 .008 .007 .008 .007 .008 .007 .008 .006 .006 .006 .006 .006 .006 .008 .008	.001 .002 .002 .002 .006 .006 .005 .009 .008 .007 .008 .007 .008 .007 .008 .007 .008 .007 .008 .008	.001 .002 .003 .003 .004 .006 .006 .004 .009 .008 .007 .006 .009 .008 .007 .006 .001 .004 .005 .005 .006 .006 .001 .006 .007 .008 .008 .009 .009 .010 .011 .011 .011 .011 .007 .006 .008 .006 .006 .006 .006 .006 .006	.001 .002 .003 .003 .004 .006 .009 .008 .007 .006 .009 .008 .007 .006 .006 .009 .008 .007 .006 .006 .001 .006 .003 .007 .008 .008 .009 .009 .010 .011 .011 .011 .011 .006 .007 .007 .008 .008 .006 .006 .006 .006 .006 .006	.001 .002 .003 .003 .007 .006 .004 .004 .004 .009 .008 .007 .006 .001 .006 .001 .001 .001 .001 .001	.001 .002 .002 .003 .007 in006 .006 .006 .005 .004 .004 in009 .008 .007 .006 .001 .001 ir.

^{*}See table B1 for gage identification system.

PEAK VALUES OF SLOWLY MOVING 22,500-LB SINGLE-WHEEL-ASSEMBLY LYSTRUMFNTATION TESTS

						LAND				a particular			
GAGE*	WEST	LIST	WEST	EAST	WEST	EAST	WYST	HAST	UTST	FAST	WIST	EAST	UNITS
						ITEM :							
1DEJT	.008	.008	.013	.011	.013		.014	.0Ui	.011	.014	.008	.nn8	in.
1DNJT	300.	.008		.208		.008	.008		.008		30C.	.008	in.
1DNJL	.022		.019	.020	.019			.013	.012	.010	.002	.002	in.
TDC				.016					,008	7,00	JCO.		in.
13PD	.005	.005		.007	.005	.005	·m	.001	·m4	.003			in.
15PD	.023			.016		.013	.228	.009		.078	.002	.001	in.
19PD	.013		.711	.012	.012		.012			.010	•002	.702	in.
						TEM 2							
DNJL	.010	.012	•209	.010		.008	.006	.008	.005	.006	.001	•200	in.
2DSJL	.015	.010	.018		.113	.010	.015	.008	.012		.001	.002	in.
S DC					- 177 -	.002		.nol		.008		.014	in.
23.PD		.008		.010		.008		.007		.006		.001	in.
25PP		.008		.011		. 206		.011		.005		.001	in.
PPD		.011		.013		.011		.010		.008		.002	in.
SSJL			38				26		19				sán/i
					I	TEM 3		Jal					
DEJT	.006	•205	.007	.507	•007	.008	300·	.008	. 709	.002	-00h	. 201	in.
DWJT	.711		.013		.014	·Cli	·OU	.715	.215	.016	80c.	.008	in.
BISJL	.010		.010			.009	.008		800.		-00L	.002	in.
3IC	.006				. 203	.003	.004	. 201	1000		.009	.010	in.
33PD	.004	.005	.007	.207	.225	.006	.775		.004	.ool	114	.001	in.
35PP	.076	.006	.008	300.	.007	.006	.006	.226	.005	.005	-		in.
SEJT	8	8	8	8	6	6	4	3	2	3			min/in
3SNJL	1,5	34					-						uin/in

^{*}See table B1 for gage identification system.

TABLE B5
TWIN-TANDEM-ASSEMBLY STATIC TESTS

GAGE*	POSITION	15,000-16 WHEEL LOAD	22,500-1b WHEEL LOAD	POSITION	15,00 WHEET	LCAD	22,500-1b WHEEL LOAD	UNITS
		ITEN 1	LOCATION -	GAGE DC				
1DEJT	1	.000	.002	2	.03	0	.000	in.
1DWJT		.007	.003		.00	4	.002	in.
1DNJL		.008	.010		.01		.013	in.
1SEJT		6	8			3	5	Pin/in
1SCL		21	34		2	9	10	Vin/i
1SCT		52	5		1		11	Pin/ii
1DEJT	. 3	.000	.007	4	.00	0	.004	in.
1DWJT		.001	.001		.00	1	.001	in.
1DNJL		.006	.010		.01	1	.017	in.
1SEJT		3	11			5	0	Pin/in
1SCL		19	16		1		38	Min/in
1SCT		7	13			8	3	Rin/i
1 DEJT	5	.000	.055	6	.00		.053	in.
1DWJT		.042	.062		.04		.061	in.
1DNJL		.013	.015		.01	3	.016	in.
1DC						er uld	.608	in.
1SEJT		19	46		1	7	38	µin/i
1SWJT					10-1			µin/i
1SNJL		1	1		70.70	- 1		µin/i
1SSJL			2				6	µin/i
1SCL		6	6			4	19	pin/ii
1SCT		13	24		1	4	38	µin/ii
1DEJT	7	.000	.054	8				in.
1DWJT		.041	.060		.04			in.
1DNJL		.015	.024		.00		•	in.
1DC					.00	3		in.
1SEJT		23	23		2			pin/i
1SCL		1	5		1			uin/ii
1SCT		16	22		3	1		µin/i

^{*} See table Bl for gage identification system.

TABLE B5 (Continued)

GACE*	POS'TICH	15,000-1b WHEEL LOAD	22,500-1b WHEEL LOAD	POSITION	15,000-1b WHIZEL LOAD	22,500-1h WHEEL LOAD	UNITS
		ITEM 1	- LOCATION	GAGE DSJL			
1DEJT	10	.001	.005	11			in.
1DWJT		.006	.010		.002	.003	in.
1DNJL		.039	.049		.036	.051	in.
1SEJT		2	3		3	8	Vin/in
1SCL		11	8		3	7	Pin/in
1SCT		20	0		8	7	Pin/i
1DEJT	12	.000	.004				in.
1DWJ%		.005	010				in.
1DNJL		.045	.066				in.
1SEJT		17	7				µin/ii
1SCL		16	9				Pin/i
		ITEM :	1 - LOCATION	GAGE 13PD			
13PD	10	.010	.012	- may any			in.
15PD		.006					in.
19PD		.038	.050				in.
		ITEM :	L - LOCATION	GAGE 15PD			
13PD	10	.009	.014	H. T. T.			in.
15PD		.004					in.
19PD		.032	.058				in.
		ITEM :		GACE 19PD			
13PD	10	.008	.015	paran will			in.
15PD	119	.004					in.
19PD		.041	.058				in.

Dann 2 of

TABLE B5 (Continued)

GAGE*	POSITION	15,000-1b WHEEL LOAD	22,500-1b WHEEL LOAD	POSITION	15,000-16 WHEEL LOAD	22,500-1b WHIEL LOAD	UNITS
		ITEM 2 -	- LOCATION G				
2DEJT	1	.004	.006	2	.006	.004	in.
2DWJT		.001	.015		.000	.003	in.
2 DNJL		.005	.006		.008	.001	in.
2DSSL		-	.010		-	.003	in.
2DC		-	.019		-	.018	in.
2SEJT		0	1		0	2	µin/in
2SWJT		-	-		0	2	Pin/in
2SNJL		11	21		-	11	Pin/in
2SSJL		19	15		19	32	Win/in
2SCL		25	32		16	19	Vin/in
2SCT		26	24		24	31	Pin/in
2DEJT	3	.003	.008	4	.001	.010	in.
2DWJT		.005	.030		.000	.040	in.
2DNJL		.005	.015		.010	.010	in.
2DSJL		.008	.010		_	.015	in.
2DC		.026	.017		-	.018	in.
SEJT		0	1		0	1	µin/in
2SWJT		0	0		0	1	Pin/in
2SNJL		10	6		1	14	Pin/in
2SSJL		10	14		23	30	µin/in
2SCL		16	26		53	29	µin/in
2SCT		22	26	à	16	33	µin/in
		ITEM 2 -	LOCATION	GAGE DWJT			
2DNJL	5	.014	.015	6	.012	.018	in.
2DSJL		.013	.016		.013	.018	in.
2DC		.006	.007		.006	.005	in.
2SNJ!		15	13		34	20	µin/in
2SSJL		1	13		13	11	µin/in
2SCT		8	5		12	1	µin/in
2SCL		27	12		10	4	µin/in
2DNJL	7	.017	.025				in.
2DSJL		.017	.024				in.
2DC		.005	.003				in.
2SNJL		12	27				uin/in
2SSJL		11	15				µin/in
2SCT		0	6				µin/in
2SCL		16	3				µin/in
2SEJT		0	2				µin/in

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TABLE B5 (Continued)

GAGE*	POS)TION	15,000-16 WHEEL LOAD	22,500-1b	POSITION		22,500-1b WEEEL LOAD	UNITS
		ITEM 2	- LOCATION	GAGE DS.'L			
2DNJL	10	.027	.039	11	.030	.044	in.
2DSJL		.026	.039		.029	.042	in.
2DC		.008	.008		.010	.012	in.
2SNJL		20	78		14	30	µin/in
2SSJL		34	32		19	10	µin/in
2SCI.		6	14		13	15	uin/in
2SCT		9	9		20	9	µin/in
2DNJL	12	.035	.050				in.
2DSJL		.030	.044				in.
2DC		.004	.005				in.
2SNJL		38	20				pin/in
2SSJL		27					µin/in
2SCL		46	66				uin/in
2SCT		9	15				µin/in
		ITEM 2	- LOCATION	GAGE 23PD			
23PD	10	.016	.035				in.
25PD		.022	.020				in.
29PD		.032	.049				in.
	to Ta	ITEM 2	- LOCATIO	N GAGE 25PD			
23PD	10		.022				in.
25PD		.020	.055				in.
29PD		.033	.030				in.
		ITEM 2	- LOCATIO	N GAGE 29PD			
23PD	10		.038				in.
25FD		.019	.007				in.
29PD		.035	.049				in.

TABLE B5 (Continued)

SV CEN	POSITION	15,000-1b 2 WHEEL LOAD W		POSITION		22,500-1b D WHEEL LOAD	UNITS
		ITEM 3 -	LOCATION	GAGE DC	. 1		
3DEJT	1	.002	.003	2	.003	.003	in.
3DWJT		•003	.005		.006	.005	in.
3DSJL		.002	.002		.003	.008	in.
3DC		.022	.027		.021	.027	in.
3SEJT		3	5		7	-	Pin/in
3SNJL		8	12		9	6	Vin/in
3SCL		1	4		15	4	· Pin/in
3SCT		8	5		15	3	Pin/in
3DEJT	3	•003	.001	4	.004	.004	in.
3DWJT		.004	.002		.006	.008	in.
3DSJL		.001	.001		.009	.010	in.
3DC		.022	.026		.021	.029	in.
3SEJT		6	7		2	9	Vin/in
3SNJL		3	8		6	12	Pin/in
3SCL		7	5		6	4	µin/in
3SCT		14	-		21	4	µin/in
		ITEM 3 -	LOCATION	DWJT			
3DEJT	5	.030	.034	6	.027	.033	in.
3DWJT		.021	.024		.020	.044	in.
3DSJL		.009	.008		.008	.010	in.
3DC		.009	.012		.007	.011	in.
3SNJL		0	0		1	3	Pin/in
3SCL		10	_		4	-	Pin/in
3SCT		9	-		14	-	Pin/in
3DEJT	7	.028	.033	8	.033	.040	in.
3DWJT		.020	.024		.020	.027	in.
3DSJL		.012	.012		.008	.010	in.
3DC		.006	.009		.006	.009	in.
3SNJL		7	6		5	8	µin/in
3SCL		7	_		5	-	Win/in
3SCT		11	-		14	-	µin/in

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TABLE B5 (Continued)

GAGE*	POSITION	15,000-15 2	2,500-1b	POSITION	15, 00-16 WHEEL LOAD	22,500-1b	UNITS
		A Commence of the Commence of	LOCATION	GAGE DUJT	THE COURT OF		
3DEJT	9	.035	.039				in.
3DWJT		.022	.026	TANK			in.
3DSJL		.010	.007				in.
3DC		.004	.009				in.
3SNJL		8	9				Vin/ir
3SCL		5					Pin/ir
3SCT		10	$A_{\sigma_{i}}$				Pin/in
			LOCATION	GAGE DSJL	07 -4 (0.7)		
3DEJT	10	.006	.010	11	-004	.004	in.
3DWJT		.006	.007		.003	.005	in.
3DSJL		.018	.050		.017	.019	in.
3DC		.009	.014		.009	.013	in.
3SNJL		22	29		15	13	Vin/in
3SCL		8	11		5	16	uin/in
3SCT		7			3	21	pin/in
3DEJT	12	.006	.008				in.
3DWJT		.005	.007				in.
3DSJL		.018	.023				in.
3DC		.006	.010				in.
3SNJL		22	33				µin/in
3SCL		11	16				µin/in
3SCT		16	16				Pin/in
		ITEM 3	- LOCATION	N GAGE 33PD			
33PD	10	.010	.017				in.
35PD		.023	.050				in.
		ITEM 3 -		GAGE 35PD			** 1
33PD	10	.012	.015				in.
35PD		.021	.028			/	in.

TABLE B5 (Concluded)

CACE*	POSITION	15,000-1b 22,500-1b 22,500-1b WHEEL LOAD WHEEL LOAD	POSITION	15,000-16 22,500-16 WHEEL LOAD WHEEL LOAD	UNITS
		ITEM 4-LOCATION	GAGE DC		
4DNJL	1	.014	2	.013	in.
4DSJL		.026		.047	in.
4DNJL	3	.014	4	.002	in.
4DSJL		.020		.028	in.
		ITEM 4- LOCATION	GAGE DSJL		
4DNJL	10	.127	11	.147	in.
4DSSL		.081		.093	in.
4DNJL	12	.146			in.
4DSSL		.080			

TABLE B6

PEAK VALUES OF SLOWLY HOVING TWIN-TANDEN-ASSEMBLY
INSTRUMENTATION TESTS

15,000 lb/wheel

					77.6	La	ne	V ·					
GAGE*	WEST	EAST	WEST	EAST		E.JT		EAST		FAST	WEST	LAST	INITE
				1				ALC:				, IEEE	
						LTE							
1 DUJT		.050		.080		.056		.060		.060	.042	.040	in.
1DNJL		.010		.008	.008	0.440.05HB1850.0	.004			.074		•	in.
1DC		.012	胆- 湖	.012		.016	.012			.010	.006	.006	in.
13PD		.008		.010		.008		LUMBER OF STREET		.004	-	• /	in.
19PD	.030	.020		.024	.026	.020		.016		.016	.006	.006	in.
1 SCL							2	2	2	2	4	4	µin/i
						ITEM	1 2						
2DEJT	.015				.016		.012		.010		.005		in.
2DWJT	.020		.064		.024		.020		.016		.008		in.
2DNJL	.008		.004		.012			.014	-	-	.008	4.41	in.
2DSJL	.030			-	.020	-	.030		.024	haliro	.008		in.
2DC			.012						-		.004		in.
2 3PD			.008						-				in.
25PD	.036												in.
29PD	.008		.028		_								in.
SNJL		21		16		21		21		11			uin/i
2SSJL		42		125		105		105		84.0		8	uin/2
2SWJT			29				57						µin/i
2SCT		11				21		21		42		16	µir./1
2P11		.6		.4		.5		.3		.3			psi
2P41		.3		.3		.1				.1			psi
2P51		.5		.6		.5		.3		.3		.1	psi
						ITE							
3DEJT	.014	.015	.016	.020	.022	.020		.020	.620	.020	.016	.014	in.
3DWJT		.016	.030		.030			.016		.016	.020		in.
3DSJL		.010		.010	.020			.010		.006	.004		in.
3DC		.004		.004	.008		.010			.006		.008	in.
33PD		.004		.006	.010		.004						in.
35PD	.012	.010		.010		.006	.010	.010	.008	.004	.004		in.
3SEJT		-	105	21	21	42	42	42	21	21	-		uin/i
3SWJT			42			_	11200						µin/i
3SNJL	4	4		4									µin/i
LDNJL	•140	.128	.106	.106	-082	.078	.066	062	.056	nd.	.010	.010	in.
LDSJL	.072	.066	.076			.058	.048	0.1.	.070		.008	.008	in.
	•015	.000	.070	•01.	•020	•020	·odo	• 044	.072		.124	.118	in.
PDC.									.012	.010	•124	.110	

^{*}See table B1 for gage identification system.

TABLE B7.

PEAK VALUES OF SLOWLY MOVING TWIN-TANDEM-ASSEMBLY
INSTRUMENTATION TESTS

22,500 lb/wheel

1					22,500		ida'T		40.000			- enteres : Nove se	
GAGE*	VEST	EAST	WEST	EAST	WEST	EAST	WEST	EAST	WEST	EAST	WEST	6 EAST	UNIT
						_1TE	м 1			+			
1DEJT	.095	.100	.060	.035		.050		.050	.050	.050	.025	.025	in.
1DWJT		.080	.072			.075	0.79.000	.080		.080	.040		in.
IDSJL		.075	.048		-		-	_		-	.030		in.
IDC					-	70.4	.010			.005	-		in.
13PD	.015	.015		.010				.010		.010			in.
9PP		.035		.025		.035		.020		.020	.005	.016	in.
STAT											15		pin/i
SNJL			18								20		uin/i
ISSJL			38								38		uin/i
SCT			54								73		µin/i
						ITE	M 2						
DEJT	.065		.092		.050		.020				.010		in.
DWJT	.050		.124		.075		.030				.010		in.
DNJL	.020		.020	17.12	-		.020					.056	in.
DSJL	.070		_		-		_				-	.112	in.
DC					.010		.025						in.
3PD			.028		.020		.020				.010		in.
SPD			-		-		.020				.020		in.
9PD			.072		.025		.010				.030		in.
SEJT			18		.023		.010				18		uin/i
SNJL		16	10	11		11		5		8	10	11	uin/i
SSJL		11		16		11		5		11		STATE OF THE STATE	pin/i
SCT								3				5	
P11		.3		.4		3				.4			µin/i
						.6		.4				.4	psi
P41 P51		.1		.3		.3		.1		.3			psi
7P13		.7		.6		.6		.6		.6		.5	psi
1113				.4									psi
	010		010	040			M 3						
DEST		.085		.060		.035		.025		.015		.020	in.
DWJT		.040		.070	.040	.035		.020		.020	.056	.020	in.
DSJL	.030	.010		.020		.010		.010		.010	.052	-	in.
DC		-	-	005	000	.010		.005		.015	.015	.015	in.
3PD		.010	.028	.005	.020	.005	.005	.005	.005	.005	.010		in.
19PD		44	.010		131	2					.010		in.
SEJT		26	131	17			- 5	5	- 5	11			uin/i
SWST		45.	102		79	, 80,541				1994	42		uin/i
SNJL			13								15		uin/i
SCL			2		4-1						21		uin/i
SCT			16								42		uin/i

^{*}See table B1 for gage identification system.

TABLE BS

ACE+	POSITION	15,000-1b WHEEL LOAD	22,500-1b WHEEL LOAD	POSITION	15,000-16 WHEST, LOAD	22,500-16 WIEEL LOAD	UNITS
		ITEM 1	-LOCATION	GAGE TWIT			
1DEJT	1	•000	•000	2		.000	in.
LIWJT		.011	.032		.011	.032	in.
LDNJL		•000			•000		in.
ldsjl			.020		SHE Alles	.010	in.
100		.000	.005		.000	.007	in.
נקנו			.001		• /	.003	in.
1ECL		וע			12		Mn/i
			-LOCATION	GAGE DNJL			
1DEJT	3	.038	•000	14	.038	•200	in.
LIWIT		•000	.008		•000	.117	in.
1DSJL			.010			.000	in.
ILC			.007			.007	in.
13PD			.001			•000	in.
15PD			.010			.000	in.
155JL		5			3		win/s
LSWJT		10			8		win/i
LSCL		6			3		win/i
		ITEM 1	-LOCATION	GAGE DSJL			
1DEJT	5	•006	•000	6	.038	•100	in.
1DMJT		.006	.008		.030	.011	in.
1DSJL			.000			.010	in.
IDC			.009			•009	in.
13PD		.003	.003		•006	•00h	in.
15PD		•007	•000		.007.	•000	in.
lsnji.		1				. 0	win/i
lssjl		0				1	win/i
LSWJT		2 2				1	Min/i
LSCL		2				0	Min/i
		ITEM 1	-LCCATION	GAGE IC			
ldejt	7 /	.011	•026	8	.033	.026	in.
ldwjt		•no8	.013		.027	.030	in.
IDSJL			•017			•011	in.
ic			.033			.033	in.
13PD		.00h	.015		.005	.015	in.
15PD		•007	•000		.007	.000	in.
LSNJL		1			1		Min/i
ISSJL		1			1		Ain/i
LSWJT		2			2		win/s
LSCL		13			23		win/i

^{*}See table Bl for gage identification system.

TABLE 88 (Continued)

GAGE*	POSITION	15,000-16	22,500-16 WHEEL LOAD	POSITION	15,000-1b WHEEL LOAD	22,500-16 WHEEL LOAD	UNITS
		ITEM 2 -	LCCATION	GAGE INJT			
SDEJT	1	.011		2	•077		in.
2DNJT		.715				.060	in.
2DNJL		.012	.069			•003	in.
21°C		.014	•031		•079	.010	in.
23PD			.021			.021	in.
25PD			.010				in.
?SCL		1.6			1.5		min/in
2SHJL		0	2		0	2	min/in
2SCT		•	2 4			1 ·	min/in
		ITEM 2 -		GAGE POJI			
2DFJT	2	.01/	•000	la la			in.
2DWJT		•000	•227				in.
2DNJL		.019			.013	.067	in.
2DSJL		.010	.021		•228	.023	in.
2DC		.018	.041			.Oll	in.
23PD			.029			•022	Lil.
2SCL		1			1		win/in
2SNJL		0	1		3	1	win'in
2SSJL		0 5 3	0 8		3	3	sein/in
2SCT		3	8		2	3	win/in
		ITEM 2 -	LCCATION	GAGE ISJI			
TLWIS	5			6		.006	in.
SDNJL		.01:6	.102		.041	.102	in.
SDSJL		.047	·05F		.743	.025	in.
SDC			·0h1			.Oli1	in.
23PD		.010	.033		.01/1	.047	in.
25PD		•007			.007		in.
SECT		3					win'in
2SNJL		1	2		0	1	Min/in
2SCT			17			17	win/in

TABLE B8 (Continued)

CACE*	POSITION	15,000-1b WHEEL LOAD	22,500-1b WHEEL LOAD	POSITION	15,000-1b WHEEL LOAD	22,500-16 WHEEL LOAD	UNITS
		ITEM 2	LOCATION	GAGE 2DC			
2DZJT	7	001	•050	3	.000	•032	in.
2DWJT			.019			.719	in.
SDINL		.729	.031		.721	.040	in.
2DSJL		.031	.031		.025	.030	in.
SDC			.009			.020	in.
23.90		.012	.006		.013	•006	in.
25PD		.007	.020		.007	.020	in.
2SCL		3			3		win/i
2SCT			9			21	win/i
		ITEM 2-	LOCATION	GAGE 2DC			
2DEJT	9			10	.018		in.
2DNJL		.042			.739		in.
SDSJL		.022			.022		in.
23PD		.018					in.
2SNJL		6			6		win/s
2SCT		6			4		#in/i
		ITEM 2	- LOCATION	GAGE 2DC			
2DEJT	11	.001		12	.002		in.
2DNJL		.024			.021		in.
SDS-JL		.025			.025		in.
SECT.		3			3		win/s
		ITEM 2	-LOCATION	GAGE 2DC			
2DEJT	13	.001		14	.001		in.
SDNJL		.025			.026		in.
2DSJL		.029			.029		in.

TABLE B8 (Continued)

GAGE*	POSITION	15,600-16 WHEEL LOAD	22,500-1b WHEEL LOAD	POSTTION	15,000-16 WIEEL LOA	22,500-1b D WHEEL LOAD	UNITS
		ITEM 3	-LOUSTION	CAGE DUJT			
3CtJT	1	.025	.03/4	2	.032	.040	in.
3UWJT		,005	.015		400.	.015	in.
3DEJL			.015			.008	in.
30.		.023	.Oh1		.015	.031	in.
33FD		San Park Street	.013			ollo.	in.
35kJT		2 2 5			2		nin/in
3SNJL		3			2 3		min/in
35CL		,			3		win/in
			-LOCATION	GACE DEJL			
3LEJT	3	.004	.013	Į;	.036	.0314	in.
3TWJT		.011	.006		.003	.016	in.
3DCJL			.013		eic. Vit Blitte	.014	in.
310		.028	.061		.024	.061	in.
33PD			.013			.007	in.
35.4JT		2			2		win/in
3SNJL		17			3		win/in
3SCL		17			12		adn/in
		ITEM 3	-ICCATION	GAGE LCJL			
3DEJT	5	.013	•003	6	.049	.036	in.
3DWJT		.011	.205		.030	.015	in.
3DSJL			.ગાા			.015	in.
31°C			-041			.041	in.
33PD		.016	.013		.019	•007	in.
35PD		.007			•006		in.
35%JT					2		uin/in
33CL		11			9		win/in
3SCT		3			3		.cin/in
		ITEM 3	-LOCATION	GAGE DC			
3DEJT	7	.007	.021	8	.021	.042	in
3FWJT		.016	.019		.032	.026	in.
3DSJL			.0.16			.018	in.
3DC			.020			.023	in.
33PD		•003	.024		·nou	.024	in.
35PD		•006			.002		in.
3SEJT		1			11		win/in
3SCT		15			22		win/in

Page 4 of 5

TABLE B8 (Concluded)

GAGE*	POSITION	15,000-1b 22,500-1b WHEEL LOAD WHEEL LOAD	POSITI ON	15,000-1b 22,500-1b WHEEL LOAD WHEEL LOAD	UNITS
		ITEM 4 - LCCATION	CAGE DSJL		
LIC	3	.011	4	•007	in.
LOSJL		.042		·143	in.
1-EWJT		•008		.009	in.
		ITEM 4 - LLCATION	CAGL DEJL		
lide	5	.003	6	.006	in.
LIDSJL		.040		·042	in.
hDaJT		•007		•2006	in.
		ITEM 4 - LCCATION	GAGE DC		
4DC	7	•014	5	.015	in.
LISJL		.019		.021	in.
IDWJT		•001		.005	in.

TABLE B9
PEAK VALUES OF SLOWLY MOVING 12-WHEEL-ASSEMBLY
INSTRUMENTATION TESTS
15,000 1b/whee1

				-		-	ane		Walley Co.				
		1		2		3		4		5		6	
CACE*	WEST	EAST	WEST	EAST	WEST	EAST	WEST	EAST	WEST	EAST	WEST	EAST	UNITS
							M1						
1DEJT	.06r	.060	.060	.060	•060	.060		.060	.060			.010	in.
1DWJT	.068	.068	.068		.064	K-1000000000000000000000000000000000000	.063			.054		.009	in.
1DNJL	.038	.038	.038		.030	.038	.030	.030	.032		.030		in.
1DC	.074	.074	.074	.071	.079	.074	079	.079	.081	.079	.081		in.
15PD	.010	.007	.008	.007	.007	.007	.007	.007	.007	.007	.007	.007	in.
1SEJT										-		21	µin/i
1SWJT	40	40	40	40	40	40	40	40	40	40	59	38	uin/i
1SNJL	81	81	81	81	83	81	83	83	79	79	83	51	uin/i
1SSJL	-	53				53		4		53	-	53	uin/i
1SCL	65		65	65	65		65	65	65	65	65		uin/i
1scr	65		65	65	65		65		65	26	65	26	µin/i
						ITI	M 2						
2DEJT		.010		.010		.010		.010					in.
2DNJL	.031		.029		.026		.025		.025		.056		in.
2DSJL	.057		.052		.011		.045		.043		.041		in.
2DC		.033		.031		.043		.043		.040		.050	in.
23PD				.001		.001		.004		.013		.013	in.
25PU		.007		.007		.007		.007		.007		.007	in.
SCL		23		23		23		23		23		23	uin/i
2SCT	2		2		2		2		2		2		uin/i
2SNJL	11		10		2		8		7		9		uin/i
2P11	2		2		2		2		7		1		psi
2P13		1	4-1	1		1		1		1		1	psi
2P44	.5		.5		.5		.4		.5		.5		psi
2P54											.8		psi
23P13		1		1		1		1		1		1	psi
27213		.2		.2		.7		.3		.2		.2	psi
27P23	.2		.2		.7		.7		.7		1.7		psi
						_ITE	M 3						
3DEJT	.033	.033	.034	.033	.033	.033	.033	.032	.032	.032	.056	.029	in.
3DWJT	.024			.023	.022			.022				.014	in.
3DNJL	.063	.059	.059	.057	.052			.052	.050			.054	in.
3DC	.029	.026	.029	.024	.024	.017		.012	.021		.019	.019	in.
3PD	.007	.005	.005	.005	.005	.005	.005	.003	.010	.010	.010	.009	in.
39PD	.012	.012	.012	.012	.012	.002	.011	.002	.012	0	.002	.002	in.
SEJT	61		57	59	59	59	62	61	42		66	42	utn/in
SSJL	117		117	117	117	117	117		119	119	119	119	uin/i
SCL	198		202	208	205	208	208		198	208	205	208	uin/i
SCT	78		78	78	78	78	78		78	72	78	78	uin/in
						ITE	M 4						
DC	.130	.115	.088	.115	.040	.026		.014	.030	.026	.035	.034	in.
DSJL		.023	.008		.018		.018		.022		.013		in.
DWJT		.096		.096	.050		.070		.049		.060		in.

^{*}See table B1 for gage identification system.

TABLE B10
PEAK VALUES OF SLOWLY MOVING 12-WHEEL-ASSEMBLY
INSTRUMENTATION TESTS
22,500 1b/wheel

						Len							
GAGE*	WEST	EAST	100	EAST	WEST	EAST	WEST	EAST	WEST	EAST		EAST	LINITE
1DEJT		.049	027	.025	025	.025	.025	025	026	006	.026		
						.025				.026		007	in.
1DWJT	.005		.007		.005		.009	.009		.011	.011	.007	in.
1DSJL	.014			.013	.019	ATTACHMENT OF		.013		.015	.012	.014	in.
1DC	.002		0	0	.002	0 .	.002	.002	0	.005	.005	0	in.
1 3PD	.009			.021	.023	.022	.022	.022		.021	.021		in.
19PD	.048	W. St. W. William	.036	.036	.036	.024	.018	.016	.008	.004	.002	0	in.
1SNJL	2	2	2	2	2	2	2	2	2	2	2	2	uin/in
1SSJL		•			-				-			57	µin/ir
1SCL		-				-	V 3.0		•	•	•	68	µin/ir
1SCT		•						•		•		10	pin/ir
						11	EM 2						
2DEJT		.052		.042		.040		.038		.036		•	in.
2DWJT		.002		.002		0		0		.002		0	in.
2DNJL	.052		.027		.027		.027		.027		.027		in.
2DSJL	.045	.011	.038	0	.029	0	.029	0	.025	0	.036	0-110	in.
2DC		.024		.017		.005		.002		0		.005	in.
23PD		.015				-		-					in.
29PD		.058		.048		.034		.034		.030		.024	in.
2SEJT		15		15		15		15		15		15	uin/ir
2SSJL	40		64		59		51		49		44		uin/ir
2SCL		120		120		120		120		120		120	uin/ir
2SCT	. 16		20		26		26		26		29		uin/ir
2P34	.8		.8		.8		.8		.8		.8		psi
2P42	1.3		1.3		1.4		1.4		1.4		1.3		psi
27P13			1.3									1.3	psi
2/173													Por
					7		EM 3						
3DEJT	100 - 100 II - 100 TO TO TO TO TO TO TO TO TO TO TO TO TO	.044		.042		.041	.040	.039		.035	.035	•	in.
3DWJT	.050	TO DOMESTIC	2.20	.052	.050	.048		.045	.048		.036	.036	in.
3DSJL		.021		.009	.019	.019		.018		.017	.015		in.
3DC	.024			.021	.021	.020	.017		.017		.012	.010	in.
33PD	.043	.040	.037	.011	.014	.039	.036	.037	.037	.036	.036	•	in.
35PD			-				-			•		.032	in.
39PD		-	•	YEARS				-			•	.006	in.
3SNJL	38	38	38	38	38	38	38	38	38	38	38	38	µin/in
3SSJL	34	34	34	34	34	34	34	34-	34	34	34	34	uin/in
3SWJT	1	1	0	0	2	2	2	2	0	0		3	uin/in
3SCL	65	62	68	65	65	65	85	81	75	72	94	81	uin/in
3SCT	9	9	10	12	13	13	14	14	14	16	17	19	uin/in

^{*}See table B1 for gage identification system.

TABLE B11
6-WHEEL-ASSEMBLY STATIC TESTS
22,500 lb/wheel

GAGE	PCSITI	CN .	PESIT	CN	POSITI	CIL	PUSITIO	CAT .	U'IIIS
THE	æ			/ ^B .	ITEM 1		•		
11EJT	2	.040	l.	.040	6	.040	3	oik.	in.
IDSJL		.071	LF 13	•002		.000		•992	in.
IDC		.003		•003	•	•073		cuo.	in.
ISEJT				1		1		1	adn/i
LSWJT		1				7			min/i
LSNJL		3		3		_		3	nin/i
ISSJL		6		3		5 6		6	n'i
ISCL		6		6		ó		7	uin/i
LSCT		3 6 6 2		6		1		2	uin'i
					ITIM 2				
PILJT	2	.040	14	.040	6	- Olio	8	cuc.	in.
2DSJL		.017		.027		•		.020	in.
DNJL				.704				.001	in.
2DC		.201		.005		•002		.005	in.
SWJT		1		.0.75		• 50 E		í	win/i
SSJL				7				6	win/i
2SCL		4		2		2		Ĭ,	uin/i
SCT		2		í		1		2	udn/i
PDEJT	10	.004	11	.201	12		13	. 224	in.
PDSJL	10	.026	11	.021	75		1)	.021	in.
		.020		.060				.050	in.
SIC								•002	in.
23PD		•003		•002					Min/i
SWJT	ń –	6		2		6		2	uin/i
2SSJL						0			
SCL		3 2		4		-		4 5	uin/i
2SCT		2				•		>	#in/i
					ITEM 3				
3DEJT	2	.030	4	•	6	.013	8	015	in.
3DSJL		.010		•		.060		.020	in.
300		.007		- 149		•006		.020	in.
33PD		•०ग्रा				.013		•018	in.
35PD		•017		.021		.021		.023	in.
SSNJL		1		1		1		1	uin/i
3SSJL		6		6		2		2	Min/i
3SCL				6		6		6	Adn'i
3SCT		15		15		15		15	win/i

^{*}See table B1 for gage identification system.

TABLE B12
PEAK VALUES OF SLOWLY HOVING 6-WHEEL-ASSEMBLY
INSTRUMENTATION TESTS
22,500 lb/wheel

							LANDS	Ł	T				
GAGE*	TIST	1 USI	912-51	5 ST 21	J) 155y	3 1 EAST	Plasy	TAY21	resi	5 PAST	Wife's	6 EAST	UNITS
					THE PARTY OF THE P	TEH 1							
1DEJT		.026	.026	.026	.026	.026	.026	.026	.026	.026	.026	.026	in.
1DSJL		.018	.058	.028	.058	.053	.056	.050	.058	.058	.056	.056	in.
1370		.017	.017	.017	.017	.017	.017	.017	.017	.017	017	.017	in.
ISEJT	2	2	2	2	2	2	2	2	2	2	2	2	Akn'in
ISNUL	27	27	27	27	. 27	27	27	27	27	27	27	27	min/in
ISCL	46	1,6	46	42	42	1,6	75	42.	37	42	142	42	min/in
1SCT	7	7	6	6	3	4	3	5	2	3	2	2	win/in
					\	ITEH 2							
2DEJT		.022		.022		.029		.030		.030		.022	in.
2DWJT		.035	.035	.035	.035	.035	.035	.035	.035	. 235	.035	.035	in.
2DNJL	.027	•0,	.029	,	.027		.016		.029		.028		in.
2DSJL		.074		.068		.060		.056		.052		.042	in.
2DC		.014		.009		.012		.007		.007		.005	in.
23PD		.046		.046		.041		.038		.047		·043	in.
2SEJT		n	11	11		11		11		11		n n	un/in
25%JT 25SJL	17	13	17	13	17	13	17	13	17	13	17	13	win/in win/in
2P34	17		7		7		6	-	2				psi
2P44					2				i		3		psi
27P13		-2		-2		-2		-2		-2		-2	pei
27P23	-0.3		-0.3		-0.3		-0.3		-0.3		-0.3		psi
						CEM 3							
3DEJT	.057	.057	.057	.056	.055		.054	.053	.052	.052	10	.049	in.
3DSJL		.024	-057	.024	.022	.022	.022	.022	olio	.018	.016	.016	in.
3DC		.038	.033	.036	.029	.031	.024	.026	.029	.026	.026	.026	in.
33PD	.004	.004	.004	.004	.00h	.noli	.204	.004	.001	.noli	.004	.006	in.
35PD	.067	.067	.067	.067	.067	.067	.067	.067	.067	.067	.067	.067	in.
39PD		.013	.040	.035	.017	.018	.013	.013	·ma	.005	.013	.009	in.
3SNJL	11	11	n	11	11	11	11	11	1	11	11	11	sin/in
3SSJL	17 88	17 85	17 85	17 85	17 85	17 85	17 85	.17	85	17 85	17 85	17	win/in
3SUL 3SCT	9	9	. 9	9	9	7	7	92	9	9	7	7	win/in
2001		No. of the	*	,	The said				- VALV	H. L. L. L. L. L. L. L. L. L. L. L. L. L.			

^{*}See table B1 for gage identification system.

TABLE B13

SUPPLEMENTAL STRAIN MEASUREMENTS Southwest Panel of Test Item 2 Single-Wheel Load of 30,000 1b

Distance from East				S	STRAIN GAGE	READINGS .				
Pavement Edge, in.	127E	90E	90E	30E	3E	120N	N06	N09	30N	ä
150	0	140	171	142	76	0	0	0	•	0
125	0	0	121	121	E	29	30	29	2	15
100	0	130	11	H	#	0	0	29		S
75	0	27	160	27	Ħ	0	•	28	S	
20	•	K	19	160	30	ည္တ	20	ដ		
25	0	K	16	0	190	26	29	140	26	170
0	0	111	171	151	130	20C	150	24C	190	190

*All strains in Min./in. C indicates compression T indicates tension

TABLE B14

SOUTHWEST Panel of Test Item 2
Twin-Tandem Load of 15,000 1b/Wheel

				STR	AIN CACE R	EADINGS *				
	1275	30E	60E	305	OE	120N	N06	60N	30N	NO
Initial Reading	CAGE	200	•	•	100	22	Ħ	3	28C	20C
Load in Position INOPERABLE for 15 minutes	INOPERABLE	ည္ဆ	S	ဗ္က	110	130	K	ioc	300	200

*All strains in jdn./in. C indicates compression T indicates tension

TABLE B15
12-HEEL-ASSEMBLY THAFFIC TESTS
GAGE NO. 13 PD TEST ITEM NO. 1 DEFLECTION IN INCHES

		1	0,1		11	112	070	176	114	121	322	910	978	224	325	276	031	978	227	023	023	020	324	326	926	325	325	926	910	020	020	025	254	.024	070
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	2	1 20	013			Ī		и					_			_	7									_								0.048	
	-	1.1	0.2		.014	.014	.017	.016	.019	.02	.037	.031	.03	.038	.034	.036	0.7	0.	.03	.03	.03	.036	.03	.03	0	.0.	.03	.03	.03	000	.040	70	.048	070	.03
		13	.0:7		.017	.022	.022	.024		.033	.041	.040	.043	.042	.038	13.	.045	.050	.047	.052	.047	.046	.046	.066	.052	.046	670	.046	-044	.052	.048	.054	. 060	.050	.050
		17	.014		.015	.024	.022	.021		.034	.040	.041	.044	.042	.039	.040	.050	.052	.048	.048	770	.042	.047	.045	.052	.048	.047	.050	770	.050	.048	.056	.057	.056	870
		16	910		.017	.021	.021	.024	.026	.035	.038	.038	970.	.045	.038	070	.050	.048	.047	.051	-047	970-	770-	770-	.054	870-	.047	.046	770.	.050	.053	.056	.056	.052	870
	3	15			.017	.018	.020	.024	.022	.031	.038	040	.036	.039	.032	.039	.045	-045	870	670	046	770	770	-044	.052	870	.057	670	.042	.050	.047	.054	.057	.052	870
		14	020		610	024	022	025	027	033	032	033	037	039	035	039	770	043	041	042	041	036	070	040	058	041	047	970	042	042	047	052	020	.052	970
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		6	.020	.021	.019	.021	.026	.029	.031	.043	.039	.042	.037	040	.033	.038	670.	970.	670	.056	.057	.055	.055	.055	.065	.062	090	090	.059	090	.058	.070	.070	.070	9
	7	8	.019	.015	.016	.021	.022	.027	.026	.028	.033	.035	.035	.037	.035	.036	770	770.	.043	.041	.043	070	.040	.042	.052	690.	.039	970	070	.643	.047	.050	.054	.052	ş
		-	.016	.015	910.	.018	.020	.022	.027	.027	.036	.037	.037	.038	.033	070	.043	770-	070	970-	970	.039	.039	.045	.052	870	670-	970-	770	870.	870.	.050	.057	.052	.020
		9	-016	910-	.017	.018	.020	.024	.026	.037	070	070	.047	.041	.032	040	.052	.047	.048	.051	670	970.	970-	.048	.052	870	.048	.042	.042	.043	.052	090	.057	.052	.050
		2	015	910	910	910	020	025	024	032	030	039	038	036	035	070	970	770	047	020	870	043	770	770	950	051	047	048	770	038	770	920	090	.052	020
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TABLE B15 (Continued)

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	_		-	1			870										
			13	.052	.052	.052	.048	.044	.048	440	.072	.072	.272	.064	.068	.068	770
			16	.056	.056	.056	.045	770	.052	878	.076	.072	790-	-064	.070	.070	970
	٦	Ì	53	870	.050	.052	970	770-	970	770	090-	890.	.068	.064	990.	.062	630
		i	1	870	770-	870.	.041	.040	770.	040	.080	080	-072	890	.058	090	950
	1		13	970	770	.040	.045	.036	0%0	070	780.	890.	.068	090-	.056	.058	057
			77	090	.063	790	.055	.052	.052	.052		.092	980.	.080	780.	.082	070
	5	REPORTER	-				.055										
T.		PASS	10	090	790	.062	.054	.053	.056	090	980	.088	.088	080	.085	.078	OBO
	7	ĺ	6	090	.063	.062	.056	670	.056	.056	.088	.088	.088	080	.085	080	080
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	1	22	954		750	.052	3	.051	.052	130	.054	.053	.057	.058	.058	.059	67.9	.077	690.	.073	.076	.078	.080	.086	.120	108	.117	.120	==	.115	.120	.125	.130	.120	.120	.120
		21	.053		.053	750	750	052	950	950	.062	.90.	.059	990	990.	.067	.087	.085	.068	.083	.075	.085	.081	.000	.130	.121	315	.120	1118	.125	.130	.133	.145	.140	130	.140
]	20 1	88		.067	071	640	29	073	990	.076	.073	.081	.081	920.	.079	.105	108	.095	077	104	113	711.	.120	.160	.170	.162	.162	.136	.150	.177	.180	.185	180	170	.180
ľ		6	990		690	190	0.68	890	170	070	0.85	080.	.085	.087	4,27	181	110	.116	.098	.107	.120	.124	.126	.132	.165	.182	.158	.170	.157	.165	.195	.200	.205	.190	.190	.200
Ī	1	-	.088		980	080	086	085		.086	.097	.095	.095	101	093	660.	.128	136	.112	.124	.124	.133	.137	.136	.175	.163	.170	170	.164	.175	.200	.203	.210	.190	.200	.200
ľ		1	.081		.085	780	080	780		.083	.60	.092	.092	101	060	760.	.120	.128	.126	.130	.140	.139	.146	.150	.190	.187	.196	.200	.178	.190	.225	.225	.235	.190	.210	.230
Ī	1	191	980			083	770	083	780	070	560	.093	760	101	.093	116	127	132	1112	130	.124	130	171	136	170	168	.169	.170	991.	.180	.210	.193	.225	190	200	160
ľ	1	13			980	082	280	085	086	087	097	097	060	101	160	100	117	124	122	132	133	139	147	152	180	190	195	198	181	190	225	180	230	220	210	220
1	1	77	100		085	103	900	100	900	000	102	960	100	108	. 860	108	121	126	112	113	3115	121	151	132	170	170	176	191	160	150	195	7.82	185	170	180	180
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		PATTERN	-	7	•	,	•	1	10	ដ	21	13	50	24	25	29	33	35	38	44	20	95	65	2	83	92	101	911	119	128	137	146	155	164	571	182

ABLE B15 (Continued)

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										PASS	MUNGEL	_									ŀ	
RN	1	2	3	4	~	0	-	70		9	=	12	=	7.	1	14	:	-	9.	5	3.5	33
161	.150	.120	200	.160	.220	1	210		260	230	270	240	5	1	9	5	450	200				*
	3776	200	000						207	25.	2	2	24.		27.	37.	27.	2007	277.	0/1.	071-	27.
	CaT.	CCT.	307	190	577.		007.		-260	. 220	. 260	. 230	.190		. 230	200	.230	. 200	.210	.190	.140	.120
	.112	.115	.190	.170	.210		.210		.230	.230	.250	.228	.187		226	105	221	170	200	170	186	110
	.121		.171	185	198		170		233	076	233	250	148		100	316	104	216	100	100	130	
	150	120	000	160	220		200		250	200	200		001.		222	* 17.	2010	1	201.	COT.	277	3
		077.	34.	001.	077.		017.		207.	067.	207.	25.	•		057	207	0+2.	2007	•	•	120	
	.140	.120	.210	.180	.230		.210		.260	.220	.250	.220	.200		.220	200	.210	190	.200	.170	071	.120
	.160	.140	. 220	190	.230		.230		270	.240			260		220	220	2.50	210	220	9	5	5
	170	170	250	220	210		210		000		200										2	2
	21	0/1.	37	077.	1147.		057.		097.	047.	087.	. 230	. 230		.250	.200	.230	.210	. 230	.200	.170	140
	130	.120	.190	.190	.210		.250		.250	.240	.250	.230	.190		-210	180	.210	190	.200	180	130	130
	.150	.150	.220	.190	.250	.200	.230	190	290	250	290	250	220	220	250	210	260	210	240	200	2	071
	.140	14.8	,		227		221		376	237	26.3	37.3	300			200	2		2	200		
							***		617.	163.	707.	C+7.	607.		047.	707.	. 635	577	077.	507.	0.1.	141.
			•	•	.240		.220		.260	.230	.260	.230	.210		.240	.200	.230	.190	.210	.170	.140	.140
	.122	1.26	206	1RO	220		104		266	237	26.3	233	104		356	202	222	300	2000	180	3.33	110

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CACE NO. 1 SHJL TEST ITEM NO. 1 STRAIM IN MICHOLNGHES

				ACTUAL S	AL 97.	Table 1	STATE OF THE PARTY	STATE OF	ALC: DOC AS		2	TIC	CINES	Street Street			Total Section	The State of the S		Part Shan	PANTINES.		Sec. 182		
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	0.00										PA	SS XU	2	100									l		
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2	23		•				53	127	139	72	8						2	24	*	2	23				3
2	*		•				13	12	2	72	77						43	31	22	33	2				9
118	•	2	=	27			17	=	3	42	3						91	2	18	91	2				E
20	=		7				20	2	2	1	33						55	=	13	2	11				-
72	2		2				91	23	2	2	\$						26	18	16	77	12				0
22	2		=				2	23	22	2	\$						2	24	17	26	16				B
Si	•		•				91	*	2	2	22						118	13	=======================================	17	13				
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×	=		1				23	42	2	69	47						2	28	21	21	•				0
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3	1	1	1				56	73	62	5	•						23	20	20	16	•				-
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65	1	•	~				20	65	55	11	28						28	28	23	22	1				
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101	~	~	~	•			29	62	55	3	33						29	29	24	11	S				1
110	1	~	•	•	7		11	62	K	33	2						2	27	4.5	2	5			V.401	
119	1	1	~	1	7		21	62	\$	117	2						200	24	26	20	9				-
128	1	1	1	-	7		20	62	22	3	32						26	23	26	26	7		M		
101	1	1	2	2	7		20	65	2	42	3						29	25	56	29					
146	~	1	8	8	. 2		76	9	53	77	*						23	23	29	24					
155	1	1	1	-	7		23	29	19	3	2						56	26	22	26	1				
161	~	~	1		7	29	23	62	×	7	2	77	2	\$		25	22	23	2	77	1	,			-
173	•	•	1	2	7		2	62	25	3	23						2	23	2.5	23	10				15

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CACE NO. 1 SCT TEST ITEM NO. 1 STRAIN IN MICROINCHES

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218	33	42	33	28	25	9	28	8	16	16	13	1	28	27	53	13	23	13	3	28	2	42
233	9	35	8	8	3	8	8	2	20	13	2	12	32	2	9	200	65	25	2	28	53	9
242	35	35	8	8	55	25	20	2	15	10	15	2	8	8	55	8	55	9	2	2	57	9
251	9	35	25	22	9	20	25	2	9	2			15	20	9	8	9	200	2	2	9	2
260	35	38	8	8	55	8	25	25	91	15	10	10	2	2	55	2	9	3	12	25	9	8
592	45	200	8	35	2	45	25	25	15	20	12	101	2	2	20	5	25	2	2	2	3	8
273	07	4.0	25	2	9	20	2	20	2	20	12	2	25	2	55	20	25	200	2	25	35	2
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CACE NO. 1SCL TEST ITEN NO. 1 STRAIN IN MICROINCHES

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4	81	6.9				09	56	52	17	17	26				32	39	9	9	61	99	73	11	8	
2	69	55				53	2	%	17	20	26				35	97	55	26	9	28	80	67	2	
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15	72	77				62	9	9	45	45					31	35	07	19	62	9	58	72	67	
18	68	2				63	65	43	77	27					9:	43	65	67	63	53	67	73	73	
20	75	75				83	55	57	17	77				•	27	37	97	26	65	•	68	71	7.4	
24	75	73				93	9	09	07	42				1	35	07	20	65	62	3	65	77	73	
25	77	72				43	23	62	9	9					31	07	87	59	59	58	63	8	38	
29	2	75				96	63	67	42	45					35	42	20	65	65	62	63	11	67	
33	63	67				2	55	25	38	37					33	37	07	9	57	62	9	72	69	
35	62	72				59	57	20	38	39					30	39	42	57	26	63	57	65	72	
38	99	9				9	24	35	38	23					35	35	57	22	62	53	9	3	67	
77	99	59				25	9	35	38	20					34	07	25	20	25	53	53	58	62	
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74	65	9				55	20	22	25	10					52	27	57	25	57	55	20	52	65	
83	24	52				20	07	20	25	13					52	22	53	20	53	53	47	22	26	
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110		•						25	22	11					22	28	58	53	25	20	20	8	58	
119	25	22				51	67	23	56	15		-			25	25	52	43	55	25	55	×	57	
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155	9	20				20	47	23	23	23					25	25	57	20	20	8	47	4.7	62	
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A. I. O. LEW LEWIS

CACE NO. 2858JL TEST ITEN NO. 2 STRAIN IN HICKOINCHES

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6	81	2	3	115									8	8	100	100	100	100	72	69	53	85
111	79	2	2	8									95	16	100	100	106	06	72	82	67	2
120	83	65	88	85	ľ									88	122		•		•		20	89
129	110	106	125	109									•									
138	195	155	80	195	3								190	186	212	190	100	180	165	160	115	1 28
147	89	8	123	110									170	155	190	220	165	100	1 32	120	100	0
156	105	110	120	120									150	120	145	135	140	140	135	135	90	3
165	100	95	120	110									130	125	135	140	125	126	105	110	00	3
174	105	901	105	115									130	130	150	135	140	135	115	311	301	2 5
192	110	95	115	125								-1	8	180	180	571	9	180	135	135	35	3 5
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261	100	8	113	110									125	130	130	120	100	110			06	50
270	65	22	8	8									100	100	105	95	85	85	06	80	65	9
279	115	120	140	130					T				125	115	120	115	88	65	07	07	30	30
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288	28	2	32	42								_	42	37	69	20	2	20	35	37	27	28
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CACE NO. 2 SCL TEST ITEM NO. 2 STRAIN IN MICHOLNICHES

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7	•	75	9 -	- 55	7		31		25		24		33	•	24		20	•	79	•	75
13	•	77	1	- 53	39	-	77		31	•	26		57		79		52		9	•	71
13	•	34	9	-	37		32		26	•	27		32		77	•	87		89		1/
24	•	74	9	99	5	-	32	•	27	•	34		3		70	•	57		67		76
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57		69			8	3 35		27	26	31	31	35	36	57	87	52	87	63	58	77	73
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84	11	69	68 6	63 5	50 48	37	35	27	29	28	8	37	35	52	52	53	43	89	58	77	75
63		11						27	26	27	27	37	35	52	53	52	20	71	69	82	79
102							-	27	29	29	29	135	35	53	45	57	87	74	69	78	73
111		79			8 52			27	27	28	31	36	36	51	45	57	17	69	79	72	79
120		75						27	26	28	27	35	32	53	52	25	47	72	19	8.	77
129		69					•	26	28	53	3	35	35	07	07	53	87	67	69	72	68
133		67				-		07	42	77	07	45	57	20	2	20	20	5.3	58	99	99
147		74						32	28	27	31	35	37	51	47	53	53	7.5	7,5	82	36
156		72						35	32	32	35	35	32	37	37	77	87	63	79	80	2
165		22					Ī	35	35	37	32	37	37	87	53	20	53	03	80	74	74
174		69					•	42	42	42	77	87	87	53	53	53	53	609	99	69	77
183		8						. 7	37	37	32	77	•	87	87	87	87	69	69	74	80
192		81						29	29	35	35	32	32	20	20	75	52	314	74	73	78
201		74						07	37	37	07		37	87	20	53	87	64	69	77	74
210		79					7 .	37	36	33	33	37	37	53	53	20	24	7.4	77	77	77
213		69						53	28	29	26	35	37	53	53	51	52	79	63	80	70
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CACE NO. 255WJT TEST ITS NO. 2 STRAIN IN MICROINCHES

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3		18	.038	.059	.057	.056	.042	.050	.059	.058	.062	.056	.058	.065	.059	990.	080	860.	•	.100	.097	.092	.098	.156	.124	. 10	.125	140	100	.102	.120	105
		17	090	.058	.056	.059	.047	.053	.056	.052	.068	.059	.058	.065	090-	990.	.080	100	.093	.102	101.	960.	101.	957.	.125	.110	.125	170	100	.108	.130	105
1		16	.057	.058	.055	.058	670.	.054	.059	.058	.070	.056	.058	.061	.058	.065	080	960.	760.	100	960.	.093	860.	.152	.126	110	.125	.140	110	.110	.120	50
3		15	,	.062	.059	.061	.048	.055	.058	.054	690.	.058	.058	.064	.057	690.	.080	.100	060.	.102	.100	960.	.100	.156	.125	.110	.125	140	001.	.110	.130	305
		14	.067	690	059	990	.052	090	890.	990.	.080	.064	.064	.070	.064	.067	080	105	760	.103	.100	.097	960-	.156	.124	.120	.120	130	ı	121	130	701
7		13 j	990	072	. 063	890	090	.063	790	990	970	790	990	070	790	690	080	106	260	105	104	660	100	160	130	130	122	140	110	.121		כנ
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	ĺ	5	.059	.065	.057	.060	.054	.055	.052	.052	.071	090	.058	.062	.065	070	.082	104	960.	.104	100	960-	104	.150	.124	110	.117	.130	110	.110	.120	ב
2		7	.047	1	.046	.050	.031	770	.048	.050	.056	.050	.048	.051	.052	.058	.068	060.	080	.089	.086	.079	.090	.140	. 102	.090	.100	.120	060	.094	ı	100
		3	.049	•	870	.050	.035	970	.042	.041	090	.050	.050	.056	.053	090.	.068	.092	780	.093	.093	.083	.088	.132	.103	060-	105	120	100	160.	.100	1007
		2	.036	1	.041	.038	.039	.034	070	-045	770	.042	.033	-044	.042	.052	.080.	.074	.064	.079	.075	.060	.071	.112	060-	.080	.083	060.	.080	.065	060.	078
			.044	1	.043	.042	870.	.037	.036	.036	.051	-042	040	.044	.047	.051	.056	.076	.072	.076	.075	.068	070	.103	060		.083	060.	.030	.076.	060.	.077
		ATTERN	н	m	4	7	13	9	24	29	33	39	45	51	57	99	75	100	93	102	111	120	129	138	147	156	165	174	183	192	201	210

ABLE B15 (Continued)

										TRAFF	IC LINI	S										
		1	7			3	7		5		5		7		477		473		2			
							8 68			PASS	NUNBE	24										
PATTERN	1	. 7	3	7	5	9	7	8	0	10	11	12	13	14	15	16	17	18	19	20	21	22
243	.080	.000	060.	.080	.100	060	001	060.	.110			110	100	060.	100	100	100	100	060	080	.070	070
252	080	030.	.100	.000	.120	.110	.120	.110	.130			130	.110	.110	.110	.110	.110	.110	.110	0.00	.080	.080
261	100	100	.120	.110	.130	.130	.130	.120	.140			140	.130	.130	130	130	•	•	.110	.120	060.	060.
270	.070	.070	100	.080	.100	.100	.100	100	110			110	.110	.100	100	.100	130	.100	.100	.080	.080	.070
279	060	100	.120	.120	.140	.140	.140	.140	.150			.150	.140	.140	.140	.130	150	.130	130	.130	.110	.100
282	060	.000	.120	.120	.140	.130	.140	.130	.150			.150	.130	.130	.130	130	30	.130	.120	.110	060.	060.
283	105	001	.115	.120	.135	.140	.130	.130	.150	.145	.150	.145	.135	.130	.130	.135	.135	135.	.120	.114	760-	.100
297	.080	0000	.100	100	.120	.115	.120	.115	.130			130	.120	110	.120	.120			120	.120	110	060
312	.085	.085	111	106	125	121	120	122	142			137	125	125	126	125	300	195	110	00,	000	080

Sheet 21 of 30

TABLE B15 (Cuntimed)
GAGE NO. 2DC TEST ITEM NO. 2 DEFLECTION IN INCHES

									T	TRAFFIC	LINES											
	-	4		2		3	7		5	-	5		7	-	٣		5		2			I
						10			P	1	NRER											-
PATTERN	-	2	3	7	2	9	7	-	-	-			-			-	-	H	-	-	21	22
111	.045		.041	170	.036	.034	.031	.027	. 026	.022	.025	.022	.031	.027	036	.033	036	033	042	0.38	04.5	100
120	.050		070	070	.032	.032	.029														043	0.73
129	.043		.041	.041	.034	.034	.031														170	770
138	.050	.056	970.	070	.036	.032	.032														050	080
147	.054		.050	.047	.043	070	.036														054	0.54
156	1		.050	.050	.043	.036	.036														050	050
165	.050		.050	.050	.043	.036	.036														.054	050
174	.050		.050	.050	.043	.043	.036														050	050
183	.054		.050	.050	.043	.036	.036														.054	.054
192	.058		.050	.050	.043	.043	.036														.056	050
201	.054		.050	•	.043	070	.036														.054	050
210	.058		.054	.052	.048	770	.038					-6									.058	.056
219	.058		.051	670.	.043	.043	.039											10			.056	.051
234	.050		.047	.043	.043	.036	.032											10			.050	04.7
. 243	.043		.043	.040	.036	.032	.029														.043	043
252	.043		.040	070	960.	. 332	.029														.043	070
261	.043		070	.036	.032	.032	.029														070	070
270	.047		.043	070	.036	.032	.032														.043	043
279	.043		070	.040	.036	.032	.029														170	043
282	.027		.025	.023	.022	.020	.018											И			.027	026
258	.027		.024	.022	.022	.020	.018														.027	027
297	.026		.025	.022	.020	.018	.018														.024	.023
312	.028		.023	.022	.020	.019	.017														.026	.025

CACE NO. 2 SNJL TEST ITEM NO. 2 STRAIN IN MICROINCHES

				2	_	3	_	7	-	5 1 5	_	2	-	7	_	-		3	-	,	L.	-
										PASS	NUMBER	2							1			1
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1	•	119		113	•	72	•	62		06		86		65		56				62		33
•	Ì		•	•	•	•	•	89	•	58		23	•	76	•	67	•	000	•	4.5	•	07
7	4	16	•		•	7	1	87		29	•	53		72	1	7		21		1.7	•	13
13	•	77		18	1	25	•	85		8	ı	75	i	99	•	20	•	. 62	•	39	•	37
18	•	•			1	1	•		1	•	•	•		1	•	•	•	4.1	•	29	•	25
24	1	27			•	37	i	62	i	26	-	57		9	•	43	•	42	•	33	•	25
29	•						1		1	57	•			58	•	17	. 1	43	•	30	•	18
33	•						•		•	65	•		•	24	1	97	•	17	•	87	•	57
39	19						99		26	62	57		99	99	07	8	37	37	28	27	19	20
45	20						62		53	58	.55		61	09	37	42	36	7	25	27	20	21
51	35					-	74		68	62	68		17	89	89	45	51	43	33	3	32	28
57	8						73		26	57	09		75	89	33	33	35	29	7	26	23	20
99	13						68		45	42	87		88	99	27	29	27	33	21	21	12	16
75	14						74		47	67	67		74	89	16	22	16	18	91	16	14	16
78	19						10		67	67	34		74	70	33	21	20	35	21	14	10	12
93	20						2		51	25	21		76	75	33	26	32	27	21	17	10	17
102	19						74		47	47	67		74	78	29	27	33	50	10	15	60	18
111	16						73		47	55	87		72	72	31	24	31	42	16	16	16	3.
120	19						74		47	47	45		74	73	33	26	31	33	21	19	20	19
129	25						78		33	57	53		75	72	30	22	9	30	23	25	27	21
138	21					78	76		55	21	21		73	73	21	28	22	37	1.8	16	16	16
147	16						74		20	62	52		72	70	25	87	25	25	21	1.5	19	17
156	•						74		67	67	67		51	25	74	76	25	23	16	16	16	16
165	18				23		82	,82	53	67	53	57	74	78	27	27	25	18	16	16	21	21
174	16	16					74		51	67	53		26	74	16	17	16	25	16	12	12	77
183	CAGE	-	9																			

CAGE NO. 33 PD TEST 'TEM NO. 3 DEPLECTION IN INCHES

										TE	FFIC L	INES				- N						
		-		2		3		3		2			7		3			3		2		
										Pr	EUN SE	ER										
PALTENN		2	3	7	2	9	1 7	8	6	10	11	12	13	14	1.5	16	17	18	19	20	21	22
2	.010	600.	.012	.011	.013	.015	.013	.013	910.									•				
2	600.	.00e	.011	.012	.012	.014	910.	.016	.018	910.	.018	.018	910.	910.	.015	910.	.012	.012	.010	.011	800.	.007
15	.007	.005	110.	.012	.014	•	.016	.018	910.	.018	.017	.018	.017	610.	.015	910.	.012	.014	.011	.013	.008	.008
20	600.	.009	.012	.011	.011	.013	.017	.017	.013	.015	.017	910.	.015	.016	.C14	.014	.013	.013	.010	.011	800.	.008
25	.008	.000	010	900.	.016	.016	.016	.014	910.	910.	.018	.016	.014	.013	.013	.012	.011	.011	.010	.011	800.	.008
35	.012	.012	.020	.019	. C24	.023	.027	.027	.031	-029	.029	.020	.027	.025	.025	.023	.024	.023	.018	.020	.013	.012
0.7	.010	010	.014	.612	.018	.018	.022	.020	.023	.022	.023	.023	.020	.018	.018	.018	.318	.018	.014	.014	.010	.011
97	-012	.010	910.	.014	.022	.023	.022	.021	.030	.027	.025	.025	.020	.019	.020		.020	.019	.018	710.	.011	.012
52	.012	.012	.019	.018	.023	.024	.022	.022	.026	.026	.026	.026	.020	.022	.022	.021	.021	. 921	910.	.018	.013	.014
60	.013	600.	.013	.014	.018	.019	.020	.023	.024	.024	.025	.021	020	.020	.021	.020	.020	.020	.015	.014	.012	.012
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5.6	.016	.016	.024	.020	.028	.028	.028	.028	.032	.032	.036	.032	.024	.028	.024	.028	.024	.028	.020	.020	.016	.014
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112	.018	.018	.019	.021	.027	.026	.024	.029	.033	.029	.034	.030	.028	.026	.025	.025	.026	.026	.020	.019	.018	.017
121	.019	010	.020	.022	.027	.027	.028	.028	.032	.030	.030	.030	.026	.026	.025	.025	.022	.025	.020	.018	.012	.015
130	.013	.014	.023	.020	.030	.026	.027	.030	.034	.035	.032	.028	.028	.027	.030	.027	.026	.025	.030	.020	.016	.614
139	.028	.024	.034	.032	070	.036	.036	070	770.	770	.044	970.	070	.040	.038	.038	.038	070	.034	.032	.028	.030
148	.024	.028	.032	.036	.036	.032	.036	.032	770	070	070	070	.036	.036	.032	.032	.032	.032	.032.	.032	.028	.028
157	.024	.024	.030	.028	.034	.032	.034	.032	.070	070	070	.038	034	.035	.032	.032	.032	.032	.028	.026	.0.3	.022
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193	.032	.023	070	.036	070	.040	070	.040	.048	.048	.052	770.	.044	.036	.052	070	770	370	.036	.032	.028	.032
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280	890.	.052	.080	790	.058	.068	.084	.068	960.	.076	960.	.076	.084	.068	.084	.068	.084	890.	.076	.064	390.	870.
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258	.068	.070	.080	.073	.088	.076	.085	.084	960.	.092	.093	.092	.083	.081	.086	.083	.088	.080	.080	.078	.067	.064
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			18		.054		.059	090.	.052	.124.	.103	.135	.140	.120	.132	149		.145	.152	.144	.143	.172	.170	.150	.138	150	.170	.150	.150	.180	.160	.150	.170	.150	.150	.180	.190	.190	181	291.	.170
			17		.055		.000	.063	670.	.120	011.	.138	.138	.123	137	.153		.152	.158	.150	.147	.172	.180	091.	.150	160	.180	.160	160	180	181	.150	.180	.170	1:0	.190.	.200	200	200	185	186
			15	-	043	052	062	190	0.52	123	901		137	121	133	155	152	145	153	146	145	172	160	150	145	150	170	150	150	165	191	140	170	150	150	180	190	190	185	191	167
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PPIC		S NUMBER	111	•	.055	.053	.058	.055	.047	.110	.108	.138	.139	.122	.133	.154	.156	.148	.156	.148	.147	.176	.174	160	.150	.160	.180	.160	.160	.180	.178	.150	.180	.170	.170	.150	. 200	200	200	.180	.185
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			89	057	054	053	190	061	660	125	100	130	133	116		151	148	140	152	139	134	168	170	140	137	140	160	140	140	160	158	135	160	150	150	170	180	180	175	160	165
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	1-0		2	.057	.053	.050	.055	.061	.053	.121	.103	.132	.135	.117	.135	.154	.156	.148	.153	.160	.146	.172	176	.150	.150	.160	.170	.160	.150	.130	.175	.148	.170	.160	•	.180	.190	200	189	.175	.177
				.034	.0	.043	.020	.655	047	. 3 . 2	969.	.125	130	.110	-127	.145	- 764	.336	.142	.138	134	.160	.164	.140	130	140	160	.140	.140	170	129	1/15	.150	.150	1	160	-230	170	171	.154	.158
			1	.054	.050	000	.052	.055	650.	.112	.085	.124	.132	.113	.132	.152	.148	777	151.	.146	.136	.168	.176	.160	.143	397	170	.160	.150	150		.145	.170	.160	,	.130	190	190	121.	168	.165
			PATTERN	7		07	7	20	25	33	07	9.7	52	58	67	75	85	36	103	112	121	130	139	148	157	166	175	184	193	202	211	220	235	246	253	262	271	280	583	298	313
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Sheet 27 of 30

Sheet 28 of 30

CAGE NO. 355MJT TEST ITEM NO. 3 STRAIN IN MICROINCHES

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CACE NO.3SSSJL TEST ITEM NO. 3 STRAIN IN MICROINCHES

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22	79	65	53	2	65				2	72	•		95	82	1	•	•	•	•	•	•	•
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35	53	20	•	•	•				1	•	•	•	*	53	61	62	62 3	9	37	8	2	21
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97	74	79	75	74	11				25	*	16	85	78	n	26	•	11	92	74	89	63	3
51	2	78	2	88.	20				93	92	95	92	85	88	85	85	83	78	78	83	989	75
28	63	52	63	55	89				73	73	1	2	73	65	78	99	89	69	63	58	57	57
67	•	80	82	97	18				95	16	92	8	95	88	76	06	102	88	95	16	62	86
92	97	100	122	122	123				123	123	131	122	122	117	122	112	118	108	100	100	96	16
8	2	65	74	2	8				82	1	88	8	79	75	78	73	•	•	•	69	2	63
96	•	•	•	92	83				8	88	82	82	2	72	75	100	80	9/	74	73	2	9
112	8	74	86	79	85				92	81	92	72	85	2	•	26	83	85	75	73	2	69
121	89	65	8	75	8				95	88	95	96	06	8	85	8	92	80	87	75	75	63
130	107	16.	116	105	123				137	128	130	128	119	116	113	128	124	121	117	116	100	101
148	~	S	2	2	20				20	20	8	25	27	10	25	20	25	25	25	25	10	15
157	2	S	2	S	20				15	2	25	20	2	9	•	•	•	•	•	•	•	•
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202	S	S	S	~	2				20	27	22	27	~	2	2	2	2	2	~	91	5	2
211	12	12	2	S	11				22	=	23	15	2	~	•	9	2	23	~	•	~	~
220	S	~	2	S	2				22	2	97	2	~	2	21	21	20	13	97	2	9	2
235	5	~	9	~	2				21	15	20	15	~	~	15	10	10	15	5	5	~	•

heet 30 of 30

CA.F. NO. 3SCT TEST 1TEM NO. 3 STRAIN IN MICROINCHES

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7		33	42	16	2	∞	∞	13	19	19	19	77	#	ដ	16	•	•	?	37	45	47
48		53	53	8	•	•	16	77	16	71	21	16	7	13	16	16	13	32	38	45	4.5
47		17	45	13	14	21	16	77	21	54	22	16	15	7	14	14	14	35	32	45	20
48		00	97	16	21	14	#	19	18	22	20	17	14	16	14	16	14	41	37	97	50
48		5,3	47	16	13	16	16	24	22	27	Ħ	2	13	2	2	31	31	07	07	53	37
7		37	07	13	13	#	#	19	13	13	21	#	#	#	=	13	13	37	35	45	4.5
4	2	37	70	#	91	#	#	24	21	21	21	13	#	#	•	13	21	35	4.5	45	38
4	1	37	38	#	#	=	2	21	25	21	24	13	ជ	∞	13	11	œ	37	33	45	97
4	2	.2	37	=	13	=	77	14	16	16	19	#	21	#	∞	0	=	07	53	45	4.8
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4	8	37	32	::	16	16	4	31	28	28	27	91	16	16	16	16	26	31	31	36	97
	7	.2	31	31	13	16	2	56	56	23	56	2	16	2	10	16	97	10	13	36	47
	20	33	R	2	10	11	16	24	56	56	92	16	16	9	7	10	œ	36	36	52	52
-,	25	3	36	13	13	21	21	53	31	3	4	12	21	10	13	13	13	36	39	67	52
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6,	25	42	47	18	15	13	13	23	21	23	17	16	18	16	13	16	18	36	77	57	57
•	25	2.7	42	16	16	16	13	56	56	56	56	87	13	13	13	16	18	36	36	55	57
	22	36	77	16	18	14	4	56	26	26	56	16	13	18	18	97	16	39	36	55	55
•1		7.7	42	13	21	2	12	9	21	77	18	10	0	16	18	18	18	77	52	62	57
0	0	39	47	18	16	18	13	56	56	56	29	18	18	18	16	16	01	36	39	09	9
_	62	52	25	23	23	22	21	18	16	26	23	18	18	18	18	18	18	42	39	99	99
9	00	25	39	21	21	18	16	23	18	23	21	21	18	16	18	16	18	47	67	68	9
9	7	42	47	17	2	11	16	76	56	26	56	21	16	16	16	16	18	77	31	9	99
S	01	65	77	18	23	23	23	26	23	56	56	23	23	18	15	15	23	47	47	68	62
9	5	27	73	13	21	71	16	29	56	56	23	21	18	18	21	21	21	52	77	68	9
9	.4	47	77	138	21	21	16	56	21	56	23	21	13	18	12	21	20	77	57	58	62
9		77	36	16	13	21	18	56	23	29	53	21	16	16	13	13	2	77	34	65	52
9		67	77	16	16	21	18	53	21	56	77	21	18	13	13	13	18	47	77	68	99

DYNAFIECT MEASUREMENTS DURING 12-WHEEL-ASSEMBLY TRAFFIC

			Item 1			
	Traffic Volume			Sensors		
Date	Patterns	1	2	3	4	_5_
			South Lane	- Position	1	
13 Oct 69	-	1.20	0.96	0.85	0.72	0.64
14 Oct 69	1	0.83	0.70	0.63	0.54	0.46
17 Oct 69	7	1.35	0.84	0.75	0.69	0.62
21 Oct 69	19	1.03	0.90	0.80	0.69	0.58
29 Oct 69	*	1.50	1.25	1.08	0.95	0.84
			South Lane	- Position 2	2	
13 Oct 69	-	1.20	0.95	0.81	0.70	0.60
14 Oct 69	1	1.03	0.78	0.64	0.55	0.49
15 Oct 69	4	1.74	0.85	0.70	0.65	0.56
21 Oct 69	19	1.20	0.83	0.70	0.62	0.53
23 Oct 69	37	1.29	1.03	0.90	0.80	0.68
29 Oct 69	37 *	1.32	1.04	0.90	0.76	0.64
8 Dec 69	301	0.85	0.75	0.64	0.55	0.49
			South Lane	- Position 3	3	
13 Oct 69	-	1.38	1.15	0.98	0.84	0.71
14 Oct 69	1	1.14	1.01	0.83	0.75	0.61
21 Oct 69	19	1.08	0.95	0.83	0.71	0.60
23 Oct 69	. 37	1.02	0.92	0.83	0.71	0.60
29 Oct 69	37*	1.20	1.03	0.91	0.80	0.66
8 Dec 69	301	0.85	0.77	0.67	0.58	0.50

NOTE: All readings are in mils (0.001")

(Sheet 1 of 4)

^{*}Initial reading after overlay was constructed (no traffic on overlay, 37 traffic patterns on base pavement).

TABLE B16 (Continued)

Item 2

_	And the second of the second			70cm -			THE RESERVE OF THE PARTY OF THE
		Traffic Volume			Sensors		
Da	te	Patterns	1	2	3	4	_5
19				South Lane	- Position 1	700	
11	Oct 69		0.65	0.60	0.58	0.54	0.49
14	Oct 69	1	0.58	0.58	0.55	0.50	0.46
22	Oct 69	30	0.65	0.60	0.58	0.54	0.49
23	Oct 69	37	0.70	0.67	0.64	0.59	0.55
				South Lane	- Position 2		
11	Oct 69		1.11	0.69	0.62	0.56	0.51
14	Oct 69	1	1.05	0.65	0.58	0.52	0.47
22	Oct 69	30	0.81	0.76	0.68	0.61	0.55
23	Oct 69	37	1.02	0.82	0.75	0.68	0.60
				South Lane	- Position 3	1	
11	Oct 69	-	1.23	1.05	0.93	0.81	0.71
14	Oct 69	1	1.41	1.24	1.08	0.93	0.85
22	Oct 69	30	0.90	0.83	0.75	0.68	0.60
23	Oct 69	37	1.25	1.15	1.03	0.93	0.83
29	Oct 69	38	1.86	1.56	1.34	1.15	0.99
19	Nov 69	176	2.04	1.88	1.65	1.34	1.18

(Sheet 2 of 4)

TABLE B16 (Continued)

Item 3

	Traffic Volume			Sensors		
Date	Patterns	1	South Lane	- Position 1	4_	5
13 Oct 69		0.48	0.46	0.45	0.43	0.40
14 Oct 69	1	0.47	0.45	0.44	0.42	0.39
22 Oct 69	30	0.41	0.40	0.39	0.36	0.35
23 Oct 69	37	0.54	0.51	0.49	0.46	0.44
			South Lane	- Position 2		
13 Oct 69	-	0.95	0.52	0.47	0.42	0.39
14 Oct 69	1	0.92	0.60	0.55	0.50	0.45
22 Oct 69	30	0.75	0.45	0.40	0.35	0.31
23 Oct 69	37	0.90	0.50	0.45	0.40	0.35
13 Nov 69		1.20	0.32	0.30	0.29	0.27
			South Lane	- Position 3		
13 Oct 69	-	0.97	0.86	0.76	0.65	0.56
14 Oct 69	1	0.97	0.86	0.76	0.65	0.56
22 Oct 69	30	0.80	0.71	0.63	0.54	0.46
23 Oct 69	37	0.86	0.78	0.70	0.63	0.55
4 Nov 69	73	1.25	1.11	0.97	0.86	0.75
10 Nov 69	112	0.71	0.66	0.60	0.51	0.46

(Sheet 3 of 4)

Item 4

	Traffic Volume			Sensors		
Date	Patterns	1	2	3	4	5
Dace	- Taccerno		South Lane	THE RESERVE OF THE PARTY OF THE		
11 Oct 69		0.94	0.88	0.80	0.70	0.56
13 Oct 69		0.89	0.85	0.76	0.65	0.57
21 Oct 69	19	1.00	0.99	0.91	0.79	0.65
29 Oct 69	40 4×	1.31	1.23	1.10	0.94	0.78
5 Dec 69	289	0.79	0.77	0.72	0.64	0.55
			South Lane	- Position 2		
11 Oct 69	_	1.80	0.80	0.66	0.56	0.46
13 Oct 69		1.80	0.8€	0.58	0.47	0.43
17 Oct 69	7	1.86	1.03	0.84	0.70	0.60
21 Oct 69	19	1.61	0.90	0.78	0.65	0.53
10 Nov 69	112	1.02	0.90	0.78	0.65	0.53
			South Lane	- Position 3		
11 Oct 69	-	1.63	1.29	.1.01	0.80	0.63
13 Oct 69	. •	1.84	1.44	1.14	0.90	0.71
21 Oct 69	19	1.46	1.20	0.96	0.79	0.60
10 Nov 69	112	0.99	0.91	0.80	0.65	0.56
9 Dec 69	312	0.69	0.66	0.60	0.56	0.47

^{**}Overlay was placed after 37 patterns.

Sheet 4 of 4

TABLE B17 TWIN-TANDEM-ASSEMBLY TRAFFIC TESTS GAGE NO. 2NSCT TEST ITEM 2 STRAIN IN MICROINCHES

			o _t		c Lines	or was made of majorital groups and where	and four the second of		Maria di Maria da Agray di Maria	or to propose .
PATTERN		THE RESERVE THE PERSON NAMED IN	the second second second second	2		3		4	TO STATE OF THE PARTY NAMED IN	5
	WEST		WEST	EAST	VEST	EAST	L WEST	EAST	WEST	EAST
1	85	95	105	122	106	103	119	117	96	117
			95	95	85	106	117	117		
			101	90	90	90	106	101		
			72	58	80	64	101	106		
10					80	101				
5	66	72	53	53	50	45	69	64	48	53
			48	48	48	40	74	66		
			53	48	48	40	72	53		
			74	64	45	37	48	48		
					72	58				
10	66	66	42	50	56	40	69	64	42	77
			90	64	50	42	72	64		
			69	50	48	37	72	69		
			40	35	45	40	69	64		
					53	42				
15	66	48	40	3?	37	30	64	53	35	29
			35	29	32	22	58	45		
			61	68	29	27	50	42		
			29	27	32	27	48	40		
					29	27				
20	58	42	40	27	37	27	45	35	37	45
			45	37	42	27	45	35		
			37	32	40	29	48	35		
			40	27	40	_	48	35		
					42	37				
25	48	42	27	21	27	24	37	29	29	24
			27	21	27	24	40	29		
			29	21	32	21	37	29		
			26	24	29	21	35	32		
					40	35		•		
30	53	42	63	27	32	27	58	27	32	27
30	73	72	37	21	32	22	42	32		
			37	21	27	32	37	37		
			37	16	37	27	37	37		
			37	10	37	27	37	٠,		
35	32	32	11	_	16	21	37	32	11	11
33	32	32	21		27	16	27	27	**	11
			21	_	21	16	. 32	53		
			16	<u>.</u>				64		
			16		16 16	11 27	27	04		
40		0-	20	0.7	~	-		, .		
40	53	85	32	27	28	32	48	44	16	11
			37	27	32	37	48	64		
			27	21	32	37	48	48		
			27	32	37	32	48	48		
			21	53	- 37	32				

Sheet 1 of 10

TABLE B17 (Continued)

			Uran Hillard	Traff	ic Lines					
PARTIE	1			2		3	1.122 C/II	NACT	WEST	1 11400
-	WEST	EAST	1 KEST	EAST	LEST 1	EAST 1	WEST 32	EAST	27	I EAST
45	43	32	16	16	11	16		37	21	42
			16	85	16	16	37			
			37	16	16	16	27	32 37		
			11	16	16	16	32	3/		
					16	16				
50	-	- 465	-	7	-	-	82			To- 1881
			21	11	11	16	43	53		
					16	16	48	43		
					2.7	16				100
55	43	43	2 J.	11	21	16	32	32	27	21
			16	16	16	21	37	32		
			21	16	21	21	27	27		
			21	21	16	16	37	43		
					16	21				
60	42	27	21	11	21	16	39	48	16	11
			16	42	16	21	37	37		
			42	11	16	27	37	37		
			16	8	16	21	37	37		
				•	21	27				
65	32	21	16	70	16	16	37	32	21	37
		-	16	53	16	11	37	32		
			11	16	16	13	37	37		
			11	16	16	16	40	37		
			11	10	11	48	40	٠.		
68	37	27	16	11	16	21	37	37	21	32
00	3/	21		11	16	21	37	32	-7	
			13	8	11	11	40	37		
			11			16	40	37		
			13	16	16		40	31		
					16	16				

Sheet 2 of 10

TABLE B17 (Continued)

GAGE NO. 2NSCL TEST ITEM 2 STRAIN IN MICROINCHES

		117		Tra	ffic Lin	es				
PATTERN		1		2		3		4		5
	WEST	EAST	WEST	EAST	WEST	EAST	WEST	LAST	WEST	EXST
1	95	106	103	111	95	103	122	127	106	106
			106	108	101	101	122	111		
			111	106	95	95	117	117		
			95	106	98	108	117	122		
				1000	106	114				
5	80	90	103	117	98	101	103	122	114	133
			101	114	93	103	109	119		
			114	117	95	101	119	119		
			125	122	98	103	101	114		
704		20.00	100		117	122				
10	74	85	95	114	95	95	111	127	114	138
			117	114	88	95	106	122		
			109	117	88	98	106	117		
			93	98	93	95	106	119		
					103	109				
15	74	74	103	111	80	90	106	119	101	114
			103	114	80	90	117	111		
			95	103	80	77	103	93		
			101	103	77	80	90	90		
	3100				77	80				
20	85	80	98	98	88	74	111	98	95	125
			95	106	92	80	111	95		
			95	103	74	74	103	103		
			109	106	77	77	106	103		
					77	80				
25	88	88	90	103	77	77	109	106	114	109
			109	109	74	74	90	88		
			103	98	72	74	95	111		
			109	109	80	80	95	106		
					80	80				
30	90	85	106	106	69	74	106	101	95	101
			106	101	74	74	106	95		
			108	108	74	74	106	103		
			101	95	69	69	101	101		
					74	74				
35	69	90	101	95	85	90	108	106	106	111
			91	101	84	84	106	111		
			85	85	80	74	106	111		
			85	85	74	85	106	122		
					85	90				
40	80	101	106	106	80	85	122	111	106	106
			95	95	85	85	111	122		
			90	106	75	90	117	122		
			95	101	86	88	117	117		
					75	80				

Sheet 3 of 10

TABLE B17 (Continued)

				Traf	fic Line					
PATTERN			2		. 3		4		5	
	WEST	EAST	WEST	EAST	WEST	EAST	WEST	EAST	WEST	EAST
45	70	80	90	90	70	70	95	101	111	106
			95	101	69	75	106	90		
			106	95	75	80	101	117		
			101	80	85	75	111	117		
					85	90				
50	111	90	95	90	80	95	80	111	101	111
			106	106	80	80	106	106		
			101	101	95	82	111	133		
			106	106	80	80	106	117		
					80	80				
55	58	80	90	95	70	80	95	117	98	106
			90	101	75	90	106	106		
			90	95	69	85	101	111		
			95	95	64	85	111	143		
					70	80				
60	80	95	90	93	70	55	95	123	106	90
			95	111	70	80	80	117		
			106	106	70	83	101	123		
			95	106	80	85	95	123		
					75	85				
65	80	80	106	117	70	70	106	111	101	127
			90	117	73	73	106	103		
			95	111	70	75	117	117		
			95	117	80	75	122	106		
					70	80				
68	. 80	101	95	95	63	85	106	122	115	127
			90	90	70	80	101	125		
			95	106	75	75	101	111		
			92	106	70	80	106	117		
					65	80		1 7 7		

Sheet 4 of 10

TABLE B17 (Continued)

GAGE NO. 2NSSWJ TEST ITEM 2 STRAIN IN MICROINCHES

Traffic Lines										
4			5							
T I LAST	WEST	MEST	EAST							
180	127	127	143							
159	175									
3 149	133									
122	127									
61	42	32	16							
53	48									
42	19									
. 43	27									
48	40	50	19							
56	42									
45	40									
42	42									
42	42	40	42							
40	40									
37	74									
37	37									
37	77	11	45							
29	35									
37	42									
	-									
45	42	13	32							
	37									
	40									
27	35									
	40		40							

Sheet 5 of 10

TABLE B17 (Continued)

GAGE NO. 2NSSEJT TEST ITEM 2 STRAIN IN MICROINCHES

		Tr	affic Li	nes				5
PATTERN	WEST 127	EAST 117	WEST 117	3 EAST 127	WEST 127 58	1 EAST 131	WEST 117	EAST 85

NO FURTHER READINGS

TABLE B17 (Continued)

GACE NO. 3NSCT TEST ITEM 3 STRAIN IN MICROINCHES

				Traf	fic Line					
PATTERN		1		2		3		4	HITTERY	5
	REST	EAST	WEST	EAST	WEST	EAST	WEST	EAST	WEST	FAST
1	93	98	127		98	103	101	111	90	138
			133	106	106	106	117	101		
			138	106	101	101	111	106		
			154	149	103	106	106	111		
					106	108				
5	12h - 11kd	90	119	109	101	101	101	95		90
				-	101	88	106	106		
			103	104	98	101	111	109		
			82	80	95	98	111	103		
					82					
6	77	82		98	82	90	80	90	53	74
				98	72	85	85	101		
			114	101	85	90	85	85		
				85	90	85	83	. 80		
					-	. •				

Sheet 7 of 10

TABLE B17 (Continued)

GAGE NO. 3NSCL TEST ITEM 3 STRAIN IN MICROINCHES

					MILLO LI	1104		*****		
PATTERN	1			2		3		4		5
	WEST	EAST	WEST	EAST	WEST	FAST	UEST	FAST	WEST	EAST
1	93	109	77	114	74	82	101	117	69	90
			80	85	69	80	101	85		
			85	90	75.	80	111	90		
			90	106	75	82	85	111		
					80	85				
5	66	90	65	98	72	80	98	98	80	80
			72	79	72	72	95	92		
			90	82	66	72	90	80		
			98	111	66	72	69	80		
					95	80				
8	80	74	45	77	66	72	88	93	72	74
			85	80	66	72	82	88		
			66	90	64	72	98	85		
			69	69	58	77	93	72		
					72	72				
9	74	76	45	-	-	-	-	-	-	-

Sheet 8 of 10

TABLE B17 (Continued)

GAGE NO. 3NSSWJT TEST ITEM 3 STRAIN IN MICROINCHES

				Tre	ffic Lin	es				
PATTERN		1	1	2		3		4	after some " is restricted as as	5
	WEST	EAST	WEST	EAST	WEST	FAST	WEST	FAST	WEST	EAS
1	85	90	106	125	111	117	117	138	122	133
			122	117	106	117	127	127		
			122	117	106	117	127	133		
			111	122	106	126	133	133		
					122	127				
5	125	111	201	221	191	186	191	186	212	233
			239	233	212	207	217	217		
			271	239	207	207	318	228		
			233	254	196	207	270	223		
					239	233				
10	154	233	48	37	32	27	74	85	53	27
			58	58	27	21	58	58		
			58	37	32	30	58	63		
			48	32	37	21	64	85		
					37	27				
14	122	170	11	- 11	11	11	16	16		-
					11	16		-		
			58	27	11	27		85		
			37		32	11	159	58		

Sheet 9 of 10

TABLE B17 (Concluded)

GAGE NO. 3NSSEJT TEST ITEM 3 STRAIN IN MICROINCHES

				Traffi	Lines					Fly.
PATTERN		1		2		3		4		5
	WEST	EAST	WEST	EAST	WEST	EAST	VEST	FAST	WEST	EAST
12	80	106				55	106	74		74
			143	111	69	64	68	58		
			122	95	69	64	* *	74		
			127	90	69	64 69	74	58		
15	85	85	101	90	58	58	69	69	58	90
			-			<u> </u>	-			
			111	127	64	58	53	58		
					58	58	69	58		
						58				
20	80	85	138	85	58	53	53	48	48	106
				in the large	53	53	64	48		
				-	- 1	-	53	58		
			58	90	53	58	58	53		
					53	64				
25	8	80	101	95	48	53	53	69	58	48
			148	90	58	53	53	58		
			90	101	53	5.3	53	58		
			95	90	58	53	53	53		
					48	48				
30	49	41	82	87	25	33	33	41	33	50
			82	62	33	33	41	33		
			39	41	41	33	41	41		
			82	65	33	33	41	49		
					41	25	-	7		
	NO REA	DINGS A	TER 34	PATTERNS						

Sheet 10 of 10

ITEM I

TEST POSITIONS

- I. CENTER OF SLAB
- 2. TANGENT TO LONGITUDINAL JOINT
- 3. TANGENT TO TRANSVERSE JOINT

ITEM 2

TEST POSITIONS

- 4. CENTER OF SLAB
- 5. TANGENT TO LONGITUDINAL JOINT
- 6. TANGENT TO TRANSVERSE JOINT
- 7. PARTIAL DEFLECTION GAGE READING 25 PD
- 8. PRESSURE CELL 2 P41
- 9. PRESSURE CELL 2PI3
- IO PRESSURE CELL 23 P 23

ITEM 3

TEST POSITIONS

- II. CENTER OF SLAB
- 12. TANGENT TO LONGITUDINAL JOINT
- 13. TANGENT TO TRANSVERSE JOINT
- 14. PARTIAL DEFLECTION GAGE READING 35 PD

ITEM 4

TEST POSITIONS

15,000-16 LOAD ONLY

IS. CENTER OF SLAB

16. TANGENT TO LONGITUDINAL JOINT

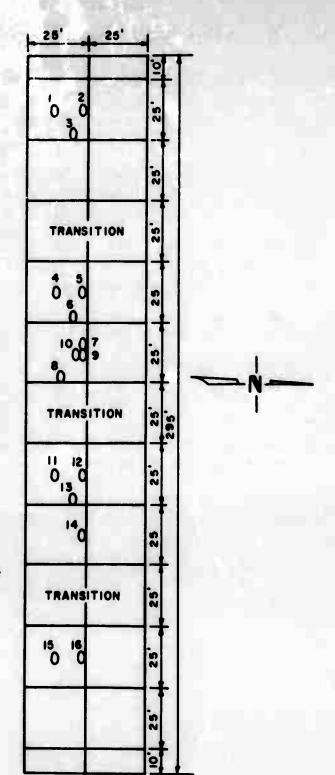


Figure Bl. Wheel Positions for Single-Wheel Static Load Tests, Rigid Pavement Test Section

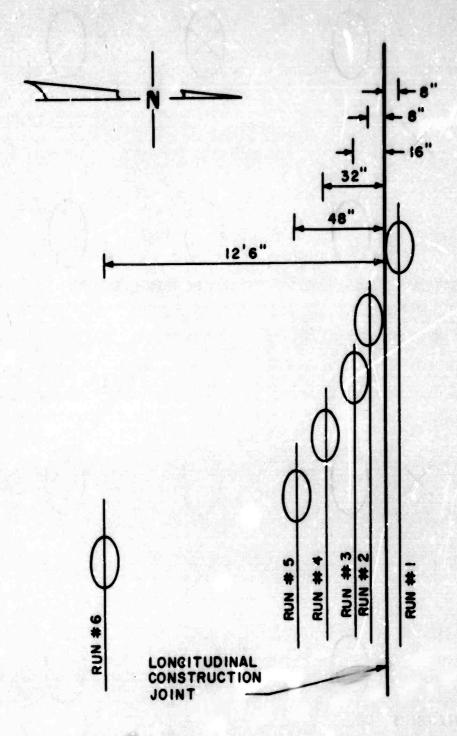
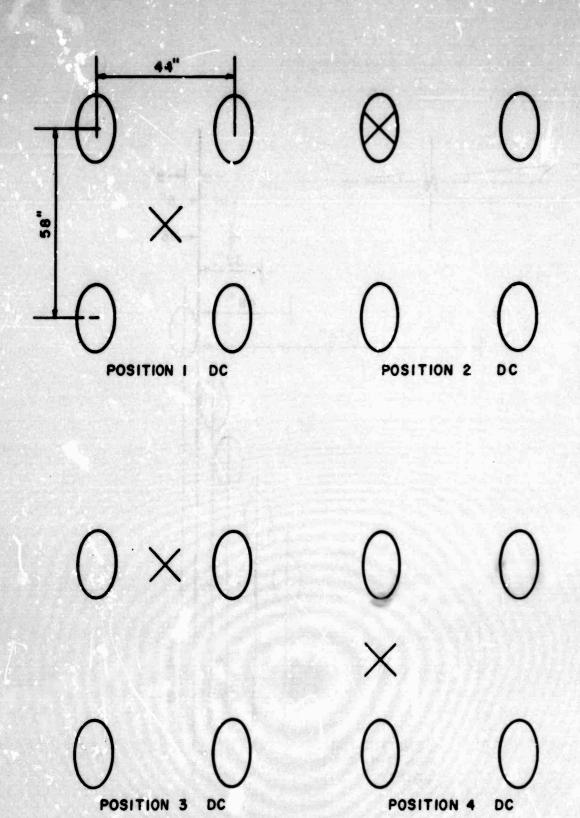


Figure B2. Wheel Positions for Single-Wheel Dynamic Load Tests on Rigid Pavement Test Section



NOTE: X = CENTER DEFLECTION GAGE

Figure B3. Wheel Positions 1-4 for Twin-Tandem Static Load Tests, Rigid Pavement Test Section

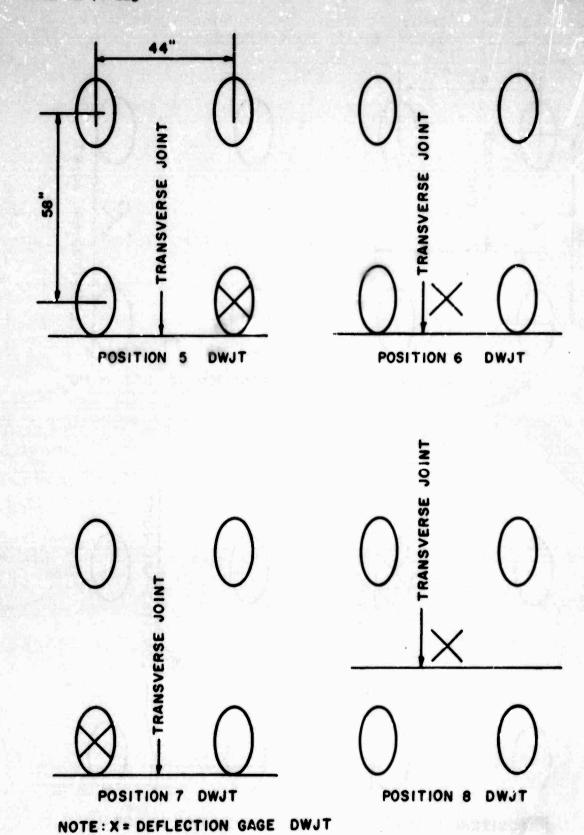


Figure B4. Wheel Positions 5-8 for Twin-Tandem Static Load Tests, Rigid Pavement Test Section

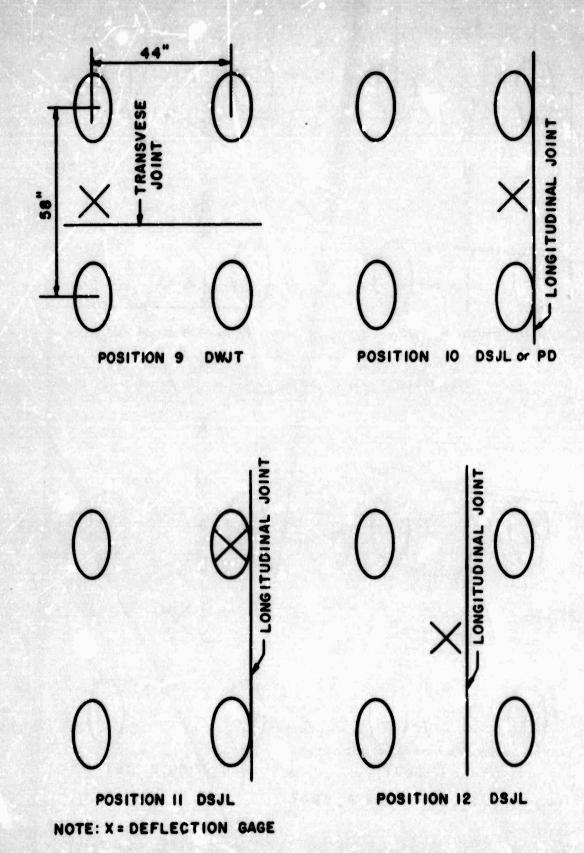


Figure B5. Wheel Positions 9-12 for Twin-Tandem Static Load Tests, Rigid Pavement Test Section

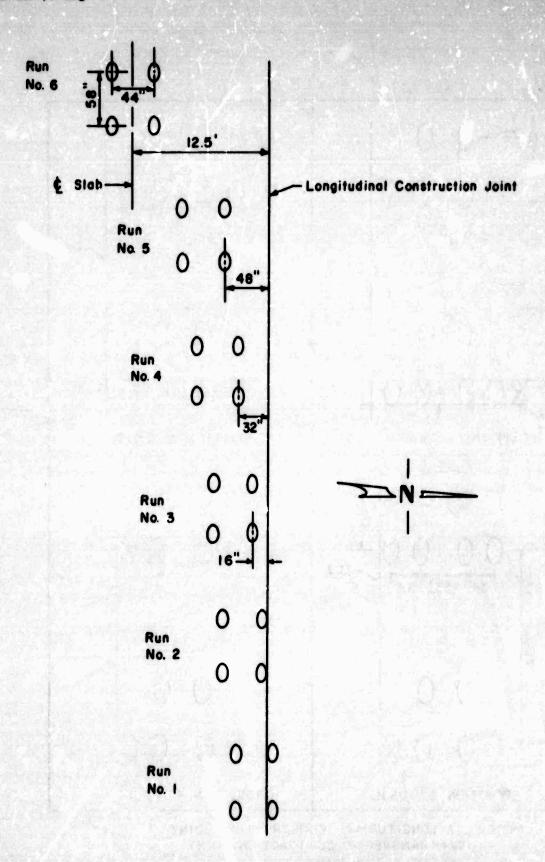
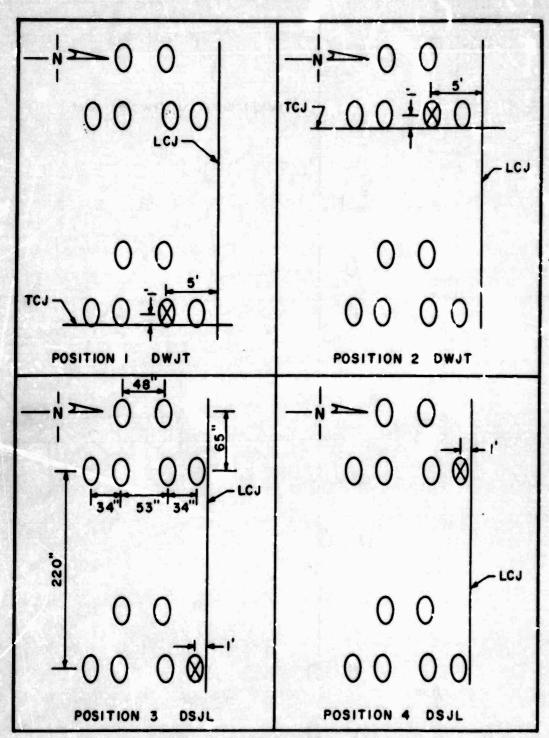
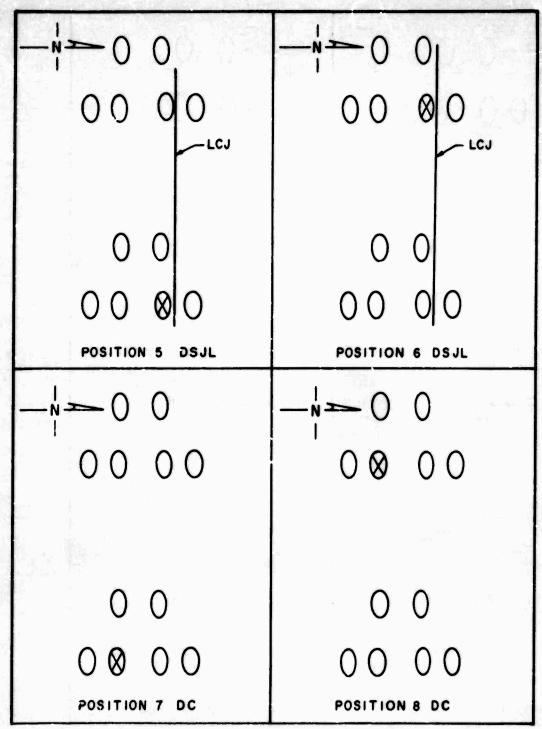


Figure B6. Wheel Positions for Twin-Tandem Dynamic Load Tests on Rigid Pavement Test Section



NOTE: LCJ = LONGITUDINAL CONSTRUCTION JOINT TCJ = TRANSVERSE CONTRACTION JOINT X = DEFLECTION GAGE

Figure B7. Wheel Positions 1-4 for 12-Wheel Static Load Tests, Rigid Pavement Test Section



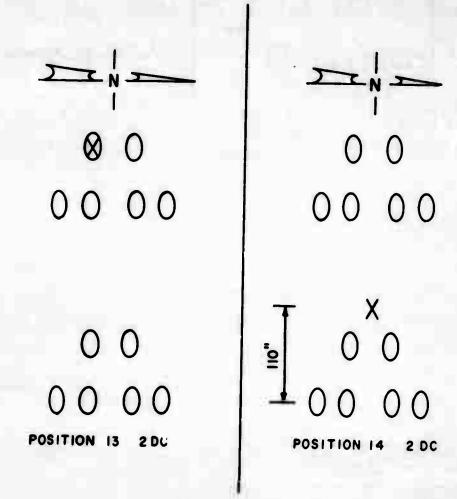
NOTE: LCJ = LONGITUDINAL CONSTRUCTION JOINT X = DEFLECTION GAGE

Figure B8. Wheel Positions 5-8 for 12-Wheel Static Load Tests, Rigid
Pavement Test Section

-h-0 0	-N=00
00 00	00 00
0 0	0 0
80 00	00 00
POSITION 9 2DC	POSITION 10 2DC
-h=00 %	$ \sim 0 \times 0$
00°00 T	00 00
0 0	0 0
00 00	0000
POSITION II 2DC	POSITION 12 2DC

NOTE: X = DEFLECTION GAGE

Figure B9. Wheel Positions 9-12 for 12-Wheel Static Load Tests, Rigid Pavement Test Section



NOTE: X = DEFLECTION GAGE

Figure BlO. Wheel Positions 13 and 14 for 12-Wheel Static Load Tests, Rigid Pavement Test Section

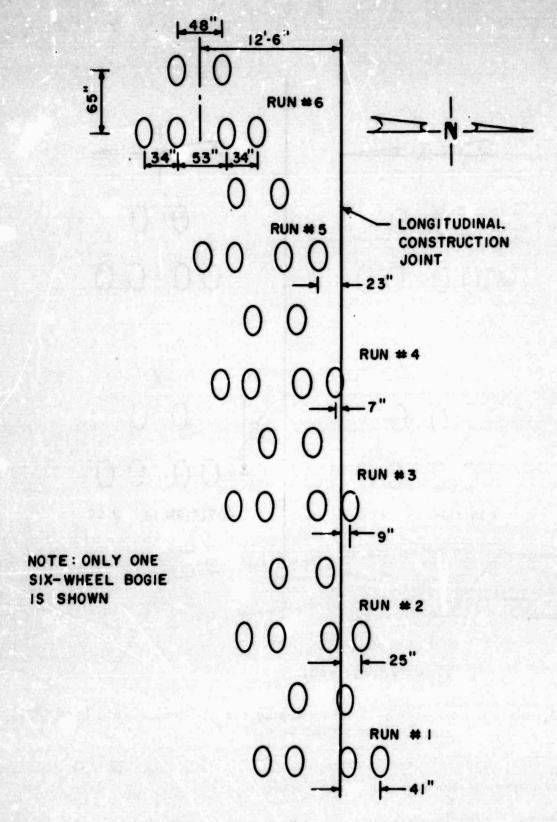


Figure Bll. Wheel Fositions for 6- and 12-Wheel Dynamic Load Tests on Rigid Pavement Test Section (Wheel Positions Were the Same for Both)

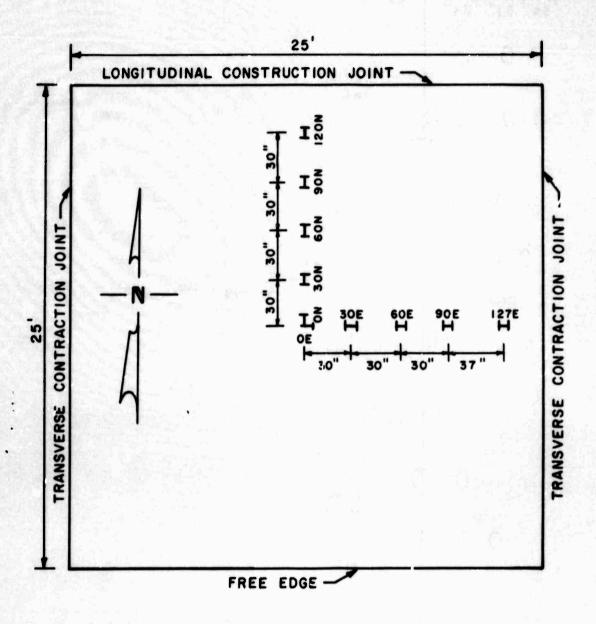


Figure Bl2. Supplemental Strain Gage Layout, Test Item 2

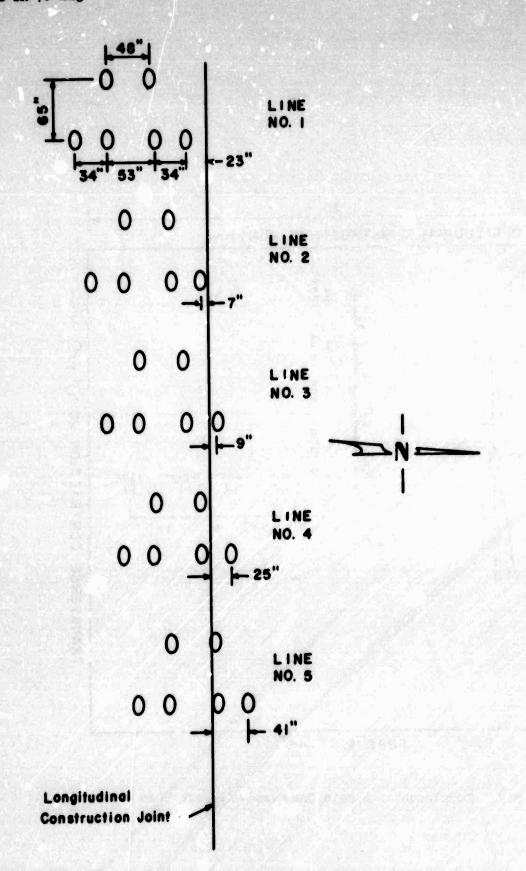
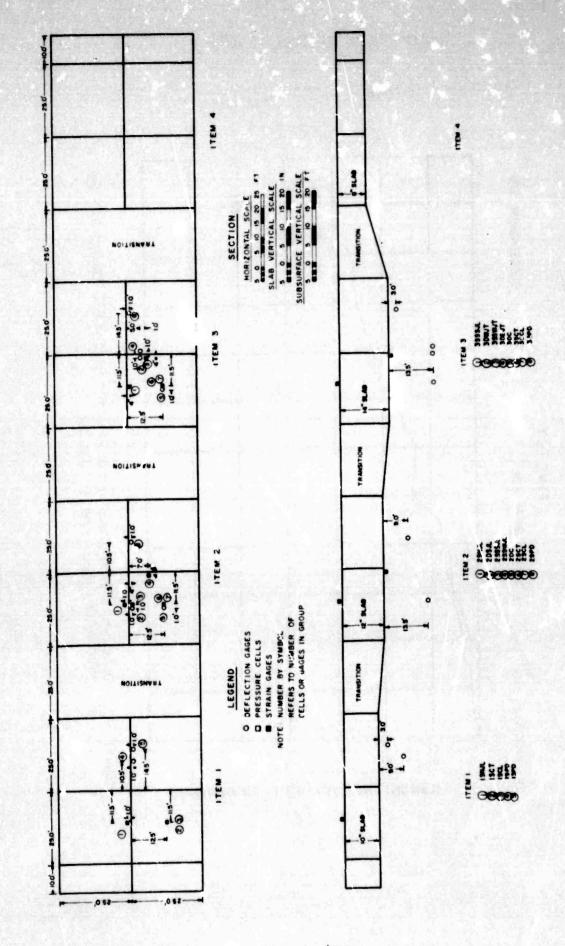
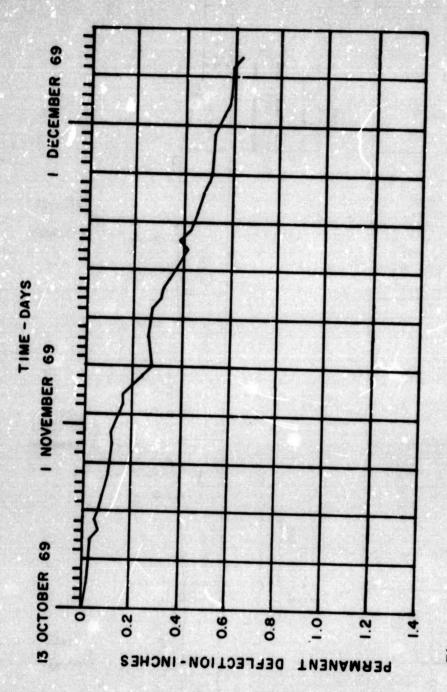


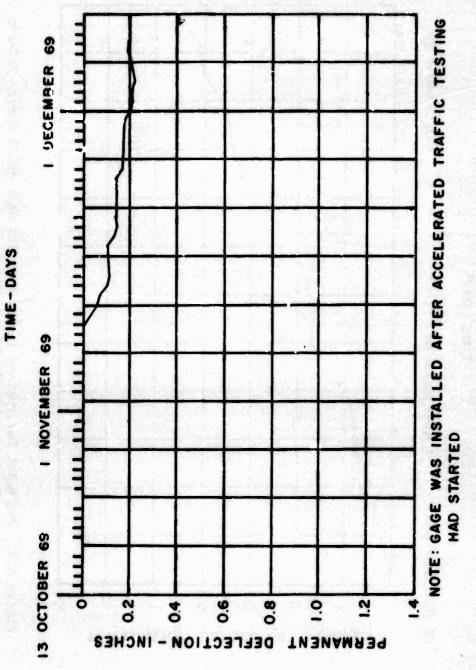
Figure B13. Traffic Patterns for the 12-Wheel Assembly, Rigid Pavement Test Section



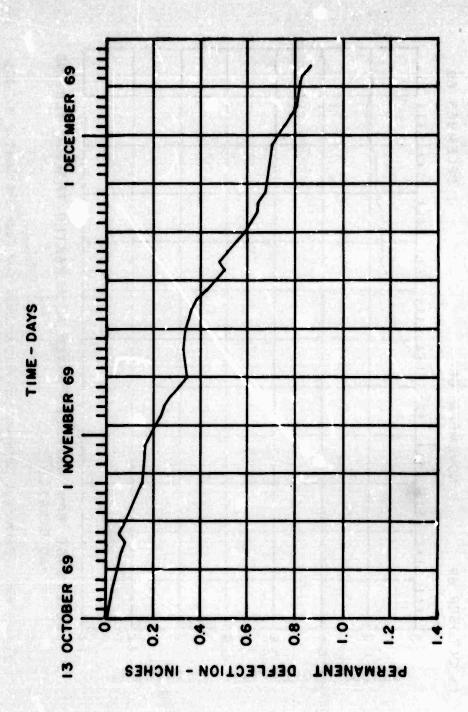
Instrumentation Layout at Start of 12-Wheel Traffic, Rigid Pavement Test Section Figure B14.



Permanent Deformation Versus Days for Gage 2DSJL During 360-kip 12-Wheel-Assembly Traffic Testing Figure B15.



Permanent Deformation Versus Days for Gage 2DC During 300-kip 12-Wheel-Assembly Traffic Testing Figure B16.



Permanent Deformation Varsus Days for Gage 3DEJT During 360-kip 12-Wheel-Assembly Traffic Testing Figure B17.

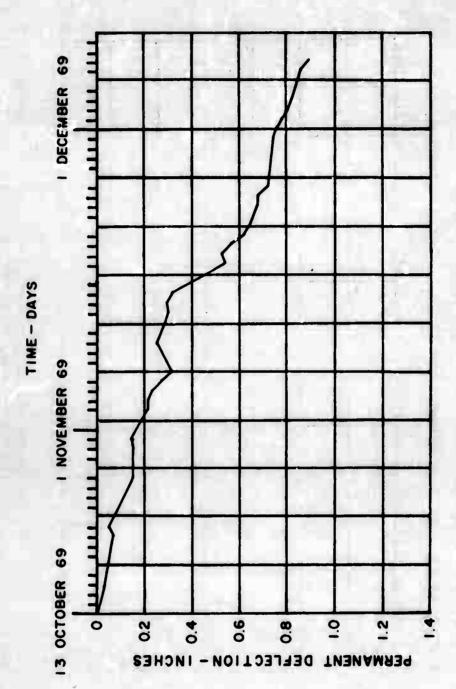


Figure B18. Permanent Deformation Versus Days for Gage 3DWJT During 360-kip 12-Wheel-Assembly Traffic Testing

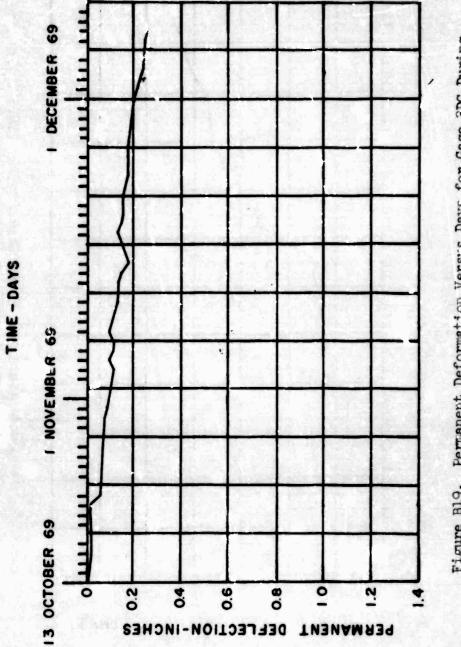


Figure B19. Permanent Deformation Versus Days for Gage 3DC During 360-kip 12-Wheel-Assembly Traffic Testing

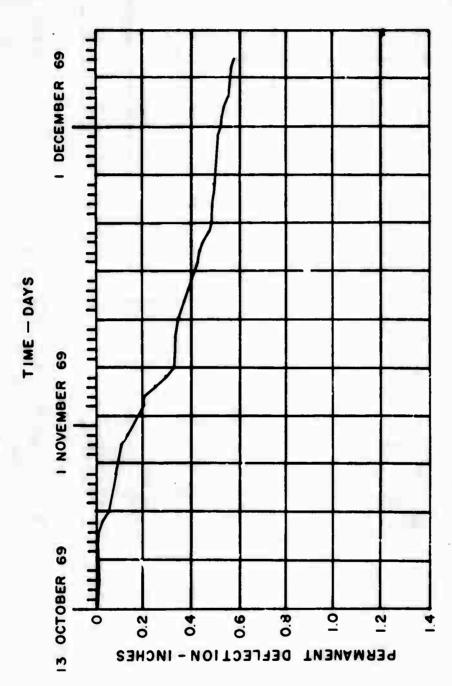


Figure B20. Permanent Deformation Versus Days for Gage 13FD During 360-kip 12-Wheel-Assembly Traffic Testing

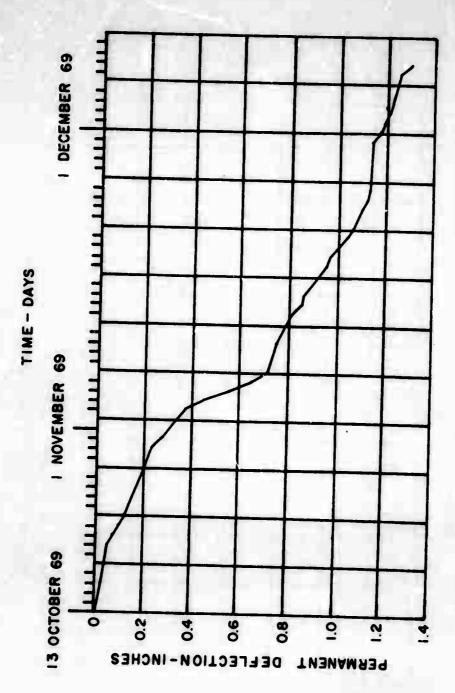


Figure B21. Permanent Deformation Versus Days for Gage 19PD During 360-kip 12-Wheel-Assembly Traffic Testing

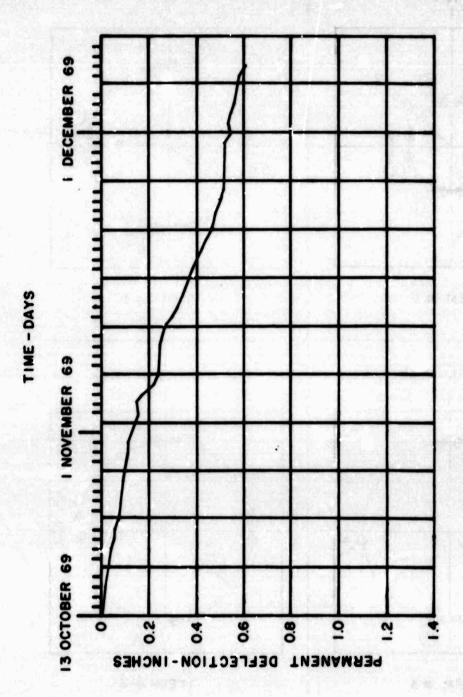


Figure B22. Permanent Deformation Versus Days for Gage 29FD During 360-kip 12-Wheel-Assembly Traffic Testing

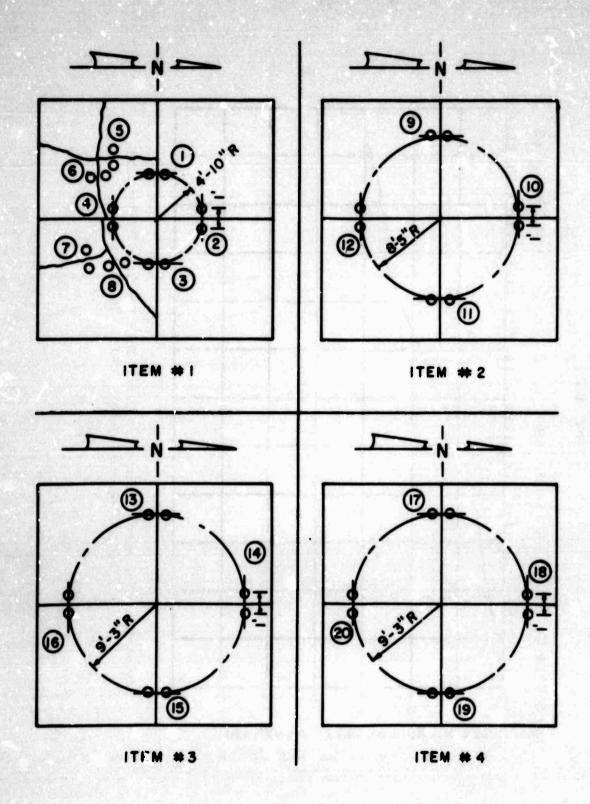


Figure B23. Whittemore Gage Locations

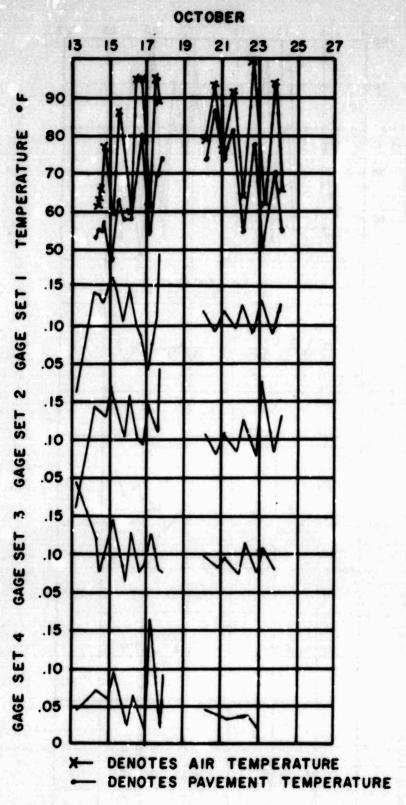


Figure B24. Test Item 1: Temperature and Whittemore Gage Readings Versus Days, Gages 1-4

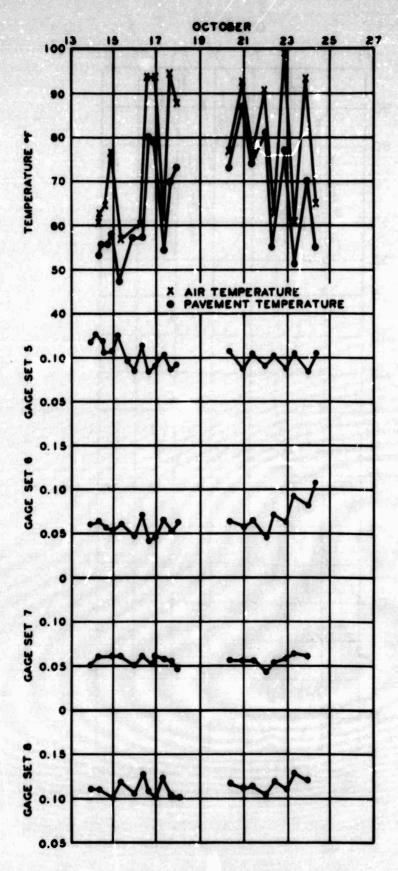
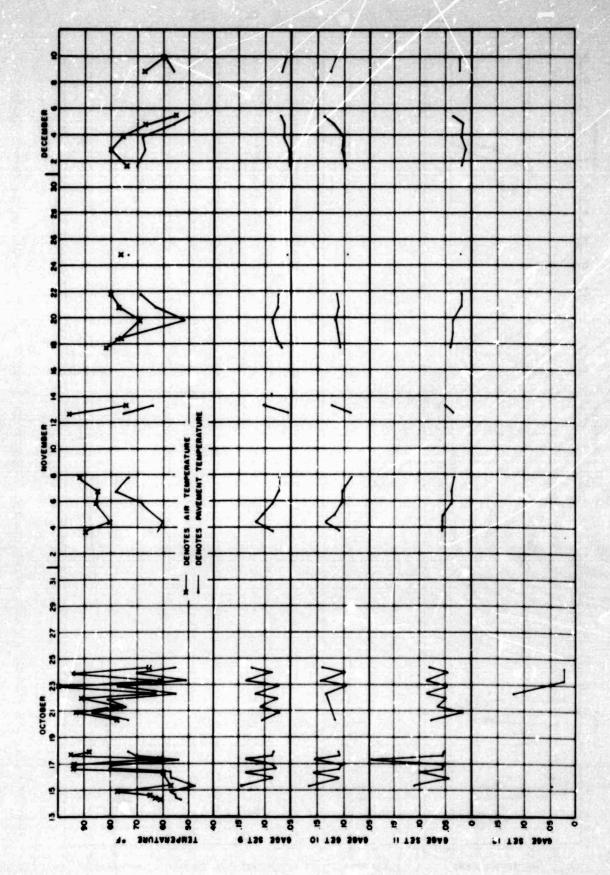
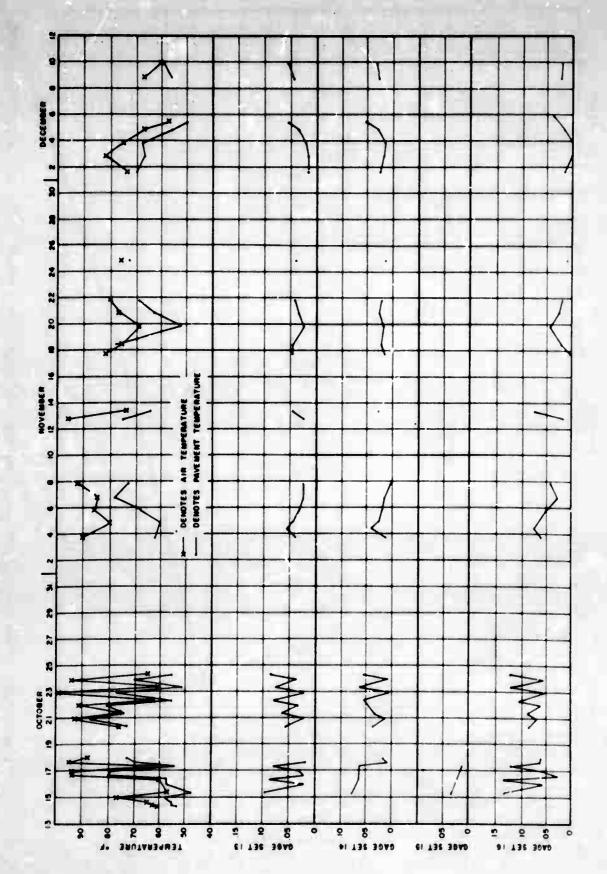


Figure B25. Test Item 1: Temperature and Whittemore Gage Readings Versus Days, Gages 5-8



Temperature and Whittenore Gage Readings Versus Days, Gages 9-12 Figure B26. Test Item 2:



Test Item 3: Temperature and Whittemore Gage Readings Versus Days, Gages 13-16 Figure B27.

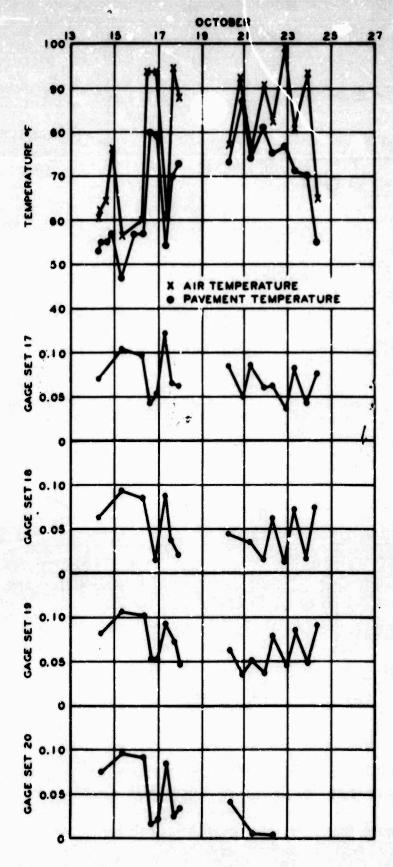
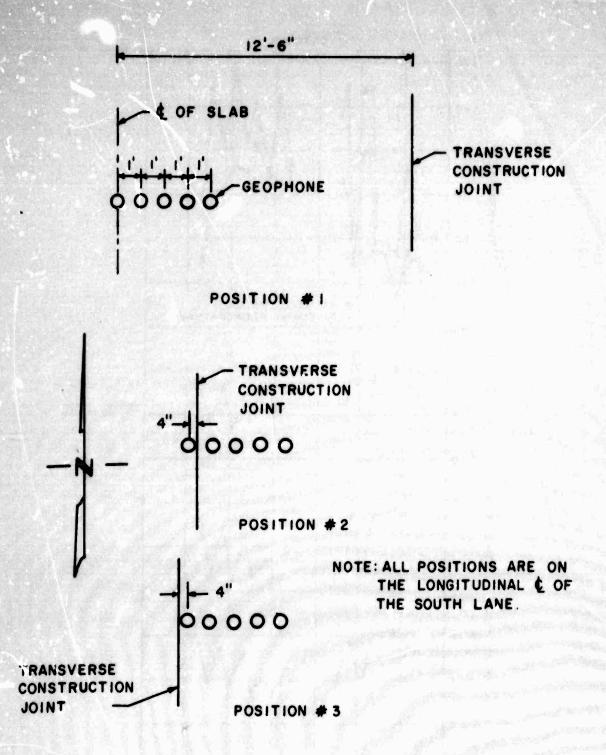


Figure B28. Test Item 4: Temperature and Whittemore Gage Readings Versus Days, Gages 17-20



TYPICAL DYNAFLECT TEST POSITIONS

Figure B29. Typical Dynaflect Test Positions

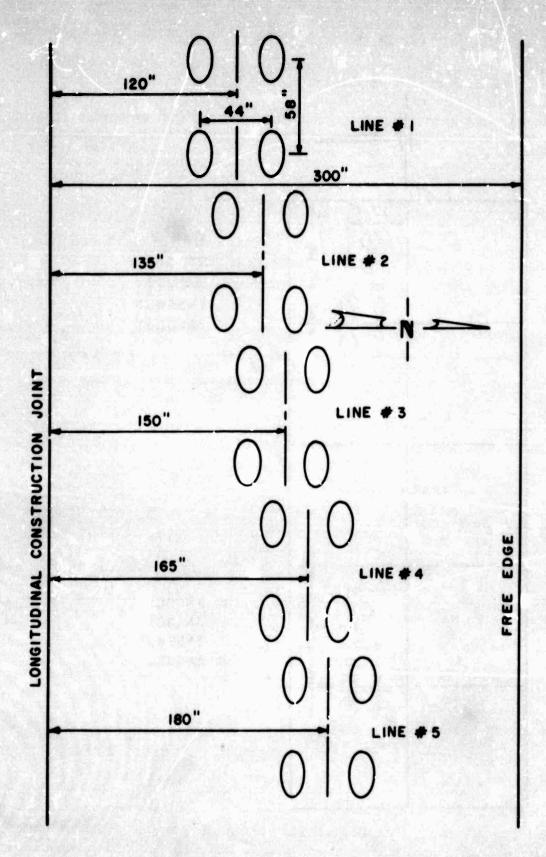
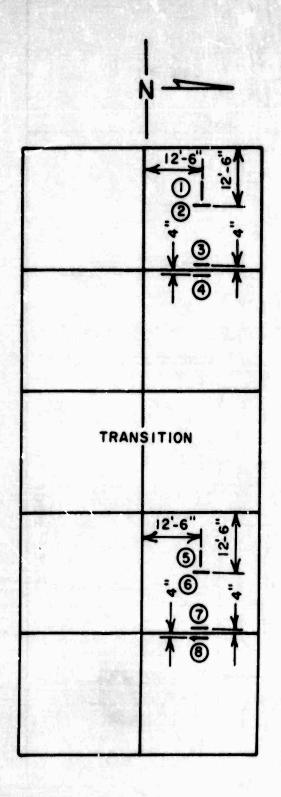


Figure B30. Instrumentation Layout for Twin-Tander, Traffic Testing



ITEM 2

- I. 2 NSSCL
- 2. 2 NSSCT
- 3. 2NSSWJT
- 4. 2NSSEJT

. ITEM 3

- 5. 3 NSSCL
- 6. 3NSSCT
- 7. 3NSSWJT
- 8. 3NSSEJT

Figure B31. Traffic Patterns for the Twin-Tandem Assembly, Rigid Pavement Test Section

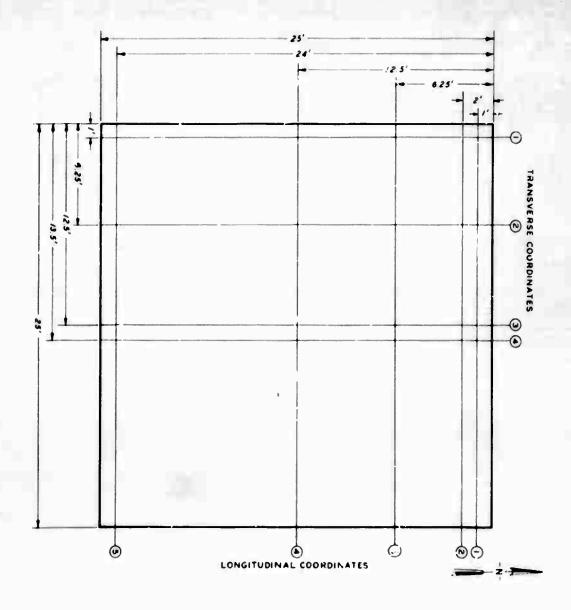


Figure B32. Locations of Pressure Cells, Item 2, Southeast Slab

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- 2. Taylor, D. W.; Soil Mechanics, John Wiley & Sons, Inc., N. Y., 1948.
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- 5. U. S. Army Engineer Waterways Experiment Station, CE, Pressure Cells for Field Use, Bulletin No. 40, Vicksburg, Miss., January 1955.
- 6. U. S. Army Engineer Waterways Experiment Station, CE, <u>Investigations of Pressures and Deflections for Flexible Pavements; Homogeneous Sand Test Section</u>, Technical Memorandum No. 3-323, Report No. 4, Vicksburg, Miss., <u>December 1954</u>.

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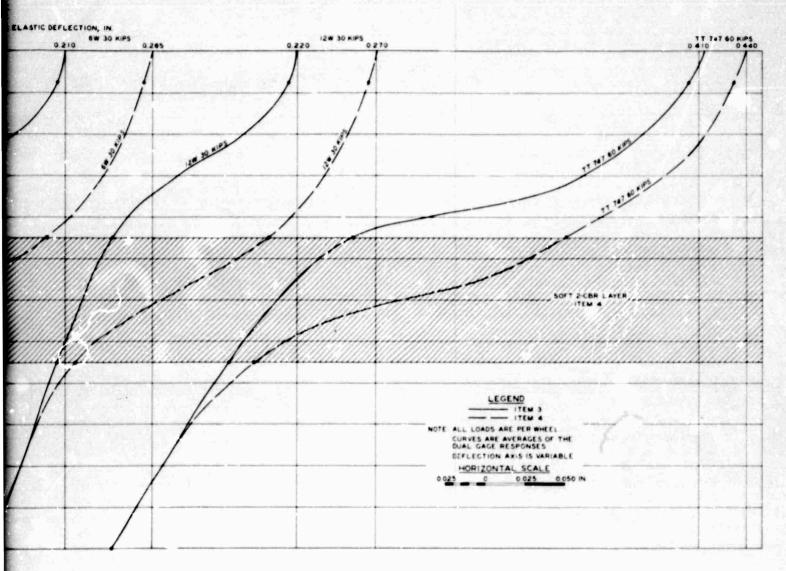
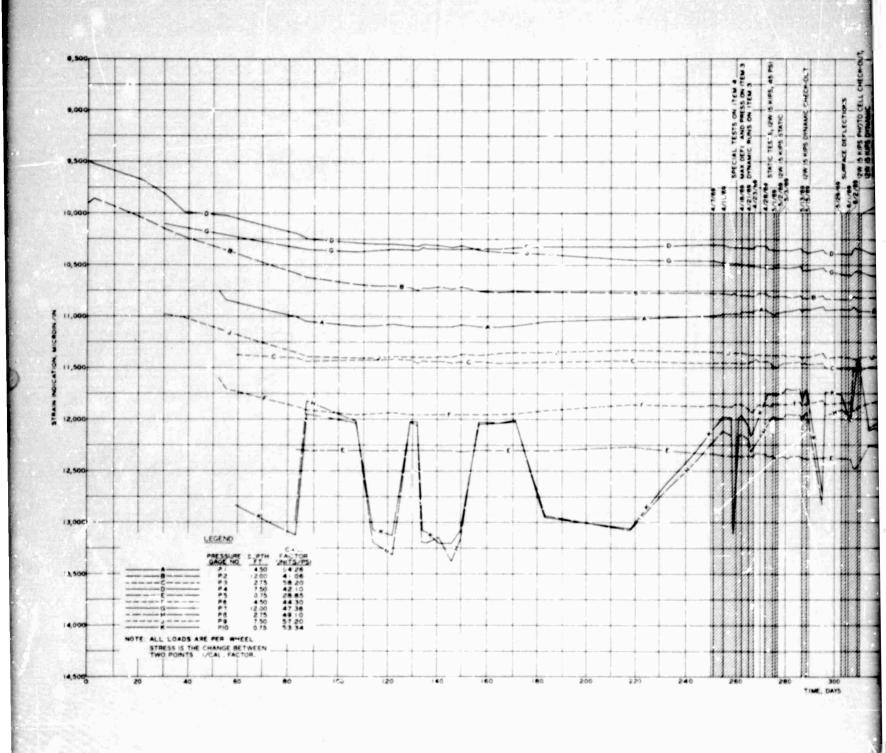
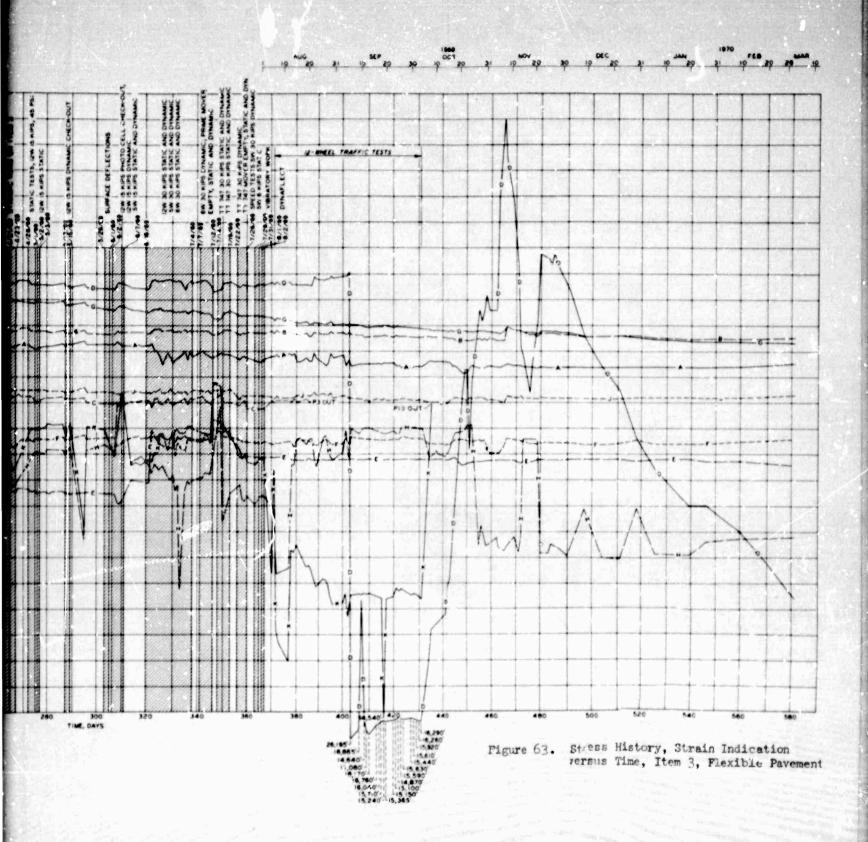
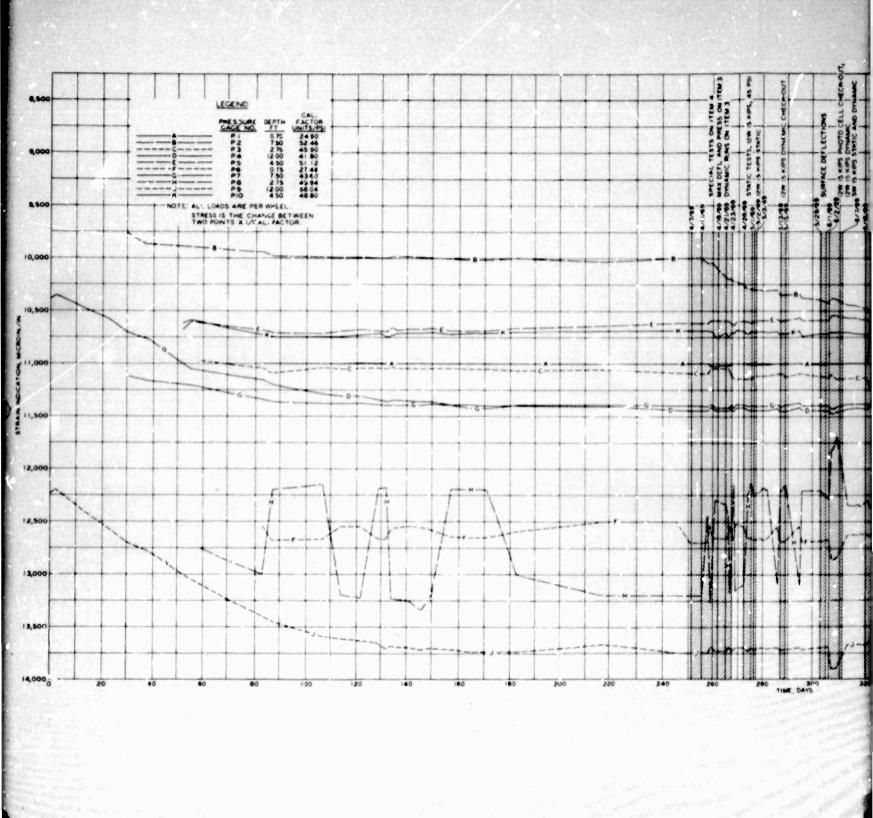


Figure 24. Item 3 Versus Item 4 Limiting Deflection Curves, Static Load Flexible Pavement Tests







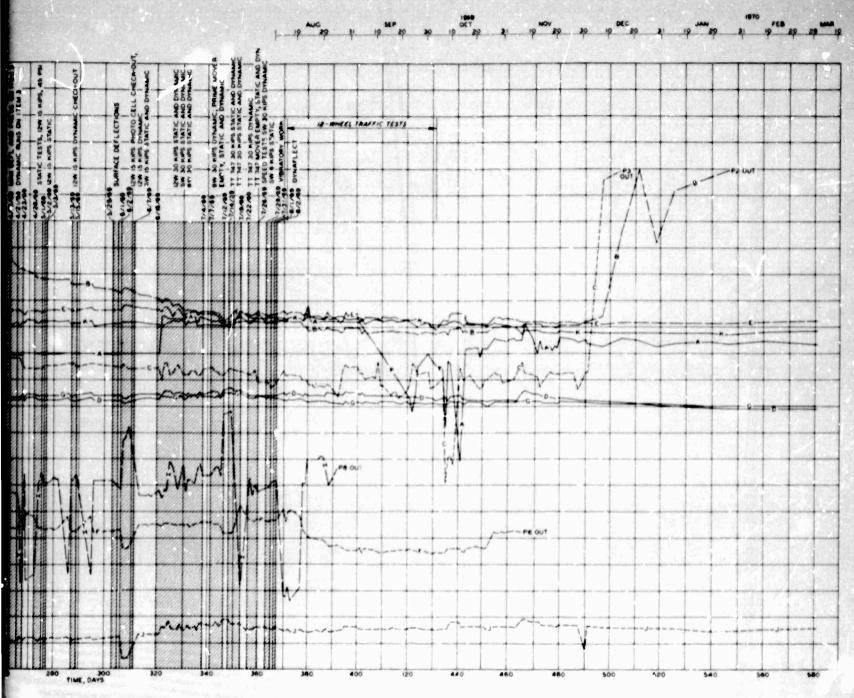
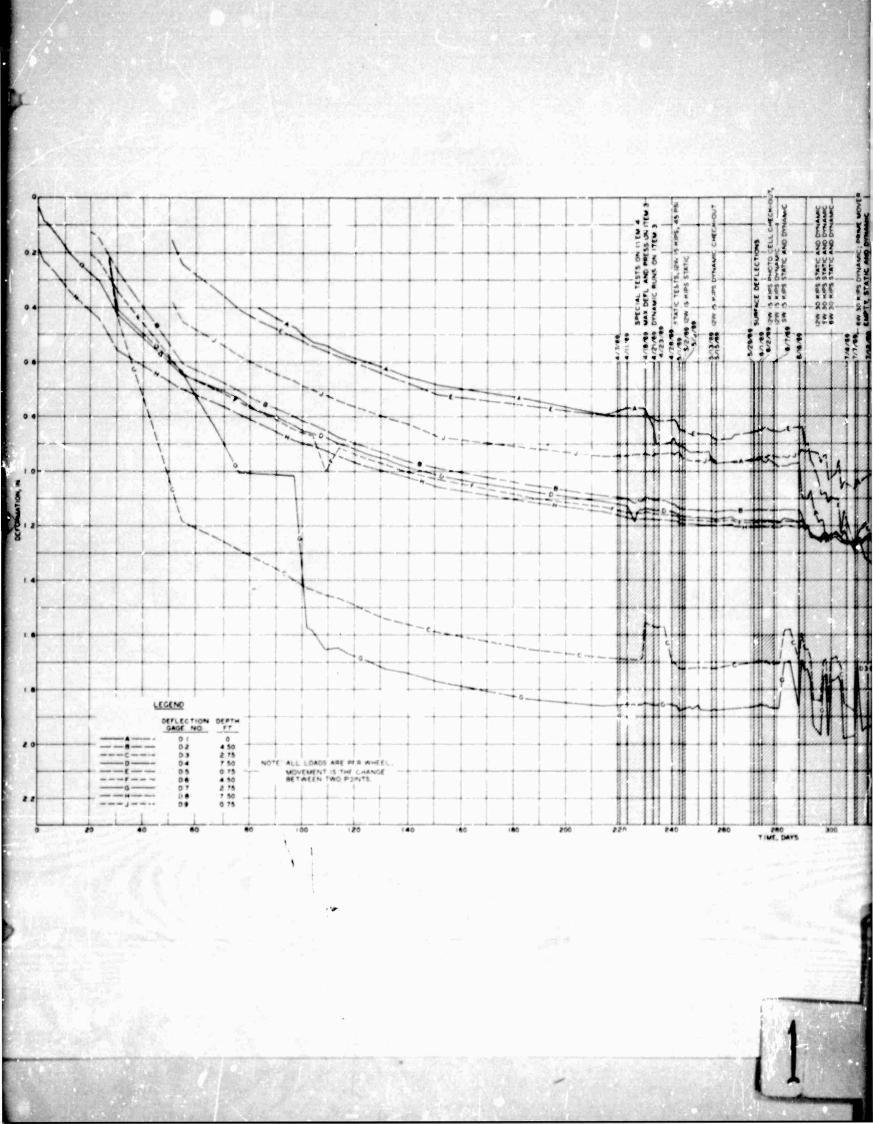


Figure 64. Stress History, Strain Indication Versus Time, Item 4, Flexible Pavement



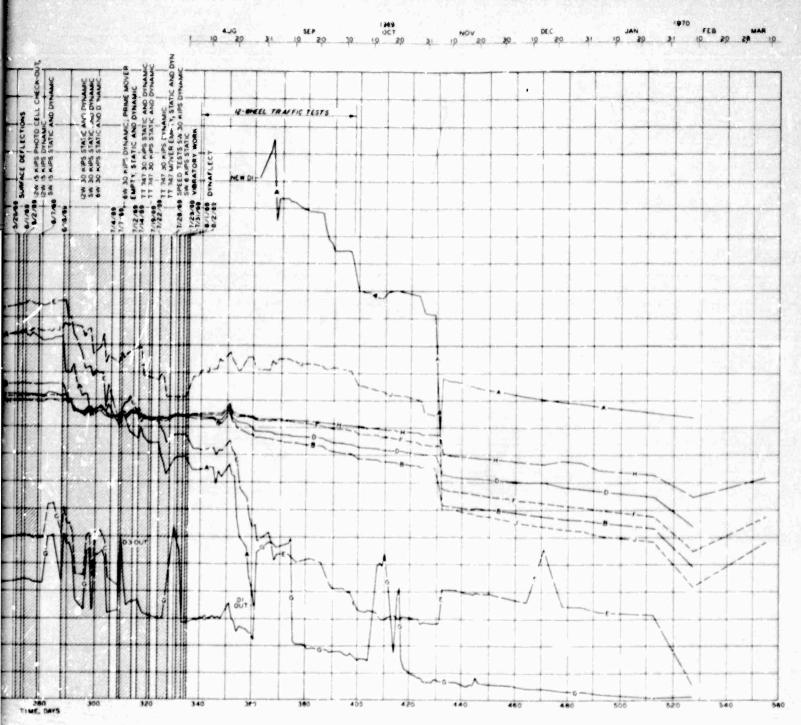
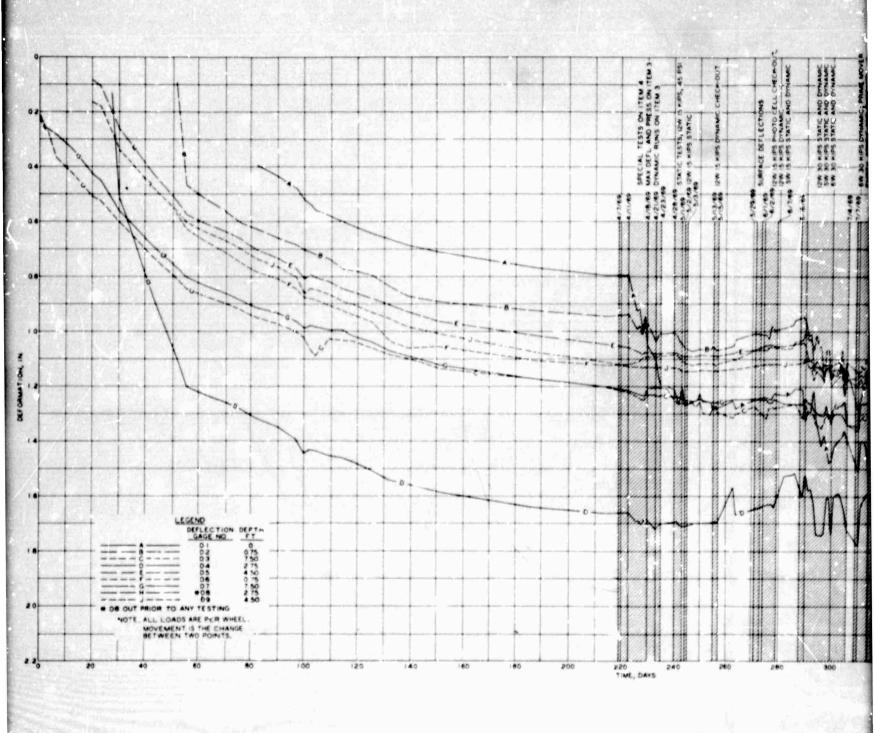


Figure 67. Deformation History, Deformation Versus Name, Item 3, Flexible Pavement



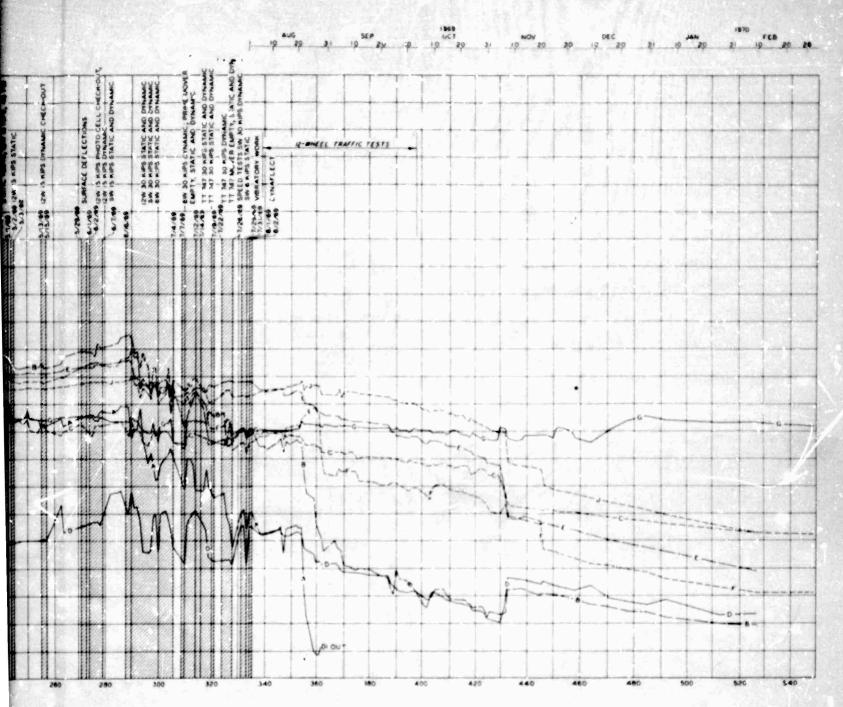


Figure 68. Deformation History, Deformation Versus Time Item 4, Flexible Pavement

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